1 Simulated retreat of Jakobshavn Isbræ during the 21st

century

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13 Abstract

The early 21st century retreat of Jakobshavn Isbræ, into its over-deepened bedrock trough was 14 accompanied by acceleration to unprecedented ice-stream speeds. Such dramatic changes suggested 15 16 the possibility of substantial mass loss over the rest of this century. Here we use a three-dimensional ice-sheet model with parameterizations to represent the effects of ice mélange buttressing, crevasse-17 depth-based calving and submarine melting, to adequately reproduce its recent evolution. We are 18 the first study on Jakobshavn Isbræ that solves for three-dimensional ice flow coupled with 19 20 representations of hydro-fracturing induced calving and mélange buttressing. Additionally, the 21 model can accurately replicate inter-annual variations in grounding line and terminus position, 22 including seasonal fluctuations that emerged after arriving at the over-deepened basin and the disappearance of its floating ice shelf. Our simulated ice viscosity variability due to shear margin 23 evolution is particularly important in reproducing the large observed inter-annual changes in 24 25 terminus velocity. We use this model to project Jakobshavn's evolution over this century forced by

ocean temperatures from 7 Earth System Models and surface runoff derived from RACMO, all
under the IPCC RCP4.5 climate scenario. In our simulations, Jakobshavn's grounding line continues
to retreat ~ 18.5 km by the end of this century leading to a total mass loss of ~ 2068 Gt (5.7 mm sea
level rise equivalent). Despite the relative success of the model in simulating the recent behavior of
the glacier, the model does not simulate winter calving events that have become relatively more
important.

Elevation (km) A) ′elocity (m a⁻¹) 1.5 Jakobshavn Isbrae 0.5 69⁰N -0.5 68⁰N 54°W 52°W 50°W C) Distance (km) Distance (km)

1 Introduction

Figure 1. A) Greenland ice sheet flow speeds from Joughin et al. (2018), with the

Jakobshavn drainage basin outlined by the solid black line and the area shown in panel B by the dashed box. B) Ilulissat Fjord and Disko Bay bathymetry from Jakobsson et al. (2012), with the CTD (Conductivity Temperature Depth) site used for ocean temperature here marked by the red star. C) Example of the mesh used with finest resolution of 500 m with modeled velocities at the beginning of 2004.

33 Jakobshavn Isbræ (Fig. 1) is Greenland's largest and fastest outlet glacier, with transient speeds of up to 17 km a⁻¹ (Joughin et al., 2014). Jakobshavn Isbræ drains ~ 6.5 % of the Greenland Ice sheet 34 (Krabill et al., 2000), and it alone contributed $\sim 1 \text{ mm}$ to global sea-level rise between 2000 and 35 2011 (Howat et al., 2011). Since 1997, measurements indicate that the water entering Ilulissat Fjord 36 37 where Jakobshavn Isbræ terminates, is about 1.1 °C warmer than it was during 1987-1991 (Holland 38 et al., 2008). This rise in water temperature coincided with the onset of dramatic thinning, speedup 39 and retreat of Jakobshavn Isbræ. By 2003 its velocity near the grounding line had reached ~ 12.6 40 km a⁻¹, more than double that of 1992, and the ice shelf in the fjord had disintegrated (Joughin et al., 2004). From 2005 to 2007, as it retreated inland, seasonal fluctuations in velocity 4 km inland 41 42 from the calving front amounted to $\pm 1 \text{ km a}^{-1}$. The winter slowdowns and summer accelerations 43 occurred in tandem with the calving front winter advance and summer retreat. By 2012 the seasonal velocity fluctuations 4 km upstream from the calving front were nearly \pm 8 km a⁻¹ and the grounding 44 line of Jakobshavn Isbræ had reached the bottom of a sub-glacial bedrock trough after years of 45 46 down-slope migration (Joughin et al., 2014).

Before 1997, Jakobshavn had a ~ 15 km long ice shelf in front of its grounding line and experienced submarine melting on its ice-ocean interface (Amundson et al., 2010). After 1998 the terminus became more crevassed, coinciding with acceleration of the glacier, implying that weakened buttressing had triggered its dramatic speed-up. A thinning rate of 230 ± 50 m a⁻¹ between the summers of 1984 and 1985 was deduced from photogrammetric surveys, with 98% contributed by submarine melting (Motyka et al., 2011). The ice shelf thickened during the mid-1990s followed by progressive thinning after 1997 (Motyka et al., 2011). From 1997 to 2008, the average ocean temperature was 1.1°C higher than during the period 1980 – 1991, which raised its thinning rate substantially, affecting the whole ice shelf that eventually collapsed in 2003. Many lines of evidence suggest that warm water was responsible for the submarine melting beneath the ice mélange and ice-shelf, brought by a buoyancy-driven, overturning circulation in Ilulissat fjord (Gladish et al., 2015).

Jakobshavn, in common with most outlet glaciers in Greenland, flows through a narrow, deeply incised bedrock trough at a much faster rate than the ice surrounding it (Joughin et al., 2010). Gravity surveys suggest a deep layer of soft till underlies much of the Jakobshavn trough (Block and Bell, 2011). This soft bed provides almost no resistance to ice flow and basal shear stress maps show that most of the gravitational driving force on the glacier is balanced by lateral drag (Shapero et al., 2016).

65 Basal drag decreased from 1995 to 2006 (Habermann et al., 2013), possibly due to fast thinning that 66 reduced the effective pressure, that is the ice overburden minus water pressure, at the bed. The 67 effective pressure distribution under the glacier is important to basal drag and approaches zero at the grounding line as the ice begins to float. Several sliding parameterizations (also termed sliding 68 69 relations or sliding laws) have been used in the literature that assume basal drag depends on sliding 70 speed (so-called Weertman sliding (Weertman, 1957)), or on effective pressure (Schoof, 2010; 71 Gagliardini et al., 2014). Tsai et al. (2015) introduced a combined Weertman and Coulomb sliding 72 law based on effective pressures with a boundary layer at the grounding line; this has a higher scaling 73 of ice flux with grounding-line thickness compared with the Weertman. However, in the Jakobshavn 74 case, both Weertman and Coulomb sliding produce very similar fluxes because the basal shear 75 stresses along the main trough are typically only 2% of the driving force (Shapero et al., 2016).

76 Simulations using a flow-band model with a crevasse-depth-based calving parameterization (Vieli 77 et al., 2011) demonstrated that loss of buttressing from the weakening mélange or enhanced 78 submarine melting could have triggered the dramatic changes seen in Jakobshavn Isbræ at the end 79 of the 20th century. Later work (Muresan et al., 2016), using a simple calving model with 80 dependence on the strain field at the terminus was able to reproduce the inter-annual retreat of 81 Jakobshavn Isbræ until 2009, when the terminus arrived at the beginning of the reverse sloping bed. 82 But retreat after 2010 was not captured by their model, and neither were the seasonal fluctuations 83 in terminus position. Bondzio et al. (2018) applied a similar calving model that removes any ice 84 where tensile stress exceeds a threshold, as simulated with a SSA (Shallow Shelf Approximation) 85 model, regardless of ice thickness. To represent seasonal fluctuation of front position, their stress 86 threshold is a stepwise constant function in time with low values in summer. After calibration, their 87 model can closely reproduce the observed behavior from 1985 to 2018 when forced only with ocean 88 temperatures.

89 In this paper we use a three-dimensional ice-flow model with a treatment of calving that successfully 90 tracks the seasonal terminus position and its retreat into the over-deepened basin. We use historic 91 observations of ocean temperature as forcing and ice shelf melting rate to scale submarine melting 92 rates for our model and thence make future projections. Our aim is to track the evolution of 93 Jakobshavn Isbræ through the 21st century under a specific climate forcing scenario. In Section 2 we describe the approach and calibration of our model, Section 3 shows the simulations for the 94 95 period to 2100 under the IPCC RCP4.5 scenario (Moss et al., 2010), Section 4 is a discussion of our 96 results with reference to other studies and suggestions for improvements, and we conclude in 97 Section 5.

98 **2 Methods and data**

99 2.1 Ice sheet model

100 We model Jakobshavn Isbræ using the BISICLES ice sheet dynamics model that is based on the 101 vertically integrated stress balance formulation of Schoof and Hindmarsh (2010), which treats 102 longitudinal and lateral stresses as depth-independent, but allows for vertical shear in the nonlinear 103 rheology (Cornford et al., 2013). BISICLES is particularly useful for Jakobshavn Isbræ as it uses 104 block-structured finite volume discretization with adaptive mesh refinement (Cornford et al., 2013) 105 allowing for high resolution modeling of critical sections of the glacier. Jakobshavn Isbræ is fed by $a \sim 400$ km long and extensive drainage basin (Fig. 1), but the fast flow area is only around 10 km 106 107 in width. Our highest mesh resolution of 500 m is used to cover the whole fast-flow-area including the shear margin (Fig. 1c), while the rest of the glacier is modeled at 1000 m resolution. 108

109 We assume the floating part of Jakobshavn Isbræ to be in hydrostatic equilibrium, thus the upper110 surface elevation s is

111
$$s = \max\left[h + b, \left(1 - \frac{\rho_i}{\rho_w}\right)h\right], (1)$$

112 where ρ_i and ρ_w are the densities of ice (917 kg m⁻¹) and ocean water (1027 kg m⁻¹), *h* is ice 113 thickness and *b* is bedrock elevation relative to sea level. The ice thickness evolves in time as

114
$$\frac{\partial h}{\partial t} + \nabla \cdot [\boldsymbol{u}h] = M_s - M_b, \quad (2)$$

where M_{s} , M_{b} are surface mass balance (SMB) and submarine melt rate respectively and u is the depth-independent horizontal velocity. No basal melting over the grounded area is allowed. The velocity u satisfies an approximate stress balance equation (Schoof and Hindmarsh, 2010)

118
$$\nabla \cdot \left[\phi h \bar{\mu} (2\dot{\boldsymbol{\epsilon}} + 2 \operatorname{tr}(\dot{\boldsymbol{\epsilon}})\mathbf{I})\right] - \boldsymbol{\tau}^{b} = \rho_{i} g h \nabla s, \quad (3)$$

119 where I is the identity tensor, s is the ice surface elevation, g is the acceleration due to gravity, $\dot{\epsilon}$ is 120 the horizontal strain-rate tensor defined by

121
$$\dot{\boldsymbol{\epsilon}} = \frac{1}{2} [\nabla \boldsymbol{u} + (\nabla \boldsymbol{u})^{\mathrm{T}}], (4)$$

122 and τ^{b} is the basal shear stress. The vertically integrated effective viscosity $h\bar{\mu}$ is given by

123
$$h\bar{\mu}(x,y) = \int_{s-h}^{s} \mu(x,y,z) dz$$
, (5)

where the vertically varying effective viscosity μ includes a contribution from vertical shear and satisfies

126
$$2\mu A(T)(4\mu^2\dot{\epsilon}^2 + |\rho_i g(s-z)\nabla s|^2)^{(n-1)/2} = 1,$$
 (6)

127 where *n* is the flow rate exponent, set to 3 in the current study, and A(T) is the rate factor, dependent 128 on the ice temperature *T* through an Arrhenius law (Cuffey and Paterson, 2010). ϕ is a stiffening 129 factor estimated by solving an inverse problem (Cornford et al., 2015) using measured surface 130 velocities.

131 We use a viscous Weertman sliding relation to define the basal friction:

132
$$\boldsymbol{\tau}^{b} = \begin{cases} -C |\boldsymbol{u}|^{m-1} \boldsymbol{u} & \text{if} \frac{\rho_{i}}{\rho_{w}} h > -b \\ 0 & \text{otherwise} \end{cases}, (7)$$

and here we assume a linear relation taking m=1. The basal traction coefficient C(x, y) is estimated simultaneously with the stiffening factor ϕ by solving the inverse problem (Cornford et al., 2015). *C* and ϕ are adjusted iteratively to reduce the misfit with a set of 2010 surface velocity observations (Joughin et al. 2010). We hold the fields *C* and ϕ constant over time throughout our simulations,

- 137 although they must actually change as the glacier retreats. We also do not thermomechanically
- 138 couple the model, but use a constant ice temperature of -10° C.
- 139 Reflection boundary conditions were applied at the edge of the domain:

140
$$\boldsymbol{u} \cdot \boldsymbol{n} = 0$$
, $\boldsymbol{t} \cdot \nabla \boldsymbol{u} \cdot \boldsymbol{n} = 0$, $\nabla h \cdot \boldsymbol{n} = 0$, (8)

- 141 where n is normal to a boundary and t is parallel to it. Normal stress across the calving front is equal
- 142 to the hydrostatic water pressure there:

143
$$\boldsymbol{n} \cdot \left[\phi h \bar{\mu} (2\dot{\boldsymbol{\epsilon}} + 2 \operatorname{tr}(\dot{\boldsymbol{\epsilon}}) \mathbf{I})\right] - \boldsymbol{\tau}^{b} = \frac{1}{2} \rho_{i} g \left(1 - \frac{\rho_{i}}{\rho_{w}}\right) h^{2} \boldsymbol{n}.$$
(9)

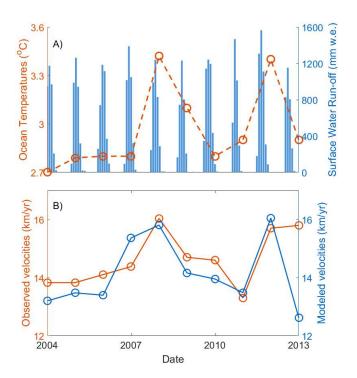




Figure 2. A) Time series of observed ~300 m deep ocean temperature (red) from near the mouth of Ilulissat fjord (See Fig. 1 for location). Blue bars are simulated monthly surface water run-off from the MAR regional surface mass and energy balance model (Alexander et al. 2016). B) Measured ice front annual mean ice flow speeds (red) from Joughin et al. (2010), compared with our modeled speeds (blue).

150 **2.2 Forcing**

Local ocean circulation in Ilulissat fjord driven by buoyancy plume brings deep water from outside 151 152 to the grounding line of Jakobshavn, and renews the fjord waters within 90 days in summer (Gladish 153 et al., 2015). Generally, Jakobshavn's fjord is ~ 800 m deep but with a sill of only ~ 200 m depth at 154 its entrance. The deepest water outside the sill can flow over the sill and reach the grounding line of Jakobshavn (Gladish et al., 2015). We use 300 m depth ocean temperatures collected from a CTD 155 site close to the mouth of Ilulissat fjord (Fig. 1) as an approximation of ocean temperatures near the 156 glacier grounding line (Gladish et al. 2015). A positive correlation (r=0.74, p<0.05) exists between 157 158 deep ocean temperatures and flow speed near the terminus of Jakobshavn Isbrae (Fig. 2) from 2004 onwards. There is no significant correlation prior to 2004, the ice shelf period. As a working 159 hypothesis we assume that the correlation since 2004 reflects the effects of the sea ice and iceberg 160 161 mélange in the fjord on the flow speed near the terminus: a warmer ocean reduces mélange and sea ice thickness and therefore buttressing. There appears to be no lag between the glacier acceleration 162 163 and change in deep ocean temperature, suggesting mélange response times are faster than 1 year. When the ice shelf was present lags in the system were likely longer, accounting for the lack of 164 165 correlation between ocean temperatures and glacier flow speed prior to 2004. It is also possible that 166 ocean temperatures reflect changes in surface runoff and basal lubrication for sliding, but we 167 consider that the runoff more strongly affects calving mechanisms as discussed later. We therefore 168 modify the driving force (Eq. 3) on the grid cells next to the calving front by multiplying by a factor 169 α that is linearly related to ocean temperature (T) as a means of representing the buttressing effects 170 of the ice mélange in the fjord.

171
$$\nabla \cdot \left[\phi h \bar{\mu} (2\dot{\boldsymbol{\epsilon}} + 2 \operatorname{tr}(\dot{\boldsymbol{\epsilon}}) \mathbf{I})\right] + \boldsymbol{\tau}^{b} = \boldsymbol{\alpha} \cdot \rho_{i} g h \nabla s, \quad (10)$$

172 $\alpha = \alpha_1 + \alpha_2 \cdot T, (11)$

173 The coefficients α_1 and α_2 are tunable with limits based on observations as discussed later in Section 174 2.4. This approach is similar to Nick et al. (2013), which also alters the stress balance at calving 175 front. Our buttressing parameterization gives a longitudinal resistance that is 18% of the driving 176 force at calving front (Eq. 10), for the instance of 2004.

We use a crevasse based calving parameterization (Benn et al., 2007; Nick et al., 2013) that calves ice where the crevasse penetration depth (D_s) is greater than upper surface elevation. D_s is defined as

180
$$D_s = \frac{s}{g \cdot \rho_i} + \frac{\rho_w}{\rho_i} \cdot \mathbf{R} \cdot \boldsymbol{\beta}, \ (12)$$

181 where S is the magnitude of extensional stress, R is surface water run-off, and β is a tuning scalar.

182 We estimate runoff from the 25 km resolution regional climate model, MAR, (Alexander et al. 2016),

driven by the ERA-Interim reanalysis (Dee et al., 2011).

184 We characterize submarine melting as a linear function of ocean forcing

185
$$M_{b} = \gamma T_{f,}$$
 (13)

where T_f is the far field ocean forcing temperature, taken in Disko Bay (CTD in Fig. 1), relative to pressure melting temperature under the ice shelf. Thus *T* and T_f are related simply by ice depth and salinity. We derive γ (Section 2.3) from the 1985 observed submarine melt rate of 1 ± 0.2 m day⁻¹ beneath the ice shelf of Jakobshavn Isbræ, when Disko Bay ocean temperatures were 4.2°C warmer than the pressure melting point at the bottom of the floating ice shelf (Motyka et al. 2011). We test the sensitivity of the modeled glacier to uncertainty in submarine melt rate in section 2.4.

193 RACMO model (Van Angelen et al., 2013) driven by the RCP4.5 scenario (Moss et al. 2010). The

¹⁹² We force Jakobshavn Isbræ in the 21st century using SMB and run-off from the 11 km resolution

194 run-off values are averaged over the nine grid points nearest to the terminus of Jakobshavn (69.1°N, 50.0°W). In general we use RACMO products to drive the model, however they only span the period 195 196 of 2006-2099. For the period 2004-2014, SMB and surface water run-off forcing come from MAR 197 model outputs. We use the common overlap period (2006-2014) to correct the bias between two 198 models outputs. The RACMO simulation was forced by the HadGEM2-ES Earth system model 199 (Collins et al., 2011), as this climate model was found to be the most realistic for present-day 200 simulations of the Greenland ice sheet (Van Angelen et al., 2013). Ocean forcing in Equations (10) 201 and (13) should relate to temperatures off the continental shelf close to the fjord mouth. Cowton et 202 al. (2018) achieved success in simulating the terminus position and yearly variability of 10 glaciers 203 along the east coast of Greenland using mean 200-400 m depth temperatures from reanalysis data. 204 For consistency with the RACMO results, we use deep ocean temperatures at ~ 300 m depth from 205 the $0.83^{\circ}\times1^{\circ}$ resolution HadGEM2-ES driven by the RCP 4.5 climate scenario from 2005 to 2100 206 at the 3 closest grids point to Disko Bay. We also compare this with results from 7 other climate 207 model simulations of RCP4.5: HadGEM2-ES (Collin et al., 2011), BNU-ESM (Ji et al., 2014), 208 MIROC-ESM (Watanabe et al., 2011), IPSL-CM5A-LR (Dufresne et al., 2013), CSIRO-Mk3L-1-2 209 (Gordon et al., 2002), NorESM1-M (Bentsen et al., 2012) and MPI-ESM-LR (Giorgetta et al., 2013).

210 **2.3 Initialization Procedure**

As we are interested in high resolution simulations and validating our model parameterizations with observations over the last decade, we take care to initialize the model as accurately as possible. Detailed bedrock topography and ice thickness data in the year 2009 comes from Gogineni et al. (2012); we chose the product because it has 500 m resolution and so matches the highest resolution of our mesh. Jakobsson et al. (2012) provides ocean bathymetry data (Fig. 1). In 2004 the floating ice shelf disintegrated, making it a convenient starting point for simulations since we might expect the system to respond differently to forcing when there was a floating ice shelf compared with the situation of ocean forcing along a near-vertical ice cliff. This is consistent with the observed good correlation between ocean temperature and flow speed after 2004 but not before. The aim of this initialization is to provide a state rather similar to 2004, that is barely retreating on inter-annual scales (Joughin et al., 2010) and small changes of annual mean velocity in the following 3 years. Therefore

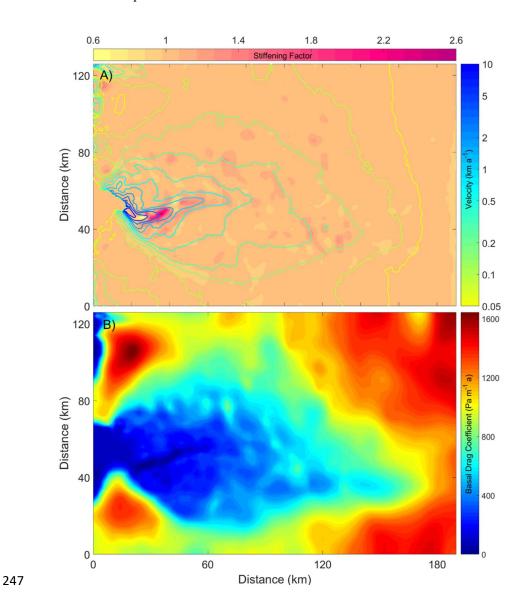
We solved the inverse problem for basal conditions (Eq. 7) and stiffening factor using 2010
 velocities (Joughin et al., 2010) and 2009 geometry (Gogineni et al., 2012), following Cornford
 et al. (2015). Our friction coefficient and stiffening factor fields are shown in Fig. 3. Fig. S1
 shows the discrepancy between observed velocity field (Joughin et al., 2010) and the velocity
 derived from the inversion.

228 2) Starting from the inversion of step 1, we let the model glacier evolve freely without calving 229 and with zero SMB and with sub-shelf melting (γ =0.0238) forced by repeating the observed 230 2004 ocean temperature for 11 years until its surface elevation profile reached a state shown in 231 Fig. S2.

232 3) We carried out several 10-year simulations each with different β values. These simulations were forced by repeatedly applying the 2004 seasonal climate forcing so that the glacier 233 234 approaches a steady state. From these, we selected the β that provided a calving front position 235 closest to that observed in 2004. The best β here is 0.034, and this is our best guess for the 2004 236 state. The annual minimum extent of Jakobshavn retreats ~ 2 km from 2004 to 2005 following the loss of ice shelf butressing, but then stabilizes until 2007 (Joughin et al. 2010). Annual 237 maximum extents are stable over the 2004-2007 period. Front velocity increase slowly from 238 2004-2007 (~5.9% a⁻¹ Joughin et al. 2010), and the model simulated velocities increase by 239

about 3% a⁻¹. This period of relative stability also makes 2004 a good time from which to start
transient simulations.

Basal friction coefficient values downstream of the 2010 grounding line were set equal to that in the nearest 2010 grounded location. This was necessary because steps 2 and 3 involved grounding line advance beyond the region for which basal friction coefficients had been inferred. The geometry after this spin up procedure, and the friction coefficient and stiffening factor distribution from the inversion in step 1 were used as the initial condition for model calibration.



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Figure 3. (A) Stiffening factor Φ (Eq. 3) and (B) basal traction coefficient *C* (Eq. 7) over the computational domain from solving the inverse problem. Contour lines in panel A show the modeled velocity (logarithmic scale).

251 2.4 Model calibration

252 The parameters in the model, α , β and γ representing mélange buttressing, crevasse depth sensitivity to surface runoff, and shelf melt sensitivity to ocean temperatures need to be estimated. The 253 254 measured relationship between ocean temperatures and sub-shelf melt rate (Motyka et al., 2011) 255 gives the value of γ to be 0.238. We manually tune parameters in equations (11) and (12): α over 256 the range 0.7–1.2 for α_1 and 0.09-0.12 for α_2 ; and β (0.04 - 0.075) to best reproduce Jakobshavn Isbræ's calving front position and surface velocity evolution for the 10 year period 2004-2013. 257 Reproducing the total retreat distance and the temporary stable state after 2012 were secondary 258 259 desirable features to match. The best set of parameters are $\alpha_l = 0.82$, $\alpha_2 = 0.111$, $\beta = 0.0638$. Since these 260 values come from a manual search we do not claim them to be the best in all parameter space. We 261 assess model sensitivity to the parameter values next.

We explore the glacier's sensitivity to two types of boundary perturbations. They are ice mélange 262 263 buttressing effect (defined by α) and submarine melting (defined by γ). We scaled submarine melt rates by multiplying it by values from 0.8-1.2, based on the range of the observation uncertainty in 264 265 melt of ~ 20% (Motyka et al. 2011). Also we varied α by multiplying by factors from 0.91 to 1.25 to represent different buttressing strengths (Eq. 10). These multiplication factors were varied 266 systematically with typical intervals of 0.1 and 0.03 respectively for the γ and α factors. We 267 268 calculated the following relative mismatches defined as (model-observations)/observations for each simulation (Fig. 4): 269

270

1. Total calving front retreat from 2004-2013 measured by the difference between 2004 and

- 271 2013's annual maximum extent.
- 272 2. Annual mean front velocities
- 273 3. Vector sum of 1) and 2)
- 274 We used β (Eq. 12) from our optimal set of parameters. Our optimal value for α is such that a
- 275 20% rise of its value does not affect modeled retreat when β and γ are kept to be their optimal
- 276 values (Fig. 4 A).

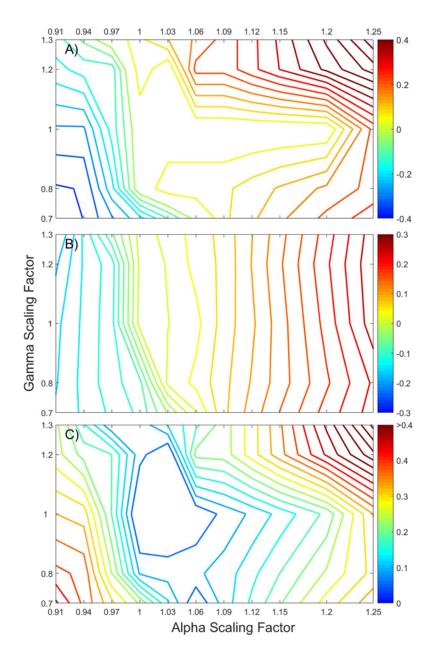


Figure 4. Relative mismatches defined as (model-observed)/observed for A) total calving front retreat, B) average of annual mean front velocity during 2004-2013, C) the vector sum of mismatches in panels A and B, $\sqrt{(A^2 + B^2)}$ in our 2-D parameter space. X- and y-axis are multipliers of α and γ .

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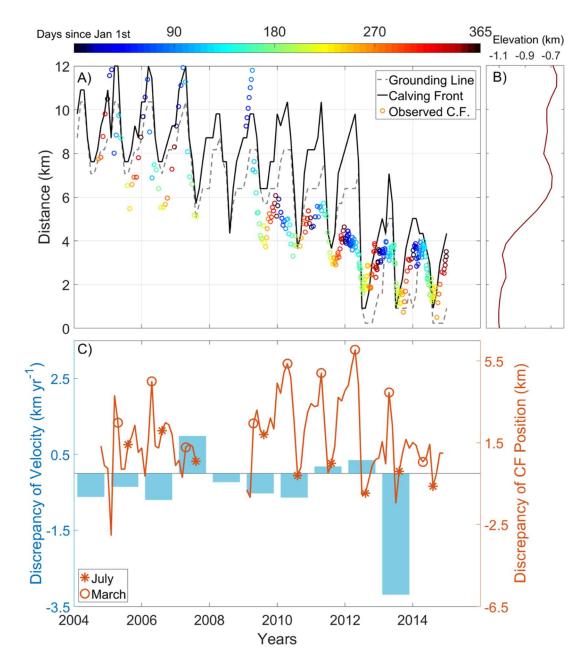




Figure 5. (A) Modeled retreat of the calving front (black solid line), grounding line (gray dashed line), and observed calving front positions (color-coded circles and scale bar) from Joughin et al. (2014). (B) Bedrock elevations. (C) Residuals (modeled minus observed) of annual mean front velocity (blue bars, left axis) and of calving front position (red lines, right axis) with typical timings of annual maximum (March) and minimum (July) extent marked. The modeled front velocities and calving positions explain about 49% and 76% of the variance in corresponding observations.

290 The two biggest mismatches occur with the 2007 and especially 2013 velocities (Fig. 5). 2013 has

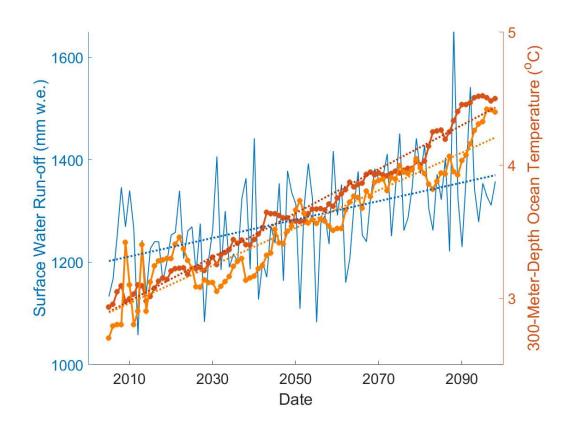
the lowest simulated surface water run-off (Fig. 2) of all the years since 2004. The Benn calving

292 model we use is sensitive to runoff, with reduced run-off leading to lower crevasse-penetrationdepth and reduced terminus fracturing thus increasing its buttressing force. Furthermore 2013 had 293 294 relatively cool ocean temperatures which were lower than the average of 2004-2013. The cool ocean 295 temperatures also increased buttressing, leading to low simulated annual mean velocities. 296 Jakobshavn Isbræ did not in fact slow down very much in 2013 because there were calving events 297 (Cassotto et al. 2015) that are unrepresented in our model. The relevant mechanisms are discussed 298 later. In 2007 high run-off caused more simulated calving and retreat than in reality. These retreat phases reduced the buttressing and lateral drag due to shear-margin-weakening, all of which lead to 299 300 excessive speed-up near the terminus.

301 Modeled calving front retreat is \sim 7 km in total from 2004-2014 (Fig. 5), which is consistent with observations (Joughin et al. 2014). In 2009 a dramatic retreat brought the grounding line to the 302 bottom of the bedrock slope, and since then it has gradually retreated with smaller seasonal 303 304 fluctuations. The run-off forcing we applied triggered major retreats in the summers of 2007 and 305 2012, due to large summer peak run-off (Fig. 2), demonstrating the sensitivity of our calving 306 parameterization to run-off forcing. Modeled timings of maximum extent and minimum extent each 307 year are in good agreement with observations, also demonstrating that summer, in particular, May 308 to July, run-off determines much of the behavior of Jakobshavn Isbræ.

The modeled range of seasonal fluctuation in front position is ~ 5 km, which is similar to observations in the period before 2008. From January 2009 to December 2011, there was an abrupt decrease in seasonal front fluctuation, with many winter calving events occurring, in contrast with previous years (Cassotto et al. 2015). These winter calving events may explain the small observed seasonal fluctuations because they limit the winter advance. Our model is unable to stimulate these winter calving events because there is no winter run-off, and as extension stresses are never enough to cause winter calving, calving is then zero. The largest discrepancy of front position occurs during
these winter calving periods (Fig. 5). Observations also showed that from 2013 to 2017, Jakobshavn
Isbræ barely retreated (Joughin et al. 2010). The decline of run-off (Fig. 2) in 2014 suggests the
reason. But since no RACMO run-off simulations are yet available for 2015 and later, our
parameterizations cannot be tested against this lack of retreat.

320 3 Future evolution



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Figure 6. Climate forcing for future projection under the RCP4.5 scenario taken as 300 m depth ocean temperatures from HadGEM2-ES (orange) compared with the ensemble mean (red) of 7 Earth System Models (HadGEM2-ES, BNU-ESM, MIROC-ESM, IPSL-CM5A-LR, CSIRO-Mk3L-1-2, NorESM1-M and MPI-ESM-LR), (right axis), with their linear trends. Annual maximum monthly surface water run-off near Jakobshavn Isbrae's terminus from RACMO (forced by outputs from HadGEM2-ES) is shown in blue.

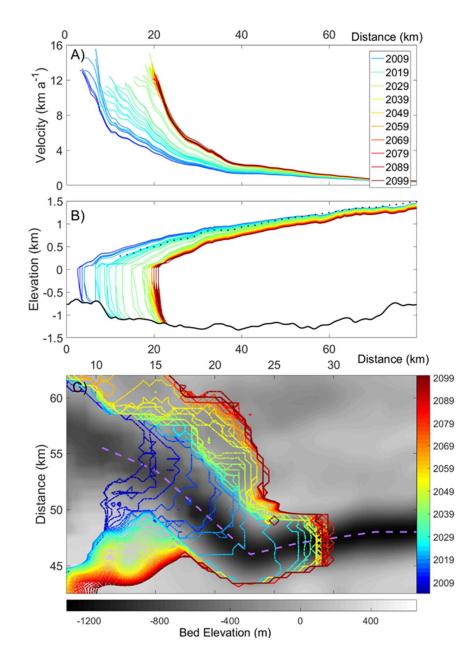




Figure 7. Modeled profiles of (A) January velocity and (B) January surface elevation along the center-flow-line (purple dash line in panel C) of Jakobshavn Isbræ from 2004 to 2099 for the RCP4.5 scenario. Bedrock elevation is shown in black. Black dotted line is the surface elevation profile extracted from radar data measured around 2010 (Gogineni et al., 2012). Profiles are shown at intervals of 1 years. Profiles are color-coded in the legend and range from blue to green and red. (C) Modeled July front positions (color bar) over its bedrock (grayscale bar) at intervals of 2 years.

336 Under the RCP4.5 scenario (Fig. 6) surface runoff slowly rises over the 21st century, with RACMO

simulating slightly greater runoff during the second half than for the first 50 years. Runoff increases

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by 14% over the century. Ocean temperature at 300 m depth in the grid cell closest to Jacobshavn increases by 52%, and, as may be expected, has less variability than runoff.

340 Under this forcing, Jakobshavn Isbræ continues its retreat (Fig. 7) for 18 years after 2013, producing 341 a total grounding line retreat of \sim 18 km upstream. As calving produces a steepening surface profile, 342 terminus velocities increase, to reach a 21st century peak of ~19 km a⁻¹ in 2031 summer. Eventually 343 the front height (relative to sea level) becomes larger than the crevasse penetration depth in the 344 calving parameterization. This leads to a stable period with little inter-annual retreat and which lasts 345 until the end of this century. During this period, nearly all of the seasonal retreats are offset by the following winter re-advances. Mass transport continually flattens and thins the ice geometry, leading 346 347 to reduced flow speeds that eventually become half those of 2031, the 21st century peak.

The surprisingly high run-off anomaly in 2088 (Fig. 6) does not affect the stable state indicating run-off fluctuation alone cannot break this retreat pattern immediately. Once the inter-annual retreats cease in 2031, the dynamic thinning rate is greatly reduced because calving front height stops increasing.

352	Table 1 Estimates of	f glacier mass loss an	d grounding line retreat	from different sources.

Source	Climate	Mass loss	Mass loss by 2100	Grounding line	Grounding line
	scenario	2004-2013 (10	(Gt)	retreat 2004-2013	retreat by 2100
		years) (Gt)		(km)	(km)
This paper	RCP4.5	234	2068 (2044-2723)	7.0	18.5 (17.5-23.0)
Muresan et al. (2016)		220			
Nick et al. (2013)	A1B		1870 - 2281		14.0 - 26.0
Observations		$225\!\pm\!15$		7.0	

Table 1 shows estimates of glacier mass loss and retreat. Under RCP4.5, total cumulative mass change of Jakobshavn Isbræ is 2068 Gt by 2100, using best set of α , β and γ with ocean temperature inputs from ensemble mean of 7 ESMs (Fig. 6). To estimate an upper bound for mass loss over this 356 century, we scale the α parameter by 1.2 giving 2680 Gt for the same forcing (Fig. 8a). Using the 357 HadGEM2-ES forcing, which is the same model used to force RACMO with α and γ set to their best estimates (Fig. 4) gives 2000 Gt. We suggest that this may be the lower reasonable bound of 358 mass loss since the HadGEM-ES ocean temperatures rise notably slower than the ensemble mean 359 360 (Fig. 6). Note that all 3 simulations of front position (Fig 7C, Fig. 8) show a relatively stable position around 18 km upstream from its 2013 location. Examination of the change in velocities during the 361 362 simulation (Fig. 9) suggests that the explanation for this stability is strong flow convergence near the future glacier front that largely offsets dynamic thinning. Notice that the South side of the fast-363 flow-area in 20th century was quite close to ice-free land, while in later half of this century 364 convergent flow in the South is fed by a substantial area of ice stream. 365

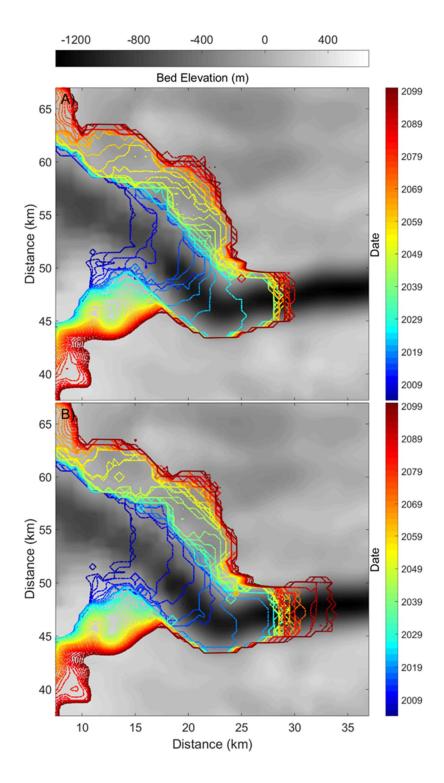
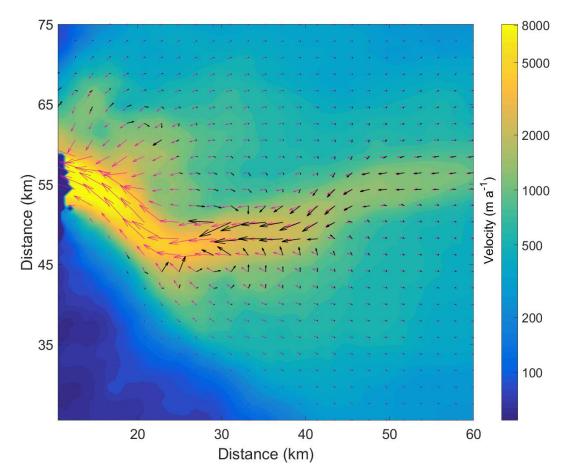


Figure 8. Upper and lower estimates of July front positions within this century with colors
 indicating the date (color bar) for A) lower bound with scalings of (1,0.8) and the HadGEM-ES
 forcing B) upper bound of mass loss projection with (α, γ) parameter scalings of (1.2,1), and the
 7-model ensemble climate forcing.



371

Figure 9. Simulated velocity vectors in 2004 (pink vectors) with their magnitudes (right color bar) and velocity difference between 2004 and 2099 (2099's minus 2004's, black vectors), for clarity vector lengths are clipped at 5 km a⁻¹.

375	Exploring the (α , γ) scaling parameter space we notice that values of (1.0, 0.8) produce a mass loss
376	over this century of 2021 Gt with the HadGEM-ES ocean forcing, almost the same value as for the
377	best set of parameters. This implies that less submarine melting (determined by γ) leads to larger ice
378	loss by dynamic processes. The reason is that lesser submarine melt allows a larger ice thickness at
379	the grounding line with stronger dynamic thinning in advancing season. Notice in our stress balance
380	equation (Eq. 3), thickness contributes to driving force term, thus ice flux across the grounding line
381	is highly nonlinear in ice thickness. This highly nonlinear relationship is also shown in our
382	sensitivity tests (Fig. 4). Over the mismatch field measured by front velocity (Fig. 4, Panel B), the
383	velocity is partly dominated by low values of γ scaling around the scaling line for $\alpha = 1.06$, while α

is almost the only control on velocity over the region where scaled $\alpha < 1.09$. Within our sample space, the non-linear and non-monotonic relationship between submarine melting and retreats is clear (Fig. 4, Panel A). Around the point of scalings ($\alpha = 1.12$, $\gamma = 1.0$), total retreat will increase no matter if γ is decreasing or increasing within the scaling range $0.8 < \gamma < 1.2$. The area where scaled $\alpha > 1.0$ in sample space is the very likely future condition for Jakobshavn Isbræ because increasing terminal ice cliff height caused by retreating into deep water will act as an amplifier to frontal driving force.

4 Discussion

4.1 Parameterization of Buttressing effect

The sudden 1.1°C rise in temperature of water entering Ilulissat fjord in 1997 (Holland et al., 2008) initiated rapid melting and disintegration of the ice shelf in 2003. This disintegration coincided with a near doubling of ice velocities. Modeling (Vieli et al., 2011) suggested that this was due to the reduction in buttressing from the ice-mélange. We can realistically reproduce the velocity variation of Jakobshavn Isbræ on seasonal and inter-annual scales using our parameterization of the buttressing effect from the ice mélange in the fjord.

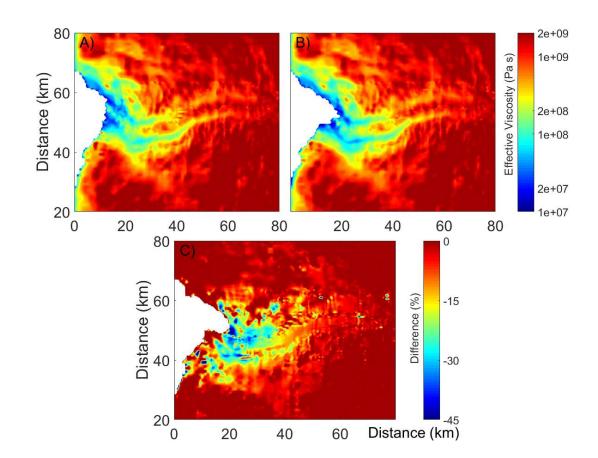
Gladish et al. (2015) analyzed glacial flow speeds from 1998 to 2014, finding no correlation with Ilulissat fjord temperatures. This is because at the beginning of 2004, Jakobshavn's evolution entered a new phase with the disintegration of the ice shelf. We find good correlations between Disko Bay temperatures and ice velocities from 2004 to 2014. The improvement in correlation with temperatures may be explained by a faster response between the grounded glacier and the fjord water temperatures after loss of the floating ice shelf.

404 Buttressing would affect the calving process by altering the longitudinal resistive stress in the glacier.

Temperatures in Ilulissat Fjord will be warmer during the 21st century under essentially all climate scenarios, even those with modest emissions, due to the thermal inertia of the oceans. Thus a new floating ice shelf is unlikely to form. Prior to 2004, there were large changes in Jakobshavn: loss of ~15 km long ice shelf and the sudden rise in fjord temperatures in 1998. There are fewer mechanisms to effect such dramatic changes in the future now that almost the entirety of the glacier is grounded. We therefore propose that our representation of the mélange buttressing mechanism, tuned for 2004-2013, is likely to maintain its validity during the 21st century.

412 **4.2 Horizontal shearing and viscosity**

413 Van Der Veen et al. (2011) estimated a maximum horizontal shear stress of ~800 kPa across the 414 shear margin of Jakobshavn Isbræ where the horizontal velocity shear reaches the peak, while the 415 bed stress is only 10-40 kPa in fast flowing regions (Shapero et al., 2016). Given that the width of 416 the Jakobshavn Isbræ fast flow region is typically under 5 km and its thickness is typically between 417 1-2 km, these numbers indicate that the shear margins provide at least an order of magnitude greater 418 total resistance than the bed. Thus, the shear margin, rather than the bed of Jakobshavn Isbræ provides most of the resistance balancing the driving force. The main trunk of Jakobshavn Isbræ 419 420 exhibits considerable seasonal velocity changes, while the slow moving ice outside the shear margin 421 has little or no seasonal cycle. This flow structure implies speed gradients perpendicular to the flow 422 direction with large seasonal variation. These velocity shears would in turn generate large seasonal 423 variations in effective ice viscosity (Eq. 6). This mechanism is due to the non-linear rheology of the 424 ice in the fast flow region: increases in the speed of fast flowing ice cause increases in horizontal 425 shear stress across the margins, reduced viscosity, and further increased horizontal velocity shear, 426 allowing further increase to speeds in the fast flow region. Observations show that, as the terminus 427 retreated into deeper water, seasonal fluctuations in terminus velocity increased (Joughin et al. 2008). By 2012, the summer time peak terminus velocity was ~ 17 km a⁻¹, more than twice the wintertime
minimum velocity (Joughin et al. 2014). This amplified seasonal velocity cycle was likely enhanced
by the shear-margin weakening mechanism.



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432 Figure 10. Modeled annual mean of vertically averaged effective viscosity $\Phi\mu$ (Eq. 5) in 2004 433 (A) and 2013 (B) and the percentage decreases from 2004 to 2013 (C).

Our modeled shear margin weakening on decadal scales is consistent with other estimates from a thermomechanical ice flow model of Jakobshavn Isbræ forced by calving front positions (Bondzio et al., 2017). Their modeled viscosity drops between 2003 to 2015 reach ~ 40% which is close to our maximum viscosity decrease of ~ 45% between 2004 to 2013 (Fig. 10). The extreme calving season we simulated in summer 2012 was accompanied by ~ 12 km a⁻¹ variations in speed at the calving front, which were facilitated by the accompanying shear margin-induced ice viscosity 440 reductions of 60% at the time of maximum terminus advance. Simpler models of Jakobshavn Isbræ, 441 using a flowband model (Nick et al., 2013) or simple calving parameterizations with no seasonal 442 cycle (Muresan et al., 2016) cannot produce these seasonal variations in shearing. However, our 443 model accommodates both the seasonal forcing from calving and the three-dimensional seasonal 444 velocity shear impacts on effective viscosity. Without this physical process, speedups during intense 445 calving events would be under-estimated, and this would lead to under-estimated mass 446 transportation during the retreat. Bondzio et al. (2017) used a thermomechanical ice flow model to 447 evolve the ice viscosity, which depends on a damage parameter that softens the ice in the shear 448 margins. But their damage parameter also stays constant in time. Thus both the models of Bondzio 449 et al., (2017) and ours only consider the contribution from strain rate weakening in time to evolving 450 viscosity. Thermodynamics could play some role in changing viscosity, presumably if the ice temperatures increased over time, but our temperatures are fixed at -10°C. 451

452 Several processes absent from our model could affect ice viscosity. Crevasses saturated by surface 453 melt water within the shear margins of Jakobshavn are visible on satellite images (Lampkin et al., 454 2013). This melt water can transfer heat throughout the ice column through discharge within 455 crevasses and moulins thus softening the ice (Phillips et al., 2010). Incorporating a continuum 456 damage model in BISICLES would further exaggerate the shear margin weakening as it raises the 457 non-linear dependence of strain rates on stress fields (Sun et al., 2017).

458 **4.3 Comparison with previous estimates**

The cumulative mass change of Jakobshavn Isbræ estimated from airborne and satellite laser altimetry for 1997–2014 was tabulated Muresan et al. (2016). The mass loss over the 10-year period 2004-2013 modeled by Muresan et al. (2016) is closer to observations than ours (Table 1). This is partly due to different tuning targets: matching observed mass change was a stated target in their 463 study, whereas our study targets ice front position and velocity. Their close match to observed mass 464 loss may be partly due to cancelling errors: 1) their modeled calving front barely moves after 2006, 465 which leads to under-estimation of mass change; and 2) the modeled fast flow widths are larger than 466 observations, which amplifies the mass flux across the calving front. These two biases will not 467 always offset each other perfectly in the future.

Muresan et al. (2016) failed to simulate the retreat of Jakobshavn Isbræ after 2010. This may be due 468 469 to the thickness threshold employed in their calving parameterization. Once Jakobshavn Isbræ 470 terminus has retreated into the deeper part of the bedrock trough, the terminus height might never 471 drop below their calving threshold of 375 m. In this case their calving rate will be solely due to the 472 eigen parameterization of strain rates. Moreover, absence of seasonality in their calving front leads to under-estimated dynamic thinning, which is a key prerequisite for further calving. In contrast, 473 our crevasse-depth calving model depends on stresses and surface water run-off with strong seasonal 474 475 variation. As the terminus retreats and the surface slope steepens the enhanced surface stretching 476 enhances the opening of crevasses in both calving parameterizations.

477 Nick et al. (2013) used a flow-band model to estimate a mass loss of 2280 Gt for Jakobshavn Isbræ by 2100 under the A1B climate scenario (Table 1). In our model we use RCP4.5 climate forcing, 478 which has lower temperature rises than A1B, especially after 2050. Nick et al. (2013) prescribed a 479 flow-band that has a near uniform width of 5 km near the terminus. Later modeling work using a 480 similar model suggested that stability of the glacier is fundamentally controlled by geometry, and in 481 482 reality the width varies along the ice-stream (Steiger et al. 2017). Nick et al. (2013) chose sets of 483 parameters that produced small inter-annual retreats of Jakobshavn from 2000-2010, which may 484 limit mass loss and retreat. The absence of the shear margin weakening feedback in their model also 485 likely causes underestimation of mass loss. This could account for the comparable projected mass

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loss to our results, and less terminus retreat (Table 1), even though their climate forcing scenario was warmer.

Another SSA model (Bondzio et al., 2018) projects larger retreats than ours, and uses a calving 488 489 parameterization that predicts the location of calving depending on tensile stress distribution, 490 regardless of ice thickness. In contrast our calving parameterization uses mélange buttressing effects 491 and calving driven by seasonal filling of crevasses with surface water run-off, while Bondzio et al. 492 (2018) drive their calving seasonality by a seasonal varying stress threshold. However, in the real 493 world Jakobshavn, calving does not have to be of the full-thickness-type and can involve vertical 494 motions (Xie et al., 2016) or the MICI (Marine Ice Cliff Instability) mechanism (Pollard et al., 2015), 495 all of which are difficult to resolve by an SSA model. These calving types are probably becoming 496 more and more important as it retreats into deep water. Therefore, we cannot confidently claim our crevasse-depth based calving parameterization is better than the calving criterion that only depends 497 on tensile stress (Bondzio et al., 2018) for the future. In the next section we discuss how the model 498 499 might be improved.

500 4.4 Model improvements

501 We overestimate mass loss relative to observations over Jakobshavn Isbræ drainage basin for 2004-2013 (Table 1). One reason for the discrepancy may be errors in initial ice thickness and real 502 geometry in 2004. Excessive dynamic thinning was simulated over the lowest ~ 20 km of the main 503 504 trunk due to over-estimated summer speed. For example, modeled front velocity soared to a peak 505 of ~ 20 km a⁻¹ in summer 2012, while the observed maximum speed is only 18 km a⁻¹ (Joughin et 506 al., 2014). In this summer, we simulated a series of full-thickness calving events that eventually left 507 an unprecedented tall ice cliff. In reality, calving events do not always occur to full thickness, thus 508 the glacier tends to form a shorter ice cliff that caters for lower velocity and less dynamic thinning.

509 Since the grounding line of Jakobshavn retreated to the bottom of a reverse bed slope in 2009, the 510 height of the calving front has generally increased, causing larger mass flux downstream across the 511 calving front. Instead of enhancing the seasonal fluctuation of calving front position, substantial 512 winter calving events have occurred instead. Given the fact that these calving events have reduced the typical winter advance from ~ 6 km to ~ 3 km since 2010, winter calving is now likely as 513 514 important as summer run-off-driven calving. During this period of low magnitude seasonal 515 fluctuations, a series of retreats gradually moved the calving front position on inter-annual scale. In 516 contrast, the inter-annual retreats before 2009 were mostly driven by single calving seasons, e.g., 517 May to July 2009. Our model using the Benn calving model is better able to simulate this earlier 518 retreat pattern, which is largely determined by each year's peak surface water run-off.

The grounding line of Jakobshavn Isbræ is unlikely to return to shallow water in the remainder of the 21^{st} century because bedrock elevations < - 1000 m beneath the main trunk further extend ~ 60 km inland. Accordingly, the latest retreat pattern including winter calving, is likely closer to the pattern of future evolution of Jakobshavn Isbræ. A short floating part due to winter calving is always accompanied by weaker lateral drag and steeper surface slope near the grounding line, all of which are conducive for faster ice-flow. So, winter calving would enhance the downstream mass transportation, a missing process in our model.

The process of winter calving must take place without any surface water. That calving must be generated by processes affecting ice front stability, and that is likely due to changes at the base rather than the surface. Evidence of calving by opening of basal crevasses and splitting comes from terrestrial radar showing the terminus lifting several days prior to a large calving (Xie et al., 2016; James et al., 2014). These observations suggest that the glacier is not in hydrostatic equilibrium during calving. Our simulation specifies the glacier is in hydrostatic equilibrium on timescales of 532 the simulation. Our model cannot simulate the process of up-lifting. Instead we assume the upper and lower surface would instantly lift to the state of floating (Eq. 1). However, there is some 533 534 evidence that Jakobshavn must behave super-buoyantly in winter. We observe that the simulated 535 grounding line of Jakobshavn retreats even after cessation of calving front retreat (Fig. 3). These 536 retreats can be explained by rapid dynamic thinning near the grounding line leading to its buoyancy 537 exceeding gravity and, consequently, floating. Winter calving can occur in later winter (Cassotto et 538 al., 2015) when calving front height is at its annual minimum and presumably at its least vulnerable 539 to structural failure. Hence, MICI cannot explain this type of calving (Pollard et al., 2015). The 540 existence of winter calving has greatly reduced the range of seasonal fluctuations in front position, 541 which inhibited the growing of a temporary ice shelf that would buttress the grounded ice. Thus, 542 lack of winter calving would cause underestimation of dynamic thinning as the glacier grows in 543 winter.

544 A combination of discrete element model and continuum ice-dynamic model (solving the 3-545 Dimensional full-stokes equation) is able to reliably replicate observed calving styles in the case of 546 a super-buoyant terminus (Benn et al. 2017). The discrete element model allows investigation of calving processes in unprecedented detail by analyzing the stress pattern dominated by glacier 547 548 geometry and boundary conditions. However, these calving processes are beyond the capability of 549 a calving parameterization based on surface crevasse depth assuming depth-independent flow. Better understanding of this buoyancy-driven calving and further model development to represent 550 551 more details such as fracture propagation are needed to accurately simulate glacier's future 552 evolution.

Ice thickness and basal topography with resolution of 150 m became available for main outlet
glaciers of Greenland (Morlighem et al., 2017) recently (Fig. S3). This eases finer mesh resolution

to be used for modeling which then might reveal more details of ice-stream behavior especially perpendicular-to-flow direction, including more precise shear-margin-weakening and calving near side walls. Our assumption of simple Weertman basal drag (Eq. 7) may be improved by implementing a physics-based basal sliding law (Schoof, 2010; Gagliardini et al., 2014; Tsai et al., 2015), although basal drag accounts for only about 2% of present-day buttressing (Shapero et al., 2016). An improved sliding relation would likely produce more speedup and retreats in model results as dynamic thinning can reduce the effective pressure, leading to lower basal shear stress.

562 **5 Conclusion**

We use a three-dimensional dynamic ice-sheet model with a physically-based calving parameterization to model the evolution of Jakobshavn Isbræ. After tuning the parameters, our model can accurately reproduce Jakobshavn Isbræ's retreats and velocity changes from 2004-2013 on both seasonal and inter-annual scale. We project Jakobshavn Isbræ's future dynamic changes with climate forcing data from RACMO (2014-2099) and an ensemble mean of 7 Earth System Models for the RCP4.5 scenario.

We successfully model two-dimensional ice velocity and viscosity structures and their seasonal variations for Jakobshavn Isbræ, which are missing from several previous modeling studies. Moreover, capturing these two-dimensional structures allows us to handle the influence of horizontal velocity shear on effective ice viscosity, which impacts on speedup processes of Jakobshavn Isbræ.

We predict that Jakobshavn Isbræ's grounding line will retreat along the deep parts of a basal trough where bedrock elevation is significantly lower than at the present grounding line until about 2070. Retreat slows as the front reaches the deepest parts of the trough, but by the end of the century acceleration is possible as the front passes that position. Using the current generation of calving parameterizations, which are essentially thickness threshold models, is challenging because of the increasing height of the calving front as Jakobshavn Isbræ retreats, meaning that crevasse penetration depths become too small to initiate calving. Our model successfully reproduced Jakobshavn Isbræ's retreat down a reverse bed slope with an elevation drop of \sim 400 m and the subsequent temporarily stable calving front position in 2013 and 2014.

583 Our results suggest that rapid dynamic thinning and calving caused by deep crevasse penetration

are responsible for most of its recent mass loss, and will be decisive processes in future mass loss.

585 Further exploration of the physics of calving and basal sliding of Greenland outlet glaciers are

586 required to improve future projections.

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767 Supplementary information

768 Simulated retreat of Jakobshavn Isbræ during the 21st century

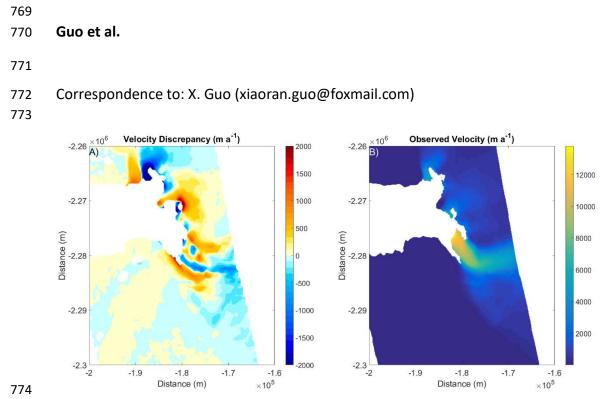


Figure S1. A) Velocity discrepancy (velocity from inversion - observed) and B) the observed
 velocity field (Joughin et al., 2010).

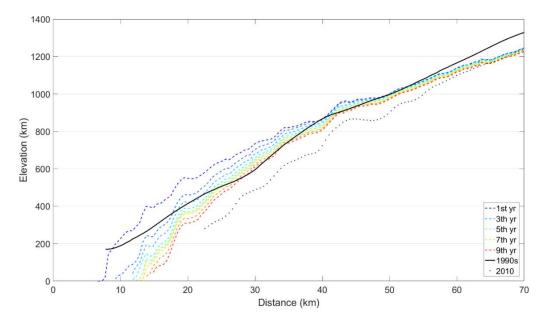




Figure S2. Profiles of surface elevation during the initialization procedure (section 2.3) step 3.
Black solid line and black dashed line show the known profiles taken in the 1990s (Bamber et al.,
2001) and 2010 (Gogineni et al., 2012) respectively. The profile with legend '1st yr' is the final
state of section 2.3 step 2. The profile '7th yr' is the geometry rebuilt for 2004's Jakobshavn, which
is the initial state for later simulations.

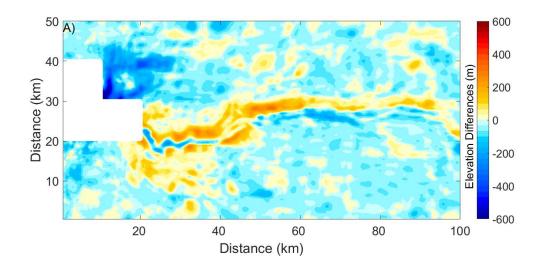


Figure S3. Bed elevation from BedMachine v3 (Morlighem et al., 2017) minus those from
 (Gogineni, 2012) used in this paper.