

# **Environmental Wind Conditions for Snow Cornice Formation tested in a Wind Tunnel**

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Snow cornices growing on the lee-leeward side of mountain ridges are a common feature common in alpine and polar regions during snow seasons. ~~They can result in potential avalanche risk when they~~ These structures may crack and fall. ~~Current studies of cornices mainly focus on their deformation, collapsing, and avalanche risk via field observations. Few studies have paid attention to the accretion process of cornices, especially on their horizontal growth which enhances the instability of cornices.~~

5 ~~In this work,~~ leading to an increase in the avalanche danger. Although cornice formation has been observed in wind tunnel tests and the field, knowledge gaps still exist regarding the formation mechanism. In particular with respect to wind conditions, which favor cornice formation. To characterize the wind effects as the main factor for cornice growth, we carried out ring wind tunnel (RWT) experiments in a cold laboratory under various wind conditions ~~are carried out to investigate the environmental conditions and the internal physical mechanism of cornice formation. We quantitatively investigated the growth rate of the~~

10 cornice in the horizontal and vertical direction, as well as the airborne particle concentration. The results show ~~that—for the specific settings in our wind tunnel—cornices appear only under moderate wind speeds which lead to necessary net mass flux divergence near the edge. The fastest growth rate is with winds~~ that cornices only appear under a moderate wind speed range (1-2.03  $\bar{u}$ ). The cornice growth rates in length and thickness are mainly determined by the combined effects of mass accumulation and erosion. The lower limit wind speed for cornice growth is approximately equal to the threshold wind speed

15 for transport. The upper limit of wind speed is when the erosion rate is over the pure deposition rate. The length growth rates of cornice reach a maximum for wind speeds approximately 40% higher than the ~~rebound~~ threshold wind speed ~~for snow transport because then the snow mass supply to the cornice edge is sufficient. Mass collection efficiency on the~~. Moreover, a conceptual model for interpreting the cornice ~~surface decreases with the increasing wind speed~~ accretion mechanism is proposed based on the mass conservation and the results of the RWT experiments. The estimated suitable wind condition for cornice growth and

20 formation are in good agreement with the field observations in Gruvefjellet, Svalbard. This work ~~improves our understanding of cornice formation~~ could be helpful in the snow avalanche prediction works.

## 1 Introduction

Snow cornices are leeward-growing masses of snow overhanging ~~at the sharp breaks in slope~~ and extending horizontally beyond the edge, usually appearing on the ridgeline of steep mountains (Seligman et al., 1936). Some cornices deform, detach, and eventually fall off, which induces cornice fall avalanches or slope erosion, and leads to a redistribution of the snow cover below (Wahl et al., 2009). For example, cornice fall avalanches accounted for 45.2 % of all 423 snow avalanches observed in the Longyearbyen area, central Svalbard, from 2006 to 2009. They triggered slab avalanches (~~16.2 %~~) and loose snow avalanches (~~12.1 %~~) as secondary avalanches on the slope below (Eckerstorfer and Christiansen, 2011). ~~These cornice~~ Cornice fall avalanches cause potential threats to local infrastructures and human lives.

~~Cornice studies have attracted many contributions from Europe (Pauleke and Welzenbach, 1928; van Herwijnen and Fierz, 2014), America (?McCarty et al., 1986; Munroe, 2018), China (Zhizhong and Wenti, 1987), Japan (Kobayashi et al., 1988; Tsutsumi, 2005), and recently more in the Arctic (Vogel et al., 2012; Eckerstorfer et al., 2013; Hancock et al., 2020; Veilleux et al., 2021), due to the potential threats of cornice fall avalanches. Most of them are field observation studies using time-lapse photography or terrestrial laser scanner methods to record the development of cornices and analyse them through meteorological data. Most studies focused on the deformation and then collapse of cornices, as well as the ensuing cornice fall avalanches.~~ Although understanding the initial evolution of cornices is a foundation ~~of~~ for predicting and treating cornice fall avalanches, only a few studies have paid attention to the initial accretion process, especially to the horizontal extension forming the main part of the snow mass overhanging the edge of a mountain crest. ~~An indirect~~ Previous research has observed that cornices grow under moderate wind speeds. However, gaps remain regarding a general rule on suitable wind conditions for cornice growth. Montagnen et al. (1968) measured the moderate wind speed range is between 7 to 15 m s<sup>-1</sup> (at 0.35 m height) for cornice formation using a hand anemometer. Naito and Kobayashi (1986) measured the suitable wind speed for cornice formation is between 4 m s<sup>-1</sup> to 8 m s<sup>-1</sup>, at 1 m above the snow surface in the field and at the center (0.5 m height) in the wind tunnel. McClung and Schaerer (2006) estimated that the threshold wind speed for cornice growth and formation is about 5 to 10 m s<sup>-1</sup> (at 10 m height) which is the threshold wind speed for loose snow transport, and scouring happens when the wind speed exceeds 25 m s<sup>-1</sup>. Vogel et al. (2012) determined that cornice accretion occurs during periods with the average wind speed of 12 m s<sup>-1</sup>, and scour when the wind speed exceeds 30 m s<sup>-1</sup> (at 2.8 m height). Hancock et al. (2020) used an experienced value of threshold wind speed of 5 m s<sup>-1</sup> (at 10 m height) as a conservative lower threshold for cornice accretion. However, to our best knowledge, this discrepancy and the conditions under which certain wind speed ranges apply have not been investigated.

Indirect evidence was presented by van Herwijnen and Fierz (2014) that snow cornices only grow under moderate to ~~high~~ strength wind strong wind, during or soon after ~~the snowfalls, as well as the remarkable agreement between observed cornice width and a snowfall.~~ The cornice width from observation is in remarkable agreement with the wind drift index calculated by the snow cover model SNOWPACK (Lehning and Fierz, 2008), which indicates that snow mass transport plays an important role in cornice formation. However, ~~due to the coarse temporal resolution (normally hours or days) and uncontrollable weather conditions outside, dynamic details of snow mass transportation could not be recorded. Thus, the main reason for the~~ cornices often grow through relatively discrete events in the field (Vogel et al., 2012; van Herwijnen and Fierz, 2014; Naito and Kobayashi, 1986; H

average observations (daily) therefore only incompletely characterize cornice growth conditions. Due to the compromise of these field observations, continuous observations on individual cornice accretion and failure events are hard to achieve (Hancock et al., 2020). Specifically, measuring the horizontal growth of snow cornice remains unclear. In addition, several hypotheses were proposed to explain the cornice formation. Due to the wedged-like shape and typical appearance on cliffs where sudden changes of air pressure and wind velocity between accelerating windward slope and decelerating leeward slope are observed, the hypothesis was put forward that the reflux vortex structure of the lee-side flow field is the main reason of cornice formation (Seligman et al., 1936). Particles, which follow the changing wind direction locally as the flow passes the ridge will stick to the growing cornice front at the mountain ridge is a widely accepted hypothesis. Later, Latham and Montagne (1970) suggested that electrification may play an important role in cornice formation through observation of the electric field strength over a cornice. However (Vogel et al., 2012) and recording dynamic details of snow mass transport simultaneously is hard to achieve. There are few laboratory experiments on cornice formation except Naruse et al. (1985) and Naito and Kobayashi (1986). Naito and Kobayashi (1986) carried out experiments both in the wind tunnel and in the field, observing the process of snow cornice growth. They described the snow cornice formation as a process in which drifting snow particles adhere one after another at the leeward edge, in the form of a thin slab of snow elongating leewards, then the slab hangs down under its weight, depositing drifted snow particles on it. However, quantitative descriptions of this process have not been reported. Their results show that the cornice growth under suitable conditions of the air temperature is between  $-20^{\circ}\text{C}$  to  $0^{\circ}\text{C}$ , the wind speed is between  $4\text{ m s}^{-1}$  to  $8\text{ m s}^{-1}$ , and fresh snow with an irregular dendritic shape. However, further quantitative analysis of experiments has not been carried out. Mott et al. (2010) have indicated that snow cornice formation is mainly through snow distribution processes driven by saltation. However, due to the lack of physical mechanism of snow cornice formation, cornice characteristic features could not be reproduced in numerical simulation of snow distribution in mountain areas (Gauer, 2001). Thus, there is no evidence to support these assumptions still no snow cornice prediction model that could be used in avalanche prevention so far. Thus, we present a wind tunnel experiment.

Therefore, wind tunnel experiments with controlled environmental conditions and quantitative descriptions of the individual cornice formation process as a pathway to improve the understanding of cornice dynamics in the field, particularly on the wind effects on cornice formation, are essential. In this work, wind tunnel experiments of snow cornice evolution on the edge of a small-scaled mountain ridge model carried out in a cold laboratory at WSL /SLF to investigate cornice formation processes. This work delivers the first insight into wind speed and mass concentration as factors influencing snow cornice accretion from a macroscopic view. Institute for Snow and Avalanche Research (SLF) are presented. Quantitative estimations on the effect of wind conditions on snow cornice formation are presented. Section 2 presents the experimental setup in the cold laboratory and the post-processing method for cornice images. General features of the snow cornice observed in the experiment under variable wind conditions are shown in section 3. Based on this, a conceptual model evaluating the growth rates of the snow cornice based on the mass conservation method is proposed in Section 4. Its application in field observation results is discussed. Section 5 summarizes the conclusions and outlook.

## 2 Methods

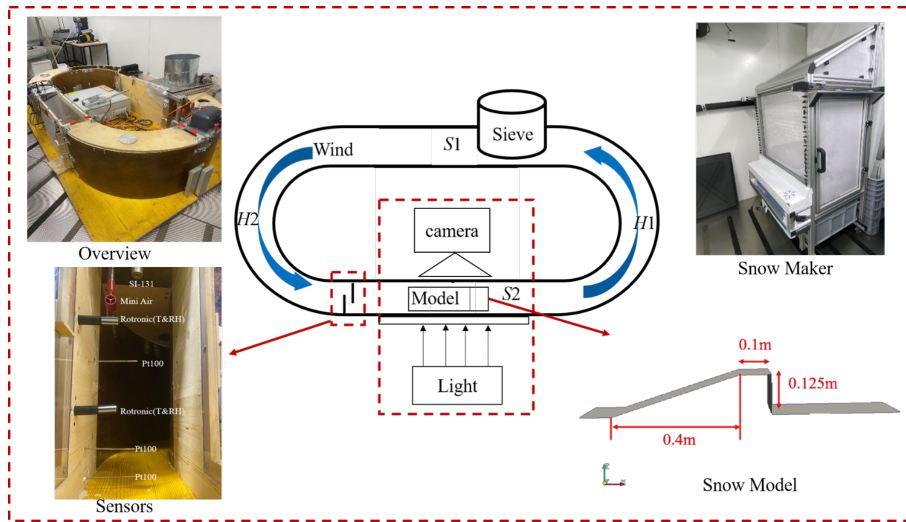
### 90 2.1 Experimental Setup

The experiments were carried out in a cold ~~lab of the WSL Institute for Snow and Avalanche Research SLF (WSL/SLF) in Davos~~Dorflaboratory of the SLF in Davos, Switzerland, where the room temperature ~~could~~can be controlled from  $-25^{\circ}\text{C}$  to  $0^{\circ}\text{C}$ . An obround, closed-circuit wind tunnel built by Sommer et al. (2017, 2018) was used to perform the investigations. ~~The~~During the experiment, the room temperature of the cold ~~lab~~laboratory was set to be ~~a constant of~~ $-5^{\circ}\text{C}$ ~~and the corresponding~~  
95 ~~relative humidity inside the tunnel is in the range of 80–90 % during the following experiments.~~

The schematic diagram of the experimental setup is shown in Fig. 1. The ~~wind tunnel ring~~wind tunnel (RWT) contains two straight sections (length = 1 m, marked as S1 and S2) and two half-circle sections (outer diameter = 0.6 m, marked as H1 and H2). Its cross-section area is 0.2 m (width)  $\times$  0.5 m (height). An electric motor with rotor blades installed inside the middle of H1 creates the wind flow with a wind speed range of ~~0–7–0–8~~0–8  $\text{m s}^{-1}$ . A sieve is installed at S1, where the tunnel has an  
100 upward open window ~~for the supply of~~to supply snow particles. Sensors monitoring the air conditions are installed at the inlet of S2, ~~and details.~~The details of the sensors are listed in Table 1. The ~~wind tunnel was cleaned before each test, and a ridge model made of compacted snow was built at~~ridge model in S2. ~~The shape and size of the ridge model affect the lee side eddy position and the snow particles' trajectories, which could have an influence on the experimental results. After multiple tests to present the best view of cornice growth, the~~with the fixed size and place is built with compacted snow each time before the  
105 ~~experiment.~~The size of the ridge model was set as 0.125 m in height and with a 0.1 m flat section (Fig. 1). ~~The angle of the slope.~~The slope angle relative to the horizontal direction is  $36^{\circ}$ . To record the growth of the cornice using shadowgraphy imaging, we placed a CMOS Camera with a spatial resolution of  $2048 \times 2048$  pixels to zoom on the edge of the ridge ~~area and~~  
We placed a LED lamp on the opposite side ~~as a light source~~for illumination.

Fresh snow particles made ~~by~~with a snowmaker developed ~~by~~at SLF (Schleef et al., 2014) were used for feeding the flow  
110 through the sieve. When using the snowmaker, the room temperature was set to  $-20^{\circ}\text{C}$ , and the water inside the ~~snowmaker~~snowmaker reservoir was set to ~~+30~~ $^{\circ}\text{C}$ ~~for the snowmaker.~~ The obtained fresh snow is a mixture of dendritic crystals and hollow columns. ~~Its density was measured by an electronic balance before each wind tunnel experiment, and the mean value was  $149 \text{ kg m}^{-3}$ . Its average diameter~~The average diameter was about  $300\text{--}500 \mu\text{m}$ , estimated by a grid plate and the amplifying lens was about  $500 \mu\text{m}$ , and the  
an amplifying lens. The specific surface area (SSA) ~~measured by  $\mu\text{CT}$  is  $75 \text{ mm}^{-1}$  (Schleef et al., 2014).~~was  
115 ~~about  $12\text{--}20 \text{ mm}^{-1}$  for the snow was stored a few days up to a week (Schleef et al., 2014).~~has been is applied for all ~~experiments.~~

~~Rebound experimental tests, and the wind tunnel is cleaned up before each test.~~Impact threshold wind speed in the experiment is determined 1) by ~~seeding fresh snow,~~ increasing the wind speed from zero until ~~saltation~~saltating particles can be observed; 2) ~~decrease by decreasing~~ the wind speed slowly, until ~~there are no saltating snow particles visible anymore while~~  
120 ~~still sieving fresh snow into the tunnel~~snow saltation is not visible anymore. The average wind speed at these two times is considered ~~as the rebound~~the impact threshold wind speed ~~correspondingly~~ (Walter et al., 2014). The average ~~value of rebound~~impact threshold wind speed was ~~found to be~~ $3.2 \text{ m s}^{-1}$  at the height of the mini-air wind sensor. Thus, seven target wind speed



**Figure 1.** Schematic diagram of the closed-circuit tunnel experimental system in the cold lab. The insets are the pictures of the ~~wind tunnel~~RWT, Snow Maker, sensors, and the snow model set up inside the ~~wind tunnel~~RWT.

**Table 1.** Instruments, variables, and data acquisition interval.

Instrument	Instrument model	Variables	Time interval (s)
CMOS Camera	LP285-40.5	Images	0.02s
Wind Speed Tester	Mini Air	$\underline{U}$ - $\underline{u}$ (m s <sup>-1</sup> )	0.2s
Snow Temperature	Pt100	$\underline{T}_s$ - $\underline{T}$ (K)	1s
Snow Surface Temperature	SI-131	$\underline{T}$ - $\underline{T}_s$ (K)	1s
Air Temperature and RH	Rotronic	$T$ (K) and RH (%)	1s

125 conditions (from 3.0 m s<sup>-1</sup> to 6.5 m s<sup>-1</sup> by steps of 0.5 m s<sup>-1</sup>) were set for the experiments. ~~The target wind speed value is set in the control system before each experiment. The actual~~ Once the propeller starts to rotate, the wind speed increases ~~continually after the electric motor rotates the propeller~~ until it reaches the target ~~wind speed value~~. The propeller ~~speed~~ angular velocity is adjusted throughout the experiment to keep the wind speed constant ~~in case larger snow particles depositions alter the flow situation inside the wind tunnel. After the experiments, the particle mass concentration, cornice length, cornice volume, and growth rate were obtained by image processing of the series of pictures.~~

## 2.2 Image Processing

130 The CMOS camera recorded 50 images with a frequency of 10 Hz ~~frequency~~ in the burst mode, and the pause between two bursts was 5 s. Thus, 50 continuous frames in 5 s as one set ~~were was~~ obtained, which could ~~be used to~~ estimate the cornice

growth rate and transport mass flux instantaneously or on average. The ~~field of view was 7.7 cm × 7.7 cm, and the depth of field was 3.5 cm for particles with the mean size of 500 μm, which are calibrated by using the method of Crivelli et al. (2016)~~. The first image, in which only the ~~model crest ridge model~~ was visible without snow particles moving across, was set as a background image, as shown in Fig. 2(a)a. For a set of 50 frames, ~~we first subtracted the images were subtracted from the background image and then transformed the result (only with ridge model) and transformed~~ to binary format (where the ~~grayscale value of~~ pixels with snow is 1, and without snow is 0), as shown in Fig. 2(e) and (d). ~~During this process, a high threshold value V1 was predefined for only presenting cornice shape without snow particles in the air. Then, the continuous value of 1 in each row-e.~~ The cornice length  $L$  (m) and cornice thickness  $H$  (m) are calculated based on the binary images (Fig. 2c-d). To avoid a wrong interpretation (as erosion or deposition) of the shape effect of bending, we used the thickness of accumulation mass on the flat as the indicator of vertical accumulation/~~column was counted, and its maximum values defined the cornice thickness/length.~~ erosion of the cornice in the following analysis.

The instantaneous cornice growth ~~rate is then calculated by~~ or erosion rate in thickness  $h_{g/e}$  ( $\text{m s}^{-1}$ ) and in length  $l_{g/e}$  ( $\text{m s}^{-1}$ ) are then calculated as the difference of two adjacent frames divided by 0.1 s, and the averaged cornice growth rate is the mean value of the instantaneous cornice growth rates in one set of 5 s. The thickness of accumulated snow represents the net amount of deposition and erosion, and the length growth rate of cornice represents the horizontal extension speed from the edge. ~~the time difference between two images  $\Delta t$  (s):~~

$$h_{g/e} = \frac{\Delta H}{\Delta t} \quad (1)$$

$$l_{g/e} = \frac{\Delta L}{\Delta t} \quad (2)$$

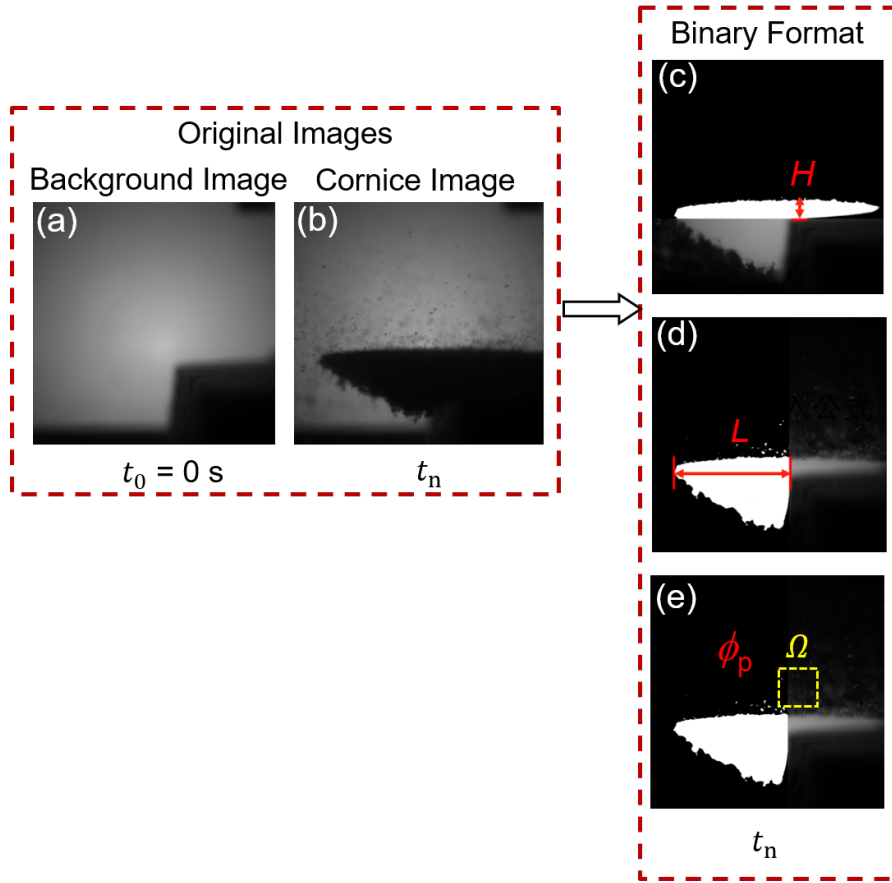
The pure deposition rates in length  $l_d$  and in thickness  $h_d$  are calculated as the sum of the growth rate and the absolute value of erosion rate:

$$l_d = l_g + |l_e| \quad (3)$$

$$h_d = h_g + |h_e| \quad (4)$$

A window  $\Omega$  with an area of 1 cm × 1 cm slightly above the snow cornice is chosen to calculate the ~~mass fluxes to avoid errors due to surface effects and background light problems, shown in Fig. 2(b).~~ The mass concentration of snow particles is calculated by predefining a low threshold value V2 which could clearly present the airborne snow particles, shown as ~~mean mass concentration of particles in the air as shown in~~ Fig. 2(e)e. Ignoring the overlapping particles, we calculate the total volume of snow particles in  $\Omega$  as the orthographic projection area of snow particles multiplied by its average diameter. Thus, the mass concentration  $\phi_p \phi_p$  ( $\text{kg m}^{-3}$ ) can be estimated as:

$$\phi_p \phi_p = \frac{\overline{\rho_i d_p \Sigma_{\Omega} g_j A_0}}{S_0 \times p} \frac{\overline{\rho_i d_p \Sigma_{\Omega} g_j A_0}}{S_0 \times p} \quad (5)$$



**Figure 2.** Post-Processing images using the grayscale method. (a)-(b) Raw images of background (a) and cornice (b). (c)-(e) Binary format of images with information of the amount of thickness accumulation / erosion and cornice  $H$  (c), length and volume growth  $L$  (d), and airborne snow particles mass concentration  $\phi_p$  captured in window  $\Omega$  (e).

where  $\rho_i$  ( $\text{kg m}^{-3}$ ) is the ice density,  $\overline{d_p}$  (m) is the averaged diameter,  $g_j$  is the binary value of the  $j^{\text{th}}$  pixel in window  $\Omega$ ,  $A_0 = \frac{7.7 \times 7.7}{2048 \times 2048} \text{ cm}^2$  is the area of a pixel,  $S_0 = 1 \text{ cm}^2$  is the area of the window  $\Omega$ ,  $p = 3.5 \text{ cm}$  is the depth of field where particles can be recognized/detected in this width range (Crivelli et al., 2016). The transport mass flux  $q_p$  ( $\text{kg m}^{-2} \text{ s}^{-1}$ ) can be estimated using:

$$q_p(z) = \phi_p(z) u_p \quad (6)$$

where  $\phi_p(z)$  is the mass concentration calculated by Eq. (1), and  $u_p$  is the averaged particle velocity, which is assumed to be 10% lower than the wind speed (Nishimura et al., 2014).

$$q_p(z) = A e^{-R_0 z} \quad (7)$$

where  $A$  and  $R_0$  are constants that change with wind speed. The transport rate  $Q$  ( $\text{kg m}^{-1} \text{s}^{-1}$ ) can be obtained by integrating the mass flux profiles over height:

$$Q = \int_0^{\infty} q_p(z) dz = \int_0^{\infty} A e^{-R_0 z} dz = -\frac{A}{R_0} e^{-R_0 z} \Big|_{z=0}^{z=\infty} = \frac{A}{R_0} \quad (8)$$

175 To quantify the exchange of snow between the mass flux and the cornice, we defined the relative mass flux collection efficiency (%) as:

$$E = \frac{S_c \times \rho_i}{Q} \times 100\% \quad (9)$$

where  $S_c = \frac{dA_c}{dt}$  is the growth rate of the cornice projected area  $A_c$ .

### 3 Results and discussions

#### 3.1 General observations on snow cornice formation

180 Using the case of  $U$  By post-processing the high-speed camera images from the experiments, the profiles of the snow cornice are obtained as shown in Fig. 3a. The time series of the cornice length  $L$ , thickness  $H$ , and the mass concentration of airborne snow  $\phi_p$  are then estimated as shown in Fig. 3b. Here, we use the case of wind speed  $u = 4 \text{ m s}^{-1}$  as an example, Figure 3(a) shows to present the cornice growth process. As is shown in Fig. 3b, the cornice size information associated with wind velocity speed and particle mass concentration are presented. The wind speed (black squares) increased from 0 to  $4 \text{ m s}^{-1}$  in about 210 s and was then kept stable during the cornice formation process. The particle mass concentration (blue circles) started to increase at  $t = 176 \text{ s}$  and reaches (marked in black dash line:  $u = u_t$ ) and reached a stable value at  $t = 250 \text{ s}$ . A The cornice started to form approximately at the same time as the drifting snow occurred with a detectable particle mass concentration. Its length (red triangles) and volume (green triangles) almost linearly increased during the stage with a stable snow concentration ( $\sim 1.4 \text{ kg m}^{-3}$ ) and wind speed ( $\sim 4 \text{ m s}^{-1}$ ). During the cornice accretion time, the cornice grew both in length and thickness, and the profiles of the cornice in different time stages are shown in the inset of Fig. 3(a). Its maximum length growth rate is  $3.2 \times 10^{-4} \text{ m s}^{-1}$ , and the average length growth rate during the stable wind speed is  $1.4 \times 10^{-4} \text{ m s}^{-1}$ . For comparison, in field observations, the measured accretion rate range is  $3.9 \times 10^{-6} - 4.7 \times 10^{-6} \text{ m s}^{-1}$  (Hancock et al., 2020) which is two orders of magnitude smaller than the experimental values. The main reason for the discrepancies between the laboratory and the field results is most likely due to observational differences. The wind speed for cornice formation in the wind tunnel is continuous and stationary, while it is fluctuating and intermittent in the field, which causes the effective time for cornice formation being much less in the field than the sampling time (several hours to days). Variation of cornice length (red triangles), cornice thickness (pink squares), cornice volume (green triangles), cornice length growth rate (light blue triangles), cornice thickness growth rate (grey triangles), wind speed (black squares) and particle mass concentration in the air (blue circles). Inset includes cornice profiles during different

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200 growth periods. (b) Two stages of cornice length (red circles) and thickness (black circles) growth for  $U = 4 \text{ m s}^{-1}$ . ( $T_{\text{air}} = -5$   
 $^{\circ}\text{C}$ ,  $U = 4 \text{ m s}^{-1}$ ) grow when the wind speed exceeded the threshold. The growth rate was not stable at first because the initial  
growth of cornice is in intermittent drifting snow when the aerodynamic entrainment is still dominant in the initial stage of  
drifting snow (Li et al., 2018). The linear length growth stage is when the wind speed and mass concentration values arrive  
stable.

205 During cornice accretion, there are two stages for the growth of cornice. As shown in Fig. 3(b), the red circles represent  
the length of the cornice, and the black circles represent the thickness of accumulated snow above the cornice the cornice.  
In the first stage, a few particles stop on edge and compose a 0.011 m small slab forms outward from the edge of the ridge  
model with a horizontal growth rate that is much higher than the vertical growth rate. and thin slab that forms leeward from the  
ridge model's edge. The shape profile of this slab is shown as from  $t_1$  to  $t_3$  in Fig. 3a. In the second stage, the cornice length  
and thickness simultaneously increase together and gradually reach a final length and final height until seeding ends. Once the  
210 seeding stops (from  $t = 430 \text{ s}$ ), mass flux disappears when stopping seeding because the redistribution of the snow depositions  
in the wind tunnel results in a surface morphology inhibiting aerodynamic entrainment. The aerodynamic entrainment happens  
on the newly formed cornice surface because the surface shear stress is over the threshold value. In this case, the aerodynamic  
entrainment only scours the thickness of the cornice.

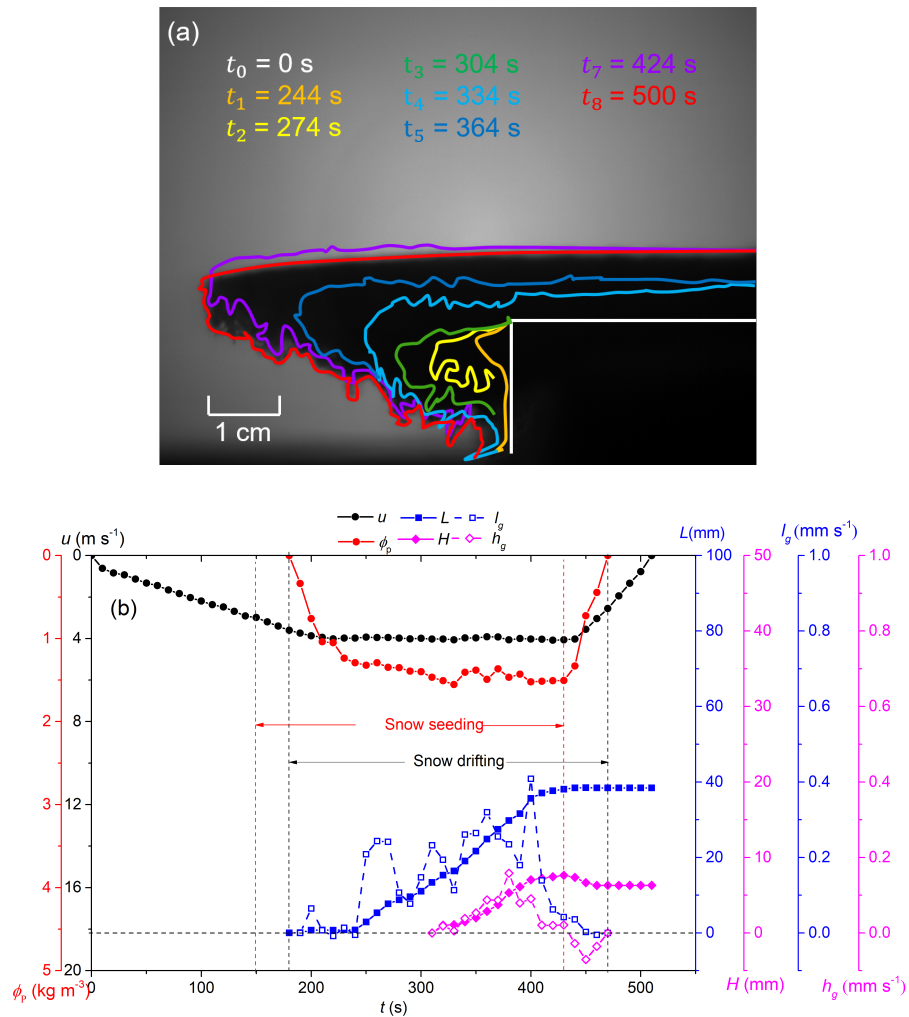
### 3.2 Suitable Wind Speed Range for Cornice Formation

215 Cornice formation was tested with wind speeds from  $3 \text{ m s}^{-1}$  to  $6.5 \text{ m s}^{-1}$  using  $0.5 \text{ m s}^{-1}$  increments. Mean cornice growth  
rates under all wind conditions were obtained by estimation of the slopes of the near-linear growth curves. As mentioned in  
Section 3.1, erosion on the newly formed snow cornice happens after stopping seeding for  $U > 3.5 \text{ m s}^{-1}$ . Therefore, in this  
section, we separately analysed the cornice growth rates (in length and in thickness) with seeding and the erosion rates (in  
length and in thickness) after seeding ended for each wind speed through a series of images shown as Fig. 4(a). 320 s in Fig.  
220 3b), the cornice thickness grows simultaneously with the length. With more layers overlapping on the surface, the cornice starts  
slightly bending down.

The growth rates in length and thickness can both be approximated by a quadratic function and reach the maximum value  
at moderate wind speeds ( $4\text{--}4.5 \text{ m s}^{-1}$ ). The erosion rates in length and thickness exponentially increase with the wind speed.  
In the cornice growing process, the length growth rate is faster than the thickness growth rate in each kind of wind. Once the  
225 wind speed is above  $4 \text{ m s}^{-1}$ , the erosion in length doesn't happen until the cornice has been eroded in thickness down to the  
original ridge model. This phenomenon indicates that the thickness erosion rate is always faster than the length erosion rate,  
which means that cornice surface thickness growth rate is more sensitive to erosion than the length growth rate.

There is no cornice formation for wind speeds equal to  $3 \text{ m s}^{-1}$  because of a missing saltation layer and snow transport.  
For wind speeds higher than  $6 \text{ m s}^{-1}$ , there are even no more chances for slabs to form on the model edge because of  
230 continuous erosion on the model surface. Moreover, it can be concluded that the thickness growth rate decreases with increasing  
wind velocity as net deposition on the surface gets smaller. The cornice length grows fastest when the wind speed value is  
approximately 40% higher than the rebound threshold wind speed in our case (Fig. 4(a)). (a) Growth rate (in red) and erosion

rate (in blue) in length (in squares) and in thickness (in triangles) under different wind speed conditions. (b) Angle  $\theta$  of snow cornice in wind speeds of  $3.5 \text{ m s}^{-1}$ – $6 \text{ m s}^{-1}$ . The results show that drifting snow at moderate wind speed is needed for cornice



**Figure 3.** (a) Cornice profiles in the growth process. (b) Variation of cornice length (blue squares), thickness (pink squares), length growth rate (blue hollow squares), cornice thickness growth rate (pink hollow square), wind speed (black circles) and particle mass concentration in the air (red circles).

235 formation, where a similar conclusion can be found from field observations. Overall, the wind speed ranges discussed above depend on the properties of drifting snow and the friction velocity affected by the local topography.

Moreover, the interplay between deposition and erosion determines the final shape of cornices. In our experiment, the cornices are wedged-like with an angle of  $18^\circ$  to  $35^\circ$ . When the cornice length reaches the boundary of the view, we stop

240 seeding. Erosion first affects the thickness of the snow cornice. The downward bending continues (outlines from  $t_7$  to  $t_8$  in  
 Fig. 3a and  $t = 430 - 440$  s in Fig. 3b). During this period, aerodynamic entrainment dominates the erosion process. As is  
 shown in Fig. 4(b), which is consistent with field observations. The angle of the cornice is one of the factors that determine  
 cornice stability. Smaller angles increase the danger of crackdown. In our experiment, the most stable structure is formed by  
 moderate wind. The higher the wind speed is, the more unstable the cornice becomes. 3b, the mass flux markedly decreases as  
 the aerodynamic entrainment is inhibited by the surface morphology formed during the redistribution of the snow deposition  
 245 in the RWT.

### 3.2 Mass flux and collection efficiency

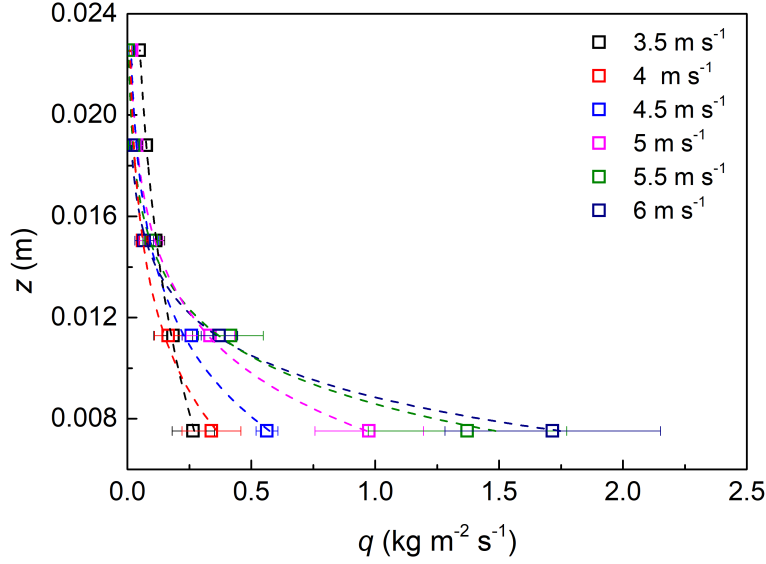
Since the magnitude of drifting snow is critical for the vertical and horizontal cornice growth rates, snow the mass transport  
 rates were calculated for the different experiments and analysed-analyzed in terms of mass exchange between the cornice  
 and the saltation layer. The results were compared to field data to underline the relevance of our results for actual outdoor  
 250 conditions. First, the transport mass flux  $q_p$  can be estimated using:-

$$q_p(z) = \phi_p(z) \bar{u}_p(z = 0.4)$$

where  $\phi_p(z)$  is the mass concentration calculated by Eq. (2), and  $\bar{u}_p$  is the averaged particle velocity, which is assumed to be  
 10% lower than wind speed (Nishimura et al., 2014). Thus, mass flux-mass flux variation with height over snow cornices can  
 be estimated by multiple windows  $\Omega$  that are continuously distributed in height under different wind conditions, as is shown in  
 255 Fig. 5. For all wind conditions, the 4. The mass flux exponentially decreases with increasing height, the increasing height in  
 each wind condition, and its value increases with the wind speed, which is consistent with previous results (Takeuchi, 1980;  
 Lehning et al., 2002; Kosugi et al., 2008; Lü et al., 2012; Crivelli et al., 2016; Melo et al., 2022). It also increases overall with  
 the increasing wind speed.-

Table 2. Coefficients of  $A$  and  $R_0$  in-for different wind speeds  $U_u$ .

Wind Speed $U_u$ (m s <sup>-1</sup> )	$A$	$R_0$
3.5	0.62	109.42
4	2.09	218.5
4.5	3.63	245.32
5	8.44	288.16
5.5	24.05	370.31
6	40.72	418.78



**Figure 4.** Mass flux variation with height under different wind conditions ( $3.5\text{--}6\text{ m s}^{-1}$ ). The dashed lines are exponential fitted.

The transport mass flux profile can be described by an exponential law (Nishimura and Nemoto, 2005; Sugiura et al., 1998)

260 ÷

$$q_p(z) = Ae^{-R_0 z}$$

where  $A$  and  $R_0$  are constants that change with wind speed. By fitting Eq. (37) using the estimated transport mass flux from the shadow images, we obtain  $A$  and  $R_0$  for different wind speeds, as summarized in Table 2. Their fitted functions are:  $A = -2092 + 1840U - 596U^2 + 84U^3 - 4U^4$  and  $R_0 = -285.95 + 118.29U$ . As is shown in Fig. 4, the transport mass flux profile can

265 be described by an exponential law (Nishimura and Nemoto, 2005; Sugiura et al., 1998).

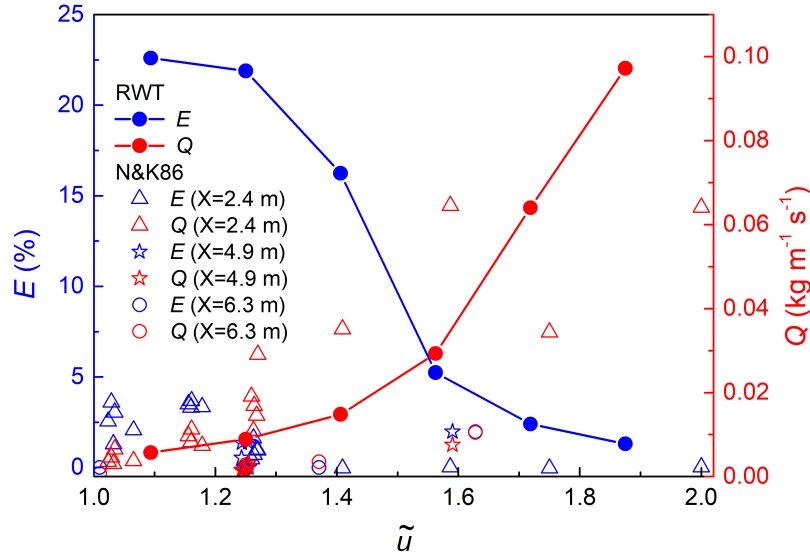
The transport rate can be expressed as:

$$Q = \int_0^{\infty} q_p(z) dz = \int_0^{\infty} Ae^{-R_0 z} dz = -\frac{A}{R_0} e^{-R_0 z} \Big|_{z=0}^{z=\infty} = \frac{A}{R_0} = \frac{-2092 + 1840U - 596U^2 + 84U^3 - 4U^4}{-285.95 + 118.29U}$$

by integrating the mass flux profiles over height. To quantify the exchange of snow between the mass flux and the cornice, we defined the mass flux collection efficiency as:

270 
$$E = \frac{S_{\text{cornice}} \times \rho_{\text{ice}}}{Q_{\text{drift}}} \times 100\%$$

where  $S_{\text{cornice}} = \frac{dA_c}{dt}$ . A non-dimensional wind speed  $\tilde{u} = \frac{u}{u_t}$  is defined here to compare with the experimental results of Naito and Kobayashi (1986). In this definition,  $u_t$  is the growth rate of the cornice projected area  $A_c$ , therefore including



**Figure 5.** Collection efficiency  $E$  (in blue) and snow transport rate  $Q$  (in red) under different non-dimensional wind speeds  $\tilde{u}$ .  $X$  represents the distance from the snow particle feeding point to the mass collection pits where the cornice grows. Lines are for ring wind-tunnel experiments, hollow scatters are for N&K86. N&K86 represents the experiment results of Naito and Kobayashi (1986)

horizontal and vertical threshold wind speed which can be considered as the lower limit wind speed value for cornice growth. As is shown in Fig. 6, the maximum collection efficiency appears for the minimum wind speed of  $3.5 \text{ m s}^{-1}$ . With 5, the mass collection efficiency in both experiments decreases with the increasing wind speed and drift rate, the collection efficiency the corresponding drift rate. Our experimental results are much larger than that in N&K86, which is mainly due to the different wind tunnel sizes.

The collection efficiency cannot directly reflect the cornice growth characteristics because it represents the proportion of snow particles on the cornice decreases. Collection efficiency  $E$  (black circles) and snow transport rate  $Q$  (blue circles) under different wind speeds:

According to Hancock et al. (2020), the appropriate wind speed range of cornice growth in the field is  $12\text{--}30 \text{ m s}^{-1}$  (in a height of 2.8 m). To compare it with our experiments, passing through the edge and stopping by. This value only reflect the effective contribution of the mass concentration in this wind speed range was estimated by the following steps for our experiments:-

1) Dimensionless snow transport rate on the flat surface  $\tilde{Q} = \frac{gQ}{\rho_a u_{*t}^3}$  can be calculated drifting snow to the snow cornice formation under different wind conditions. Thus, to characterize the growth rate of cornice, it is necessary to analyze the absolute amount of accumulated particles as a function of the dimensionless wind velocity  $\tilde{u} = \frac{u_w}{u_{*t}} = \frac{U}{U_t}$ , where  $u_{*t} = 0.25$  time and wind speed which is introduced in the Section 3.3.

### 3.3 The suitable wind speed range for cornice formation

290 Cornice formation was tested with wind speeds from 3 m s<sup>-1</sup> is the threshold friction velocity Leonard et al. (2012), U<sub>T</sub> is the  
corresponding threshold wind speed at a certain height (U<sub>10.4</sub> = 3.2 m to 6.5 m s<sup>-1</sup> in wind tunnel and U<sub>12.8</sub> = 11 m using 0.5 m  
s<sup>-1</sup> in field), ρ<sub>a</sub> = 1.23 kg m<sup>-3</sup> is the air density. Several common formulas of the function are shown in Table 3. Dimensionless  
snow transport rate,  $\tilde{Q}$  Dimensionless Transport Rate Author and Year  $\tilde{Q} = C \sqrt{\frac{d}{d_R}} \tilde{u}^3$ , C = 2.8 (non-uniform size), C = 1.5 (uniform size)  
Bagnold, 1941  $\tilde{Q} = \tilde{u}^3 (1 - \frac{1}{\tilde{u}^2}) (2.6 + 2\frac{1}{\tilde{u}} + 2.5\frac{1}{\tilde{u}^2})$  Sørensen, 2004  $\tilde{Q} = \tilde{u}^3 (1 - \frac{1}{\tilde{u}^2}) (3.7 + 4.7\frac{1}{\tilde{u}} - 4\frac{1}{\tilde{u}^2})$  Li et al., 2018  $\tilde{Q} = C(\tilde{u}^2 - 1)$ , C = 8.5  
 295 Durán et al., 2011

2) Blowing snow particle concentration in the air can be calculated as Pomeroy and Gray (1990):-

$$\phi_{\text{sal}} = \frac{Q}{h_{\text{sal}} U_{\text{sal}}}$$

where saltation height and saltation layer wind speed can be expressed as:-

$$h_{\text{sal}} = 1.6 \frac{u_*^2}{2g}$$

$$300 \quad U_{\text{sal}} = 2.8 u_{*t}$$

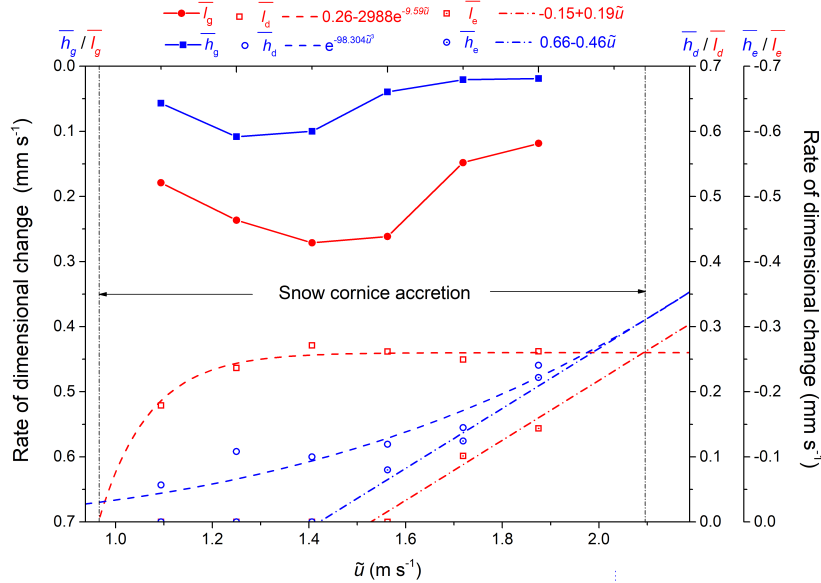
After substituting increments. In each wind condition, the averaged cornice growth rates in length and thickness are:  $\bar{l}_g$  (m s<sup>-1</sup>)  
and  $\bar{h}_g$  (m s<sup>-1</sup>) (with seeding), and erosion rates:  $\bar{l}_e$  (m s<sup>-1</sup>) and  $\bar{h}_e$  (m s<sup>-1</sup>) (without seeding) are obtained by estimating the  
slopes of the near-linear growth/erosion curves as is shown in the Fig. 3. Thus, the averaged pure deposition rates in length  $\bar{l}_d$   
 305 and thickness  $\bar{h}_d$  can be calculated by the Eq. (??) and Eq. (??) into Eq. (6), the saltation particle mass concentration can be  
expressed as:-

$$\tilde{\phi}_{\text{sal}} = \frac{\phi_{\text{sal}}}{\rho_a} = \frac{\tilde{Q}}{2.24 \tilde{u}^2}$$

Figure. 7 shows the comparison of mass concentration between field situations and our wind tunnel conditions. When  $1.1 < \tilde{u} < 1.9$ , the mass concentration values in the wind tunnel are of the same order of magnitude as the estimated results of field situations (Bagnold, 2012; Sørensen, 2004; Li et al., 2018). However, due to the limit and size influence of the ring wind tunnel itself, the local wind speed on top of the cornice surface increases due to a reduction of the wind tunnel cross-section. Thus, when  $\tilde{u} > 1.9$ , the mass concentration in the wind tunnel experiment has already reached the value of that in site observation with  $\tilde{u} \approx 2.6$ , which results in the severely scouring and erosion on the model edge, which may not commonly happen in nature. 3-4).

315 For the wind tunnel experiment and the natural situation, neither weak wind ( $\tilde{u} < 1.1$ ) nor strong wind ( $\tilde{u} > 2.7$ ) is suitable for the cornice growth, and only under moderate wind speed ( $1.1 \leq \tilde{u} < 2.7$ ) cornices grow. This result is in good agreement with the other field observation results with the As is shown in the Fig. 6, there is no cornice formation for wind speed lower than the threshold wind speed because of a missing saltation layer and snow transport. The extension line of the pure deposition rate in

Dimensionless particle concentration in different wind velocity conditions. Dash lines in colours represent the field experiment values in different models, and the red circles represent the wind tunnel experiment values.



**Figure 6.** Growth rates, erosion rates, and the pure deposition rates in length and thickness under different wind conditions. The fitted functions are plotted in dashed lines.

length tends to zero around the threshold wind speed for snow transport. Thus, we can conclude that the lower limit wind speed ranges of  $10\text{--}32.4\text{ m s}^{-1}$  (Vogel et al., 2012; Eckerstorfer et al., 2013; McClung and Schaerer, 2006). Thus, our wind tunnel experiment reflects the necessary mass concentrations of natural situations for cornice growth. The lower/upper limit of for cornice accretion is close to the friction velocity for cornice growth can be estimated, which can be helpful for the prediction of cornice formation and collapse. For example, in the case of  $z_0 = 6.3 \times 10^{-5}\text{ m}$  (Nishimura and Nemoto, 2005), threshold wind speed for snow transportation, which is consistent with the field study (McClung and Schaerer, 2006; Hancock et al., 2020).

The cornice length growth rate  $l_g$  reaches its maximum when the corresponding proper friction velocity range for wind speed is approximately 40 % higher than the threshold wind speed. At this wind speed, the net deposition rate ( $l_d - l_e$ ) in length reaches maximum. The erosion rates in length and thickness approximately linearly increase with the wind speed. In the cornice growing process, the length growth rate ( $l_g$ ) is higher than the thickness growth rate ( $h_g$ ) at all wind speed conditions. The erosion in length takes place later than in thickness, and the thickness erosion rate is always approximately 30 % higher than the length erosion rate ( $l_e = 0.7h_e$ ).

The pure deposition rate in length  $l_d$  increases rapidly at first and stabilizes with the wind speed, while the erosion rate in length  $l_e$  linearly increases with the natural situation is  $0.45\text{--}1.12\text{ m s}^{-1}$ , wind speed. The values of  $l_d$  and when the friction velocity  $u_* > 1.12$   $l_e$  arrive equivalent at the wind condition of about  $6.5\text{ m s}^{-1}$ , at which point the mass of the

pure accumulation and the erosion is balanced. Thus, the upper limit wind speed of snow cornice formation in our case is 6.5  
335  $\text{m s}^{-1}$  ( $U > \bar{u}^{-1}$  which is 2.03 times of threshold wind speed).

Overall, the cornice growth process has two stages: In the first stage, a thin slab grows and overhangs at the edge. In the  
second stage, cornice thickness and length both increase simultaneously. The collection efficiency, reflecting the effective  
contribution of the drifting snow to the snow cornice formation, cannot directly reflect the cornice growth characteristics.  
Instead, the pure deposition rates, the erosion rates, and the growth rates both in length and thickness were analyzed separately  
340 for all wind conditions. From the results we can conclude that in all wind conditions, the cornice starts to grow when the wind  
speed exceeds the threshold value, and starts to scouring when the erosion rate is over the pure deposition rate. The cornice  
only grows at a moderate wind speed range (1-2.03  $\bar{u}$ ). The length erosion rate of the cornice is typically  $30 \text{m s}^{-1}$ , the newly  
formed snow cornice surface starts being scoured by wind or cracked off which leads to a snow mass loss. % lower relative to  
the thickness erosion rate. The length growth rate gets maximum at the wind speed is 40 % over the threshold. The presented  
345 framework for characterizing cornice accretion may provide a basis for future field and laboratory studies under different  
conditions.

## 4 Discussion

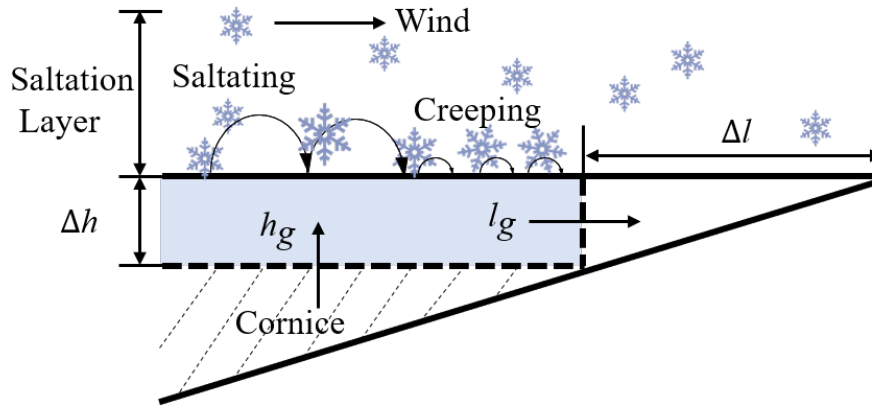
From the experimental results, we can conclude that cornice growth is a process of mass accumulation overgrowing the ridge  
under the action of wind force, accompanied by bending and erosion. The growth process of snow cornice has two stages,  
350 which can be described with a schematic shown in Fig. 7. The first stage can be assumed as a formation of the one-particle  
diameter-thickness snow slab composed of sticking particles at the edge. The first process is mainly determined by the spatial  
variation of the mass transport rate along the flow direction. The second stage can be assumed as a repeated process of length  
growth-thickness growth. The length growth is considered as a horizontal creeping of the newly formed snow layer, driven  
by the drifting snow. The thickness growth is considered as a comprehensive result of particle deposition and erosion at the  
355 edge. Thus, the second growth process is mainly dependent on the wind speed, the non-dimensional, spatial variation of mass  
concentration, and the particle interaction force.

### 4.1 A conceptual model for cornice formation

In here, we analyze the snow cornice as the shaded area shown in the Fig. 7. Based on the law of mass conservation, the cornice  
thickness growth rate  $h_g$  can be calculated as the difference between the pure deposition rate in thickness  $h_d$  and the thickness  
360 erosion rate  $h_e$ . In which, the pure deposition rate in thickness  $h_d = K_d \frac{\phi_p}{\rho_c}$  is calculated by the deposition rate of mass on the  
surface per unit time. Thus, the thickness growth rate  $h_g$  can be written as:

$$h_g = K_d \frac{\phi_p}{\rho_c} - h_e \quad (10)$$





**Figure 7.** Schematic of snow cornice growth.

where  $K_d$  is the deposition coefficient ( $\text{m s}^{-1}$ ),  $\rho_c = 147 \text{ kg m}^{-3}$  is the average snow density of the cornice as measured during the experiments. This value is close to the fresh snow and lower than that in the field of  $\sim 300 \text{ kg m}^{-3}$  (Naruse et al., 1985), which might be related to the long-term compaction of the snowpack in the field.

The cornice length growth is considered as the forward creeping of the surface layer which is driven by the drifting snow saltation. The cornice length growth rate  $l_g$  can be estimated as the difference between the pure deposition rate in length  $l_d$  and the length erosion rate  $l_e$ . In which  $l_d$  is considered as the moving distance  $\Delta l$  (m) of a newly formed snow layer (blue area in Fig. 7) with one particle diameter in thickness  $\Delta h$  (m) per unit time. The pure deposition rate in length  $l_d$  is related to the mass transport rate  $Q$  and the non-dimensional horizontal collection coefficient  $f_i$ :

$$l_g = \frac{Q f_i}{\rho_c d_p} - l_e \quad (11)$$

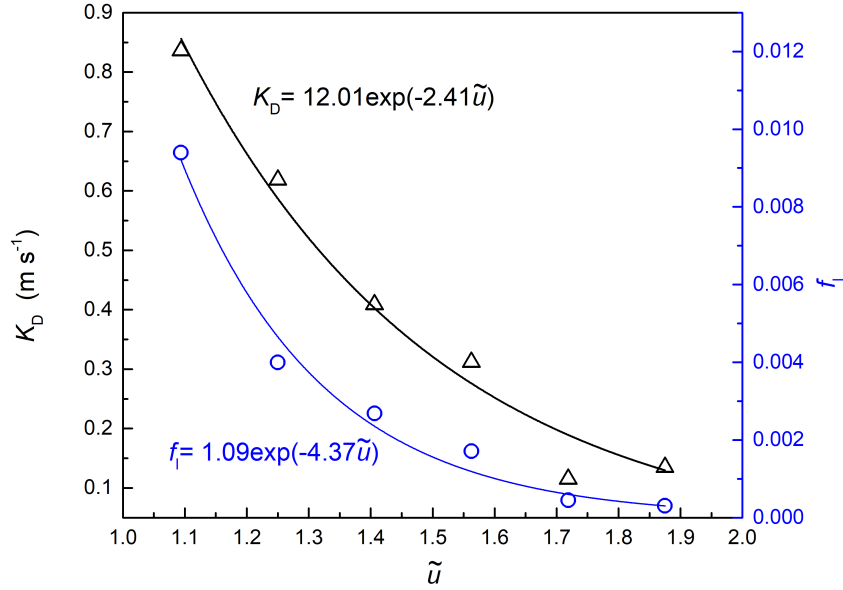
As we already measured the cornice thickness growth rate  $h_g$ , thickness erosion rate  $h_e$ , the cornice length growth rate  $l_g$ , length erosion rate  $l_e$ , the air mass concentration  $\phi_p$ , and the mass transport rate  $Q$ , the deposition coefficient and the horizontal collection rate can be estimated as  $K_d = \frac{(h_g + h_e)\rho_c}{\phi_p}$  and  $f_i = \frac{(l_g + l_e)\rho_c d_p}{Q}$ , which exponentially decrease with the wind speed, as shown in Fig. 8.

## 4.2 Field predictions

To validate our conceptual model, we compare the results with two cases of the field observations.

### 4.2.1 Case I: Comparison of suitable wind condition with Vogel et al. (2012)

Vogel et al. (2012, abbr. as VF2012) showed cornice evolution along the ridgeline of the Gruvefjellet plateau mountain above Nybyen in the period 2008–2010. They found that the cornice accretion happened during the entire snow seasons, when the averaged hourly maximum wind speeds exceeded  $12 \text{ m s}^{-1}$ , with a minimum of at least  $10 \text{ m s}^{-1}$ .



**Figure 8.** Deposition coefficient and the horizontal collection rate in all wind conditions. The solid lines are the fit curves.

Considering the cornice accretion always appears in snowstorms, we assume that the snow transport rate  $Q$  in the field can be expressed as the same value as its value in the saturated saltation (Sørensen, 2004):

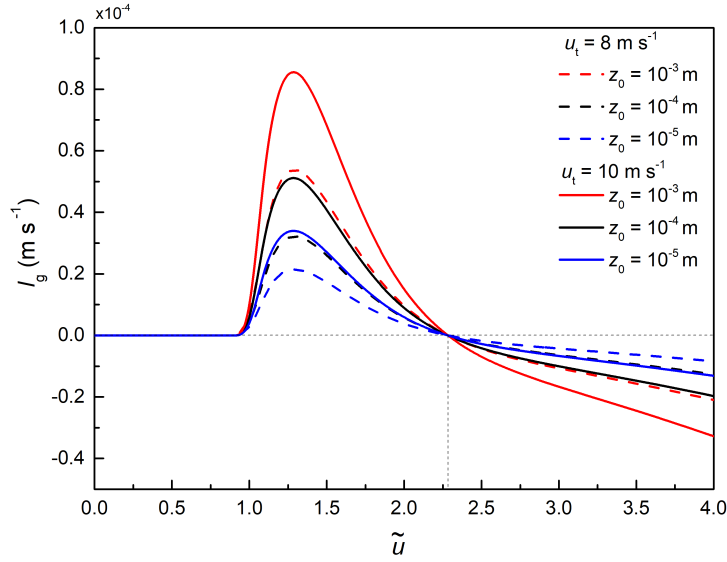
$$Q = \frac{\rho_a}{g} u_*^3 \left(1 - \frac{u_{*t}^2}{u_*^2}\right) \left(2.6 + 2 \frac{u_{*t}}{u_*} - 2.5 \frac{u_{*t}^2}{u_*^2}\right) \quad (12)$$

385 where  $u_* = \frac{\kappa u_f}{\ln(z_f/z_0)}$  is the friction velocity ( $\text{m s}^{-1}$ ) which is calculated with the field wind speed  $u_f$  ( $\text{m s}^{-1}$ ) at height  $z_f = 2.8$  m.  $\kappa = 0.4$  is the Von Kármán constant,  $g = 9.8 \text{ m s}^{-2}$  is the gravitational acceleration and  $z_0$  (m) is the aerodynamic roughness length.  $u_{*t}$  ( $\text{m s}^{-1}$ ) is the threshold friction velocity which is calculated based on the local threshold wind speed  $u_t$  ( $\text{m s}^{-1}$ ).

Then we can estimate the potential maximum erosion rate as the aerodynamic entrainment rate by:

$$390 M_e = m_p \cdot \eta_{ae} \rho_a (u_*^2 - u_{*t}^2) \quad (13)$$

where  $m_p = \frac{1}{6} \pi d_p^3 \rho_i$  is the mass of a snow particle, in which the average particle diameter  $d_p$  in the field is assumed as  $300 \mu\text{m}$  (Nishimura et al., 2014).  $\eta_{ae} = 6 \times 10^5$  ( $\text{grains N}^{-1} \text{ s}^{-1}$ ) is an empirical parameter (Clifton and Lehning, 2008).



**Figure 9.** Estimations of cornice length growth rates in the fields.

Considering the ratio of erosion rate in thickness and length  $l_e/h_e$  is about 0.7, the erosion rate in thickness can be written as  $h_e = 0.7 \frac{M_e}{\rho_c}$ . Thus, we can rewrite the length growth rate  $l_g$  in Eq. (11) as:

$$395 \quad l_g = \frac{Q f_t}{\rho_c d_p} - 0.7 M_e / \rho_c \quad (14)$$

Thus, we could infer that the length growth rate  $l_g$  is only depended on variables of the field wind speed  $u_f$ , the threshold wind speed  $u_t$ , and the roughness length  $z_0$ . To test the sensitivity of the input parameters, we choose different  $z_0$  and  $u_t$  to estimate the length growth rate in the wind speed range of VF2012, shown as Fig. 9. The automatic weather station in Gruvefjellet is located at  $\sim 300$  m from the cornice on the plateau. The wind station is at a flat field, and the roughness length  $z_0$  can be assumed as the measurement values on the flat snow surface. The roughness lengths  $z_0$  vary in snow covers (Clifton et al., 2006), which typically vary over two orders of magnitude: from  $10^{-5}$ - $10^{-3}$  m for the fresh snow in the fields (Brock et al., 2006; König-Langlo, 1985). As is shown in the Fig. 9, the roughness length and the threshold wind speed only have effects on the magnitude of the maximum value of growth rates, while the suitable non-dimensional wind speed range remains the same. The predicted wind range for snow cornice formation is about  $1 \sim 2.26$  times threshold wind speed, namely  
405  $10 \sim 22.6 \text{ m s}^{-1}$ , which agrees with the field observations. And the maximum value is about 30 % higher than the threshold wind speed. There is no available length growth rate data in VF2012, so we use the follow case to validate the length growth rate. For it is in the same site, we use  $z_0 = 10^{-4}$  m and  $u_t = 10 \text{ m s}^{-1}$  in the following modeling.

#### 4.2.2 Case II: Comparison of the length growth rate with Hancock et al. (2020)

Hancock et al. (2020, abbr. HF2020) used a Riegl® Laser Measurement Systems VZ-6000 ultra-long-range terrestrial laser scanner to repeatedly scan the Gruvefjellet and Platåberget cornice systems throughout the 2016–2017 and 2017–2018 winter seasons. Three cornice accretion events were recorded with the mean length growth rate over  $10 \text{ mm h}^{-1}$ , which is about  $3.9\text{-}4.7 \times 10^{-6} \text{ m s}^{-1}$ . However, in our experiment, the average length growth rate range is  $1.2\text{-}2.7 \times 10^{-4} \text{ m s}^{-1}$ . The main reason for the discrepancies between the laboratory and the field results is due to the temporally and spatially constrained estimations of the threshold wind speeds for cornice accretion and cornice horizontal length growth rate (Vogel et al., 2012; Hancock et al., 2020). In the field, snow cornices have multiple growth periods in snowstorms that last a few hours. While in the RWT experiment, we mainly focused on a continuous growth process of a snow cornice. The fluctuating and intermittent wind in the field differs from the steady and stationary wind in the RWT, and this also causes the effective time for a cornice formation being much less than the sampling time (several hours to days). The sampling frequency is not sufficient to catch the complete accretion period for the wind in the field is gusty and intermittent. Also, in the field the cornice may partially collapse from time to time which is not recognized during the storm without any laser scanning. Thus, it is difficult to estimate the cornice length growth rate based on the daily averaged wind speed from HF2020. Here, we use the Weibull probability density function to reproduce a high resolution time series of wind speed (Fig. 10a), which can be expressed as:

$$p(u) = \left(\frac{k}{\lambda}\right) \left(\frac{u}{\lambda}\right)^{k-1} e^{-\left(\frac{u}{\lambda}\right)^k} \quad (15)$$

in which,  $k$  is the shape factor which is normally between 1.5 to 3, depending on the wind variability. Smaller  $k$  represents more gusty wind. For example  $k=2$  represents for the moderately gusty wind (Seguro and Lambert, 2000). In here, we assumed it as 1.7.  $\lambda$  is the scale factor which is calculated based on the daily averaged wind speed  $\bar{u}$  and the gamma function of the inverse of the shape factor  $k$ :

$$\lambda = \frac{\bar{u}}{\Gamma\left(1 + \frac{1}{k}\right)} \quad (16)$$

Figure 10a shows an example of wind speed time series produced by using Eq. 15 with a mean wind speed of  $5.43 \text{ m s}^{-1}$  and time interval of 10 minutes. From the time series, we can estimated the length growth rate as:

$$l_g = \frac{1}{T} \int_0^T \left( \frac{Q(u) f_l(u)}{\rho_c \bar{d}_p} - 0.7 E(u) / \rho_c \right) dt \quad (17)$$

where  $T$  (min) is the sampling time of the scanner images. The transport rate  $Q(u)$ , horizontal collection rate  $f_l(u)$ , and the mass erosion rate  $E(u)$  are the functions of wind speed  $u$  in time series. To test the sensitivity of the time interval  $dt$  (min), we use values of 5 min, 10 min, 15 min, 30 min, 1 hour, 2 hour, and the estimated growth rates are shown in Fig.10b. The length growth rate trends to a stable value when the time interval is shorter than 10 minutes. Thus, in the following analysis, we used 10 minutes as the time interval of wind data sampling.

Table 3 shows the averaged length growth rates in three cornice accretion events in HF2020. The averaged length growth rates  $l_g$  calculated from the model are comparable with that values from TLS data  $l_g^f$  ( $\text{m s}^{-1}$ ) in the field (Hancock et al., 2020), which indicates that our model has the potential ability to predict the cornice accretion in the field.

**Table 3.** Comparison results with field observations.

Location	Dates	$l_g^f \times 10^{-6}$ ( $\text{m s}^{-1}$ )	$l_g \times 10^{-6}$ ( $\text{m s}^{-1}$ )
Plataberget	Feb17-Feb28	4.72	1.70±0.49
Gruvefjellet	Jan12-Jan21	4.72	1.47±0.74
Paltaberger	Apr25-May01	3.80	1.37±0.52

440 What needs to be mentioned is that to enhance the model accuracy, the values of  $K_d$  and  $f_l$  inferred in this prediction model still need re-estimation and corrections for the natural larger-scale snow cornice. These two parameters may be influenced by the local topographical features. For future accurate field predictions on the cornice on a larger scale, more field measurement data are needed, such as the snowpack thickness on the root of a cornice, the mass concentration, the threshold friction velocity, roughness length, and cornice density to calculate the proper values for  $K_d$  and  $f_l$  in the field.

## 445 5 Conclusions and Outlook

~~This manuscript introduced the wind tunnel experiment of the snow cornice accretion process, investigated by applying the method of shadow photography. In our experiments,~~

We carried out the RWT experiments and studied the suitable wind condition for cornice formation and growth. The results show that the snow cornices only grow at moderate wind speed ( $3.5\text{--}6\text{ m s}^{-1}$ ) with with a sufficient snow mass flux over the ridge of the model. The ~~final shape of the cornice is wedge-like due to the different growth rates in horizontal and vertical directions~~ cornice growth process has two stages. The vertical growth ~~was found to be~~ rate of the cornice is typically lower relative to the horizontal growth. ~~Erosion of newly formed cornice starts for wind speeds higher than  $4\text{ m s}^{-1}$  and first reduces the thickness of the~~ The mass collection efficiency decreases with the increasing wind speed and the corresponding drift rate, which can not be considered the indicator for cornice growth. Instead, the growth rates of cornice in length and thickness are determined by the combined effects of mass accumulation and erosion. The lower limit of wind speed is the threshold wind speed for snow transport, and the upper limit value of wind speed is when the deposition rate and the erosion rate arrive balanced. The most favorable wind condition in the experiment for cornice growth is  $4.5\text{ m s}^{-1}$ , which is approximately 40 % higher than the threshold wind speed for snow transport. ~~Mass collection efficiency, reflecting particulate matter exchanges between the air and the ground surface, is put forward in this work. During the experiment, the mass collection efficiency decreases with the increasing wind speed and the corresponding drift rate. A comparison of the mass concentration during snow drifting in the wind tunnel and field experiments under the corresponding wind conditions shows that our experimental results,~~

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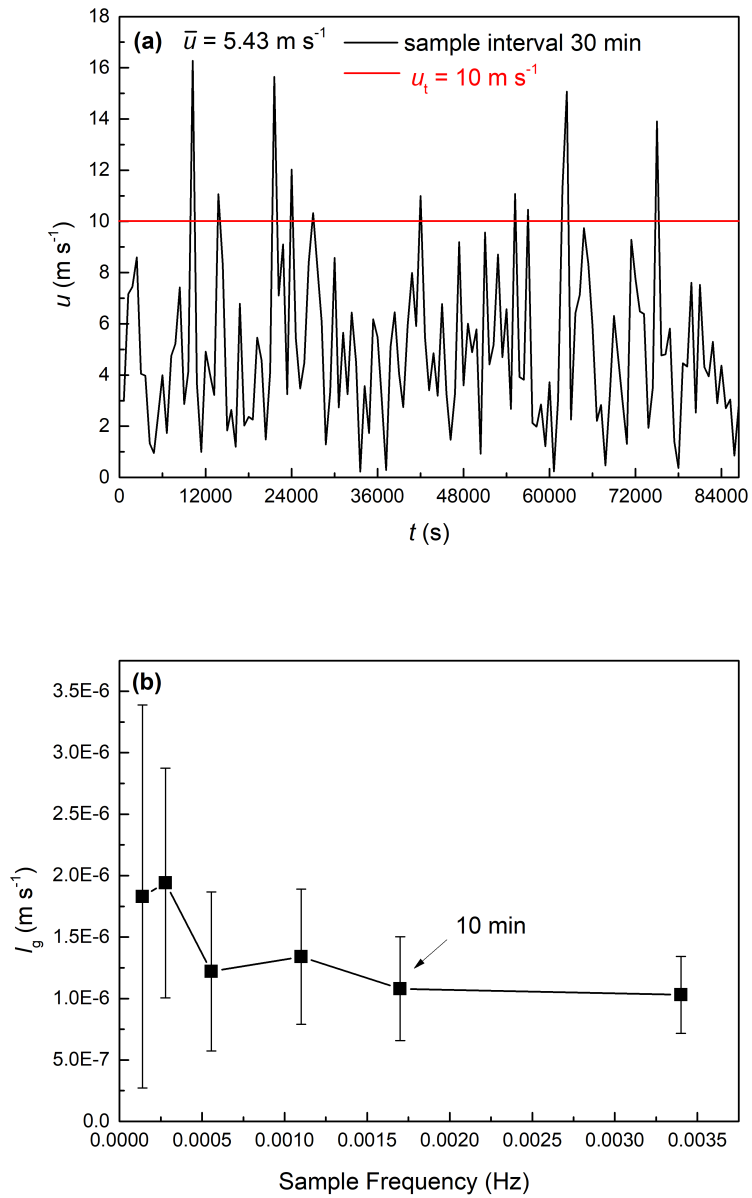


Figure 10. (a) Time series of wind speed  $u$  in one day. (b) Average length growth rates in different sample frequency.

~~when properly non-dimensionalised, represent environmental conditions for cornice formation.~~, at which the net deposition rate in length gets maximum.

This work is a preliminary quantitative investigation of snow cornice formation. More detailed studies on the deposition process on snow cornices should be conducted in the future, e.g., As one of the main meteorological factors, Based on the experimental results, a conceptual model is proposed for interpreting the mechanism of cornice growth. The model can be applied to fields to predict the length growth rates and the suitable wind speed range, mainly determined by the parameters such as roughness length and the temperature will also potentially impact cornice formation. For example, higher environmental temperature could enhance fast sintering, which may be an essential mechanism. Still, it could also decrease air mass flux due to the stronger cohesion force, making it more difficult for particle entrainment. In this manuscript, we only take one kind of temperature  $T = -5^{\circ}\text{C}$  as an example and will study the temperature influence in the future. Wind speeds for which value the growth rate reaches its maximum and the wind speed limit threshold wind speed, thus the local surface snow conditions. From the estimations at the study site of Gruvefjellet, we can conclude that the wind speed range of cornice growth is from 1-2.5 times of the threshold wind speed, which is in line with the previous observations in the fields. It is found that the most favorable wind condition for cornice growth ~~may differ for different temperatures and particle shapes. According to previous studies, the electrostatic force of snow particles may also play a significant role but hasn't been confirmed yet. The shape of the ridge model should be another critical factor~~ is approximately 30 % higher than the local threshold wind speed. The discrepancies in the knowledge of the suitable wind speed range in the previous wind tunnel experiment and the field observations are mainly due to the different turbulent structures produced behind the leeward area. To investigate these influencing factors, high-speed images of snow particle motion over snow cornices would be helpful differences in the local roughness lengths and the threshold wind speeds. In a future study, improvements of our model, such as predicting the snow cornice growth rates more accurately, still need higher frequency observation data on cornice growth and erosion and the measurements on the relevant parameters.

*Author contributions.* YHX, LG, and BW designed the experiments. YHX and LG carried out the experiments, performed the data analysis, and prepared the first draft. ML, ZJ, and BW reviewed and edited the paper. HN and ML organized this study, contributed to its conceptualization, discussion, and finalized the paper.

*Competing interests.* The authors declare that they have no conflict of interest.

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