



1 Evaluating Simplifications of Subsurface Process

2 Representations for Field-scale Permafrost Hydrology Models

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Abstract. Permafrost degradation within a warming climate poses a significant environmental 6 7 threat through both the permafrost carbon feedback and damage to human communities and 8 infrastructure. Understanding this threat relies on better understanding and numerical 9 representation of thermo-hydrological permafrost processes, and the subsequent accurate 10 prediction of permafrost dynamics. All models include simplified assumptions, implying a tradeoff between model complexity and prediction accuracy. The main purpose of this work is to 11 investigate this tradeoff when applying the following commonly made assumptions: (1) assuming 12 13 equal density of ice and liquid water in frozen soil; (2) neglecting the effect of cryosuction in 14 unsaturated freezing soil; and (3) neglecting advective heat transport during soil freezing and thaw. 15 This study designed a set of 62 numerical experiments using the Advanced Terrestrial Simulator (ATS v1.2) to evaluate the effects of these choices on permafrost hydrological outputs, including 16 17 both integrated and pointwise quantities. Simulations were conducted under different climate 18 conditions and soil properties from three different sites in both column- and hillslope-scale 19 configurations. Results showed that amongst the three physical assumptions, soil cryosuction is 20 the most crucial yet commonly ignored process. Neglecting cryosuction, on average, can cause 10% 21 $\sim 20\%$ error in predicting evaporation, 50% $\sim 60\%$ error in discharge, 10% $\sim 30\%$ error in thaw 22 depth, and $10\% \sim 30\%$ error in soil temperature at 1 m beneath surface. The prediction error for 23 subsurface temperature and water saturation is more obvious at hillslope scales due to the presence 24 of lateral flux. By comparison, using equal ice-liquid density has a minor impact on most 25 hydrological variables, but significantly affects soil water saturation with an averaged $5\% \sim 15\%$ error. Neglecting advective heat transport presents the least error, 5% or even much lower, in most 26 the chose n conceptory variables for a general Arctic tundra system, and can decrease the simulation time at hillslope 27 scales by $40\% \sim 80\%$. By challenging these commonly made assumptions, this work provides 28 29 permafrost hydrology modelers important context for better choosing the appropriate process what is such a "general system"? Too broad





- 30 representation for a given modeling experiment.
- 31

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40 1 Introduction

Permafrost describes a state of ground which stays frozen continuously over multiple years, which 41 may cover an entire region (e.g., Arctic tundra) or occur in isolation (e.g., alpine top). From the 42 perspective of scope, permafrost occupies approximately 23.9% (22.79 million km²) of the 43 44 exposed land area of the northern hemisphere (Zhang et al., 2008), as well as alpine regions and 45 Antarctica in the southern hemisphere. Permafrost areas store a vast amount of organic carbon, of which most is stored in perennially frozen soils (Hugelius et al., 2014). If the organic carbon is 46 47 exposed due to permafrost thaw, it is likely to decay with microbial activity, releasing greenhouse 48 gas to the atmosphere and exacerbating global warming. In Arctic tundra, permafrost also plays 49 an important role in maintaining water, habitat of wildlife, landscape, and infrastructure (Berteaux 50 et al., 2017; Dearborn et al., 2021; Hjort et al., 2018; Sugimoto et al., 2002). Permafrost 51 degradation may cause significant damage to the local ecosystem, reshape the surface and 52 subsurface hydrology, and eventually influence the global biosphere (Cheng and Wu, 2007; 53 Jorgenson et al., 2001; Tesi et al., 2016; Walvoord and Kurylyk, 2016). Therefore, the occurrent and potential impacts motivate the development of computational models with the goal of better 54 understanding the thermal and hydrological processes in permafrost regions, and consequently 55 MOR predict permafrost thaw accurately. 56 57 Simulating soil freezing and thaw processes is a challenging task that incorporates mass and energy

58 transfer among atmosphere, snowpack, land surface (perhaps with free water), and a variably 59 saturated subsurface. Several hydrological models with different complexity and applicable scales





Shold refinie Grenier et al. 2018 (AWR) somewhere

have been developed to investigate the complicated interactions. A comprehensive review of 60 permafrost models based on empirical and physical representations using analytical and numerical 61 solutions can be found in (Bui et al., 2020; Dall'Amico et al., 2011; Jan et al., 2020; Kurylyk et 62 al., 2014; Kurylyk and Watanabe, 2013; Riseborough et al., 2008). Process-rich models which aim 63 to predict permafrost change through direct simulation of mass and energy transport, such as 64 65 the Advanced Terrestrial Simulator (ATS; Painter et al., 2016), GEOtop (Endrizzi et al., 2014), CryoGrid 3 (Westermann et al., 2016), PFLOTRAN-ICE (Karra et al., 2014), and SUTRA-ICE 66 (McKenzie et al., 2007), have been demonstrated to describe thermal permafrost hydrology under 67 various climate conditions. Nominally, representing more physical process complexity should 68 improve accuracy, but how much accuracy and at what computational expense (and therefore 69 tradeoff in ability to run larger, or larger ensembles of, simulations) is not always theoretically 70 71 known. Thus, certain assumptions or simplifications about the system are a significant part of 72 model development.

First Even in the most process-rich models of permafrost change, three such physics simplifications are often made: representing water at constant density (thereby neglecting the expansion of ice relative to liquid water), neglecting cryosuction of water in unsaturated, partially frozen soils, and neglecting advective heat transport.

First, because of the lower density of ice than liquid water, freezing water must expand the volume 77 78 of the porous media, push liquid water into nearby volume, or otherwise expand the volume 79 occupied by that water. As all of the current set of models operate under the assumption of a rigid 80 solid matrix and thus the absence of mechanical equations describing matrix deformation or frost 81 heave, including this expansion typically results in large pressures that must be offset by grain compressibility or another mechanism. Therefore, the densities of ice and liquid water are 82 83 frequently assumed equal (e.g., Dall'Amico et al., 2011; Devoie and Craig, 2020; Weismüller et 84 al., 2011). It is uncertain whether this simplification affects predictions of permafrost change and 85 thermal hydrology.

Second, cryosuction describes the redistribution of water in partially frozen, unsaturated soils caused by increased matric suction. At the interface of ice and liquid water, negative pressures result in the migration of liquid water toward the freezing front and the subsequent increase of ice content. Several approaches representing cryosuction in models are used (Dall'Amico et al., 2011; Noh et al., 2012; Painter and Karra, 2014; Stuurop et al., 2021), either in an empirical form or



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91 physically derived from the generalized Clapeyron equation. Other process-rich models have 92 ignored cryosuction entirely (McKenzie et al., 2007; Viterbo et al., 1999). Dall'Amico et al. (2011), Painter (2011) and Painter and Karra (2014) evaluated their respective Clapeyron equation 93 94 based cryosuction models in soil column freezing simulations and presented a good match between 95 simulations and laboratory experiments in total water content (liquid and ice). Recently, Stuurop 96 et al. (2021) applied an empirical expression, a physics-based expression, and no cryosuction in 97 simulating soil column freezing process. They compared the simulated results with observations 98 from laboratory experiments. This comparison demonstrated minor differences between empirical 99 and Clapeyron-based cryosuction expressions, but the simulation without cryosuction cannot 100 predict the distribution of total water content in a laboratory-scale soil column. To our knowledge, 101 there is still no literature showing the effect of cryosuction on plot-scale permafrost predictions. 102 Third, heat transport in process-rich models is described using an energy conservation equation, 103 mainly including heat conduction, latent heat exchange, and heat advection. From a continuumscale perspective, conductive heat transport is expressed in the form of a diffusive term based 104 105 on Fourier's law. Latent heat exchange accompanies phase change which alters the system enthalpy. 106 Advective heat transport describes the energy exchange caused by the flow of liquid water driven 107 by a hydraulic gradient (i.e., forced convection), which is expressed through an advective term in 108 energy balance equations. Additionally, other mechanisms that control heat transport, such as 109 water vapor movement, thermal dispersion, radiant energy, etc., are neglected by nearly all models too ol of permafrost and are not considered here. Among these heat transport mechanisms, it is 110 assumed Х 111 commonly recognized that heat conduction predominates heat transport in the subsurface (Nixon, 112 1975). However, there are also studies demonstrating the importance of advective heat transport in permafrost hydrology through field observation analysis or modeling comparison. Such 113 transport situations where advective heat makes important contributions roughly fall into three categories. 114 ee 115 The first centers on the development of taliks beneath lakes, ponds, snowmelt water and rainfall 116 induced runoff, or in the existence of supra-/sub-permafrost groundwater flow (e.g., Luethi et al., 2017; McKenzie and Voss, 2013; Rowland et al., 2011). The second focuses on microtopographic 117 118 features that focus significant amount of water flux through small areas. This includes both low-119 center ice wedge polygons associated with the formation of thermokarst ponds (e.g., Abolt et al., 120 2020; Harp et al., 2021) and thermo-erosion gullies (e.g., Fortier et al., 2007; Godin et al., 2014). In these cases, large, focused flows across small spatial scales allow advective heat transpor 121

See also Dagenais et al 2020 (Hydrogeology J.) (companison & Conduction Livet al 2022 (WRR), (Talik vs Advection - conduction to real site)

case





122 dominate. The last category includes those studying the construction and maintenance of 123 infrastructure influenced by groundwater flow (e.g., Chen et al., 2020). Thus, these studies focus 124 on either location-specific or scale-limited problems. As McKenzie and Voss (2013) stated, 125 whether heat advection outweighs heat conduction depends on soil permeability, topography, and groundwater availability. Relative to these special cases, we are more interested in to what extent 126 127 advective heat transport associated with liquid water flow contributes to permafrost hydrologic 128 change in a hillslope-scale or larger Arctic system. To clarify the significant differences in model representations of permafrost, we investigate the 129 130 influence of including or not including these processes on permafrost change at plot-to-hillslope scales. We take the advantage of the flexibility offered by ATS to express multiple options of 131 132 process representation to implement this study in numerical experiments. For ice density, we 133 compare simulations with and without differences in ice density relative to water density; for 134 cryosuction, we compare simulations using a Clapyron equation-based expression and excluding 135 the cryosuction effect; and for heat transport, we compare simulations including or neglecting advective heat transport. All comparisons are carried out across a range of Arctic climate 136 137 conditions and soil properties from three different sites. Both 1D soil-column-scale and 2D 138 hillslope-scale models are considered, in which varying hillslope geometries (i.e., convergent/divergent hillslope) and aspects (i.e., north/south) are included. The aim of this study 139 140 is to provide permafrost hydrology modelers with crucial comparisons for better choosing a model 141 representation for a given study by formally considering the tradeoff between model complexity,

142 accuracy, and, at least for one code, performance.

143 2 Theory

144 The Advanced Terrestrial Simulator (ATS v1.2) (Coon et al., 2020) configured in permafrost mode 145 (Jan et al., 2018, 2020; Painter et al., 2016) was used to implement all numerical experiments in 146 this study. ATS is a process-rich code developed for simulating integrated surface and subsurface 147 hydrological processes, specifically capable of permafrost applications. It has been shown to 148 successfully compare to observations of seasonal soil freezing and thaw processes at different 149 scales. This includes 1D models of vertical energy transport typical of large-scale flatter regions (Atchley et al., 2015), and 2D models admitting lateral flow and transport in Arctic fens (Sjöberg 150 151 et al., 2016), and polygonal ground (Jan et al., 2020).





alspension "conduction"

(2)

152 The permafrost configuration of ATS comprises coupled water flow and energy transfer within variably saturated soils and at land surfaces, a surface energy balance model describing thermal 153 processes in snow, and a snow distribution module for surface microtopography (Painter et al., 154 2016). The subsurface system solves a three-phase (liquid, ice, gas), two-component (water vapor, 155 air) Richards-type mass balance equation with Darcy's law and an advection-diffusion energy 156 balance equation. The surface system includes an overland flow model with diffusion wave 157 approximation, and an energy balance equation with an introduced temperature-dependent factor 158 describing the effect of surface water freezing. The subsurface system and surface system are 159 160 coupled through the continuity of pressure, temperature, and the corresponding fluxes by incorporating the surface equations as boundary conditions of the subsurface equations (Coon et 161 162 al., 2020). The evolution of a snowpack and its effect on the surface energy balance is described using an energy balance approach based on a subgrid model concept that includes all major heat 163 fluxes at the land surface. For a more detailed description of the permafrost configuration and 164 165 implementation in ATS, as well as key mathematical equations, the reader is referred to Painter et al. (2016). Changes in this "most complex" model of permafrost hydrology are enabled by the 166 167 Arcos multiphysics library leveraged in ATS; this allows the precise model physics to be specified 168 and configured at runtime through the use of a dependency graph describing swappable 169 components in the model physics (Coon et al., 2016).

170 **2.1 Ice density**

171 The density of ice (kg/m³) is represented as a Taylor series expansion in both temperature and

172 pressure:

173
$$\rho_{i} = [a + (b + c\Delta T) \times \Delta T] \times (1 + \alpha \Delta p)$$
(1)

174 and the density of liquid water (kg/m^3) is represented as:

175
$$\rho_1 = [a + (b + (c + d\Delta T) \times \Delta T) \times \Delta T] \times (1 + \alpha \Delta p)$$

176 where
$$\Delta T = T - 273.15$$
, $\Delta p = p_1 - 1e5$, T and p_1 are temperature (K) and liquid pressure (>101325

177 Pa), respectively; and a, b, c, d, α are constant coefficients, listed in Table 1. Under conditions of

178 equal density, we assume $\rho_i = \rho_i$.

Table 1 Coefficients in density of ice and liquid

	а	b	с	d	α
$ ho_{ m i}$	916.724	-0.147143	-2.38e-4	-	1.0e-10
ρ_{1}	999.915	0.0416516	-1.01e-2	2.06e-4	5.0e-10





180 2.2 Cryosuction

- Painter and Karra (2014) proposed a constitutive relationship for phase partitioning of water in
- 182 frozen soils based on Clapeyron equation and Van Genuchten model (Van Genuchten, 1980): 183 $s_{l} = \begin{cases} S_{*}(-\beta \rho_{l}L_{f}\vartheta), \vartheta < \vartheta_{f} \\ S_{*}(p_{g}-p_{l}), \vartheta \geq \vartheta_{f} \end{cases}, \ \vartheta = \frac{T(K)-273.15}{273.15}, \ \vartheta_{f} = -\frac{\psi_{*}(1-s_{g})}{\beta L_{f}\rho_{l}}$ $s_{i} = 1 s_{l}/S_{*}(p_{g}-p_{l})$ KX usually e.ged (3)

where s_n is the saturation of *n*-phase and the subscripts n = 1, i, g are liquid, ice, and gas phases, 184 respectively; β is a coefficient; L_f is the heat fusion of ice; p_n (n = 1, g) is the pressure of *n*-phase; 185 S_* is the Van Genuchten model. This physically derived formulation can describe the change of 186 matric suction in the frozen zone due to the change of ice content, and thus has the capacity to 187

188 represent cryosuction.

Alternatively, to exclude the effect of cryosuction in this study, we used the Van Genuchten model 189

- to determine the total water content, including liquid water and ice. The liquid water content is 190 191 achieved by an empirical relationship (soil-freezing characteristic curve) which describes that the
- liquid water content only relates to temperature through an exponent function (McKenzie et al., 192

194
$$s_{l} = s_{r} + (s_{sat} - s_{r}) \exp\left[-\left(\frac{T(K) - 273.15}{\omega}\right)^{2}\right]$$

$$s_{i} = S_{*}(p_{g} - p_{l}) - s_{l}$$
(4)

- where s_r , s_{sat} are saturations of liquid water at residual and saturated conditions, respectively; ω is 195
- a constant coefficient. 196

- conductive

2.3 Advective heat transport 197

198 The energy conservation equation of the subsurface system is given by:

199
$$\frac{\partial}{\partial t} \left[\phi \sum_{n=l,i,g} (\rho_n s_n u_n) + (1-\phi) c_{v,\text{soil}} T \right] + \underbrace{\nabla \cdot (\rho_l h_l \mathbf{V}_l)}_{\text{advective heat}} \underbrace{-\nabla \cdot (\kappa_e \nabla T)}_{\text{conductive heat}} = Q_E$$
(5)

- where ϕ is porosity; u_n is the specific internal energy of phase $(n \in \{1, i, g\})$; $c_{v,soil}$ (J m⁻³ K⁻¹) is 200
- the volumetric heat capacity of the soil grains. The second and third terms represent the advective 201
- and conductive heat transport in subsurface, in which h_1 (J/mol) is the specific enthalpy of liquid; 202
- V_1 (m/s) is the velocity vector of liquid water determined by Darcy's law; and κ_e (W m⁻¹ K⁻¹) is 203
- 204 the effective thermal conductivity of the bulk material including soil, air, liquid water, and ice. $Q_{\rm E}$
- is the sum of all thermal energy sources (W/m^3) . 205
- 206 Similarly, the energy balance equation of the surface system is:





$$207 \quad \frac{\partial}{\partial t} \{ [\chi \rho_{l} u_{l} + (1-\chi)\rho_{i} u_{i}] \delta_{w} \} + \underbrace{\nabla \cdot (h_{l} \chi \rho_{l} \delta_{w} \mathbf{U}_{w})}_{\text{advective heat}} \underbrace{-\nabla \cdot \{ [\chi \kappa_{l} + (1-\chi)\kappa_{i}] \delta_{w} \nabla T \}}_{\text{conductive heat}} = Q_{\text{net}}$$
(6)

in which χ is the unfrozen fraction determined by surface temperature; δ_w is ponded depth (m); 208 209 U_w (m/s) is the velocity vector of liquid water on the surface determined by the diffusion-wave 210 approximated St. Venant equations (Gottardi and Venutelli, 1993) and Manning equation (Wasantha Lal, 1998); κ_n (W m⁻¹ K⁻¹) is the thermal conductivity of *n*-phase (n = 1, i); Q_{net} (W/m³) 211 212 is the net thermal energy into and out of surface, including that from solar radiation, rain and snow 213 melt, water loss by evaporation and to the subsurface, and conductive and advected heat transport 214 to/from the subsurface. The second and third terms represent the (lateral) advective and conductive 215 heat transport that occur across the land surface.

216 3 Methods

To evaluate the impact of representation of ice density, cryosuction, and advective heat transport 217 in permafrost modeling under different climate conditions and soil properties, we selected three 218 sites for their variance in climactic condition: Utgiagvik (Barrow Environmental Observatory, 219 220 71.3225° N, 156.6231° W), the headwaters of the Sagavanirktok (Sag) River (68.251° N, 149.092° 221 W), and the Teller Road Mile Marker 27 site on the Seward Peninsula (64.73° N, 165.95° W) in 222 Alaska. The simulated hydrological outputs for each site are compared in both column and 223 hillslope scenarios. Column scenarios represent expansive flat regions typical of the Arctic coastal 224 plains dominated by vertical infiltration and heat transport, and hillslope scenarios are 225 representative of the headwater, hilly terrain typical of the more inland permafrost.

226 In hillslope scenarios, hillslopes with northern and southern aspects are considered to investigate 227 physics representation comparisons under the same climate and soil condition (i.e., at a given site) 228 but different solar radiation incidence. Furthermore, hillslopes with both convergent and divergent 229 geometries are included to compare the sensitivity of simulated discharge on process 230 representation. These scenarios can incorporate many types of Arctic systems at the described plotto-regional scales, but explicitly ignore the effects of microtopography or other local-scale 231 focusing mechanisms such as water tracts or thermo-erosion gullies. The objective is to reach a 232 conclusion on the influence of the three physics representation that can be widely applicable in 233 234 many Arctic systems.

235 3.1 Field data description





236 For each site, data used in each simulation comprises meteorological forcing datasets for the period

237 2011-2020, averaged wind speed, and soil properties.

238 Meterological forcing datasets are taken from the Daymet version 4 dataset (Thornton et al., 2020), 239 which provides observation-based, daily averaged weather variables through statistical modeling 240 techniques at 1 km spatial resolution (Thornton et al., 2021). Variables that are used in simulations 241 include daily average air temperature (calculated as the mean of Daymet's daily minimum and 242 maximum values), relative humidity (calculated from air temperature and Daymet's vapor pressure), incoming shortwave radiation (W/m²) (calculated as a product of Daymet's daylit 243 244 incoming radiation and daylength), and total precipitation (m/s), which is split into snow and rain based upon the air temperature. Figure 1 illustrates the precipitation of rain, snow, and air 245 temperature in the three sites from 2011 to 2020, where the points represent the corresponding 246 averaged values per year. In terms of the forcing conditions, the annual rainfall of the Sag and 247 248 Teller sites range between 20 and 40 mm/d over the ten years, more than twice the rainfall typical 249 of the Barrow site. In addition, Sag has a significantly larger amount of snow every year that is over double of that at the Teller site and almost five times larger compared to the Barrow site. For 250 251 the air temperature, Sag and Barrow are similar and colder than Teller by 7-8 degrees. In general, 252 the Barrow site is dry and cold, the Sag site is wet and cold, and the Teller site is wet and warm.



253

254 Figure 1 Precipitation and air temperature of site Barrow, Sag, and Teller from year 2011 to 2020

In addition to the time series of forcing data from Daymet, we used an average wind speed for each site. For Barrow and Teller, the average wind speed was estimated from the measurement taken by the Next-Generation Ecosystem Experiments (NGEE) Arctic project. At Barrow, the measurement was taken at area A (71.2815° N, 156.6108 ° W) at the height of 1.3 meters above surface (Hinzman et al., 2014). At Teller, the measurement at 3.8 m above the surface of a lower level of the watershed (Busey et al., 2017) was used. For Sag, the average wind speed was estimated based on the measurement at the Toolik Lake field site (near to Sag River) at the height





262 of 3.1 m above surface, which is accessible through the National Ecological Observatory Network

- 263 (NEON, 2021).
- The soil properties of Barrow, Sag, and Teller, including porosity, permeability, Van Genuchten 264 265 parameters, and thermal conductivity parameters, were chosen from previous modeling studies at 266 these sites (Atchley et al., 2015; Jafarov et al., 2018; O'Connor et al., 2020), see (Table 2). Roughly, 267 the soil profile of each site is composed of two materials: the top organic-rich layer comprising 268 mosses, peats, and other organic rich soils measuring approximately 10-30 cm thick, and the 269 principal mineral soil. There is minor difference in thermal conductivity parameters among the 270 three sites, and soil permeability is also at the same order of magnitude. The soil-water characteristic curve (SWCC) of the principal mineral soil of Barrow, Sag, and Teller, shown in 271 Figure 2, indicates that the soil property between Barrow and Teller is relatively similar, while Sag 272 differs from the other two with a relatively flat SWCC. 273 10



274

275 Figure 2 Soil-water characteristic curve (SWCC) of soil in Barrow, Sag, and Teller

276 Usually, at the hillslope scale, the thickness of organic layers of a watershed varies from the toe-277 slope, through a steeper mid-hill, up to the flat top. Typically, thicker organic layers may exist at 278 the top and bottom compared to the mid-hillslope. The low thermal conductivity of organic layers 279 can impede the heat transport between the air and the underlying mineral soil, resulting in varying 280 thaw depth (or permafrost table depth) along a hillslope, which has been observed at the site Teller 281 (Jafarov et al., 2018). In this paper, hillslope meshes were constructed following this observation 282 so that the organic layers are thicker at the top and bottom of a hillslope, as described in the next 283 section.

284 3.2 Mesh design and material properties

285 The comparison of different physics representations was conducted in both column and hillslope





286 scenarios.

- 287 The column model was designed as a one-dimensional, 50 m deep domain. The column domain was discretized into 78 cells with gradually increasing cell thickness, starting from 2 cm at the soil 288 289 surface to 2 m at the bottom of the domain. We assigned different material properties to the cells to represent different soil layers. A column domain is divided into three layers, and the thickness 290 291 of each layer was designed differently among the three sites according to geological observations 292 (Jan et al., 2020; O'Connor et al., 2020; NGEE-Arctic). Specifically, from top to bottom, the three 293 layers of the Barrow soil column are 2 cm-thick moss, 8 cm-thick peat, and mineral; for Teller, the 294 soil column consists of a 4 cm moss layer, a 22 cm peat layer, and mineral; and the three layers of the Sag soil column are acrotelm, catotelm, with thickness of 10 cm and 14 cm, respectively, and 295 296 the remainder mineral. The soil properties of each layer at three sites are listed in Table 2.
- 297

Table 2 Soil properties of three soil layers of all sites used in this paper

Site Barrow				Sag		Teller			
Layers	moss	peat	mineral	acrotelm	catotelm	mineral	moss	peat	mineral
Porosity	0.9	0.876	0.596	0.878	0.796	0.457	0.9	0.55	0.45
Permeability (m ²)	1.7e-11	9.38e-12	6e-13	2.64e-10	9.63e-12	3.98e-13	5e-11	5e-12	2e-13
VG α (Pa ⁻¹)	2.3e-3	9.5e-4	3.3e-4	7.93e-4	1.75e-4	8.06e-5	2.35e-3	2.93e-4	5.45e-4
VG n	1.38	1.44	1.33	1.405	1.566	1.571	1.38	1.269	1.236
Residual saturation	0.056	0.388	0.334	0.0073	0.0662	0.	0.1	0.	0.1
Thermal conductivity, unfrozen (Wm ⁻¹ K ⁻¹)	0.446	0.427	0.788	0.519	0.630	1.309	0.57	0.67	1
Thermal conductivity, dry (Wm ⁻¹ K ⁻¹)	0.024	0.025	0.104	0.066	0.086	0.265	0.07	0.07	0.29

298

299 In the hillslope scenario, we designed the mesh based on observations at Teller to represent a 300 generalized, varying-thickness low Arctic hillslope. A hillslope mesh was created first by 301 generating a pseudo-2D surface mesh with 50 cells and then extruding the 2D mesh downward by 302 50 m. The pseudo-2D surface was designed in a trapezoidal shape with a single, variable-width 303 cell in the cross-slope direction to represent convergent/divergent hillslopes, the short and long 304 sides of which are 200 m and 800 m, respectively (see Figure 3). Vertically, from surface 305 downward, the grid size distribution was the same as the column mesh for each site. The domain 306 is also composed of three layers, same as the column, while the numbers of cells representing each 307 soil layer (i.e., soil layer thickness) are different along the hillslope. The thickness distribution of the first two layers of each site is shown in Table 3. The third layer of a hillslope for all sites is the 308 principal mineral soil. Additionally, hillslope meshes with different aspects (i.e., north, south) were 309





310 also created.



311(a) Convergent hillslope(b) Column312Figure 3 Schematic domain mesh and soil layer partition: (a) example of a convergent hillslope domain, (b)313column domain.



Table 3 Thickness distribution of the organic layers along hillslope for each site

Site	Horizontal x range (m)	Barrow layer thickness (cm)	Sag layer thickness (cm)	Teller layer thickness (cm)
I	$0 \sim 200$	2	14	8
Layer 1 Moss/Acrotelm	$300 \sim 700$	2	6	4
Moss/Acrotenni	$800 \sim 1000$	2	14	8
I	$0 \sim 200$	12	18	22
Layer 2 - Peat/Catotelm -	$300 \sim 700$	6	8	22
Peat/Catoleini	$800 \sim 1000$	12	18	22

315 3.3 Model setup

Not a "process"

To study how the representations of the three physical processes (i.e., ice density, cryosuction, and 316 317 advective heat transport) affect simulated hydrological outputs at different scales and hillslope topography features, and under various forcing and soil conditions, 62 model simulations were 318 319 conducted, summarized in Table 4. To examine the validity of the assumption of equal density between ice and liquid, we included cryosuction and advective heat transport in models. To 320 321 investigate the role of cryosuction in permafrost modeling, we used different density, while 322 neglecting advective heat transport to decrease the computation cost. Note that neglecting 323 advective heat transport in these runs can reduce the effect of cryosuction on simulation predictions, 324 as cryosuction moves water which would itself advect energy. To compare the difference between neglecting and including heat advection, we used different density expressions for ice and liquid, 325





and included cryosuction. Particularly, in order to understand the impact of advective heat transport on permafrost process when soil is at its wettest, we designed two extreme cases under the warm, wet conditions of the Teller site in which soil evaporation was artificially reduced. These runs were designed to maximize water flux and therefore maximize the potential for advective heat transport to affect predictions.

Table 4 Ensemble of models designed in this study

To compare	Site	Scale	Geometry	Aspect	Remark
		column	-	_	
• $\rho_i \neq \rho_l$, Eq. (1)	Barrow	hillslope -	t	north	 heat advection
	Sag		convergent	south	
• $\rho_i = \rho_i$, Eq. (2)	Teller		1	north	• cryosuction
			divergent	south	
		column	-	_	
T 1 1 1	Barrow Sag Teller	hillslope	aanvargant	north	• $\rho_i \neq \rho_1$
• Include heat transport			convergent	south	
• Maalaat haat tuonon out			divergent	north	cryosuction
• Neglect heat transport			uivergent	south	
	Extreme case, Teller	hillslope	convergent	north	 reduced evaporation
		column	-	_	
 Include cryosuction 	Barrow Sag	hillslope	t	north	• $\rho_i \neq \rho_1$
			convergent	south	
 Neglect cryosuction 	Teller		divensent	north	• no heat advection
			divergent	south	_

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Prior to simulating all cases, two steps of initialization are carried out for each site. First, a column 333 model with a given initial water table depth and above 0 °C temperature was frozen by setting the 334 335 bottom temperature at a constant value of -10 °C until a steady-state frozen soil column is formed. 336 The initial water table depth is chosen to ensure that the frozen column's water table, after 337 accounting for expansion of ice, is just below the soil surface. The pressure and temperature 338 profiles of the frozen column were used as the initial conditions of the second step initialization. 339 Before proceeding, the observed forcing data (period of 2011-2020) was averaged across the years 340 to form a one-year, "typical" forcing year, which was then repeated 10 times. Using this typical 341 forcing data and the solutions of the first step, we solved the column model in a transient solution, calculating an annual cyclic steady-state and obtaining the pressure and temperature fields at the 342 end of the 10^{th} year. The final state was then used as initial condition in formal simulations listed 343 in Table 4. The temperature at bottom was constant at -10 °C. 344

345 3.4 Evaluation metrics





To fully assess the effect of representation of ice density, advective heat transport, and cryosuction 346 in permafrost hydrology modeling, we used root mean squared error (RMSE) and normalized 347 Nash–Sutcliffe efficiency (NNSE) as performance metrics. RMSE has the same dimension with q 5348 349 the corresponding variables, which can be used to evaluate the average absolute deviation from a 350 benchmark, defined by: $\text{RMSE} = \sqrt{\frac{\sum_{t=1}^{N} (x_t - y_t)^2}{N}}$ 351 (7)where x_t and y_t are the two modeled datasets to compare from the initial time point (t = 1) to the 352 353 end (t = N). NNSE is a normalized dimensionless metric describing the relative relationship between an 354 355 estimation and a reference, which is oftentimes used for evaluating hydrological models NNSE = $1/\left(1 + \frac{\sum_{t=1}^{N} (x_t - y_t)^2}{\sum_{t=1}^{N} (x_t - \bar{x})^2}\right)$ 356 (8) where the modeled results x_t (obtained without physics simplification) $\frac{1}{40}$ considered as the 357 benchmark, and \bar{x} is the mean value of the benchmark. NNSE approaching $\frac{1}{2}$ 1 indicates perfect 358 correspondence between two observations. and sime lations. 359 In addition, we also used normalized mean absolute error (MAE) to quantify the percentage change 360 of results obtained with simplified physics relative to full physical representations (see Section 361 362 4(4) Normalized MAE = $\frac{\sqrt{\sum_{t=1}^{N} |x_t - y_t|/N}}{\text{normalizing reference}} \times 100\%$ 363 (9) Two normalizing references were selected considering different model output variables. For 364 instance, in terms of temperature and saturation which fluctuate between two non-zero values, the 365 annually averaged variation range was chosen as the reference 366 Normalizing reference = $\frac{\sum_{y \neq ar=1}^{num of y \neq ars}(maximum - minimum)}{number of y ears}$ 367 368 For variables with zero as the smallest value, such as evaporation, discharge, and thaw depth, the 369 corresponding average value was selected as the reference.

370 4 Results

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al processes This section compares simulated outputs over the period of 2011-2020 for the three physics under 371

- different simulating conditions. We focus on the impact on integrated variables, such as 372
- evaporation, discharge, averaged thaw depth, and depth-dependent variables, such as temperature, 373





and total water saturation (ice and liquid). For hillslope models, we chose five surface locations
according to the slope geometry to collect simulated data, which were then averaged to obtain a
single outcome for each variable of interest.

377 4.1 Ice density

To evaluate the representation of ice density on permafrost process simulation, we compared evaporation, discharge, thaw depth, and total water saturation between simulations using equal and different ice density expressions. Figure 4 and Figure 5 show an example of the comparison under conditions of Sag at column and hillslope scale, respectively. Results are compared in both time series and correlation.

Generally, at both column and hillslope scale, assuming equal density between ice and liquid has 383 minor impacts on evaporation, discharge, and thaw depth over the 10-year simulation, except at a 384 few deviated points as shown in the correlation figures. According to column-based models, the 385 RMSEs of evaporation, discharge, and thaw depth are 0.101 mm/d, 0.001 m³/d, and 1.648 cm, 386 respectively, one order of magnitude smaller than the corresponding variable values. At hillslope 387 scale, see Figure 5) the south-facing divergent hillslope is selected to show modeling comparison 388 on evaporation and thaw depth, in that they are potentially mostly affected when a hillslope has a 389 390 south orientation and divergent geometry. Likewise, the north-facing convergent hillslope is 391 chosen to compare discharge and water saturation from simulations with different density expression. Even then, RMSEs of the three variables are 0.064 mm/d, 111.073 m³/d, and 0.825 cm, 392 respectively, two orders of magnitude smaller than the corresponding variable values at hillslope 393 scale. Besides, NNSEs of the three variables output from both column and hillslope simulation are 394 395 over 0.9, approaching 1 especially at the hillslope scale. Therefore, all indicate good performance 396 of equal ice-liquid density assumption in predicting integrated variables and thaw depth. By comparison, the estimation of water saturation is relatively affected by the density assumption 397 398 during cold seasons within a year, as shown by Figure 4 (d) and Figure 5 (d). This is reasonable in that when water mainly exists in the form of ice, equal ice-liquid density assumption will 399 400 overestimate the water content.







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Figure 4 Comparison of column simulations between different and equal ice-liquid density under conditions of Sag, in (a) evaporation, (b) discharge, (c) thaw depth, and (d) water saturation at 5 cm beneath surface 404 from year 2011 to 2020.



405 406 Figure 5 Comparison of hillslope simulations between using different and equal ice-liquid density under 407 conditions of Sag, in (a) evaporation, (b) discharge, (c) thaw depth, and (d) water saturation at 5 cm beneath 408 surface from year 2011 to 2020.

409 In addition, we investigated how much the assumption of equal ice-liquid density can affect simulation time at hillslope scale. Using 10-year simulations with real ice density as references, 410 411 the percentage change of time consumed after applying equal ice-liquid density was calculated and 412 displayed in Figure 6. Overall, under the density assumption, it may take less time (positive 413 percentage), but no more than 25% and on average lower than 10%. However, it may also increase computational time (negative percentage) mainly under wet conditions, such as at Sag and Teller. 414 Thus, given a long-period large-scale modeling of permafrost freezing and thaw process, there is 415 no consistent conclusion on whether equal ice-liquid density can ease computational cost. It 416





417 depends on both the weather conditions and soil properties.



418
 419 Figure 6 Decreased percentage of simulation time under the assumption of equal ice-liquid density compared
 420 to the real ice density representation for all hillslope scale simulations.

421 4.2 Cryosuction

To evaluate the effect of cryosuction on permafrost process predictions, we compared evaporation, 422 423 discharge, thaw depth, total water saturation, and temperature obtained through simulations including and neglecting cryosuction. Figure 7 through Figure 9 illustrate column-scale 424 comparisons of these variables under conditions at three sites (Barrow, Sag, and Teller). Figure 7 presents the effect of excluding cryosuction on evaporation and discharge. RMSE of evaporation 425 426 from the three sites ranges between 0.25 mm/d and 0.35 mm/d, still one order of magnitude smaller 427 428 than the common evaporation rate. Evaporation NNSEs of the three sites are around 0.9. For discharge, RMSEs are also one order of magnitude smaller than the average, whereas NNSEs fall 429 between 0.6 and 0.9. Generally, cryosuction plays a more important role in predicting discharge 430 compared to evaporation, especially under warm and wet climate conditions, such as Teller. 431









Figure 7 Comparison of column simulations between including and neglecting cryosuction under conditions 434 of Barrow, Sag, and Teller, in (a) evaporation, (b) discharge.

Figure 8 shows the effect of cryosuction on column-scale simulated thaw depth and total water 435 saturation at 5 cm beneath surface. RMSEs of thaw depth range from 3 cm to 8 cm. Though still 436 437 one order of magnitude smaller than the average annual thaw depth, the estimation error due to 438 neglecting cryosuction is obvious in summer, especially at areas with cold temperature and low rainfall like Barrow. By comparison, at Teller, where the largest thaw depth is over double of 439 440 Barrow and Sag due to its higher temperature, soil cryosuction does not essentially affect thaw 441 depth compared to the other two sites. Similarly, for the total water saturation, at Barrow, the effect of cryosuction is more clearly observed, not only during cold seasons as observed for density 442

443 representation (section 4.1), but also in summers.





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Finally, we also compared soil temperature obtained from models with or without cryosuction included; see Figure 9. Surface temperature is little affected by cryosuction, except at the Sag site, where the surface temperature is overestimated during winter. At 1 m depth, soil temperature of Barrow is slightly changed in summer due to neglecting cryosuction. At both Sag and Teller, the fluctuation range of temperature at 1 m beneath land surface is underestimated if cryosuction effect is not considered, especially at Sag, NNSE decreases to 0.6 approximately.

Therefore, from Figure 7 to Figure 9, neglecting cryosuction effect at column scale simulation has less impact on integrated hydrological variables, but will cause significant difference when estimating thaw depth and location-based variables. The difference among variables varies under different climate conditions. Influence on integrated variables, such as evaporation and discharge, are more obviously under warm and wet conditions (Teller); thaw depth and water saturation are affected more under cold and low-rainfall conditions (Barrow); and soil temperature tends to be influenced greater under cold and high precipitation (rain and snow) conditions (Sag).









Figure 9 Comparison of column simulations between including and neglecting cryosuction under conditions 462 of Barrow, Sag, and Teller, in (a) surface temperature, (b) temperature at 1 m beneath surface.

463 Neglecting soil cryosuction has a similar impact on hydrological outputs in hillslope scale models. 464 Figure 10 shows the comparison of the variables discussed above under the Sag climate. 465 Evaporation, thaw depth, and temperature are presented based on south-facing divergent hillslope 466 models, while discharge and water saturation are from hillslope models with north-facing 467 convergent geometry. In general, neglecting soil cryosuction has a smaller effect on integrated 468 variables (evaporation and discharge) compared with other pointwise variables. Though thaw depth presents a high NNSE, approximately 0.94, and low RMSE, about 4.5 cm compared to the 469 470 average, indicating a good match between models considered and excluded cryosuction, the 471 estimation error during summer may reach as high as 10 cm, particularly from 2011 to 2017, as shown in Figure 10 (c). Obvious errors in water saturation and temperature, similar with column-472 473 scale models, occur almost annually with respect to extrema during winter and summer. Overall, 474 compared to column-scale models, differences in evaporation, discharge, thaw depth, and surface temperature due to neglecting cryosuction effect are relatively reduced at hillslope scale if 475 comparing NNSEs (Table 5). Localized subsurface variables, such as water saturation and 1m-476 477 depth soil temperature, show increased errors from column to hillslope scale models, which is primarily caused by lateral flux exchange captured by hillslope modeling. 478







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Table 5 NNSE of outputs from column and hillslope models under conditions of Sag shown in Figure 7 through Figure 10

Scale	Evaporation (mm/d)	Discharge (m ³ /d)	Thaw depth (cm)	5cm-depth water saturation (-)	Surface temperature (K)	1m-depth temperature (K)
Column	0.936	0.631	0.904	0.926	0.864	0.613
Hillslope	0.973	0.846	0.934	0.686	0.900	0.597

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486 4.3 Advective heat transport

487 This section evaluates the performance of advective heat transport in modeling permafrost process. As above, we investigated the influence of neglecting heat advection on evaporation, discharge, 488 489 thaw depth, total water saturation, and temperature. Overall, heat advection does not play a vital 490 role in a normal Arctic system after comparing all hydrological outputs from models with different 491 heat transport representations. Comparisons based on column-scale and hillslope-scale models are 492 not shown here (see Supplement); instead, the extreme case under conditions of Teller is presented (Figure 11). Teller is abundant in rainfall over the period of 2011-2020 (Figure 1). In the extreme 493 494 case, evaporation was reduced factitiously to almost a quarter of the original value (see Figure 7 495 (a) at Teller and Figure 11 (a)) for the purpose of increasing water flow rates. For instance, 496 discharge has quadrupled after adjusting evaporation by comparing Figure 11 (b) and Figure 7 (b)







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497 at Teller. This specific scenario is chosen to maximize the potential effect of advective heat 498 transport in a hillslope-scale Arctic system. Figure 11 illustrates comparisons on all outputs 499 mentioned above from hillslope models without heat advection and with full thermal 500 representation. Apparently, all RMSEs are extremely small, at least two orders of magnitude lower 501 than the corresponding variable average. Almost all NNSEs are approximately one, even for thaw 502 depth, localized water saturation, and temperature. Therefore, for most Arctic systems at this scale,

- 503 it is reasonable to neglect advective heat transport.



504 505 Figure 11 Comparison of hillslope simulations between including and neglecting advective heat transport 506 under extreme conditions of Teller, in (a) evaporation, (b) discharge, (c) thaw depth, (d) water saturation at 5 507 cm beneath surface, (e) surface temperature, (f) temperature at 1 m beneath surface.

508 In addition to simulated results, we also compared simulation times in percentage change between 509 hillslope models neglecting and including heat advection. ATS uses Algebraic Multigrid method 510 as preconditioner for solving, which has a relatively deficient performance in dealing with 511 hyperbolic equations. Thus, incorporating advective heat transport will aggravate computational cost, particularly in case of both large spatial and temporal scale. Figure 12 shows the relative 512 513 percentage reduction in computational time for 10-year simulations after excluding heat advection 514 in both surface and subsurface thermal flux. It drops by 70% ~ 80% under wet conditions (e.g., Sag and Teller) and $40\% \sim 60\%$ under dry conditions (e.g., Barrow). Hence, neglecting advective 515 heat transport considerably improves the performance of large spatial-temporal permafrost 516 Computational cost should be irrelevant. If advantive heat transport is relevant. I needs to 22 be included.





517 hydrology simulations.



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 Figure 12 Decreased percentage of simulation time after neglecting heat advection compared to full thermal
 520 representation for all hillslope scale simulations.

521 4.4 Comprehensive comparison

522 In the above three sections, we discussed time-series simulation comparisons. This section will 523 analyze the effect of equal ice-liquid density, neglecting cryosuction, and neglecting heat 524 advection on permafrost modeling outputs from holistic, average perspectives.

525 First, we extracted NNSEs of all variables obtained from all comparing models for qualitative 526 analysis. Table 6 shows an example based on column-scale models under conditions of three 527 different sites. Red numbers highlight the obviously reduced NNSEs of one or two processes 528 among the three for each variable. Overall, neglecting advective heat transport has the least influence on model outputs. Equal ice-liquid density primarily affects saturation and has less effect 529 530 on other variables. Excluding soil cryosuction makes the greatest impact on almost all variables, 531 especially in a relatively wet environment. Among the variables, evaporation and surface 532 temperature are less affected by the three physical process representations, while location-based 533 water saturation is most affected.

534

Table 6 A summary of NNSEs of variables obtained through column model comparison

Variables	Barrow				Sag		Teller		
	Heat advection	Ice density	Cryosuction	Heat advection	Ice density	Cryosuction	Heat advection	Ice density	Cryosuction
Evaporation	0.9971	0.9942	0.8991	0.9926	0.9917	0.9365	0.9989	0.9958	0.9033
Discharge	0.9235	0.6282	0.8615	0.9962	0.9377	0.6305	0.9854	0.9874	0.6175
Thaw depth	0.9970	0.9961	0.8517	0.9910	0.9791	0.9036	0.9969	0.9887	0.9524
5cm-depth sw	0.9959	0.9335	0.7851	0.9916	0.7260	0.9260	0.9979	0.5618	0.8690
40cm-depth sw	0.9932	0.0221	0.2130	0.9951	0.0622	0.3111	0.9990	0.2807	0.8498
Surface T	0.9999	0.9999	0.9871	0.9993	0.9990	0.8642	0.9999	0.9996	0.9554
1m-depth T	0.9999	0.9999	0.9207	0.9997	0.9996	0.6127	0.9997	0.9991	0.7366
			1 1 -	20					

Do you really need of digits? 3 seems enough.





physical processes,

535 $* s_w$ and T in Table 6 are water saturation and temperature, respectively.

Furthermore, to compare across the physics quantitively, we calculated the mean absolute error 536 (MAE) for each variable of interest over the simulation period of 2011-2020. For evaporation, 537 538 discharge, and thaw depth, the MAEs are normalized by the corresponding variable average 539 (numbers in Figure 13 (a)); for water saturation and temperature, the MAEs are normalized by 540 their average annual fluctuation range (numbers in Figure 13 (b)). All normalized MAEs are 541 presented in percentage, displayed in Figure 13 according to column- and hillslope-scale (e.g., 542 south-facing convergent hillslope) models under three different climate conditions. Hillslope-scale 543 model output under conditions of Barrow is not shown in that flat land occupies a majority of the 544 area. A larger normalized MAE percentage indicates greater impact on the variable resulted from 545 a physical process.

From the perspective of 10-year average, in general, each physical process of Arctic system 546 547 discussed in this paper presents a similar impact on variables between column and hillslope scales. 548 Under climate and soil conditions of three different sites, neglecting cryosuction in permafrost 549 modeling leads to the greatest influence on hydrological prediction amongst the three physical 550 assumptions. As seen in Figure 13 (a), it will result in $10\% \sim 20\%$ deviation in evaporation, 50% 551 $\sim 60\%$ in discharge, and $10\% \sim 30\%$ in thaw depth. Evaporation is the least affected among the 552 three variables. Discharge is more affected in regions with abundant rainfall (Teller), while in 553 regions with less precipitation, evaporation and thaw depth are relatively affected (Barrow). By 554 comparison, assuming equal ice-liquid density and neglecting advective heat transport may only cause 10% and 5% or even much lower error, respectively, in reference to the annual average of a 555 variable. Specially, in Barrow, models utilizing the same ice and liquid densities and ignoring 556 advective heat seem to make an obvious impact on discharge, whereas this also results from its 557 extremely low discharge (Figure 7 (b)). 558

Figure 13 (b) illustrates the normalized MAEs of water saturation at 5 cm beneath surface, as well as temperature at surface and 1 m depth. The assumption of equal ice-liquid density primarily affects the estimation of water saturation profile. It can lead to about $5\% \sim 15\%$ error relative to the annual change range, and the error percentage tends to slightly decrease when applying hillslope-scale models due to the inclusion of lateral flow. Apart from this, neglecting soil cryosuction still makes the largest impact. Surface temperature is the least affected variable among all these model outputs even if cryosuction is not included in modeling. However, at 1 m depth,







566 error can increase to $10\% \sim 30\%$ by simulation without cryosuction representation.

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569 570 571 Figure 13 Normalized average absolute error of variables over the period of 2011-2020, compared among

three physical assumptions at column and hillslope scales. Variables: (a) evaporation, discharge, and thaw 572 depth, numbers in figures are the average values of the corresponding variables; (b) water saturation, and

573 temperature, numbers in figures are the average annual fluctuation range of each variable.

574 5 Conclusion

⁽b) Variables to compare, normalized by average annual fluctuation of variables





575 Simplification of Arctic process representation is an essential consideration when developing these an 576 process-rich models for thermal permafrost hydrology. There are three subsurface processes that are commonly described in a simplified approach for many Arctic tundra models: (i) ice is 577 prescribed the same density as liquid water; (ii) the effect of soil cryosuction is neglected; (iii) 578 advective heat transport is neglected. Here we investigated the influence of these simplified 579 580 representations on modeling field-scale permafrost hydrology. 581 To do this, we conducted an ensemble of simulations using the Advanced Terrestrial Simulator 582 (ATS v1.2) to evaluate the impact of the above three process simplifications on field-scale predictions. The ensemble of simulations consisted of 62 numerical experiments considering 583 584 various conditions, including different climate conditions and soil properties at three sites of 585 Alaska, and different model scale conceptualizations. For evaluation, we compared integrated 586 variables (evaporation, discharge), averaged thaw depth, and pointwise variables (temperature, 587 total water saturation), among different models to access the deviation of applying a simplified 588 modeling assumption. The main conclusions of this study are summarized as follows:

- 1) Excluding soil cryosuction in permafrost models can cause significant bias in most, hydrological variables. Especially, according to this study, the average deviation in 589 590 591 evaporation, discharge, and thaw depth may reach $10\% \sim 20\%$, $50\% \sim 60\%$, and $10\% \sim 10\%$ 592 30%, respectively, relative to the corresponding annual average values. The prediction 593 error for discharge may grow if rainfall rates increase. In the case of pointwise variables, 594 the error in temperature increases from a small amount at the surface up to $10\% \sim 30\%$ at 595 1 m beneath surface. The prediction of subsurface temperature and water saturation is 596 especially affected when considering hillslope scale models. Therefore, soil cryosuction 597 should be included when modeling permafrost change.
- Assuming equal ice-liquid density will not result in especially large deviations when
 predicting most of the hydrological variables, particularly at hillslope scales. It primarily
 affects the prediction of soil water saturation profile and can cause 5% ~ 15% error relative
 to the annual saturation fluctuation range. This difference may have consequences for the
 carbon cycle with regards to the production of methane versus carbon dioxide. Assigning
 liquid water density for ice may reduce computational time to a small extent in ATS,
 dependent on simulating conditions and spatial and temporal scales.
- 605 3) For a general Arctic tundra system, the prediction error in most variables after neglecting

validate?



advective heat transport is less than 5%, or even much lower. In the case of ATS, the 607 simulation time cost for hillslope-scale models can decrease by 40% to 80% under 608 conditions in this study. Ignoring heat advection in the absence of local, flow-focusing 609 mechanisms, such as thermo-erosion gullies, seems a reasonable decision.

Through the comparison of permafrost hydrological outputs obtained from ensemble model setup 610

targeted at field scale, we confirm the importance and necessity of including soil cryosuction effect 611

in predicting permafrost changes, and valid application of equal ice-liquid density and neglecting 612

advective heat transport for a general Arctic system. The latter two may also ease computational 613

cost dependent upon simulation conditions. We expect that this study can contribute to the 614

615 development of permafrost hydrology models, as well as better selection of physical process

616 representations for modelers.

617 **Code availability**

Advanced Terrestrial Simulator (ATS) is an open-source code for solving ecosystem-based, 618

integrated, distributed hydrology, and available at https://github.com/amanzi/ats. Simulations were 619

conducted using version 1.2 (Coon et al., 2021). 620

621 **Data availability**

622 Data sources of wind speed are cited in the text. The raw forcing data acquired from Daymet, the

623 processed forcing data used for simulation, and simulation output data are available through

624 https://github.com/gaobhub/data for paper model comparison.

625 Author contributions

626 Bo Gao did some revision of the code to add options for process representations, designed

- 627 numerical experiments and setup models, did data analysis and interpretation, drafted and revised
- 628 the article. Ethan T. Coon implemented the code in which the study was done, conceptualized the
- 629 study, helped debug the runs, and helped draft and revise the article.

630 **Competing interests**

631 The authors declare that they have no conflict of interest.





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