



1 Three-Dimensional Stefan Equation for Thermokarst Lake and Talik

- 2 Geometry Characterization
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19 Abstract

20	Thermokarst lake dynamics, which plays an essential role in carbon release due to permafrost
21	thaw, is affected by various geomorphological processes. In this study, we derive a three-
22	dimensional (3D) Stefan equation to characterize talik geometry under a hypothetical
23	thermokarst lake in the continuous permafrost region. Using the Euler equation in the calculus
24	of variations, the lower bounds of the talik were determined as an extremum of the functional
25	describing the phase boundary area with a fixed total talik volume. We demonstrate that the
26	semi-ellipsoid geometry of the talik is optimal for minimizing the total permafrost thaw under
27	the lake for a given annual heat supply. The model predicting ellipsoidal talik geometry was
28	verified by talik thickness observations using transient electromagnetic (TEM) soundings in
29	Peatball Lake on the Arctic Coastal Plain (ACP) of Alaska. The lake width-depth ratio of the
30	elliptic talik can characterize the energy flux anisotropy in the permafrost although the lake
31	bathymetry cross section may not be elliptic due to the presence of near-surface ice-rich
32	permafrost. This theory suggests that talik development stabilizes thermokarst lakes by ground
33	subsidence due to permafrost thaw while wind-induced waves and currents are likely responsible
34	for the elongation and orientation of thermokarst lakes in certain regions such as the ACP of
35	northern Alaska.





36 1. Introduction

37	Thermokarst lakes are abundant in regions underlain by ice-rich permafrost including the Arctic
38	Coastal Plain (ACP) of northern Alaska, northwestern Canada and Siberia (Grosse et al., 2013).
39	These lakes are formed due to permafrost degradation and their basin evolution is fundamentally
40	different from lakes formed in temperate and tropical regions. Thermokarst lakes affect the
41	thermal regime of the surrounding permafrost, which affects the geomorphology and evolution
42	of the lake basin. If the lake bed has a mean annual temperature greater than 0°C, the sub-lake
43	permafrost will begin to thaw (Burn, 2002; Arp et al., 2016). This typically occurs in lakes
44	deeper than the maximum winter ice thickness, where the ice cover floats above an unfrozen
45	water body. In this case, unfrozen lake bed sediments persist and the thaw front continues to
46	penetrate deeper into the underlying permafrost. This creates a "talik", or a perpetually unfrozen
47	zone confined by permafrost, beneath the lake depending on local anomalies in thermal,
48	hydrological, hydrogeological, or hydrochemical conditions (van Everdingen, 1998). In ice-rich
49	permafrost, the conversion of ice to water with thaw causes a volumetric reduction in the
50	unconsolidated material and the lake bed consequently subsides. The total depth of subsidence is
51	determined by the depth and distribution of excess-ice content in the permafrost. As the lake
52	expands by lateral thermomechanical erosion (thermal abrasion) of the banks, mineral and
53	organic sediments from retreating shores are delivered to the lake basin (Farquharson et al. 2016).
54	However, thaw-induced ground subsidence effectively deepens the basin, so volumetric capacity
55	can actually increase over time. Over decades and centuries, the talik increases in thickness and
56	lake bed subsidence continues as long as the thawing permafrost is ice-rich.
57	In certain ice-rich permafrost regions in the Arctic, there is a preferential orientation and elliptic

58 shape to the numerous thermokarst lakes that occur there (Black and Barksdale, 1949; Hinkel et





59	al., 2005; Grosse et al., 2013). On the ACP of northern Alaska, many elliptical thermokarst lakes
60	have a long axes oriented 10-20 degrees west from true north, which is nearly perpendicular to
61	the prevailing wind direction (Sellmann, 1975; Carter, 1981). Hinkel et al. (2005, 2012) also
62	showed significant correlation between lake orientation and summer wind direction by analyzing
63	the geometric shape metrics of the thermokarst lakes and drained thermokarst lake basins
64	(DTLB) on the ACP of Alaska. It has been proposed that winds at the lake surface cause currents
65	and generate a two-cell circulation pattern which triggers thermomechanical bank erosion,
66	resulting in asymmetrical elliptical orientation (Livingstone, 1954; Rex, 1961; Carson and
67	Hussey, 1962; Mackay, 1992; Arp et al., 2011). The sublittoral shelves and bars typically found
68	in the deeper thermokarst lakes may also be formed by wind-driven currents and waves, and
69	warmer water temperatures (Carson and Hussey, 1962). The axis-oriented sublittoral shelves
70	make the orientation appear more pronounced in larger basins. Other processes also influence the
71	orientation of thermokarst lakes such as historical drained lake geometry, ground ice distribution,
72	and dune ridge orientation by aeolian sand transport (Carter, 1981).
73	Several numerical models have been proposed and applied that describe permafrost thaw for the
74	purpose of analyzing water and carbon cycles (e.g. Kessler et al., 2012). However, Schuur et al.
75	(2015) stress the need to better represent talik formation and geometries to more effectively
76	parameterize numerical models. Painter et al. (2016) demonstrated a coupled surface/subsurface
77	permafrost thermal hydrology model at the ice-wedge polygon scale. Kessler et al. (2012)
78	simulated carbon mobilization over 10,000 years on two neighboring thaw lakes located on
79	organic-rich Yedoma permafrost terrains in the northern Seward Peninsula, Alaska using a 3D
80	numerical thermal model. They demonstrated the effectiveness of model simulations for methane
81	emission from thermokarst lakes. Ling and Zhang (2003b) provided a numerical parametrization





82	of lake talik development, and showed that shallow thermokarst lakes are a significant heat
83	source affecting permafrost and talik geometries. Rowland et al. (2011) advanced the technique
84	by including parameter of advective heat transport on talik evolution. West and Plug (2008) and
85	Plug and West (2009) characterized the lake bathymetry including the effects of lake ice and
86	littoral shelves. These thermal models use long-term mean lake temperature as the Dirichlet
87	boundary condition and a uniform annual mean temperature profile as the initial condition.
88	Analytical and numerical models can provide dynamic solutions for the heat transfer equation
89	under quasi-steady state climate conditions. However, the existing models require prescribed
90	lake shapes (circle or ellipse) to obtain information on talik depths as opposed to modeling the
91	likely influence of talik evolution on lake shape - this work, in part, attempts to address this
92	shortcoming.

93 Direct drilling measurements of taliks below thermokarst lakes are difficult to obtain and only 94 exist in a few rare case studies (Brewer, 1958; Johnston and Brown, 1966; Roy-Leveilee and 95 Burn, 2017; Heslop et al., 2015). Geophysical methods can be used (e.g. Schwamborn et al., 96 2000; Parsekian et al., 2019; Creighton et al., 2018; Sullivan et al., 2021; O'Neill et al., 2020); 97 however, it is time consuming and laborious to produce 3D subsurface images at the large scale 98 of lakes found in permafrost lowland regions. Since field measurements (coring, geophysics, 99 etc.) are spatiotemporally limited, numerical and analytical modelling is used to gain critical 100 insights into talik evolution. Mackay (1962) obtained the analytical vertical temperature profiles 101 below the water at the center of a circular lake by analytically solving the heat transfer equation. 102 Burn (2002) subsequently extended the solution for an elongated lake. This analytical model has 103 been used for lake process characterization because the quasi-steady state model was able to 104 reasonably quantify the talik thickness. For example, Hinkel and Arp (2015) applied the





- 105 temperature profile to 2100 lakes and found that larger, long-lived lakes (more than 66 ha) may
- 106 have taliks that penetrate through the permafrost (throughgoing talik) to the ground-water system
- 107 below in a region with permafrost that is up to 600 m thick.

108 These existing models require the prescribed lake shapes (circle or ellipse) to obtain the talik 109 depth; in fact, no existing studies explicitly provide an answer to the fundamental question: why 110 do thermokarst lakes tend to be elliptical and/or round? Also, in spite of several decades of 111 research focused on the orientation of thermokarst lakes in certain regions, no existing studies 112 explicitly explain why thermokarst lakes in some regions orient perpendicular to the prevailing 113 wind direction. The objective of this work is to implement a novel mathematical framework that 114 concurrently describes both the oriented nature of the thermokarst lakes and the talik depth 115 below the lakes. Previous models have calculated the talik development due to heat flow, though 116 most use some simplifying assumptions to reduce dimensionality. Separately, researchers have 117 hypothesized about elliptical lake morphology by invoking winds, currents, and erosion. Here, 118 we couple both the talik evolution and lake shape questions together in a single mathematical 119 model. Additionally, we intend to use this theory to demonstrate that the thermal gradient could 120 exert control on the depth/width ratio of the talik. In other words, the proposed theory aims to 121 isolate the most important process – sub-lake permafrost thaw and subsidence - from other 122 effects such as wind-wave erosion, thaw slumping, sediment redistribution and incoming 123 radiation imbalance, using thermally optimized lake geometry.





124 **2. Theory**

125 2.1 Basin integrated energy equation

- 126 Heat energy collected by a waterbody is used for phase boundary expansion as well as heat
- 127 conduction into the adjacent permafrost (e.g. French, 1996). From the energy balance equation
- 128 around the phase boundary, the energy for permafrost thaw is expressed as the subtraction of
- 129 heat conduction from the input energy at the phase boundary (Carslaw and Jaeger, 1959; Patel,
- 130 1968; Lunardini, 1981). Therefore, the energy conservation equation at the phase boundary can
- 131 be expressed as,

$$q_f = q_{in} - q_c , \qquad (1)$$

where q_f is heat for fusion or thawing (W/m²); q_{in} is heat input at the phase boundary (W/m²); and q_c is heat conduction to the permafrost (W/m²). These heat fluxes can be evaluated by the following formulas:

136
$$q_f = \phi v \rho L \quad , \tag{2}$$

137
$$q_{in} = q_{suf} - k_L \frac{dT}{dn} \quad \text{, and} \tag{3}$$

$$q_c = -k_p \frac{dT}{dn} \quad . \tag{4}$$

139 where ϕ is volumetric water content; v is thaw rate or advancement of talik boundary (m/s); ρ is 140 density of water (kg/m³); L is latent heat for fusion (liquid-solid) of water (J kg⁻¹); q_{suf} is 141 additional heat input from ground surface around the lake shore (W/m²); k_L is thermal 142 conductivity of unfrozen soil or lake water; and k_p is thermal conductivity of frozen soil 143 (permafrost); T is temperature (C); and n is outward normal from the interface into the soil (m).



144



When heat input from the surface is consumed for phase change without any loss ($q_c = q_{suf} =$ 145 0), the well-known Stefan equation can be obtained from Equations (1) through (4) under the 146 quasi-steady state approximation (Stefan, 1891; Kurylyk & Hayashi, 2016). This study also 147 adopts the quasi-steady state approximation for the talik shape characterization. 148 As the thawing process is direction-dependent, it is convenient to use vector notation (Figure 1). 149 That is. 150 $\boldsymbol{q}_f = \boldsymbol{q}_{in} - \boldsymbol{q}_c.$ (5) 151 The letter in bold denotes a vector. The fusion heat flux vector corresponds to thaw direction, 152 which is affected by the other two heat fluxes. Figure 1 also illustrates the thermal profiles 153 around the thaw lake in warm and cold seasons. The horizontal near-surface heat conduction is 154 influenced by the seasonality of the surface heat budget while the vertical heat conduction under 155 the lake remains unidirectional throughout the years. Clearly, the presence of the thaw lake considerably alters the heat environment of the permafrost while the temperature slope at the 156 157 bottom of the permafrost may be approximated by the geothermal gradient in regions with thick 158 continuous permafrost such as the ACP. This directionality in the heat environment around the 159 lake may cause anisotropic talik expansion. Here, the phase change heat vector is expressed as 160 proportional to the normal heat input q_{in} , as follows:

161
$$\boldsymbol{q}_{f} = (q_{f,x}, q_{f,y}, q_{f,z}) = (\xi q_{in}, \eta q_{in}, \zeta q_{in}) = q_{in}(\xi, \eta, \zeta)$$
(6)

162 where q_{in} is the input heat normal to the phase boundary, ξ , η , and ζ are the fusion energy 163 fractions of the heat input normal to the phase boundary with respect to x, y, and z directions, 164 respectively. The depth of the phase boundary, $z = \varphi(x, y)$, may be expressed as an arbitrary 3D 165 surface as,





166
$$g(x, y, z) = \varphi(x, y) - z = 0.$$
 (7)

167 Hence, the normal vector \mathbf{n} at any location on the phase boundary g can be written as follows:

168
$$\boldsymbol{n} = \frac{\nabla g}{|\nabla g|} = \frac{1}{|\nabla g|} \left(g_x, g_y, g_z \right) = \frac{1}{\sqrt{\varphi_x^2 + \varphi_y^2 + 1}} \left(\varphi_x, \varphi_y, -1 \right)$$
(8)

169 where the subscript in this expression denotes partial derivative (e.g. $\varphi_x = \partial \varphi / \partial x$) and ∇ is a

170 vector differential operator $(\partial/\partial x, \partial/\partial y, \partial/\partial z)$. As such, the vector of the input heat to the

171 phase boundary φ is

172
$$\boldsymbol{q}_{in} = |\boldsymbol{q}_{in}| \boldsymbol{n} = q_{in} \boldsymbol{n} = \frac{q_{in}}{\sqrt{\varphi_x^2 + \varphi_y^2 + 1}} (\varphi_x, \varphi_y, -1),$$
 (9)

173 and the corresponding fusion heat vector is,

174
$$\boldsymbol{q}_f = \frac{q_{in}}{\sqrt{\varphi_x^2 + \varphi_y^2 + 1}} \left(\xi \varphi_x, \eta \varphi_y, -\zeta\right). \tag{10}$$

175 Next, the fusion heat magnitude can be evaluated using a Euclidian norm as,

176
$$\left| \boldsymbol{q}_{f} \right| = \frac{q_{in}}{\sqrt{\varphi_{x}^{2} + \varphi_{y}^{2} + 1}} \sqrt{\xi^{2} \varphi_{x}^{2} + \eta^{2} \varphi_{y}^{2} + \zeta^{2}} = \frac{\zeta q_{in}}{\sqrt{\varphi_{x}^{2} + \varphi_{y}^{2} + 1}} \sqrt{\alpha_{x}^{2} \varphi_{x}^{2} + \alpha_{y}^{2} \varphi_{y}^{2} + 1}$$
(11)

177 where

178
$$\alpha_x = \frac{\xi}{\zeta}, \ \alpha_y = \frac{\eta}{\zeta} \qquad (12)$$

179 The parameters α_x and α_y describe the anisotropic thermal condition between horizontal and

180 vertical directions. The parameters α_x and α_y are greater than one when the vertical temperature

- 181 gradient is steeper than in horizontal direction. The total fusion energy over the lake can be
- 182 computed by the area integral on the phase boundary Γ . That is,





183
$$\int_{\Gamma} |\boldsymbol{q}_f| \, d\Gamma = \iint_{B} |\boldsymbol{q}_f| \, \sqrt{\varphi_x^2 + \varphi_y^2 + 1} \, dx \, dy$$

184

$$= \zeta q_{in} \iint_B \sqrt{\alpha_x^2 \varphi_x^2 + \alpha_y^2 \varphi_y^2 + 1} \, dx dy. \tag{13}$$

This expression indicates that the heat required for lake expansion is proportional to the weightedphase boundary area.

187 **2.2 Optimum phase boundary shape as extremum**

188 The calculus of variation, often referred to as a functional analysis, is the mathematical technique 189 to find an extremum (minimum or maximum) of the system in terms of a function type instead of 190 a variable (e.g. Courant and Hilbert, 1954; Gelfand and Fomin, 1963). Here, we present the 191 thermally optimum function type $\varphi(x, y)$ of the phase boundary using this method. As presented 192 in the previous section, the heat consumption rate for talik expansion is represented by the 193 weighted phase boundary area while the time-integrated heat supply is equivalent to the thawed 194 permafrost volume. Assuming heat thaws the most susceptible region of the permafrost near the 195 heat source first, the shape of a talik may minimize the total permafrost thaw with a given 196 amount of incoming energy. Hence, this variational principle states that the optimum talik shape 197 should minimize the phase boundary area for the total talik expansion. The weighted phase 198 boundary area A and its volume V can be expressed as follows:

199
$$\begin{cases} V[\varphi] = \iint_B \varphi \, dx dy \\ A[\varphi] = \iint_B \sqrt{\alpha_x^2 \varphi_x^2 + \alpha_y^2 \varphi_y^2 + 1} \, dx dy \end{cases}$$
(14)

200 The functional *F* is defined as

201
$$F[\varphi] = \lambda V[\varphi] + A[\varphi] = \iint_{B} \left(\lambda \varphi + \sqrt{\alpha_{x}^{2} \varphi_{x}^{2} + \alpha_{y}^{2} \varphi_{y}^{2} + 1}\right) dx dy$$
(15)





202 where λ is a constant. Extremum of the functional *F* can be determined for $\lambda < 0$ because both

203 V and A are monotonic functions. Let

204
$$f(\varphi, \varphi_x, \varphi_y) = \lambda \varphi + \sqrt{\alpha_x^2 \varphi_x^2 + \alpha_y^2 \varphi_y^2 + 1}.$$
 (16)

205 Equation (15) becomes,

206
$$F[\varphi] = \lambda V[\varphi] + A[\varphi] = \iint_B f(\varphi, \varphi_x, \varphi_y) \, dx \, dy.$$
(17)

207 To find the extremal phase-boundary shape φ that minimizes the functional $F[\varphi]$, the Euler's

208 Equation can be formulated as,

209
$$\frac{\partial f(\varphi,\varphi_x,\varphi_y)}{\partial \varphi} - \frac{\partial}{\partial x} \left(\frac{\partial f(\varphi,\varphi_x,\varphi_y)}{\partial \varphi_x} \right) - \frac{\partial}{\partial y} \left(\frac{\partial f(\varphi,\varphi_x,\varphi_y)}{\partial \varphi_y} \right) = 0.$$
(18)

210 Substituting Equation (16) to (18) yields,

211
$$\lambda - \frac{\partial}{\partial x} \left(\frac{\alpha_x^2 \varphi_x}{\sqrt{1 + \alpha_x^2 \varphi_x^2 + \alpha_y^2 \varphi_y^2}} \right) - \frac{\partial}{\partial y} \left(\frac{\alpha_y^2 \varphi_y}{\sqrt{1 + \alpha_x^2 \varphi_x^2 + \alpha_y^2 \varphi_y^2}} \right) = 0.$$
(19)

By analogy to two-dimensional application in Ohara and Yamatani (2019), an ellipsoid is one of
the solutions of Equation (19), as follows:

214
$$z = -\varphi = -\sqrt{\frac{4}{\lambda^2} - \frac{x^2}{\alpha_x^2} - \frac{y^2}{\alpha_y^2}} + d, \text{ or}$$
(20)

215
$$\left(\frac{x}{\frac{2\alpha_x}{|\lambda|}}\right)^2 + \left(\frac{y}{\frac{2\alpha_y}{|\lambda|}}\right)^2 + \left(\frac{z-d}{\frac{2}{|\lambda|}}\right)^2 = 1.$$
(21)

216 Detailed alternative derivation using isoperimetric inequality is available in the Appendix A. The

- 217 coefficients d and λ can be determined by further variational analysis explained in Appendix B.
- 218 As such, Equations (20) and (21) become





219
$$\varphi = \sqrt{D^2 - \frac{x^2}{\alpha_x^2} - \frac{y^2}{\alpha_y^2}}$$
, and (22)

220
$$\left(\frac{x}{\alpha_x D}\right)^2 + \left(\frac{y}{\alpha_y D}\right)^2 + \left(\frac{z}{D}\right)^2 = 1$$
, respectively. (23)

221 D is the talik center depth, $\alpha_x \& \alpha_y$ are the cross-sectional aspect ratios. Hence, the semi-

ellipsoidal geometry of the phase boundary (i.e., the boundary between the permafrost and talik)
was explicitly derived as a thermally optimum shape based on the variational principle using the
thermal quasi-steady state approximation; this is the 3D Stefan Equation for the talik beneath a
thermokarst lake.

226 **2.3 Thermokarst lake bathymetry and phase boundary geometry**

227 When top-down permafrost thaw dominates the process, the thermokarst lake bottom shape 228 $\psi(x, y)$ may be similar to the phase boundary shape, as illustrated in Figure 2. However, the 229 lake bathymetry can be related to the permafrost degradation rate defined as,

230
$$r_{deg} = \frac{D_{thaw}}{D_{frzn}} \sim 1 - \frac{\psi(x,y)}{\varphi(x,y)} \sim 1 - \frac{H}{D} \quad , \tag{24}$$

231 where *H* and *D* denote the water depth and the talik thickness at the lake center, respectively. 232 D_{frzn} is the frozen soil thickness (m) and D_{thaw} is the corresponding thawed soil thickness depth 233 (m), which is strongly dependent on the excess ground ice content; excess ice is defined as the 234 volume of ice in the ground which exceeds the total pore (van Everdingen, 1998; Kanevskiy et 235 al., 2013). Therefore, thaw settlement is typically computed from wedge-ice volume content and 236 the thickness of the layer with excess ground ice. However, as the consolidation settlement 237 effect, which is a function of void ratio and effective stress, may not be separated, we use the 238 simple permafrost degradation rate (Equation 24) in this study.





- 239 If the permafrost degradation rate is uniform and constant throughout the basin (Panel A:
- 240 uniform permafrost in Figure 2), the lake bathymetry tends to be an ellipsoid shape. However, as
- the ice-rich layer (ice wedges) is typically developed near the surface on the ACP (e.g.
- 242 Kanevskiy et al., 2013, 2016), the bathymetry may have a flatter bottom like a rectangular cross
- section (Panel B: layered permafrost in Figure 2) because the ice-rich layer is characterized by
- 244 much higher thaw settlement than the ice-poor permafrost at depth. Therefore, proportionality
- 245 between talik thickness and lake water depth or uniform permafrost is unlikely reasonable
- assumption due to the ice rich layer presence. Indeed, Hinkel et al. (2012) showed many flat-
- 247 bottomed lakes through the extensive bathymetry surveys across the ACP of Alaska using a
- 248 GPS-enabled sonar from a boat.
- Additionally, as hydrology also affects the lake water level, the apparent lake bathymetry or lake water depth, h(x, y) must be adjusted by the water loss (or gain) per unit area. Therefore,

251
$$h(x, y) = [1 - r_{sub}]\varphi(x, y) - H_{loss} , \qquad (25)$$

where H_{loss} (m) is the elevation difference between the current water surface and original ground surface before lake formation. At the lake center,

254 $H = [1 - r_{sub}]D - H_{loss} \qquad (26)$

Thus, the thermokarst lake bathymetry is affected by the ice-rich layer thickness, interannual water balance, lake age, and talik geometry.





257 **3. Case study**

258 **3.1 Study area**

- 259 Peatball Lake (70°42.40N, 153°55.50W; 3 m above sea level) on the ACP of Alaska was chosen
- 260 for the demonstrative model application in this study as it has been relatively well-documented.
- Figure 3 shows the location of Peatball Lake as well as the subregions that will be presented later.
- 262 Peatball Lake, named for the abundant submerged peat balls on the lake bed, is a subcircular lake
- 263 on the Outer Coastal Plain of Alaska with a surface area of 1.18 km². Permafrost in this area is as
- thick as 410 m (Jorgenson et al., 2007), and the average volumetric ground ice content is about
- 265 77% in the near surface to a depth of 4 m (Kanevskiy et al., 2011). A talik has formed under
- 266 Peatball Lake because the maximum water depth of 2.5 m exceeds the maximum winter ice
- thickness of 1.5 to 2.0 m (Arp et al., 2015; Lenz et al., 2016). The talik depth was estimated as
- 268 91 m at the lake center based on noninvasive TEM measurements (Creighton et al., 2018).
- 269 However, the talik may not be present beneath the sublittoral shelves on the western shore from
- the bathymetry (Lenz et al., 2016). Additionally, Lenz et al. (2016) reported that, based on
- 271 remote sensing imagery, Peatball lake has expanded laterally between 0.02 m/year and 1.36
- 272 m/year between 1955 and 2002.

273 **3.2 Geophysical survey of talik**

274 Geophysical field methods are effective for identifying and visualizing the frozen-unfrozen

- interface, which is a key feature in permafrost dynamics (e.g. Pilon et al., 1985; Doolittle et al.,
- 276 1990; O'Neill et al., 2020; Rangel et al., 2021). For lake taliks in the continuous permafrost zone,
- 277 Schwamborn et al. (2002) analyzed the sedimentary history of Lake Nikolay in the western Lena
- 278 River Delta using seismic reflection and ground penetrating radar (GPR). Other geophysical





279	methods such	as surface 1	nuclear ma	agnetic resonat	nce (NMR)	can be	used to	detect lake ta	ıliks

- 280 (Parsekian et al., 2019) and remnant taliks in drained lake basins (Rangel et al., 2021). At
- 281 Peatball Lake, Creighton et al. (2018) estimated the talik depth using transient electromagnetic
- 282 (TEM) surveys along transects perpendicular to lakeshores.
- 283 We applied the derived 3D Stefan equation to Peatball Lake based on the 27 talik thickness point
- 284 measurements across the lake (Figure 4), estimated using TEM soundings (Creighton et al.,
- 285 2018) during spring 2016 and 2017. Figure 4 shows the observed talik thicknesses by the TEM
- sounding (dots) and the fitted theoretical talik thickness estimates (contour lines) superimposed
- 287 over the corresponding lake bathymetry measured by Lenz et al., 2016.

The geometric parameters of the semi-ellipsoid model such as the talik center depth (*D*), the cross-sectional aspect ratios ($\alpha_x \& \alpha_y$), lake orientation azimuth angle and the lake center

290 location were systematically determined by grid searching to minimize the root mean square

291 difference (RMSD) between the model and thaw front obtained from the TEM data. The

- 292 optimum parameters for the smallest RMSD (5.94 m) are shown in Figure 4. Unexpectedly, the
- basin orientation angle was found to be 23 degrees east from true north, unlike the orientation of
- 294 other surrounding lakes in the region. Comparison between the extrapolated talik geometry and
- the lake bathymetry (Lenz et al., 2016) suggests the possibility of coalescence of two basins in
- the past; a relatively common occurrence on the ACP of Alaska. However, if we had more TEM
- 297 measurement points, particularly in the "possible talik sub-basin", the fitted talik geometry could
- be different as the model was only fitted for the 27 TEM soundings. Lake taliks tend to have a
- semi-ellipsoidal shape, at least locally, as indicated by the very good fit of the elliptic model to
- 300 the TEM measured talik thicknesses (see Figure 4 with overall RMSD = 5.94 m). The idealized,





- 301 thermally optimum geometry model can be used to analyze lake formation history of the
- 302 irregular talik associated with multi-generation lakes such as Peatball Lake.
- 303 Additionally, the gaps between the shoreline and the modeled talik extent located along north
- 304 and east shores occur where lake expansion is occurring most rapidly (Lenz et al., 2016). It has
- 305 been reported that thaw lake banks continuously retreat through a combination of thermal and
- 306 mechanical processes, although there is significant variability in rate of bank retreat depending
- 307 on region (Hopkins, 1949; Hopkins et al., 1955; Tomirdiaro, 1982; Rampton, 1982; Burn and
- 308 Smith, 1990; Jones et al. 2011, Lenz et al., 2016). Cross-sectional numerical thermal models
- demonstrated that the expansion rates are affected by the talik thickness (Plug and West, 2009)
- 310 and seasonal snow cover (Ling and Zhang, 2003a). The disagreement between the lake and talik
- 311 extents on the north and east shores of Peatball lake implies that rapid horizontal lake expansion
- 312 can locally dominate permafrost thaw and subsidence processes even in a lake with a talik.
- 313 Figure 5 compares the observed lakebed and talik profiles in Peatball Lake along the north-south 314 center line and along transects (b) -(c), respectively. Note that the TEM transects for the talik is 315 not a straight line (See figure 4); therefore, the fitted theoretical line shows irregularity. Figure 316 5A illustrates that the lakebed profile is characterized by flatter trapezoidal geometry compared 317 to the elliptic talik. In fact, there is a clear inflection in the linear regression line at a talik depth 318 of ~50 m in Figure 5B. From the slopes of the regression lines, the permafrost degradation rates r_{deg} are computed as 97.3 % and 99.7 % for the shallow talk section (50 m or less) and the deep 319 320 section (50 m or more), respectively. This analysis suggests that the subsidence due to permafrost thaw continues even after the shallow ice-rich part of the permafrost (about 4 meters, 321 322 Kanevskiy, 2011) is thawed while it has diminished around the depth of 50 meter under Peatball





- 323 lake. This case study demonstrates a link between lake bathymetry and talik thickness associated
- 324 with a layered permafrost structure and the wind erosion effect.

325 **3.3 Depth-width ratio and temperature gradient**

- 326 The analysis (Equations 22 & 23) suggests the proportional relationship between lake/talik
- 327 geometry and thaw energy. That is,

328
$$a: b: D = \alpha_x: \alpha_y: 1 = \xi: \eta: \zeta = q_{f,x}: q_{f,y}: q_{f,z}$$
 (27)

Combining Equations (27), (1) and (4), the depth-width (radius) ratio of the talik may be written as follows:

331
$$a: D = \left(q_{in,x} + k_p \frac{dT}{dr}\right): \left(q_{in,z} + k_p \frac{dT}{dn}\right)$$
(28)

332 where r and n are the horizontal and vertical distances from the original permafrost surface 333 center, respectively, and a is the representative horizontal radius of the lake. This expression 334 states that the anisotropic top-down permafrost thaw is caused by anisotropy of the thermal 335 gradient for uniform incoming energy and uniform thermal properties of near surface 336 permafrost. For example, since the vertical thermal gradient is typically steeper than the 337 horizontal gradient during the critical summer months (Carson and Hussey, 1962; illustration in 338 Figure 1), the heat energy in the vertical direction is used more for heat conduction rather than 339 permafrost thawing. The vertical temperature gradient is always negative near the talik boundary in the permafrost $\left(\frac{dT}{dn} < 0\right)$ at the center of the lake while the inter-seasonal average 340 of the horizontal thermal gradient may be negligible $\left(\frac{dT}{dr} \approx 0\right)$. Assuming the normal heat flux 341 to the phase boundary is uniform throughout the phase boundary surface $(q_{in,x} = q_{in,z} = q_{in})$, 342 343 Equation (28) can be simplified as follows:



344



$$\frac{D}{a} = 1 + \frac{k_p}{q_{in}} \frac{dT}{dn} \quad \text{, or} \quad q_{in} = -\frac{ak_p}{a-D} \frac{dT}{dn} \quad . \tag{29}$$

This simple expression may be a useful tool to link the lake depth-width ratio, the lake average 345 heat flux q_{in} , and the vertical temperature gradient $\frac{dT}{dn}$ at the base of the talik. Since $\frac{dT}{dn} < 0$ in 346 347 the permafrost near the talik boundary, the D/a is always less than 1 (flatter than a semi-sphere). 348 However, the depth-width ratio of the talik depends on the vertical temperature slope near the 349 talik boundary, which is likely affected by talik age. For instance, Mackay's analytical model 350 (1962) suggests that the vertical temperature gradient below the lake center begins steeply at the 351 talik initiation, and then over time it approaches a lower slope at equilibrium. Therefore, the 352 formula in Equation (29) suggests that a younger talik should be flatter while an older talik 353 approaches a deeper semi-spheric shape $(D/a \rightarrow 1)$. 354 Table 1 shows the estimated incoming heat flux with the key parameters using the proposed 355 formula (Equation (29)). Creighton et al. (2018) applied the CRYOGRID2 model (Westerman et 356 al., 2013) to Peatball Lake. The temperature slope at the talik bottom at the lake center was 357 estimated by the Mackay's analytical model assuming the lake age of 1400 years since the talik 358 initiation with the same model configuration Creighton et al. (2018) adopted. Creighton et al. 359 (2018) estimated the interannual mean heat flux q_{in} to be 0.070 (W/m²), which is very close to 360 our estimate. As this simplified formula is consistent with the well-configured modeling result, 361 the horizontal thermal gradient contribution to the vertical aspect ratio of the talik seems to be 362 very small in Peatball Lake. 363 Moreover, this relationship may be useful to incorporate the three-dimensional talik expansion 364 effect in a simple analysis without fully integrated permafrost thermal modeling. For example, if

the mean energy flux increases 10 percent from current climate conditions (e.g. shorter lake





- 366 freeze period), assuming all other properties are equal, the talik depth-width ratio D/a would shift
- from 0.171 to 0.234 toward the new equilibrium state. Therefore, this analysis suggests that the
- 368 warmer climate may promote permafrost thaw in the vertical direction more than in the
- 369 horizontal direction. Hence, it is important to quantify the vertical thawing as well as the visible
- 370 lake horizontal expansion in order to evaluate the impact of the climate change on permafrost
- thaw beneath thermokarst lakes.

372 **4. Discussion**

4.1 Relationship between hypothetical models

To illustrate the applicability of the thermal model presented here, the available hypothetical

375 models of thermokarst lake growth are compiled in Figure 6. This diagram focuses on the

376 physical processes after the lake initiation stage assuming the bio-ecological effects are

377 negligible.

378 Figure 6 illustrates the evolution of the talik in ice-rich permafrost over time, with driving

379 processes shown in the right panel. In Stage A, the mechanical processes of wave erosion and

thaw slumping along lake margins dominate lake expansion in summer, and shallow water favors

381 grounded lake ice in the winter. In time (Stage B), the lake deepens from thaw subsidence

382 beneath the older lake center. Winter ice may freeze to the lake bed, but heat loss is insufficient

- to freeze the underlying thawed lake bed sediments. A shallow talik develops as thermal
- 384 processes work in tandem with mechanical processes, the latter now enhanced by more vigorous
- 385 lake circulation. By Stage C, the talik is well developed beneath the entire lake basin as ground
- 386 subsidence continues. Eventually (Stage D), the winter ice cover no longer extends to the lake
- 387 bed, but instead floats atop a residual pool of lake water, while milder vertical temperature





388	gradient beneath the lake deepens the talik as the lake matures. Thermomechanical erosion of
389	lake margins, especially if there are prominent banks in hilly terrain, promotes sedimentation on
390	near-shore shelves, and the underlying talik may begin refreezing. If the lake hasn't drained by
391	this point (Stage E), the talik beneath the lake center extends deeper into the permafrost although
392	subsidence may cease as the excess ice content diminishes with depth. Where many large, old
393	lakes exist, the permafrost may be riddled with deep taliks, and some may eventually penetrate to
394	the permafrost base to create a through-going talik.
395	Talik development is a natural processes governed by local conditions, but can be impacted by
396	direct and indirect human activities. Conditions that favor talik initiation and growth include:
397	• Deepening lake waters triggered by greater precipitation and/or reduced evaporation,
398	which promotes a floating ice regime
399	• Presence of ice-rich sediments (e.g., Yedoma) beneath lakes
400	• Warmer lake water induced by regional warming or by longer ice-free summers
401	• Thinner winter ice cover due to warmer winter temperatures and/or deeper snow
402	Conversely, talik growth cessation or contraction can occur when these same drivers are reversed,
403	if the lake partially or completely drains, or when the lake basin is filled with sediments. The
404	latter scenario is more likely in hilly terrain when the expanding lake erodes high banks and lake
405	currents redistribute sediments.





406 **4.2 Thermal process and preferential expansion**

407 **4.2.1 Lake geometry and heat balance**

- 408 The analytical expression of the lake geometry may be useful to analyze the horizontally oriented
- 409 lakes as well. From Equation (27) and (1), we have,

410
$$a: b = q_{f,x}: q_{f,y} = (q_{in,x} - q_{c,x}): (q_{in,y} - q_{c,y}),$$
(30)

411 where *a* and *b* are the semi-major and -minor axes of the elongated lake, respectively. When

412 horizontal heat conduction into the tundra is negligible, $(q_{c,r} = k_p \frac{dT}{dr} \approx 0)$, this equation can be

413 reduced to,

414
$$a: b = q_{in,x}: q_{in,y}.$$
 (31)

415 Hence, the aspect ratio of elliptic lakes can be explained by heat supply inequality if the lake

416 geomorphology process is dominated by thermal process. As expressed in Equation (3), there are

417 two different components in the incoming heat flux to the lake banks: surface energy flux and

418 heat conduction from the lake water body. Thus, the lake aspect ratio may be written as,

419
$$a: b = \left(q_{suf,x} - k_L \frac{dT}{dx}\right): \left(q_{suf,y} - k_L \frac{dT}{dy}\right)$$
(32)

420 4.2.2 Incoming radiation imbalance effect

421 One of the incoming surface energy flux inequalities q_{suf} may be caused by shortwave radiation

422 along the lake shoreline. The daily potential solar irradiation on a sloping surface can be

423 computed by the trigonometric function (e.g. Equation B.11 in DeWalle and Rango, 2008). The

- 424 total daily radiation is a function of latitude and bank slope angle, which depends on the
- 425 permafrost degradation rate, the maturity of the talik, and ground ice distribution.





426	Figure 7 shows the computed mean daily potential solar irradiation on the sloping lakeshore (I'_q)
427	relative to a flat surface (I_q) during the summer period (June-August) at three different latitudes.
428	The shape of this diagram may correspond to the shape of a thermokarst lake as the enhanced
429	radiation results in more permafrost thaw. The difference in relative incoming radiation will
430	diminish as bank slope angle lessens. In general, the south facing slope along the northern shore
431	tends to receive more radiation than the north facing slope (e.g. Séjourné et al., 2015). This
432	tendency is more pronounced in lower latitude zones due to the higher mid-day sun angle.
433	It is interesting that at 65 and 60 degree latitude the north and south facing banks receive slightly
434	less radiation than east and west facing slopes, while an opposite result occurs at 70 degree
435	latitude (Figure 7). Therefore, the radiation imbalance may partially explain the north-south
436	elongation along the 70 degree latitude line and the west-east elongation of lower latitude (60-65
437	degrees) of lowland thermokarst lakes shown by Grosse et al. (2013, Figure 19). However,
438	because these small differences in incoming radiation imbalance alone are insufficient to result
439	in the distinctive lake elongation in the ACP, they likely introduce rather minor additional
440	complexities in lake spatial shape.

441 **4.3 Wind wave erosion and preferential expansion**

Wind wave erosion plays an important role in horizontal expansion of shallow lakes because waves can undercut the vegetated bank (Hopkins, 1949). Wind wave asymptotically makes the water bodies (e.g. lakes and bays) round by local net sediment flux even in low latitude regions (e.g. Ashton et al., 2009). The effect of waves on shoreline morphology has been analyzed in the coastal engineering field: for example, Silvester (1974) investigated the equilibrium shape of bays under different wave conditions using laboratory wave experiments and found that the





448	stable beach in the bay adapted a half-heart or cardioid shape for a fixed wave direction in the
449	absence of sediment supply. Reeve et al. (2018) showed theoretically that the equilibrium
450	coastline shape can be expressed as a diffusion type equation through incorporating the wave
451	diffraction effect, which makes the wave crest line nearly parallel to the shore. However,
452	according to the shallow water wave theory, which is applicable for small fetch distances on
453	lakes in the ACP, water waves do not cause any sediment transport without current, although
454	wave motion is a key factor for the mobilization of the sediment (e.g. Carson and Hussey, 1962).
455	Wind-induced water circulation in a shallow, oval lake was perhaps first analyzed by
456	Livingstone (1954) who showed theoretically that the current around the lake ends may be
457	accelerated efficiently by wind-induced return rip currents. However, the lake water circulation
458	pattern assumed in his study (shown in the left side of Figure 8) was less common than the
459	pattern described by Carson and Hussey (1962), who observed reverse circulation patterns near
460	the lake ends, as shown in the right side of Figure 8. For convenience, we refer to two distinctive
461	current patterns: the Livingstone type and the Carson & Hussey (C&H) type. C&H type
462	circulation can indeed explain the commonly observed peat and sediment bars near the leeward
463	lake side shores. Carson and Hussey (1962) noted that sedimentation on the leeward lake side
464	can provide protection from mechanical wave erosion as well as insulation from permafrost thaw,
465	which result in lake elongation. They also observed that preferential bank erosion is typically
466	focused in zones oriented 50 degrees to wave approach. The return flow was found to
467	concentrate around the windward lake side, which accelerates the mechanical erosion and
468	sediment transport at the lake ends. However, the Livingstone type circulation might occur
469	depending on the local wind field as it can explain the sublittoral shelf formation on the
470	windward shore. In either case, the wind-induced current effect on lake elongation can be





471	supported by Livingstone's theory (1954) which should be valid for both circulation types. Thus,
472	the combination of wind wave mobilization and lake water circulation is the most accepted
473	hypothesis for lake elongation during the relatively young shallow lake expansion stage (Carson,
474	1968; Arp et al., 2011, Hinkel et al., 2012).
475	The shallow wave theory states that the sediment mobilization due to wind wave only occurs in
476	shallow water (wave height >4 % of water depth, e.g. Reeve et al., 2018). Therefore, the
477	contribution of the wind wave effect to lake elongation may be reduced as the lake deepens.
478	Figure 9 shows a plot of lake length: width ratios versus the percent of lakes with a bedfast ice
479	regime in seven study regions in Alaska determined with satellite-based synthetic aperture radar
480	imagery (Engram et al., 2018). The study regions represent differences in permafrost
481	characteristics and climate that appear to be reflected in this comparison of length:width ratio
482	and the percent of lakes in a region that freeze to their bed and thus likely do not have a sub-lake
483	talik. For example, lakes in the Teshekpuk Lake and Kuparuk study areas have a shape that is
484	nearly twice as long as it is wide. In both of these regions, more than 80% of the lakes freeze to
485	their bed and likely do not have a talik. This is contrast to lakes located near Umiat and on the
486	Seward Peninsula, that have primarily developed in Yedoma permafrost deposits. Lakes near
487	Umiat and on the Seward Peninsula tend to be more circular (L:W = 1.3 to 1.4) and more than
488	90% likely have a talik since they do not freeze to their bed in the winter. The differences
489	observed here relative to elongation of lakes and whether the region primarily has lakes that
490	freeze to their bed or not likely demonstrates a key aspect related to the role of wind-wave
491	erosion. In general, the shallower lakes common in coastal areas, such as Teshekpuk, Barrow,
492	and Kuparuk, are more elongated likely due to wind wave erosion. Whereas lakes in Umiat and
493	Inigok with a thicker ice-rich permafrost layer tends to rounder because of more rapid talik





494 development and more subsequent subsidence. This remote-sensing based evidence implies that

- the wind effect seems to be limited by the lake thermal subsidence due to talik development
- 496 underneath while the lake with the bedfast ice may continue elongating by the wind erosion.

497 **4.4 Applicability of the 3D Stefan equation**

498 The limitations of the derived 3D Stefan Equation (Equation 22) are summarized in this section

499 along with Figure 6. Once a seasonal pond is formed on the permafrost, it primarily expands

500 horizontally by wind wave erosion and the thaw slump process (Carson & Hussey, 1962;

501 Livingstone, 1954; Rex, 1961; Hinkel et al., 2012, Grosse et al., 2013) because the active layer

502 beneath the pond likely freezes every year. On the flat ACP of Alaska, lake thaw slump tends to

503 be the result of topography (e.g. slope and aspect of the ground surface) while lake elongation is

504 likely caused by wind wave erosion. As described above, preferential bank thaw at the lake ends

505 can be explained by the insulation effect of the sediments carried by the water current (likely, the

506 C&H type circulation) because the sublittoral shelf may be initiated at this stage.

507 When seasonal thawing penetrates more deeply than the annual freezing depth, a talik may be

508 initiated, typically around the deepest point near the center of the lake (Lachenbruch et al. 1962).

509 Sellmann (1975) described this process, which is one of the mechanisms for shelf formation in a

510 thermokarst lake. For the horizontal expansion stage A in Figure 6, the proposed quasi-steady

state thermal model may not be appropriate because the lakeshore expansion imbalance occurs at

512 least minimally throughout the lake expansion process. However, the 3D Stefan equation may

513 be able to characterize the talik in the initiation stage B in Figure 6.

514 Once the talik is established, the 3D Stefan's thermal model proposed here suggests that the talik

515 may begin to influence lake geometry. Since sediment mobilization due to wind-driven waves





516	occurs in shallow water, lake elongation by waves may diminish as the lake deepens via ground
517	subsidence (Figure 9). Lake water effectively collects energy from the surface during summer
518	and the talik stores the excess heat throughout the winter. Arp et al. (2010, 2011) and Jefferies et
519	al. (1999) discussed the difference in heat conduction between a grounded ice lake and a floating
520	ice lake. Their observations are generally consistent with the proposed theory because a deeper
521	talik under a floating ice lake should have a greater heat capacity. Since lake elongation likely
522	occurs before talik formation, the horizontal lake characterization derived in this study may not
523	be fully applicable to the analysis of thaw lakes on the ACP. In fact, the disagreement of the
524	talik and lake extents in Peatball Lake application illustrates the multiple effects on the lake
525	bathymetry and orientation. Clearly, however, talik expansion and concurrent subsidence
526	stabilizes lake geometry and contributes to lake roundness.
527	The applicability of the proposed 3D Stefan equation must be limited for lakes with high
528	sediment influx and for lakes with through talik. The paired sublittoral shelves on both lake sides
529	are commonly found in the sand dune areas of the southern ACP. The talik shape is likely altered
530	by uneven sediment deposition that affects the temperature gradient normal to the phase
531	boundary as mentioned by several researchers (Mackay, 1992; Hunter et al., 1981; West and
532	Plug, 2008). The shelves created by sediment redistribution due to lake water circulation adds
533	complexity to the ellipsoidal talik shape described in this study. Finally, if the talik penetrates
534	through the permafrost and becomes a throughgoing talik (Hinkel and Arp, 2015), the proposed
535	thermal theory herein is no longer applicable for thermokarst lake and talik characterization.





536 **5. Conclusions**

537	The theory presented here addresses the origin of the thermokarst lake ellipticity on the ACP.
538	Elliptic lake geometry results from minimizing overall thawing energy consumption for a given
539	incoming energy load. This is particularly applicable for mature, deep thermokarst lakes with
540	well-developed taliks. Additionally, existing hypothetical models were reviewed to illuminate
541	the thermal effect on the thermokarst lake morphology.
542	The derived ellipsoid talik model integrates the atmospheric forcing (or incoming energy), the
543	vertical thermal gradient, the thermal diffusivity of the permafrost, and the talik geometry. Heat
544	flux by conduction into the permafrost depends on the heat gradient of the underlying permafrost
545	(Fourier's law). As the vertical temperature slope diminishes with talik maturation, the depth-
546	width ratio of the talik becomes larger creating a deeper talik; thus, much of incoming energy is
547	likely consumed for vertical rather than horizontal expansion. Conversely, during the early stages,
548	thermo-mechanical processes such as wind-driven wave erosion dominates horizontal expansion
549	and elongation of the lake. Consequently, this theory elucidates how talik expansion and
550	concurrent permafrost degradation stabilizes the shape of thermokarst lake to one that is more
551	round rather than elliptical.
552	The semi-ellipsoidal 3D Stefan equation is, to our knowledge, the first geometric model
553	explicitly derived only from the energy conservation equation at the phase boundary. The vector
554	form of the energy conservation equation (Equation 5) in a 3D anisotropic thermal field was
555	integrated at the phase boundary area under the isolated general-shaped lake to quantify the total
556	energy balance. It was shown that the total lake fusion energy or lake expansion rate is
557	equivalent to the weighted phase boundary area. The optimum talik shape function was





558	determined by the variational principle as an extremum of the functional that minimizes the total
559	thawing energy consumption. Thus, the resultant semi-ellipsoid equation (Equation 22) can be
560	considered the 3D Stefan equation because it describes the optimum geometry of phase boundary.
561	The derived semi-ellipsoid function was applied to Peatball Lake, ACP of Alaska, where the
562	talik was extensively surveyed using TEM soundings. The pure geometric fitting exercise met
563	the 27 measured TEM data point well with RMSD of 5.94 m, although the talik orientation
564	disagreed with orientation of Peatball Lake and other surrounding lakes. This may be induced by
565	the irregularity due to the rapid and uneven horizontal lake expansion, or possibly by basin
566	coalescence. Comparing the observed talik thickness to the observed lake bathymetry indicated
567	two distinctive permafrost degradation scenarios: significant subsidence by near-surface ice-rich
568	layer thaw and minor contribution of subsidence due to ice-poor permafrost thaw at depth.
569	Consequently, lake water depth is affected by uneven subsidence of thawing permafrost, the
570	interannual water balance; the spatial lake shape irregularity was determined during earlier stage
571	of development. Therefore, careful consideration is required for the analysis of the relationship
572	between lake bathymetry and talik thickness. Nevertheless, this theoretical technique can be
573	used as guidance to partition various effects such as talik development and thaw subsidence,
574	wind wave erosion, lake ice thickness, surficial geology type, and sediment transport by lake
575	water current.

576 Appendix A: Alternative derivation using isoperimetric inequality

577 Alternative derivation may provide the thermally optimum talik shape minimizing the phase 578 boundary area A with a fixed talik volume V. Equation (14) establishes talik volume and phase 579 boundary area under the thermokarst lake by a general function of the phase boundary φ . The





580 horizontal coordinate system may be transformed by $(u, v) = \left(\frac{x}{\alpha_x}, \frac{y}{\alpha_y}\right)$. Then, the phase

581 boundary can be expressed as a scaled function,

582
$$\hat{\varphi}(u,v) = \varphi(x,y) = \varphi(\alpha_x u, \alpha_y v), \quad (u,v) \in \hat{B}.$$
(A1)

583 According to,

584
$$\begin{cases}
\frac{du}{dx} = \frac{1}{\alpha_x}, \\
\frac{dv}{dy} = \frac{1}{\alpha_y}, \\
\frac{\partial}{\partial u}\hat{\varphi}(u, v) = \frac{\partial}{\partial u}\varphi(\alpha_x u, \alpha_y v) = \alpha_x \varphi_x, \\
\frac{\partial}{\partial v}\hat{\varphi}(u, v) = \frac{\partial}{\partial v}\varphi(\alpha_x u, \alpha_y v) = \alpha_y \varphi_y
\end{cases}$$
(A2)

the talik volume and the phase boundary area can be written as,

586
$$\begin{cases} V[\varphi] = \alpha_x \alpha_y \iint_{\hat{B}} \hat{\varphi} \, du dv \\ A[\varphi] = \alpha_x \alpha_y \iint_{\hat{B}} \sqrt{\hat{\varphi}_u^2 + \hat{\varphi}_v^2 + 1} \, du dv = \alpha_x \alpha_y \int_{\hat{S}} d\hat{S} \end{cases}, \tag{A3}$$

587 where \hat{B} denotes the extent of $\hat{\varphi}(u, v)$ on the uv plane, and \hat{S} is the surface on $z = \hat{\varphi}(u, v)$ as,

588
$$\hat{S} = \{ (u, v, z) \in \mathbb{R}^3 \mid (u, v) \in \hat{B}, \ z = \hat{\varphi}(u, v) \}.$$
(A4)

589 The horizontal scaling transform makes it a symmetric closed surface on z = 0,

590
$$S^* = \left\{ (u, v, z) \in \mathbb{R}^3 \mid (u, v) \in \hat{B}, \ z = \pm \hat{\varphi}(u, v) \right\} .$$
(A5)

591 It is known that volume U enclosed by the ovaloid surface S^* and its surface area satisfy the

isoperimetric inequality for an ovaloid surface, which can be written as,

593
$$\left(\int_{S^*} dS^*\right)^3 \ge 36\pi U^2$$
 (A6)





As the volume and the surface area of the convex closed surface
$$S^*$$
 can be expressed as

595
$$U = 2 \left| \iint_{\hat{B}} \hat{\varphi} \, du dv \right| = \frac{2}{\alpha_x \alpha_y} \left| V[\varphi] \right|, \text{ and}$$
(A7)

596
$$\int_{S^*} dS^* = 2 \int_{\hat{S}} d\hat{S} = \frac{2}{\alpha_x \alpha_y} A[\varphi] \text{, respectively,}$$
(A8)

597 we have,

598
$$\left(\frac{2}{\alpha_x \alpha_y} A[\varphi]\right)^3 \ge 36\pi \left(\frac{2}{\alpha_x \alpha_y} V[\varphi]\right)^2, \text{ or }$$

599
$$A[\varphi] \ge \sqrt[3]{18\pi\alpha_x\alpha_y(V[\varphi])^2} .$$
 (A9)

600 The equality in Equation (A9) holds only if the surface S* is a sphere, which maximizes the

601 volume. Let the radius of this sphere,

602
$$D = \sqrt[3]{\frac{3}{4\pi}V} = \sqrt[3]{\frac{3|A[\varphi]|}{2\pi\alpha_x \alpha_y}}$$
 (A10)

From the symmetricity to the plane z = 0, we can obtain,

604
$$\hat{\varphi}(u,v) = -D\sqrt{1 - \left(\frac{u}{D}\right)^2 - \left(\frac{v}{D}\right)^2}, \quad (u,v) \in \hat{B}.$$
(A11)

Inverse scaling coordinate transformation yields the ellipsoid phase boundary function asfollows:

607
$$\varphi(x,y) = -D \sqrt{1 - \left(\frac{x}{\alpha_x D}\right)^2 - \left(\frac{y}{\alpha_y D}\right)^2}, \quad (x,y) \in B , \qquad (A12)$$





- 608 where D is the depth of the talik at the center. The ellipsoid, the three-dimensional Stefan
- 609 Equation for talik, can be obtained by the isoperimetric inequality as well as the functional

610 analysis.

611 Appendix B: Determination of the coefficients d and λ

- 612 We can determine two coefficients in the ellipsoid (Equation 21) by further application of the
- 613 variational principle. Let

$$D = \frac{2}{|\lambda|}.$$
 (B1)

Also, let the intersect *d* proportional to the vertical radius of the ellipsoid, as follows:

616
$$d = tD \quad (-1 \le t < 1),$$
 (B2)

617 where *t* is a parameter describing the relative elevation of the basin to the original ground surface.

618 Then, Equations (20) and (21) can be rewritten as,

619
$$z = -\varphi = -\sqrt{D^2 - \frac{x^2}{\alpha_x^2} - \frac{y^2}{\alpha_y^2}} + tD , \text{ and}$$
(B3)

620
$$\left(\frac{x}{\alpha_x D}\right)^2 + \left(\frac{y}{\alpha_y D}\right)^2 + \left(\frac{z-tD}{D}\right)^2 = 1, \text{ respectively.}$$
(B4)

621 Now, the phase boundary area and volume can be evaluated as functions of the parameter *t*:

622

$$V[\varphi] = \iint_{B} \varphi \, dx dy = \iint_{B} \left(-\sqrt{D^{2} - \frac{x^{2}}{\alpha_{x}^{2}} - \frac{y^{2}}{\alpha_{y}^{2}}} + tD \right) \, dx dy$$

$$= \pi \alpha_{x} \alpha_{y} \int_{-(1-t)D}^{0} \{D^{2} - (tD - z)^{2}\} dz$$

$$= \frac{\pi}{3} \alpha_{x} \alpha_{y} D^{3} (t^{3} - 3t + 2)$$
(B5)





$$\begin{split} A[\varphi] &= \iint_{B} \sqrt{\alpha_{x}^{2} \varphi_{x}^{2} + \alpha_{y}^{2} \varphi_{y}^{2} + 1} \, dx dy \\ &= \iint_{B} \frac{1}{\sqrt{1 - \left(\frac{x}{\alpha_{x} D}\right)^{2} - \left(\frac{y}{\alpha_{y} D}\right)^{2}}} \, dx dy \\ &= \pi \alpha_{x} \alpha_{y} D^{2} \left\{ (1 - t^{2}) + \int_{1}^{\frac{1}{t}} \left(\frac{1}{z^{2}} - t^{2}\right) dz \right\} \\ &= 2\pi \alpha_{x} \alpha_{y} D^{2} (1 - t) \end{split}$$
(B6)

623

624 Eliminating *D* from these expressions yields,

625
$$A[\varphi]^3 = M \frac{(1-t)^3}{(t^3 - 3t + 2)^2}$$
(B7)

626 where *M* is a positive constant. Therefore, as

627
$$\frac{d}{dt}(A[\varphi]^3) = M \frac{3t}{(1-t)^2(t+2)^3} > 0 \quad (-1 \le t < 1),$$
(B8)

628 the phase boundary area $A[\varphi]$ is the minimum at t = 0. Hence, d = 0 that corresponds to a semi-

629 ellipsoid with depth *D* at the center.

630 Author contribution

- 631 Ohara and Yamatani developed the theory, and all other co-authors, especially Hinkel, Jones,
- 632 Parsekian, and Kanevskiy, offered crucial advice in interpretation. Jones and Parsekian provided
- 633 the field observed data for the case study of Peatball Lake. Jones performed the statistical
- 634 analysis on the oriented lakes based on SAR-satellite remote-sensing data. Ohara prepared the
- 635 manuscript with contributions from all co-authors.

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Parameter	Estimates	Unit	Note
Porosity	0.18		Sandstone >15 m deep; Creighton et al., 2018
Thermal conductivity of permafrost	2.20	W/(m·K)	From porosity and typical thermal properties of ice and mineral in this region
Talik depth, D	88.0	m	Fitted ellipsoid
Talik width (radius), a	514.8	m	Fitted ellipsoid
Aspect ratio, D/a	0.1709		Fitted ellipsoid
Geothermal gradient	0.0250	K/m	Kessler et al., 2012
dT/dz at the talik bottom	-0.0259	K/m	From Mackay model (1962)
Basin average heat flux, qin	0.0689	W/m ²	Computed from Equation (29)

833 Table 1: Computed incoming heat flux with the estimated parameters

834







836

Figure 1: Definitions of variables associating with the overall shape of phase boundary ϕ during warm

838 (Upper left panel) and cold seasons (Lower left panel) and incoming and outgoing heat transfers on

839 $\varphi(x, y)$ (Right panel). Incoming heat (red colored vector) is perpendicular to the phase boundary

840 $\varphi(x, y)$ while that direction (blue colored vector) is modified by the anisotropic heat conduction (green

841 colored vector) in the permafrost.







843

844 Figure 2: Lake bathymetry models for a thermokarst lake and the talik underneath based on the quasi-

steady state. (A) The lake bathymetry is proportional to the talik geometry with uniform ice distribution.

846 (B) However, the lake bathymetry tends to have a flat bottom due to the widespread ice-rich layer near

the surface.







849

850 Figure 3: Map of the study area: Peatball Lake and subregions for lake characterization (red).







852

- Figure 4: The theoretically extrapolated talik thickness map (contour lines) based on 27 TEM soundings
- 854 (dots) in Peatball Lake, ACP of Alaska. The red contour lines and the observation points are consistent.
- The corresponding observed lake bathymetry (adopted from Lenz et al., 2016) is also included in blue
- gradation. The TEM sounding transects start on the lakeshore and end near the center of the lake.







858

859 Figure 5: Cross sectional comparisons of the lakebed and the talik profiles along two TEM transects (b)

through (c) (Lenz et al., 2016) in Peatball Lake. Panel (B) displays the cross plot of the observed talik

and lake depths at all 27 TEM data points.







863

864 Figure 6: Combined hypothetical models of thermokarst lake evolution and diagram of major influencing

865 factors through time. The left column represents summer conditions, the center column represents winter

866 conditions, and the right column indicates the corresponding importance of mechanical vs. thermal

- 867 processes through time as the lake ages (top is younger, bottom is older). Row (A) indicates the early
- 868 processes under bedfast ice conditions before talik initiation. Row (B) shows the onset of vertical thaw
- 869 and subsidence as talik begins to develop. Row (C) shows early, shallow talik growth conditions. Row
- 870 (D) indicates later stage processes on deepened talik due to vertical thaw. Row (E) is the mature stage of
- 871 development when complex bathymetry has set in as a result of sediment transport.







873

874 Figure 7: Computed mean daily potential solar radiation on sloping lakeshore relative to the flat surface

during summer period (June-August) with respect to latitude. I_q is the potential solar radiation on a flat

876 surface, and I'_q is radiation on sloping lakeshore.







879 Figure 8: Two distinctive lake water circulation patterns created by unidirectional wind. Livingstone type

880 circulation and Carson & Hussey type circulation causes opposite flow directions around lake ends. This

also results in difference in sediment and peat deposition patterns.

882







883

884 Figure 9: Comparison of Length to Width ratio versus the percent of a particular region exhibiting a

bedfast lake ice regime for seven study areas in Arctic Alaska. This analysis is based on SAR-satellite

remote-sensing data presented in Engram et al., 2018. Lakes that are more elliptical in shape tend to

887 occur where the majority of the lakes in the area freeze to their bed and thus likely do not have a talik.

888 Lakes that are more circular in shape tend to occur where the majority of lakes in an area do not freeze to

their bed and thus likely have a sub-lake talik.