Final response to editor Etienne Berthier for the manuscript: Impact of frontal ablation on the ice thickness estimation of marine-terminating glaciers in Alaska by Beatriz Recinos et al.

Dear Etienne Berthier,

We apologize for the delays accumulated during the discussion of our manuscript. We now believe that we have addressed all points raised by the reviewers and herby submit the revised version together with a point by point reply to each of the reviewers comments, which has no substantial changes to those replies uploaded during the discussion stage of the manuscript (pp. 2-11 of this document).

Since our first manuscript submission, several model developments happened in OGGM. In this revised version, we now used an updated model version (OGGM v1.1), which coincides with the model publication in Geoscientific Model Development. The details of the new additions and changes in OGGM can be found here.

Modifications to the frontal ablation parametrisation tool were also needed. A correction to a bug found in the iterative procedure now makes the result of the parameterisation compatible with mass conservation. The changes implemented can be found **here** and are now part of the main OGGM code.

These additions did not change our manuscript main findings or the model results in a significant way. But the performance of the frontal ablation parametrisation tool improved for individual glaciers estimates compared to the initial version of the code (see the discussion section and Fig. 11 of our manuscript).

We have also implemented the changes suggested by reviewer #1 and added a new section explaining the convergence of the iterative procedure (see section 3.5). We have also clarified those points that caused confusion in our manuscript for both reviewers.

Please find the changes to our manuscript highlighted in blue at the end of the replies (from p. 12).

Reply to Douglas Brinkerhoff

We would like to thank Douglas Brinkerhoff for taking the time to read our manuscript and give us a chance to answer to his concerns before the end of the review process. We hope that our response is clarifying the motivation behind our study, and we remain available for further questions.

Here we present a detailed point by point response (the reviewer's comments are given in italics, our answer in normal font).

RC: Eq. 2. This equation is not valid for non-rectangular cross-sections. Rather, it is depth-averaged velocity for a particular location over a cross-section. To make this into depth and width averaged velocity, we need to introduce a parameterization of h (parabolic, for example), and then width integrate. If we do this (assuming a centerline depth of h_0 and margin thickness of zero, we get an additional multiplicative factor of $\frac{128}{315}$ (assuming n=3). Thus, fluxes are being overestimated by a factor of nearly 3.

AR: yes, we should have been more precise in the formulation here. In OGGM we support rectangular, parabolic and trapezoidal bed shapes. For all cases, we compute the ice velocity at the maximum thickness h_0 , then multiply this velocity by the cross-section area to compute the flux. The section area is $S = \frac{2}{3}h_0w$ in the parabolic and $S = h_0w$ in the rectangular case (with w the section width). This is physically not correct (we are missing a non-linear term in the variation of τ with the parabola), and is indeed an overestimation of the flux with respect to a true parabolic bed.

Nye (1957) gives analytical solutions as to how much this overestimation could be (his Tables IIIa and IIIb). He gives solutions for the section average velocity and the surface velocity at the parabola's center, i.e. providing an upper bound of the error in our approach: this overestimation ranges from a factor 1.48 to 2.25 depending on the parabola's width to depth ratio.

That being said, we have to emphasize here that OGGM is of the "paremeterized" ice model type, aiming at the simulation of a very large number of glaciers with unknown boundary conditions. We could implement the correct solution (and will happily add an option to use it, as we've recently done by implementing lateral drag shape factors following Adhikari and Marshall, 2012, follow this link for the implementation).

However, the current implementation has several practical advantages: it allows us to use the same numerical solver for all bed-shapes (Maussion et al., 2018), is computationally efficient and consistent between the inversion and the forward model. This alone should not be used as an argument to justify our method. More importantly, this simple approach reduces the difference in fluxes between different bed shapes, which are unknown a priori (and are neither parabolic nor rectangular in reality). Hence, the sensitivity of the model to this unknown parameter is reduced as well.

In the case of the ice thickness inversion, the flux is prescribed by the apparent mass-balance anyway, so that the implied uncertainties are transferred to the cross-section's thickness and volume (and each section is independent from another). The same equations are used to solve for h_0 with a given flux. This results in a polynomial of degree 5 with a unique solution for h_0 in \mathbb{R}_+ . Therefore, for any given glacier with unknown bed-shape and prescribed apparent mass-balance, we will have a volume ratio of approx. $\frac{2}{3}$ between the two cases¹. In practice,

 $[\]frac{1}{3} \times \frac{3}{2}^{\frac{1}{5}} = 0.72298$ to be exact, in the case n = 3 and without sliding

OGGM relies on geometrical considerations to decide if the shape is parabolic or rectangular (Maussion et al., 2018).

Finally, it must be added that the inversion model used in this study is the same as the one used in Farinotti et al. (2017) (where OGGM ranked amongst the best models able to process a large number of glaciers), Maussion et al. (2018), and Farinotti et al. (accepted). While this doesn't mean that the model is error-free (there is no such thing anyway), a systematic error of a very large magnitude is unlikely to have been left unnoticed.

The interested reader can find the corresponding code implementation at the following locations (links):

- ice thickness inversion
- forward model
- tests of the forward model where we compare our implementation to the solver by Jarosch et al., 2013.
- tests of the inversion model in ideal cases simulated by the forward model

RC: Eq. 6. The interpretation of these symbols doesn't make sense. Ω , in this case needs to be the contributing area for a given cross section, not the cross-section itself. This correct form leads to units of kgs^{-1} . However, the definition of $F_{calving}$ is in units of volume per time, and thus we have a misfit. This would be (numerically) fine if this parameter were solved for because this error could be absorbed into k. However, the authors set this to a value previously computed by Oerlemans and Nick, and thus the scaling of the terminal versus surface fluxes is incorrect.

AR: you are fully right, Ω is of course the contributing area (we call it "catchment area" in the model code), this was a bad typo. We convert between volume and mass using an ice density of 900 kg m⁻³. The conversion is implemented here.

RC: Eq. 10. This expression for depth makes no sense to me, partially because the terms included are not well defined. What is the elevation of the glacier terminus, Et? Were dealing with vertical ice cliffs here, so is this the base of the cliff (i.e. bedrock elevation) or the top? In either case, the resulting d is not consistent with the definition of depth used in Oerlemans and Nick frontal ablation parameterization. Also, I fail to understand the difficulty implied about lake terminating glaciers. The definitions are fairly simple: Hf needs to be the terminus ice thickness, d needs to be the water depth. Neither depend on sea level being zero. (This is not to say that there is no difference between marine and lake-terminating glaciers; k should be different between them).

AR: the water depth d is estimated from free-board, using the terminus elevation obtained by projecting the RGI outline to the DEM. I.e., the terminus elevation is the top of the cliff. The Terminus elevation (E_t) minus the thickness of the ice (H_f) is the water depth (negative values) at that point, or as Oerlemans and Nick (2005) definition of d (bed elevation with respect to sea level, See Figure 1 from Oerlemans and Nick, 2005). We are not able to estimate a water depth for lake-terminating glaciers, because for that we would need to know the free-board of the glacier terminus, i.e. the elevation of the glacier lake surface (for the elevation of the ocean surface, we assume that it is 0 m a.s.l.).

We leave the discussion about k for the next section.

RC: Sect 3.4 It is not clear what this iterative procedure accomplishes, especially if μ^* is being altered, as is indicated. It seems that for a fixed surface mass balance and terminus position,

there are any number of valid solutions that respect the constraints that $H_f \geq 0H$. Is it trying to match a specific $F_{calving}$ based on observations? In that case, I can see the utility in changing μ^* .

AR: Thanks for this comment - we will have to better explain our intent in the manuscript, as this is also a point that Reviewer #1 was asking to improve. We will make further experiments and graphics to explain the procedure, but to expedite the review process, we attempt an explanation here:

First of all, all inversion methods based on mass-conservation assume a mass-flux of zero at the terminus, unless constrained either by a prescribed calving value (e.g. Huss et al., 2015) or by observed ice velocities (e.g. Frst et al., 2017). In OGGM, we use the equilibrium assumption to calibrate a first guess μ , which assumes an ice flux of zero at the terminus as well. Therefore, if k and water depth (or the calving flux) would be known, we could derive μ from them.

In the absence of observations, we go the other way around. The main objective of the iteration is to find a frontal ablation flux and ice thickness compatible both with the frontal ablation parameterization and with mass conservation, in order to compute the first ice thickness inversion and initialize the glacier in the model (black line of Figure 3c). This allows calving glaciers in OGGM to have a terminus thickness bigger than zero and a non-zero ice flux at the end of the glacier (Figure 3c and Figure 5), which is then fed again to the mass-balance model to re-calibrate μ .

Importantly, the experiments described in Sect. 4.1, 4.2 and 4.3 use OGGM's default configuration set up (described in Sect 3.1 and 3.3). During these experiments, we do not make use of any observations² to restrict or calibrate $F_{calving}$. One of the most important result of our study (the ratio of underestimated ice volume because of calving) is robust to the parameter choice and remains approximately constant regardless of the true total ice volume.

Physically, $F_{calving}$ in these experiments (and during the iteration) is limited by the amount of annual accumulation. μ^* changes at each step during the iteration in order to reconciliate the (now non-zero) frontal ablation flux with mass conservation, while the boundary conditions (most importantly, accumulation) remain fixed. To illustrate how μ^* varies, we refer you to Fig. 4b and Eq. 5, as well as further experiments that will be realized as a result of the questions raised by Reviewer #1.

RC: But it seems to me that altering k would be more reasonable, since frontal ablation parameterizations are far more uncertain that surface mass balance parameterizations.

AR: Indeed it will be easier to modify the value of k to match previously calculated regional estimates, or individual calving flux observations. But the ultimate goal of OGGM and our iteration method is to compute a frontal ablation flux for any calving glacier of the world (we are not there yet). Many areas do not have regional estimates or with enough individual calving flux observations to constraint k.

We will add an extra section and figure to the revised manuscript in order to illustrate the importance of this iterative procedure when we lack frontal ablation observations or additional data (e.g., depth and terminus width) to restrict our boundary conditions. We will also add some idealized experiments to help the readers to understand this section.

RC: The above issues are problematic individually, but taken together, they call into serious question the validity of the results. I forego further comment until such a time as they are

²In the second part of the experiments (Sect. 4.4 - 5) is when we make use of previously calculated frontal ablation fluxes from McNabb et al, 2015.

addressed.

Thank you for your comments. We hope that we were able to restore your confidence in our results and we will do our best to clarify those points that caused confusion in our manuscript.

Reply to Anonymous Referee # 1

We would like to thank the reviewer for taking the time to read our manuscript and give us insightful comments on the methodology, as these comments led us to formulate new experiments, to improve the code and the manuscript. We agree that this important point was missing from our manuscript and will provide a new section better explaining our method and our objectives.

Here we present a point-by-point response (given in normal font) to the related issues made by the reviewer (given in *italics*). Additionally to this response, we have prepared a **Python Notebook**, where we explain the new experiments and elaborate on the iterative procedure implemented in the Open Global Glacier Model (OGGM) to find a frontal ablation flux. We think that the notebook addresses best the issues raised by the reviewer: our answer is self-contained but is based on these simulations. Interested readers can try the experiments themselves by visiting the interactive version of the notebook.

RC: Convergence of iterative procedure.

Looking at your iterative calibration procedure from the perspective of an optimisation, I wonder what target quantity is minimised. In other words, what is the reason for this procedure to converge or reach the stopping criterion. Starting from an initial thickness guess, you infer $F_{calving}$ and update the temperature sensitivity μ^* in the surface mass balance equation (5). Then, you re-run the reconstruction and get an updated frontal thickness value. From all involved equations, I cannot see a good reason why the following updates should produce values with a gradually reducing relative differences. A reason for non-divergence is that the thickness update involves a polynomial relation with an exponent smaller than one. Yet even if convergence is reached, I wonder about the physical meaning of this specific solution. Please do not misunderstand me here, but I really think that this is an important point with serious implications for the expedience of your approach. I unfortunately do not have a good suggestion for a useful target quantity or another potential quick fix. To convince the reader about the functionality of this calibration procedure, I think you have to expand the article by another section, which will elaborate on the stability and the convergence behaviour for a few test cases. I am particularly interested in figures showing the iterative changes in the frontal thickness. Is it monotonous or are the over-shootings. The latter seems unlikely considering the underlying equations. An interesting test would be to check what happens if you started from a too large thickness value (for a well-studied glacier). I would expect an even higher calving flux and thus a further increase in ice thickness. I ultimately miss a relation which counter-balances a steady increase during the iterations. In general, you should assure that the final thickness profile does not depend on the initial thickness quess. Another informative analysis would be to see what happens if the stopping criterion is ignored and you continue the iterations for 100 or even 1000 steps. Do the relative differences in the frontal thickness decrease further? This would be a requirement for the introduction of the suggested stopping criterion. To put my whole concern in simple words: by introducing a calving flux in the mass budget, you have to reduce the amount of necessary melt (for a balanced situation) This reduction further increase the necessary calving flux in each iteration. To break this run-away cycle, you need another physically motivated relation that penalises either low melt values, high calving fluxes or high frontal thicknesses. Such a counterbalance effect might already be at work by the underlying functional dependencies but without a clear physical motivation.

AR: To answer this issue we have followed the reviewer's suggestion and are preparing a new section in our revised manuscript with experiments that illustrate the converges of the parameterisation. This new section will be based on the notebook linked above, where we experiment with the LeConte Glacier (RGI60-01.03622). Note that it is possible to test any another marine-terminating glacier as well (see the **interactive version** of the notebook).

We use a simple calving law borrowed from Oerlemans and Nick (2005), which relates frontal ablation $F_{calving}$ to the frontal ice thickness H_f , the water depth d and the terminus width w:

$$F_{calving} = kH_f dw$$

with $F_{calving}$ in km³ yr⁻¹, k a calibration parameter (default 2.4 yr⁻¹) and d the water depth calculated as:

$$d = H_f - E_t$$

where E_t is the free board.

As explained in our manuscript, ice conservation methods applied to tidewater glaciers *must* take into account this mass-flux at the terminus, otherwise the ice thickness is underestimated. In fact, the default OGGM ice thickness inversion procedure assumes an ice flux of zero at the terminus.

In Fig. 1, we examine how this frontal ablation flux would change if we increase the terminus ice thickness, while keeping the free board fixed (the free board is the only variable we know "with certainty", from the DEM surface elevation at the terminus).

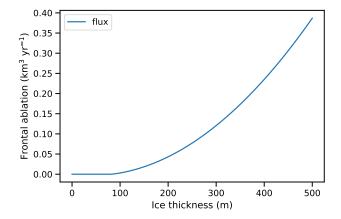


Figure 1: Frontal ablation flux computed by the calving law as a function of the terminus ice thickness.

The flux remains equal to zero as long as the frontal ice thickness is not thick enough to reach water, after which the water depth is positive and calving occurs. The calving flux varies with H_f as a polynomial of degree 2.

We are unaware of the *real* value for the calving flux at this glacier. But from here, we can make some very coarse assumptions:

• The Oerlemans and Nick calving law is perfectly exact

- \bullet The tuning parameter k is known
- Our glacier is in equilibrium (mass-conservation inversion in OGGM)
- Ice deformation at the glacier terminus follows Glen's flow law

Under these assumptions, we set up a new experiment where we compute a frontal ablation flux (from the calving law) for a range of prescribed frontal ice thickness (see Fig. 2), then give this flux back to the OGGM inversion model, which will use this flux to compute the frontal ice thickness according to the physics of ice flow (see the **OGGM documentation** or our manuscript for more information). Fig. 2 shows that there is a unique value for the frontal thickness (H_f) that complies with **both** the calving law and the ice thickness inversion model of OGGM.

We already know that the calving law relates the ice thickness to the flux with a root of degree two (blue curve of Fig. 2). But for the the orange curve in Fig. 2, it is Glen's flow law, which relates the ice thickness to the flux with a 5th degree root (assuming n=3). Showing the reason why there is one (and only one) non-zero solution to the problem of finding a calving flux; a flux which is compatible with both the calving law and the physics of ice deformation (under our simplified framework).

Note that changing Glen's deformation parameter A or adding sliding does not change the problem: we will still solve a polynomial degree 5 in OGGM, with a new term in degree 3 (see green curve in Fig. 2).

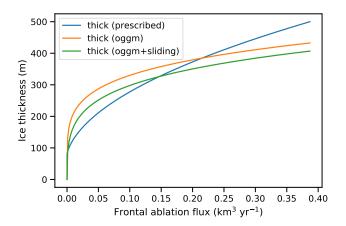


Figure 2: Ice thickness per frontal ablation flux calculated at each iteration. The blue line is the flux calculated by prescribing a thickness and using the calving law. The orange line is the flux calculated by OGGM using the iterative procedure. The green line is the flux calculated by OGGM using the iterative procedure and adding a sliding velocity.

There are several ways to find this "optimal" calving flux (or optimum frontal ice thickness), where mass-conservation inversion and the calving law are compatible. In OGGM, we implement an iterative procedure converging to this value in a few iterations (see Fig. 3).

The procedure starts with an initial water depth equal to 1/3 of the terminus altitude E_t , then iteratively feeds the calving flux back to the mass-conservation inversion function of OGGM, which adapts the mass-balance model to cope with a non-zero ice flux at the front. In order to do that, the temperature sensitivity of the glacier μ^* has to be reduced (per construction, the original μ^* is defined such that the flux at the front is zero). Convergence is reached when the

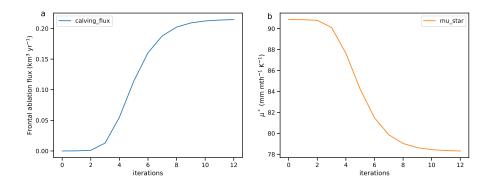


Figure 3: Right: Frontal ablation flux at each iteration. b: Temperature sensitivity μ^* of the glacier at each iteration.

OGGM flux equals the calving law flux within 0.1%. Thanks to the uniqueness of the solution, the method always converges regardless of the starting water depth (Fig. 4).

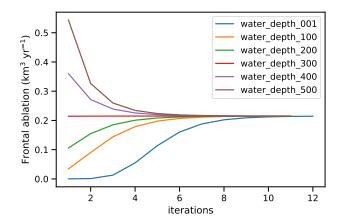


Figure 4: Frontal ablation flux calculated from different starting points. The different colors represent different water depths at the beginning of the iteration procedure.

However, for some glaciers the calving flux given by the calving law is larger than a flux that can be explained by climate alone, i.e. even without melt, the computed flux is larger than the total accumulation over our glacier. This can happen for several reasons:

- precipitation is underestimated
- the flux is overestimated because of uncertainties in k and the terminus geometry
- the equilibrium assumption is not valid

During these conditions our iterative search can "overshoot". Fig. 5 simulates this case where we set an unrealistically large calving parameter (k equal to 10 yr⁻¹ in this experiment). If this happens during the iteration, OGGM is going to set μ^* to zero and compute the corresponding flux (the maximal physically possible value).

RC: Manuscript structure The structure of the manuscript is not very clear and only after reading all of the results, I finally got my head around the overall strategy to set up the method. A major drawback is that the calibration of the proportionality factor k in the calving relation

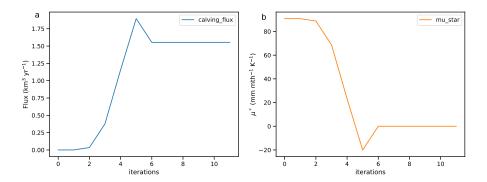


Figure 5: a: Frontal ablation flux per iteration. b: Temperature sensitivity μ^* per iteration. With a k value of 10 yr⁻¹.

with respect to available regional estimates of the frontal ablation is presented rather late in the text. I think that a calibration section will be very useful at the end of the methodology (P9). This section can also serve to explain that you will use two variants of the model: one with sliding and another without.

AR: We would like to clarify that the calibration of the proportionality factor k with respect to available regional estimates of frontal ablation does not take part in the iteration procedure described in section 3.4. During the iteration procedure and in most of the study experiments, we keep k constant with a value of 2.4 yr^{-1} . We only modify k to match regional estimates during the sensitivity experiments (see section 4.4 and 4.5) with the intention of showing that regardless of the parameter configuration chosen, we can still estimate the relative part of the ice volume that is missed when ignoring frontal ablation in the inversion. We consider that this part of the text does not belong on the methods section, since our optimum goal is to make OGGM independent of frontal ablation observations. Hopefully, the clarification of the iterative procedure above helps clarify this point, too.

RC: Specific comments.

Suggestions for the iterative calibration procedure.

A. Initial thickness

Concerning the first two steps in your iterative process (P8L19-22), you determine an initial guess for the calving flux, by assuming a frontal ice thickness which is 1m higher than the surface elevation. I think that it will be beneficial to use the flotation criterion here, making an assumption on the ocean water density. This criterion is simple to implement, it will give a larger first guess and it will therefore speed up your convergence.

B. A-priori limits

The flotation criterion for the frontal ice thickness also provides a lower bound Hminto the "real" frontal thickness value. The reason is that most tidewater glacier will likely be thicker and firmly grounded. An upper bound for the frontal thickness (Hmax) is given by integrating the accumulation field. This will provide the maximum ice flux possible along the glacier. Alternatively, you could integrate the SMB above the ELA. This will give smaller maximum flux values (these will however dependent on μ^*). The maximum flux can then be translated into an upper bound for the frontal thickness value (Hmax) via Eqs. (8-10). A conflict between the upper and lower bound (Hmin > Hmax), will indicate inconsistencies in the climatology and thereby give useful information.

C. Stopping criterion

The stopping criterion is chosen to be an absolute flux value. In this way, the stopping criterion

is easier to be reached for small glaciers with overall lower flux values. I do not think that this is a desirable behaviour and it was not communicated as a deliberate decision. I would therefore suggest that you define the threshold as a fraction of the annually received precipitation volume. If this should not be feasible, you could use a constant values that scales either with glacier area or the terminus width.

AR: For the issues addressed here, please refer to the first section of the reply: convergence of iterative procedure.

In addition to the changes mentioned above, modifications to the code were needed in order to correct a bug found in the iterative procedure which now makes the result of the parameterisation compatible with mass conservation. The changes implemented can be found **here**.

We will add an explanation of all the modifications to the code in our revised manuscript.

Our main result of the ice volume underestimation when ignoring frontal ablation is still the same after this correction.

We thank you for your comments again and for helping us to improve our method. We will do our best to clarify those points that caused confusion in our manuscript.

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Impact of frontal ablation on the ice thickness estimation of marine-terminating glaciers in Alaska

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Abstract.

Frontal ablation is a major component of the mass budget of calving glaciers, strongly affecting their dynamics. Most global scale ice volume estimates to date still suffer from considerable uncertainties related to i) the implemented frontal ablation parameterisation or ii) for not accounting for frontal ablation at all in the glacier model. To improve estimates of the ice thickness distribution of glaciers, it is thus important to identify and test low-cost and robust parameterisations of this fundamental process. By implementing such parameterisation into the ice-thickness estimation module of the Open Global Glacier Model (OGGM v1.0.1), we conduct a first assessment of the impact of accounting for frontal ablation on the estimate of ice stored in glaciers in Alaska. We find that inversion methods based on mass conservation systematically underestimate the mass turnover, and therefore the thickness, of tidewater glaciers when neglecting frontal ablation. This underestimation can rise up to 17 amount to up to 16 % on a regional scale and up to 4730 % for individual glaciers. The effect strongly depends on the size of the glacier. Additionally, we perform different sensitivity experiments to study the influence of i) a constant of proportionality (k) used in the frontal ablation parameterisation, ii) Glen's temperature-dependent creep parameter (A) and iii) a sliding velocity parameter (f_s) on the regional dynamics of Alaska tidewater glaciers. OGGM is able to reproduce previous regional frontal ablation estimates applying a number of combinations of values for k, Glen's A and f_s . These different model configurations show that volume estimates, after accounting for frontal ablation are 15 to 17, are 14 to 16 % higher than volume estimates ignoring frontal ablation. Our sensitivity studies also show that differences in thickness between accounting for and not accounting for frontal ablation occur mainly at the lower parts of the glacier, both above and below sea level. This indicates that not accounting for frontal ablation will have an impact on the estimate of the glaciers' potential contribution to sea-level rise. Introducing frontal ablation increases the volume estimate of Alaska marine-terminating glaciers from $9.01-9.31\pm0.35$ to 10.43-0.37 to 10.75 ± 0.44 -0.39 mm SLE, of which 1.41-1.53 ± 0.18 (0.58-0.07 mm SLE (0.60 ± 0.05 -0.03 mm SLE when ignoring frontal ablation) are found to be below sea level.

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1 Introduction

Estimates of the spatial distribution of ice thickness are necessary, needed as initial conditions for glacier modelsand, for attempting to understand how glaciers respond to climate changeand, and for quantifying their contribution to sea-level rise. Despite this importance, ice thickness measurements around the globe are scarce, performed only in approx. 600 glaciers (Gärtner-Roer et al., 2014) out of more than 200,000 identified in the latest latest Randolph Glacier Inventory (RGI v6.0, Pfeffer et al., 2014). In order to overcome this under-sampling problem, a number of methods have been developed to infer the total volume and/or the ice thickness distribution of glaciers from characteristics of the glacier surface properties. Some of these methods rely on scaling approaches relating the length, slope and area of the glacier to its total volume (e.g. Bahr et al., 1997; Lüthi, 2009; Radić and Hock, 2011; Grinsted, 2013). Others rely on parameterisations of basal shear stress (e.g. Paul and Linsbauer, 2012; Linsbauer et al., 2012; Frey et al., 2014), on observed surface velocities (e.g. Gantayat et al., 2014), or on applying the shallow-ice approximation (e.g. Oerlemans, 1997; Cuffey and Paterson, 2010) and/or an integrated form of Glen's flow law (see Farinotti et al., 2017, for a review of all these methods) (see Farinotti et al. (2017), for a review of all these methods and Farinotti et al. (2019), for a global-scale intercomparison).

One method presented by Farinotti et al. (2009) and successfully applied several times since then (e.g. Morlighem et al., 2011; Huss and Farinotti, 2012; Clarke et al., 2013; Maussion et al., 2019), combines ice flow dynamics and mass conservation principles to constrain mass fluxes through given glacier cross-sections. The method infers ice thickness from estimates of ice fluxes derived from the assumption that ice fluxes balance the surface mass budget (Farinotti et al., 2009). The results are thus sensitive to the spatial distribution of the mass flux and the mass balance. For calving glaciers, the surface mass budget cannot be considered balanced, even assuming equilibrium between glacier and climate. The derived ice thickness estimate for these glaciers hence depends on estimates of frontal ablation.

Frontal ablation (mass loss by calving and frontal melting (Pope, 2012)) (mass loss by calving and frontal melting Pope, 2012), is an efficient process to deliver ice from glaciers and ice sheets into the ocean. It has contributed substantially to sea-level rise in the past and played an important role in the stability of ice sheets and tidewater glaciers during the Pleistocene (Benn et al., 2007). Calving is strongly coupled with dynamical processes inside the glacier. An increase in the ice flux can trigger a calving event and in turn this event can accelerate the movement of the ice. External aspects like ocean temperature, fjord bathymetry and, in polar areas, sea-ice concentration along the calving front can also influence the discharge of solid ice to the ocean (Straneo et al., 2013). As a consequence of the diverse nature of calving processes, the development of parameterisations of frontal ablation in numerical ice sheet models and in global glacier models remain and glacier models remains an important challenge. There is a wide spectrum of parameterisations approaches that vary in scale and complexity, justified through the diversity of intended applications of the models (Price et al., 2015).

There have been many successful efforts to represent frontal ablation for individual glaciers (e.g. Ultee and Bassis, 2016; Åström et al., 2014; Todd and Christoffersen, 2014; Oerlemans et al., 2011; Nick et al., 2010). While these are very encouraging approaches achieve encouraging results, it is unlikely that they can be implemented in a global glacier model anytime soon, because of the amount and quality of data needed to constrain this type of model. The crevasse-depth criterion proposed by

Nick et al. (2010) for example, requires knowledge of surface melt and refreeze rates at the crevasses of the glacier tongue, and crevasse depth observations to calibrate and validate these rates. These kinds of observations are hard to obtain for entire glaciated regions: e.g., the 198 calving glaciers in Alaska investigated here, or the 3,222 glaciers classified as calving (marine-and lake- terminating) glaciers in the RGI v6.0. Other recent calving models that use discrete particles or a full-Stokes model approach (e.g. Åström et al., 2014; Todd and Christoffersen, 2014; Todd et al., 2018) are too computationally expensive to be included in global glacier models that seek to consistently simulate past and future global scale glacier changes.

At the regional and global scale, very few estimates of frontal ablation fluxes of glaciers outside the ice sheets exist (Blaszczyk et al., 2009; Burgess et al., 2013; McNabb et al., 2015; Huss and Hock, 2015). From all the global glacier models published in the last decade, only Huss and Hock (2015) accounts account for frontal ablation of marine-terminating marine-terminating glaciers. However, this model, along with the rest of ice thickness inversion methods, still suffers from considerable uncertainty associated with the parameter uncertainty of the frontal ablation parameterisation.

For improving ice thickness distribution estimates at the global scale, it is thus important to identify and test low-cost and robust parameterisations of frontal ablation, that might not resolve all the dynamical processes at the calving front (e.g. subaqueous frontal melting, subaerial frontal melting and sublimation), but that can estimate the amount of ice passing through the terminus of the glacier during a mass balance year.

Using the ice-thickness estimation module of the Open Global Glacier Model (OGGM v1.0.1), we assess the impact of frontal ablation on the estimate of ice stored in glaciers of the Alaska region classified as marine-terminating in the RGI v6.0 (also referred as tidewater to tidewater glaciers in this study).

Alaska glaciers cover approximately 12 % of the global glacier area outside of the ice sheets (Kienholz et al., 2015). In the RGI (v6) there are 27109 glaciers in the region occupying an area of 86776.6 km², this includes including adjacent glaciers in the Yukon and in British Columbia. From these glaciers, 51 have been classified as marine-terminating (74 km of tidewater margin) and 147 as lake- and river-terminating glaciers (420 km of lake/river margin) occupying an area of 11962.4 km² and 16720.6 km², respectively. Calving glaciers (marine- and lake- terminating) occupy approximately 33 % of the Alaska glacier area (Fig. 1; Pfeffer et al., 2014; Kienholz et al., 2015).

The glaciers are divided into six subregions in the RGI. Subregions 1 and 3 contain only land terminating glaciers. Calving glaciers are mostly concentrated in the subregions 4, 5, and 6, along the mountain ranges of the southern Alaska coast (Fig. 1), an area characterised by maritime climate and topography reaching > 5000 ma.s.l (Kienholz et al., 2015). Glaciers contained in the RGI in this region range in size from a few square kilometres (Ogive Glacier, 2.8 km²) to many thousands of square kilometres (Hubbard Glacier, 3400 km²; McNabb and Hock, 2014).

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The subregions 4 and 5 are well studied glacierised areas of Alaska. McNabb et al. (2015) presented a 28 year record (1985 - 2013) of frontal ablation for a subset of marine-terminating marine-terminating glaciers that include the 27 most dominant tidewater glaciers of the region. They represent 96 % of the total tidewater glacier area in the gulf of Alaska. The total mean rate of frontal ablation was estimated to be 15.11 ± 3.63 Gt yr⁻¹ (16.48 ± 3.96 km³ yr⁻¹), over the period 1985 - 2013. Other studies also reported similar values (e.g. Larsen et al., 2007). Frontal ablation in this region is heavily dominated by two glaciers in particular: Hubbard and Columbia Glacier (McNabb et al., 2015). Additionally, McNabb et al. (2015) identified 36

actively calving tidewater glaciers in Alaska; 27 of those were used to estimate the total mean rate of frontal ablation presented in McNabb et al. (2015).

We implement a simple parametrisation of frontal ablation in OGGM, following the approaches proposed by Oerlemans and Nick (2005) and Huss and Hock (2015). By performing sensitivity studies on the model, i) we we i) investigate the effect of accounting for frontal ablation on the ice thickness estimation of OGGM and on the ice volume estimate for these glaciers, and ii) we study the impact of varying several OGGM parameters (the calving constant of proportionality k, Glen's temperature-dependent creep parameter A, and sliding velocity parameter f_s) on the regional frontal ablation rates of Alaska.

2 Input data and pre-processing

2.1 Glacier outlines and local topography

The glacier outlines used in this study are those defined in the region 1 of the RGIv6. Four glaciers (Columbia, Grand Pacific, Hubbard and Sawyer Glacier) were merged with their respective pair branches (West Columbia, Ferris, Valerie and West Sawyer Glacier) into a single outline. A local map projection is defined for each glacier in the inventory following the methods described in Maussion et al. (2019). A Transverse Mercator projection is used, centred on the glacier in order to conserve distances, area and angles. Then, topographical data is chosen automatically depending on the glacier's location and interpolated to the local grid. For this study we used a combination of the Shuttle Radar Topography Mission (SRTM) 90 m Digital Elevation Database v4.1 (Jarvis et al., 2008) for all latitudes below 60°N and the Viewfinder Panoramas DEM3 product (90 m, http://viewfinderpanoramas.org/dem3.html) for higher latitudes. For the Columbia Glacier, we used the DEM from the the Ice Thickness Models Intercomparison eXperiment (ITMIX) (Farinotti et al., 2017, ITMIX) instead ¹(Farinotti et al., 2017). All the datasets are re-sampled to a resolution depending on glacier size (Maussion et al., 2019) and smoothed with a Gaussian filter of 250 m radius.

2.2 Glacier flowlines, catchment areas and widths

The glacier centrelines are computed following the automated method an automated method based on the approach of Kienholz et al. (2014). Fig. 2a illustrates an example of this geometrical algorithm applied to the Columbia Glacier. The centrelines are then filtered and slightly adapted to represent glacier flowlines with a fixed grid spacing (Fig. 2b). The geometrical widths along the flowlines are obtained by intersecting the normals at each grid point with the glacier outlines and the tributaries' catchment areas. Each tributary and the main flowline has a catchment area, which is then used to correct the geometrical widths. This process assures that the flowline representation of the glacier is in close accordance with the actual altitude-area distribution of the glacier. The width of the calving front, therefore, is obtained from a geometric first guess multiplied by a correction factor. This may lead to uncertainties in the frontal ablation computations, as discussed in Sect. 5.

¹See Sect. 5 for a discussion about the importance of reliable topographic data for the frontal ablation estimate.

2.3 Regional frontal ablation estimates

Frontal ablation for 27 marine-terminating marine-terminating glaciers presented by McNabb et al. (2015) are used to compare the results of the model and calibrate the calving constant of proportionality k. These estimates were calculated from satellite-derived ice velocities and modeled estimates of glacier ice thickness.

5 2.4 Climate data and mass balance

The mass balance (MB) model implemented in OGGM uses monthly time series of temperature and precipitation. The current default is to use the gridded time-series dataset CRU TS v4.01 (Harris et al., 2014), which covers the period of 1901-2015 with a 0.5° resolution.

This raw, coarse dataset is downscaled to a higher resolution grid (CRU CL v2.0 at 10' resolution, New et al., 2002), following the anomaly mapping approach described in Maussion et al. (2019), allowing OGGM to have an elevation-dependent climate dataset from which the temperature and precipitation at each elevation of the glacier are computed, and then converted to the local temperature according to a temperature gradient (default: 6.5 K km⁻¹). No vertical gradient is applied to precipitation, but a correction factor p_f =2.5 is applied to the original CRU time series (see Maussion et al., 2019, appendix A for more information).

The MB model (see Sect. 3.2) is calibrated with direct observations of the annual surface mass balance (SMB). For this, OGGM uses reference mass-balance data from the World Glacier Monitoring Service (WGMS, 2017) and the links to the respective RGI polygons assembled by Maussion (2017).

3 Open Global Glacier Model (OGGM) and frontal ablation parameterisation

For this study, a simple frontal ablation parametrisation is implemented into the Open Global Glacier Model (OGGM v1.0.1). OGGM is developed to provide a global scale, modular and open source numerical model framework for consistently simulating past and future global scale glacier change. The mathematical framework of the model and its capabilities have been explained in detail by Maussion et al. (2019). In this section, we will only describe the modifications done to the mass-balance and ice thickness inversion modules of OGGM, together with the frontal ablation parametrisation implemented in order to improve the initialisation of the model for marine-terminating glaciers. Sect. 3.3 provides details on the limitation of applying the parameterisation to lake-terminating glaciers.

3.1 Ice thickness

The method of estimating ice thickness from mass turnover and principles of ice-flow dynamics in glaciers was first introduced by Farinotti et al. (2009). The aim is to estimate ice thickness distribution from a given glacier surface topography, which can be achieved assuming that the mass-balance distribution should be balanced by the ice-flux divergence. This method has

been modified in OGGM in order to implement a new ice thickness inversion procedure physically consistent with the flowline representation of the glaciers and taking advantage of the mass-balance calibration procedure of OGGM (see below).

The flux of ice q (m³ s⁻¹) through a glacier cross-section of area S (m²) is defined as:

$$q = uS \tag{1}$$

with u being the average cross-section velocity (m s⁻¹). By applying the well known shallow-ice approximation (Hutter, 1981, 1983; Cuffey and Paterson, 2010; Oerlemans, 1997) and making use of the Glen's ice flow law, u can be computed as:

$$u = \frac{2A}{n+2}h\tau^n\tag{2}$$

with A being the ice creep parameter (which has a default value of $2.4 \times 10^{-24} \text{ s}^{-1} \text{ Pa}^{-3}$), n the exponent of Glen's flow law (default: n=3), h the local ice thickness (m), and τ the basal shear stress defined as:

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$$\tau = \rho g h \alpha$$
 (3)

with ρ the ice density (900 kg m⁻³), gg the gravitational acceleration (9.81 m s⁻²) and α the surface slope (computed along the flowline). Optionally, a sliding velocity u_s can be added to the deformation velocity to account for basal sliding, using the following parametrisation (Oerlemans, 1997; Budd et al., 1979):

$$u_s = \frac{f_s \tau^n}{h} \tag{4}$$

with f_s a sliding parameter (default: 5.7×10^{-20} s⁻¹ Pa⁻³).

Following the approach defined described in Maussion et al. (2019), u and q can be estimated, combining the physics of the ice flow and the mass-balance field of a glacier. If u and q are known, S and the local ice thickness h (m) can also be computed, providing some assumptions about the geometry of the bed and by solving Eq. 1. This equation becomes a polynomial in h of degree 5 with only one root in \mathbb{R}_+ , easily computable for each grid point. The equation varies with a factor 2/3 depending on whether one assumes a parabolic ($S = \frac{2}{3}hwS = \frac{2}{3}hw$) or rectangular (S = hwS = hw, with w being the glacier width) bed shape. The default in OGGM is to use a parabolic bed shape, unless the section touches a neighbouring catchment or neighbouring glacier (ice divides, computed from the RGI). For the last five grid points of tidewater glaciers, the bed shape is also assumed to be rectangular. Singularities with flat areas are avoided since the constructed flowlines are not allowed to have a local slope α below a certain threshold (default: 1.5° , see Maussion et al., 2019).

25 3.2 Mass-balance and ice flux q

OGGM's mass balance model is an extension of the model proposed by Marzeion et al. (2012) and adapted in Maussion et al. (2019), to calculate the mass balance of each flowline grid point for every month, using the CRU climatological series

as boundary condition. The equation governing the mass-balance is that of a traditional temperature index melt model. The monthly mass-balance m_i (kg m⁻² s⁻¹) at elevation z is computed as:

$$m_i(z) = p_f P_i \frac{Solid}{solid}(z) - \mu^* \max \left(T_i(z) - T_{\underline{Melt} \underline{melt}}, 0 \right)$$
(5)

where $P_i^{\rm Solid}$ psolid is the monthly solid precipitation, p_f a global precipitation correction factor, T_i the monthly temperature and $T_{\rm Melt}$ $T_{\rm melt}$ is the monthly mean air temperature above which ice melt is assumed to occur (default: -1°C). Solid precipitation is computed as a fraction of the total precipitation: 100 % solid if $T_i <= T_{\rm solid}$ (default: 0°C), 0 % if $T_i >= T_{\rm tiquid}$ $T_{\rm liquid}$ (default: 2°C), and linearly interpolated in between. The parameter μ^* indicates the temperature sensitivity of the glacier, and it needs to be calibrated: in a nutshell, the MB calibration consists of searching for a 31-year climate period in the past for which the glacier would have been in equilibrium while keeping its modern-time geometry, implying that the mass balance of the glacier during that period in time $m_{31}(t)$ is equal to zero. With , with $m_{31}(t)$ being the glacier integrated mass-balance computed for a 31 yr period centred around the year t (e.g. $t^* = 1962$ for most glaciers in Alaska) and for a constant glacier geometry fixed at the RGI outline's date (e.g. 2009 for the Columbia Glacier). It ean should be noted that the mass balance calibration in OGGM excludes MB measurements from tidewater glaciers as reference data, for reasons described below.

This "equilibrium mass-balance" $(m_{31}(t))$ is then assumed to be equal to the "apparent mass-balance" $(\tilde{m} = \dot{m} - \rho \frac{\partial h}{\partial t})$ as defined by Farinotti et al. (2009), where the flux of ice q through a glacier cross-section catchment area (Ω can be) is defined as:

$$q = \int_{\Omega} (\dot{m} - \rho \frac{\partial h}{\partial t}) dA = \int_{\Omega} m_{31} dA \tag{6}$$

If the glacier is land-terminating, $\int m_{31} = 0$ by construction (a property which is used to calibrate μ^* in Eq. 5). q is then obtained by integrating the equilibrium mass-balance m_{31} along the flowline(s). q starts at zero and increases along the major flowline, reaches it's maximum at the equilibrium line altitude (ELA) and decreases towards zero at the tongue (Maussion et al., 2019).

However, this assumption does not hold for tidewater glaciers, where a steady state implies that:

$$\int m_{31} = F_{calving} \tag{7}$$

Where $F_{calving}$ is the frontal ablation of the glacier in mmyr⁻¹. A more precise definition would be that $F_{calving}$ is the average amount of ice that passes through the glacier terminus in a MB year for a glacier in equilibrium with climate forcing. This has direct consequences for the calibration of temperature sensitivity parameter μ^* . With all other things kept equal, two otherwise identical glaciers (a calving, one calving, one non-calving) will have a different to have different temperature sensitivities μ^* : the calving glacier will have a lower μ^* , resulting in a lowered Equilibrium Line Altitude (ELA), a positive

surface mass budget, and finally to a mass flux through the terminus. $F_{calving}$ can be understood as the frontal ablation of the glacier at equilibrium, that allows. The objective here is to allow the model to grow a calving front, with the goal of improving the glacier thickness inversion computed by OGGM.

3.3 Frontal ablation parameterisation

To account for frontal ablation of marine-terminating marine-terminating glaciers we employ a calving law proposed by Oerlemans and Nick (2005) and already applied at larger scale by Huss and Hock (2015). The annual frontal ablation $F_{calving}$ is computed as a function of the height (H_f) , width (w) and estimated water depth (d) of the calving front as:

$$F_{calving} = max(0; kdH_f) \cdot w \tag{8}$$

where k is a calibration parameter (set to 2.4 yr⁻¹ by Oerlemans and Nick, 2005).

 H_f is unknown *a priori*. Assuming for now that we know the area A_t of the terminus glacier cross-section (see Sect. 3.4 for how we obtain an estimate), we can simply infer:

$$H_f = \frac{A_t}{w} \tag{9}$$

assuming a rectangular bed shape. The water depth (d) is estimated from free-board, using elevation and ice thickness data obtained from the model output:

$$15 \quad d = H_f - E_t \tag{10}$$

Where E_t is the elevation of the glacier terminus. For surface at the terminus. Here, the water depth (d) is estimated using the terminus elevation (E_t) obtained by projecting the RGI outline to the DEM (i.e., the terminus elevation is the top of the cliff). We follow the same definition as Oerlemans and Nick (2005) where d is the bed elevation with respect to sea level. For lake-terminating glaciers, one would have to take into account the altitude of the lake above sea levelto estimate the water depth: for glaciers, we are not able to estimate a water depth since one would need to know the free-board of the glacier terminus, i.e. the elevation of the glacier lake surface (for the elevation of the ocean surface, we assume that it is 0 m a.s.l.). For this reason, most of our experiments and results focus on marine-terminating marine-terminating glaciers only, with the exception of the experiment presented in section 4.2.

3.4 Iterative calibration procedure

25 $F_{calving}$ is then converted to units of specific MB mmyr⁻¹ before being pass to Eq.7.

3.4 Iterative calibration procedure

The ice thickness calculation depends on estimates of frontal ablation, but frontal ablation is also a function of the ice thickness itself. In order to solve this problem, we implement an iterative method as follows:

- 1. Using the ice-thickness estimation module of OGGM, we estimate an initial glacier thickness distribution without adding a frontal ablation estimate (i.e.: we set $F_{calving} = 0$ in the MB Eq. 7).
- 2. Then we assume that the glacier has an initial calving front height thickness of $H_f = \frac{E_t}{E_t} d_0 + E_t$. With d_0 being the the initial water depth (set to 1/3 of the terminus elevation (E_t) as default). From this, a "first guess" frontal ablation is calculated following Eq. 8, 9 and 10 (see Sect. 3.5 for test results with different starting water depths).
- 3. We add the $F_{calving}$ from step 2 to the MB equation (Eq. 7) and a new glacier thickness distribution and H_f is computed . This H_f is far smaller than according to the physics of ice flow (Sect. 3.1). At this point we are unaware of the real thickness of the calving front, but H_f is large enough to initiate the iterative process that follows.
- 4. From the H_f obtained in step 3, we calculate again a new estimate of $F_{calving}$ (Eq. 8, 9 and 10), add it to the MB equation (Eq. 7) and compute a new glacier thickness distribution and H_f . This step repeats itself until the frontal ablation converges (convergence is reached when the difference between the last two computed $F_{calving}$ is less than $0.05 0.01 \text{ km}^3 \text{ yr}^{-1}$). For most glaciers, convergence occurs between the 4th and 6th iteration step (see Sect 3.5 for an explanation of the convergence of the method).
 - 5. Finally, we compute the definitive glacier ice thickness distribution and volume from the $F_{calving}$ obtained in step 4.
- Based on this procedure, the single free parameter that changes at each iteration is the temperature sensitivity μ^* , which changes in order to accommodate for the growing frontal ablation flux ($F_{calving}$). As explained in Sect. 3.2, μ^* should however not be understood only as a simple tuning parameter: for a frontal ablation flux to exist, the surface mass-balance must be unbalanced, and the local climate must allow this imbalance to occur.

In most of the cases, it is possible to find a realistic μ^* compatible with a frontal ablation flux (e.g. The LeConte Glacier, Fig. 5 a and b). There are however some exceptions: sometimes μ^* gets close to zero without converging (in other words: even without glacier melt, the total accumulation over the glacier is too small to close the frontal mass budget). This can be due to two equally likely main factors: solid precipitation is underestimated, or the frontal height and therefore frontal ablation is overestimated. When this occurs, we stop the iteration when μ^* reaches zero . Finally, $F_{catving}$ is also set to zero if the first water depth estimate from free board returns a negative value (e.g. Fig. 5 c and d).

25 3.5 Idealised experiments on the LeConte Glacier

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In this section we use the LeConte Glacier (see Fig. 3) as a test case to illustrate the stability and convergence of the parameterisation and the iterative procedure. Fig 3b shows the result of the model's default ice thickness inversion procedure, which assumes an ice flux of zero at the terminus ($F_{calving} = 0$). Note that by default, the ice thickness is zero at the glacier front.

First we examine how the frontal ablation flux from the calving law (Eq. 8) would change if we increase the terminus ice thickness of the glacier, while keeping the free-board fixed (E_t is the only variable known in Eq. 10 "with certainty", from the DEM surface elevation at the terminus). Fig. 4a shows that the flux remains equal to zero as long as H_f is not thick enough to

reach water, after which the water depth is positive and calving occurs. $F_{calving}$ varies with H_f as a polynomial of degree 2. At this point, we are unaware of the real frontal ablation for this glacier, but we make some very coarse assumptions:

- Oerlemans and Nick (2005) calving law is perfectly exact.
- The tuning parameter k is known.

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- Our glacier is in equilibrium with climate (we assume mass-conservation inversion in OGGM).
 - Ice deformation at the glacier terminus follows Glen's flow law.

Under these assumptions, we set up a new experiment where we compute a frontal ablation flux (from the calving law, Eq.8) for a range of prescribed frontal ice thicknesses (see Fig. 4b, blue line), then give this flux back to the OGGM inversion model (Eq. 7), which will use this flux to compute a frontal ice thickness according to the physics of ice flow (see Sect. -5 for an explanation of why negative water depthvalues occur3.2 and Fig. 4b, orange line). As shown in Fig. 4b, there is a unique value for the frontal thickness (H_f) that complies with both the calving law and the ice thickness inversion model of OGGM. The calving law from Eq. 8 relates the ice thickness (H_f) to the flux with a root of degree two (blue curve of Fig. 4b). But for the orange curve in Fig. 4b, it is Glen's flow law, which relates the ice thickness to the flux with a 5th degree root (assuming n = 3). This illustrates why (under our simplified framework) there is one (and only one) non-zero solution to the problem of finding a frontal ablation flux. Note that changing Glen's deformation parameter A or adding sliding does not change the problem qualitatively: we will still solve a polynomial degree 5 in OGGM, with a new term in degree 3 (see green curve in Fig. 4b).

There are several ways to find this "optimal $F_{calving}$ " (or optimum frontal ice thickness), where mass-conservation inversion and the calving law are compatible. Fig. 5 illustrates the iterative procedure applied to the LeConte Glacier, where convergence is reached when the OGGM flux equals the calving law flux within 0.01 % (see Fig. 5a). Thanks to the uniqueness of the solution, the method always converges regardless of the starting water depth, as shown in Fig. 4c.

However, for some glaciers the frontal ablation flux given by the calving law is larger than a flux that can be explained by climate alone, i.e. even without melt, the computed flux is larger than the total accumulation over our glacier. During these conditions our iterative search can "overshoot". Fig. 5c, simulates this case where we set an unrealistically large calving parameter (k equal to 10 yr^{-1} in this experiment). If this happens during the iteration, OGGM is going to set μ^* to zero and compute the corresponding flux (the maximal physically possible value, see Fig. 5d).

4 Results

We apply this frontal ablation parameterisation to all marine-terminating glaciers in Alaska. We study the impact of including this parameterisation on the estimated glacier thickness, volume and ice flow velocity. The following sections describe different sensitivity experiments: i) varying the frontal ablation flux added to the MB model and assessing the impact on glacier volume, ii) varying several model parameters (Glen's flow law ice creep parameter A, a sliding parameter f_s , and the calving constant

of proportionality k) and assessing each parameter's impact to the regional frontal ablation of Alaska, and iii) show the impact of different model configurations to the total volume of Alaska marine-terminating marine-terminating glaciers.

4.1 Case study: Columbia Glacier

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The Columbia Glacier located in south-central Alaska, is likely the most studied tidewater glacier in the world. With a detailed record of its retreat since 1976, it is the single largest contributor of the Alaska glaciers to sea-level rise (Berthier et al., 2010). The ice flow, ice discharge and tidewater retreat of the glacier are all extensively documented, providing rich insight into the underlying processes that modulate tidewater glacier behaviour and stability (Mcnabb et al., 2012). These reasons motivated the selection of the Columbia Glacier as an exemplary study site to illustrate our results for an individual glacier, while the goal of our approach is the ability to improve the model representation of any calving glacier.

Following the iterative process described in section 3.33.3 and 3.4, we calculate a virtual frontal ablation for the Columbia Glacier of $\frac{12.9}{2.98}$ km³ yr⁻¹ ($\frac{11.8}{2.73}$ Gt yr⁻¹). This flux represents the estimated amount of ice passing through the terminus of the glacier, if the glacier was in equilibrium with the climate for a constant glacier geometry fixed at the RGI outline's date (e.g. 2009 for this glacier). This estimate was obtained using the model's default values for the parameters k, k and k are k and k and k and k and k and k are k and k and k and k and k are k and k and k are k are k and k are k and k are k and k are k are k and k are k and k are k are k and k are k and k are k are k are k are k and k are k and k are k are k and k are k and k are k are k are k and k are k are k are k are k and k are k are k and k are k are k and k are k and k are k and k are k and k are k are

When computing the ice thickness distribution map of the glacier, the impact of accounting for frontal ablation is mainly reflected in the two adjacent branches of the Columbia Glacier (Fig. 37b) and at the glacier terminus (Fig. 37c). An overview of the glacier main centreline profile is shown in Fig. 37c, together with the 2007 thickness map published by Mcnabb et al. (2012), a study that provided a reconstructed bed topography and ice thickness, based on velocity observations of the Columbia Glacier and mass conservation.

By accounting for frontal ablation in OGGM's MB and thickness inversion modules, we can compute a bedrock profile closer to the 2007 bed map, especially close to those points located at the terminus of the glacier. The frontal ablation parameterisation allows OGGM to grow a thick calving front at the glacier terminus. Additionally, we observe that both bed estimations from OGGM (grey and black lines, Fig. 37c) diverge primarily below sea level.

4.2 Frontal ablation and glacier volume

In this experiment, we assign a frontal ablation flux ranging from $0 - 5 \text{ km}^3 \text{ yr}^{-1}$ to each glacier classified as calving in the RGI v6.0, keeping the model's default values for the parameters A and f_s . The aim is to calculate the changes in volume for each glacier per frontal ablation value, while keeping the rest of the aspects that control the volume of the glacier the same (e.g. solid precipitation, outline, topography, basal sliding). As a result of the automated workflow of OGGM, we are able to

calculate the changes in volume of all 198 calving glaciers in Alaska², for each value in the frontal ablation flux range. The results of this experiment are shown in Fig. 47.

The impact of accounting for frontal ablation in the glacier volume estimate depends on the glacier size and the frontal ablation value. Glaciers with a small volume are more sensitive to large frontal ablation fluxes added to their mass balance, almost doubling their volume for fluxes values ranging between 0 and 1 km³ yr⁻¹. While larger glaciers (volume \geq 100 km³) only experience an increment in volume of $\frac{2010\%}{100}$ to 30% their initial volume without accounting for frontal ablation, for flux values ranging between 1 and 5 km³ yr⁻¹ (Fig. 47a).

Additionally, we look at the temperature sensitivity μ^* of each glacier per frontal ablation flux value (Fig. 47b). Eq. 5 and 7 indicate that a value of $\mu^* \leq 0$, would imply that the glacier is producing a frontal ablation larger than its annual accumulation $(p_f P_i^{Solid}(z))$. To prevent this effect, we clip μ^* to zero, setting a physical limit to the frontal ablation of each individual calving glacierand, explaining the rapid drop of the temperature sensitivity μ^* of small glaciers in Fig. 47b.

4.3 Effect of frontal ablation on ice velocity

To analyse the effect of frontal ablation on ice velocity, we keep the same model configuration (default values of k, A and f_s) and calculate the average ice velocity along the main flowline for all marine-terminating glaciers that produced a frontal ablation flux. Fig. 5–8 shows the difference between the average velocity output of the model when accounting for frontal ablation and without accounting for frontal ablation. When taking frontal ablation into account, the glaciers experience an increase in ice velocity towards the terminus. This increase of velocities is due to an increase of the mass flux (and therefore ice thickness) when we account for frontal ablation.

These results highlight the importance of applying a frontal ablation parameterisation at the initialisation stages of the model in order to recreate a realistic tidewater glacier behaviour. Without this extra term on the mass balance, velocities go to zero towards the terminus. Note that while using OGGM for forward model runs (either reconstructing or projecting glacier change) it could be possible to rely on the ice velocities determined by the model to compute a simple frontal ablation (e.g. surface velocities across a cross section of the glacier located upstream of the terminus, Burgess et al., 2013; McNabb et al., 2015), this is not the case for the initialisation and first ice thickness inversion procedure.

25 4.4 Sensitivity studies in Alaska marine-terminating glaciers

We perform different sensitivity experiments to study the influence of i) the calving constant of proportionality k, ii) Glen's temperature-dependent creep parameter A and iii) sliding velocity parameter, on the regional frontal ablation of Alaska. The results of these experiments are shown in Fig. 69. In the first experiment we vary the calving constant of proportionality k in a range of $0.24 - 2.52 \text{ yr}^{-1}$ and used the model default values for Glen A and sliding parameter. Fig. 69a shows that our estimate for the regional frontal ablation matches the regional estimate by McNabb et al. (2015) if k has an approximated value of 0.61

²Only in this section we include lake-terminating glaciers in the experiments, because we are not calculating a frontal ablation flux but assigning a specific value to the mass-balance equation (Eq. 7).

³Note that these velocities are not surface velocities but velocities computed from ice flux divided by the glacier cross-section.

 0.63 yr^{-1} , in the case of excluding sliding ($f_s = 0$), or if k is equal to $0.70 \cdot 0.66 \text{ yr}^{-1}$ in the case of including a sliding velocity (with $f_s = 5.7 \times 10^{-20} \text{ s}^{-1} \text{ Pa}^{-3}$). It is important to emphasise emphasize that the regional frontal ablation from McNabb et al. (2015) only comprises of 27 glaciers but that they represent an estimated 96% of the total frontal ablation of Alaska.

We then keep these two values of k and vary the values of Glen A creep parameter and sliding parameter (f_s) . The results are shown in Fig. 6.9 b and c. It is well known that ice flow models are sensitive to the values chosen for parameters describing ice rheology and basal friction (e.g. Enderlin et al., 2013; Brondex et al., 2017). As expected, our frontal ablation estimates are also sensitive to different values of Glen k and sliding velocity, but highly dependent on different values of k, mainly as at least for the first part of the k values range $(0.24 - 0.80 \text{ yr}^{-1})$. The linear relationship between k values k at the beginning of Fig. 9a is mainly a consequence of the calving law used in the parameterisation. For larger k values k values k values of the curve is due to OGGM's physical constraint of clipping k to zero and calculating the maximum k allowed by the local climate (see Sect. 3.5 and Fig. 5 c, d).

Maussion et al. (2019) showed that both sliding and ice rheology (A) have a strong influence on OGGM's computed ice volume, hence a strong influence on the thickness of the glacier and in this case the frontal ablation estimate. Like in Maussion et al. (2019); Fig. 6.9 shows that one could always find an optimum combination of Glen A and sliding parameters that lead to (in this case) previously calculated frontal ablation estimates. Enderlin et al. (2013) also showed that when such flowline models are applied to a tidewater glacier, there is a non-unique combination of these parameter values that can produce similar stable glacier configurations, making k, Glen A and f_s parameters highly dependent on observations of either frontal ablation, ice velocity or glacier ice thickness.

4.5 Regional volume of marine-terminating marine-terminating glaciers for different model configurations

Finally, we compute the total volume of marine-terminating marine-terminating glaciers for different "equally good" parameter sets based on the results of Fig. 69 a, b. A summary of the different parameter sets used for each model run can be found in Table 1 and the results of each configuration are shown in Fig. 710. Each configuration was run twice: once setting $F_{calving} = 0$, then a second time accounting for frontal ablation.

Similarly to the results shown in sections 4.1 and 4.2, Fig. 7–10 shows that there are significant differences between total volume estimates without accounting for frontal ablation (blue bars) and total volume estimates after and with accounting for frontal ablation (green bars). Volume estimates after accounting for frontal ablation are $\frac{15 \text{ to } 1714 \text{ to } 16\%}{10\%}$ higher than the volume estimates ignoring frontal ablation, considering all model configurations shown in Table 1, indicating a robust relationship. We find that there are no significant differences between the resulting volumes for different k values and that the differences in volume estimates between configurations are mainly due to adding or ignoring a sliding velocity or varying the value of Glen A creep parameter.

Additionally, we also calculate the regional ice volume below sea level. The results for the Columbia Glacier discussed in section 4.1 might create the impression that the differences in thickness along the main centerline, before and after with and without accounting for frontal ablation, are not relevant for the potential glacier contribution to sea level sea-level rise, since most of the differences in thickness (grey and black line in Fig. 37c) are found below sea level. However, Fig. 7-10 shows

that considering the whole region, a significant fraction of the total volume difference is found above sea level, implying that accounting for frontal ablation will directly impact the estimate of these glacier's contribution potential to sea-level rise. By introducing frontal ablation, we increase the volume estimate of marine-terminating glaciers in Alaska from $9.01-9.31 \pm 0.35$ 0.37 to an average of $10.43-10.75 \pm 0.44-0.39$ mm SLE, of which $1.42-1.53 \pm 0.17-0.07$ mm SLE are found to be below sea level (instead of only $0.58-0.60 \pm 0.05-0.03$ without)⁴.

5 Discussion

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We have shown that our the model is capable of computing regional frontal ablation estimates by tuning model parameters with published regional-scale estimates of frontal ablation, but the question of model performance for individual glaciers still remains open. In areas with no observational data or previous knowledge of frontal ablation, OGGM could make use of physical constraints (e.g. that μ^* must be greater than zero) as well as bathymetry and terminus width estimates to calibrate the model at the glacier scale. In the following section, we will explain such calibration and calibrations, discuss other parameters that affect frontal ablation estimates and discuss these estimates for individual glaciers.

In all previous model runs, we used the standard OGGM terminus geometry computation without correcting the width and water depth at the glacier front using potentially known values from other sources. As a result, not all of the glaciers classified as marine-terminating glaciers are able to in the RGI produce a frontal ablation flux in OGGM. This is mainly due to a constraint in the frontal ablation parameterisation, in which wrong estimation of the water depth from free-board. These glaciers typically have a high terminus elevation (e.g. $E_t = 130$ m.a.s.l for the Grand Pacific Glacier, RGI60-01.26732), for which the only possible value of $F_{calving}$ is set to zero if the first water depth estimate from free board returns a negative value. This can that complies with both the calving law and the ice thickness inversion model of OGGM is a $F_{calving} = 0$, since there is not enough mass turnover to grow a calving front under our mass conservation assumptions (see Sect. 3.5). The wrong water depth estimation can thus be best be explained by a poor DEM resolution surface altitude estimation at the calving front (e.g., corresponding to a different year than the RGI outline of the glacier), leading to wrong estimate of the terminus altitude E_t . The problematic surface altitude estimation in turn can probably be explained by a mismatch between the acquisition dates of the DEM and and the glacier outline.

Maussion et al. (2019) noted that a number of glaciers will suffer from poor topographic information, especially those located in the high latitudes. Most marine-terminating glaciers are located in regions where cloud free satellite measurements are difficultrare. Therefore, the DEM of these regions might present errors that will spread to water depth estimations from free-board (see Eq. 10). The possibility of using higher resolution DEM's such as the ArcticDEM was explored during this study but was quickly eliminated because of large data voids present on the data, especially for big glaciers (e.g. Hubbard Glacier). However, new data sets such as the TanDEM-X (Wessel et al., 2018) are currently being explored for future versions of OGGM.

⁴The uncertainties presented here are the standard deviation of the model configurations shown in Tab. 1.

For 36 marine-terminating glaciers, we assess the model performance in comparison to the estimates by McNabb et al. (2015), with and without corrections for these errors (Fig. 8).

11). Calving front widths were corrected with the Alaska Tidewater Glacier Terminus Positions database (McNabb and Hock, 2014). The database contains terminus positions for 49 marine-terminating glaciers. Since three of these glaciers (Grand Pacific, Hubbard and Sawyer Glacier) were merged with their respective pair branches (Ferris, Valerie and Sawyer western Glacier), we are left with a total of 46 glacier terminus widths. The widths are computed by selecting the terminus positions closest to the glacier's RGI outline and by averaging the widths that resulted from the projection of the vector lines selected. These widths are used to correct OGGM's flowline width at the calving front in the cases where the model is not able to represent the real calving front width. The last flowline width of the glacier is then clipped to the width value estimated from the database. To smooth the transition between the clipped value and OGGM's flowline width; we linearly interpolate between the clipped value and 5 pixels upstream on the flowline. We then correct the modified widths to preserve the same glacier area than the RGI's. By doing this, we slightly modify the altitude-area distribution of the glacier.

In addition Additionally, multi-beam bathymetry data from NOAA National Centers for Environmental Information (2004) was used to estimate the water depth in front of the glacier terminus. This data was used only for glaciers where the DEM's resolution would not allow an estimate of the water depth from elevation data and ice thickness (free-board). The bathymetry data was compiled into a raster format and provided to us by Robert McNabb (pers. comm.). Both corrections were used for Fig. 8-11 only.

Fig. 8–11 demonstrates that without calibrating any OGGM parameter (only using the model default values for Glen A, f_s and k), but making use of additional data (e.g. terminus positions and bathymetry), we are able to estimate a frontal ablation flux for individual glaciers within the same order of magnitude as those estimated by McNabb et al. (2015). We reduce the model Root Mean Square Error The model root mean square error (RMSE) from 4.89 is reduced from 1.08 km³ yr⁻¹ (mean deviation of 1.251) to 0.63-0.30) to 0.53 km³ yr⁻¹ (mean deviation of -0.0470.11). Even though part of these errors may arise from the fact that glaciers are in a disequilibrium state at the time of the McNabb et al. (2015) estimate, errors in boundary conditions (e.g., topography date not coinciding with the glacier outline date and uncertainties in the frontal width) and plain model errors may also contribute. By using bathymetry and real terminus width estimates we improve the boundary conditions of the parameterisation that are highly dependent on the DEM's quality.

When these corrections (terminus width and water depth) are not implemented and errors occur while estimating the real terminus geometry, OGGM has to rely on clipping μ^* to be larger than or equal to zero, setting a physical limit where the frontal ablation flux for each individual tidewater glacier cannot be larger than its annual accumulation ($p_f P_i^{Solid}(z)$). This is not ideal, because it implies that all of the glacier's ablation in an equilibrium setting is due to frontal ablation and nor-no surface melt occurs, which is unrealistic in the climate conditions of Alaska. For applications on the global scale, bathymetry data and terminus mapping will be very valuable in regions with poor topographic resolution and where no observations of frontal ablation exist.

6 Conclusions

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We have implemented a frontal ablation parameterisation into OGGM and shown that inversion methods ignoring frontal ablation systematically underestimate the mass flux and thereby the thickness of calving glaciers. Accounting for frontal ablation in ice thickness inversion methods based on mass conservation (as listed in Farinotti et al., 2017) increases estimates of the regional ice mass stored in marine-terminating marine-terminating glaciers by approximately 15 to 17-14 to 16 %. While for individual glaciers, ice volume may be underestimated by up to 4730% when ignoring the impact of frontal ablation, the effect strongly depends on the size of the glacier. Implementing a frontal ablation parameterisation allows OGGM to represent a non-zero thickness calving front, which is necessarily the case when no ice flux is assumed to cross the glacier terminus. This parameterisation is key for initialising the glacier's thickness in the model.

The model was able to reproduce previously calculated regional frontal ablation estimates by finding the best combination of values for k, Glen's A and the sliding parameters. Note that this comparison is limited by the equilibrium condition imposed on OGGM during initialisation, which is not the case in observations. The best-performing parameter set for transient runs of OGGM may be different.

Our sensitivity studies also show that the differences in thickness (between adding or not frontal ablation to the MB model) occur mainly at the lower parts of the glacier, but often above sea level. This indicates that not accounting for frontal ablation will have an impact on the estimate of this glacier's potential contribution to sea-level rise.

Additionally, our experiments highlight the need for bathymetry data and terminus mapping, as they may constrain model parameters when the DEM's quality is not sufficient to provide an realistic estimate of the terminus geometry.

Code availability.

The OGGM software together with the frontal ablation parameterisation module are coded in the Python language and licensed under the GPLV3 free software license. The latest version of the OGGM code is available on Github (https://github.com/OGGM/oggm), the documentation is hosted on ReadTheDocs (http://oggm.readthedocs.io), and the project webpage for communication and dissemination can be found at http://oggm.org. The code for the frontal ablation parameterisation module is available on Github ()and data used to generate all figures and analyses of this paper can be found at https://github.com/ bearecinos/cryo_calving_2019. The OGGM version used for this study is available in a permanent DOI repository (https://doi.org/10.5281/zenodo.2580277).

Author contributions.

BM and FM are the initiators of the OGGM project and conceived this study. BR is the main developer of the frontal ablation parameterisation module and wrote most of the paper. FM is the main OGGM developer and was largely involved with the development of the frontal ablation parameterisation module. TR made significant contributions to the OGGM code and the

frontal ablation parameterisation module and is responsible for the successful deployment of the code on supercomputing environments.

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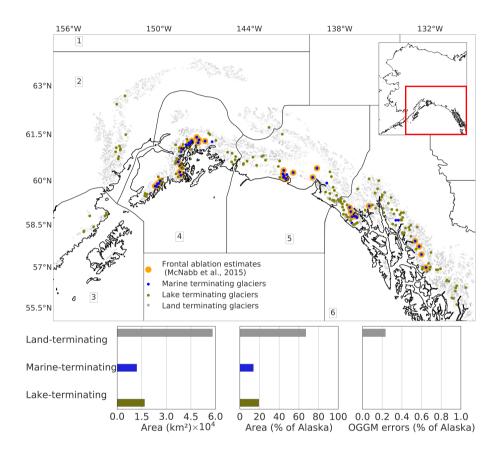


Figure 1. Upper panel: map of the RGI sub-regions of Alaska; the dots indicate the location of glaciers classified as land- (grey dots), lake- (olive dots) and marine- (blue dots) terminating in the Randolph Glacier Inventory (RGI v6). Yellow dots indicate the location of the glaciers from which there are frontal ablation estimates (McNabb et al., 2015). **Lower panel:** region regional glacier types and basic statistics of the database (area of glaciers per terminus type, regional contribution to the Alaska area in percent, and percentage of the regional area which cannot be modelled by OGGM).

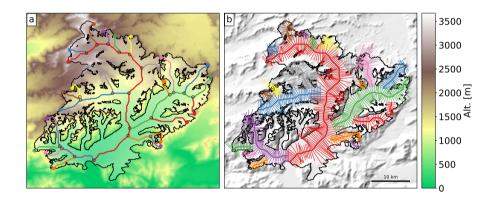


Figure 2. Columbia Glacier model workflow; **a:** topographical data preprocessing and computation of the flowlines; **b:** width correction according to catchment areas and altitude-area distribution.

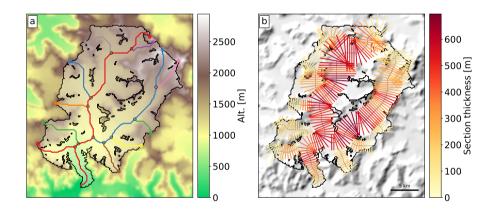


Figure 3. LeConte Glacier model workflow; **a:** topographical data preprocessing and computation of the flowlines; **b:** thickness distribution before accounting for frontal ablation.

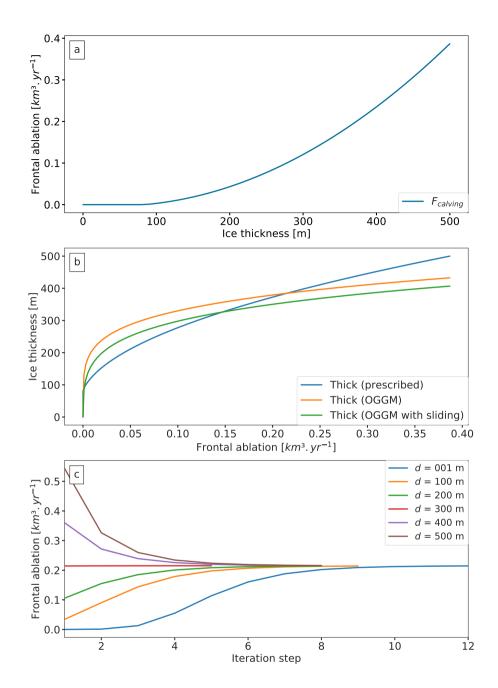


Figure 4. Idealised experiments applied to the LeConte Glacier. **a:** Frontal ablation flux computed by the calving law when prescribing a terminus thickness, with H_f ranging from 0 to 500 m. **b:** Terminus ice thickness per frontal ablation flux obtained; i) by the calving law (blue curve, same as **a**), ii) by OGGM using the iterative procedure (orange curve) and iii) by OGGM using the iterative procedure and adding a sliding velocity (green curve). **c:** Frontal ablation fluxes calculated using the iterative procedure but from different starting points; the different colors represent different water depths at the beginning of the iteration procedure d_0 .

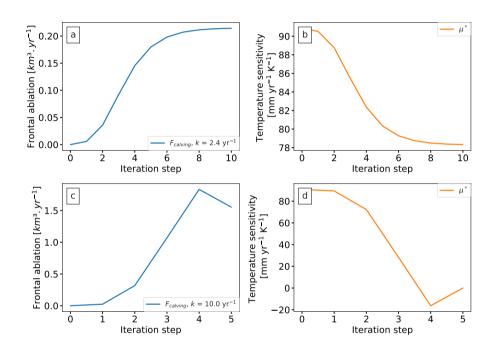


Figure 5. Iterative calibration procedure applied to the LeConte Glacier. **a:** Frontal ablation flux at each iteration step with $k = 2.4 \text{ yr}^{-1}$. **b:** Temperature sensitivity μ^* of the glacier at each iteration step with $k = 2.4 \text{ yr}^{-1}$. **c:** Frontal ablation flux at each iteration with $k = 10 \text{ yr}^{-1}$. **c:** Temperature sensitivity μ^* of the glacier at each iteration step with $k = 10 \text{ yr}^{-1}$.

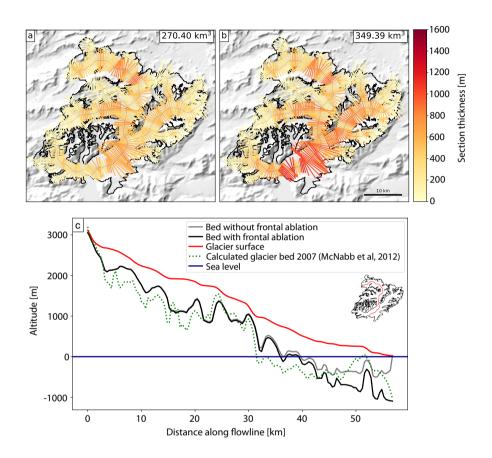


Figure 6. Ice thickness inversion results for the Columbia Glacier; **a:** thickness distribution before accounting for frontal ablation; **b:** thickness distribution after accounting for frontal ablation, with a frontal ablation flux computed by the model of $\frac{12.9}{2.98}$ km³ y⁻¹; **c:** Columbia Glacier main centreline profile, comparison between the 2007 estimated bed map (green doted line) from (Menabb et al., 2012) Menabb et al. (2012) and model output before accounting for frontal ablation (grey line) and after accounting for frontal ablation (black line).

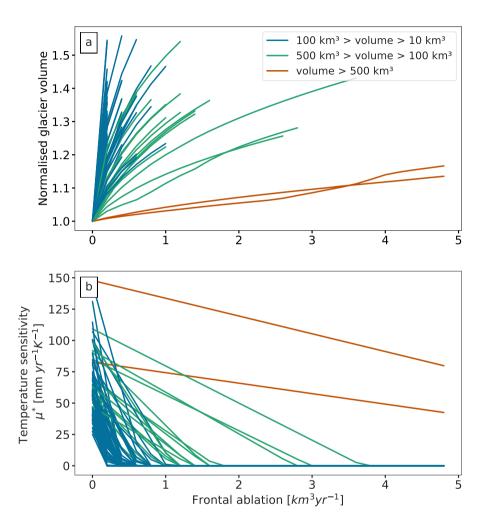


Figure 7. a: Normalised glacier volume as a function of prescribed frontal ablation; b: temperature sensitivity (μ^*) of individual glaciers, computed with different frontal ablation fluxes. The different colors represents different glacier sizes.

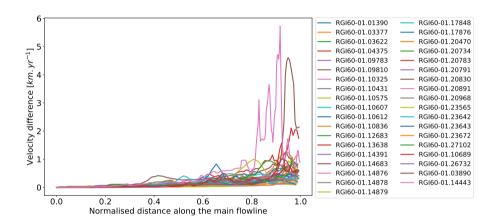


Figure 8. Glacier average velocity differences between the two outputs of the model for a subset of marine-terminating glaciers. The differences are between the model output before accounting for frontal ablation and after accounting for frontal ablation in points along the main flowline. The x-axis has been normalised.

Total frontal ablation of Alaska marine-terminating glaciers computed with varying OGGM parameters. The dashed dark line indicates the Alaska regional frontal ablation calculated by McNabb et al. (2015), light gray shading indicating the standard errors as provided in the study, at ealying constant of proportionality (k); bt Glen A parameter, the coloured dashed lines represent zero sliding; et sliding parameter

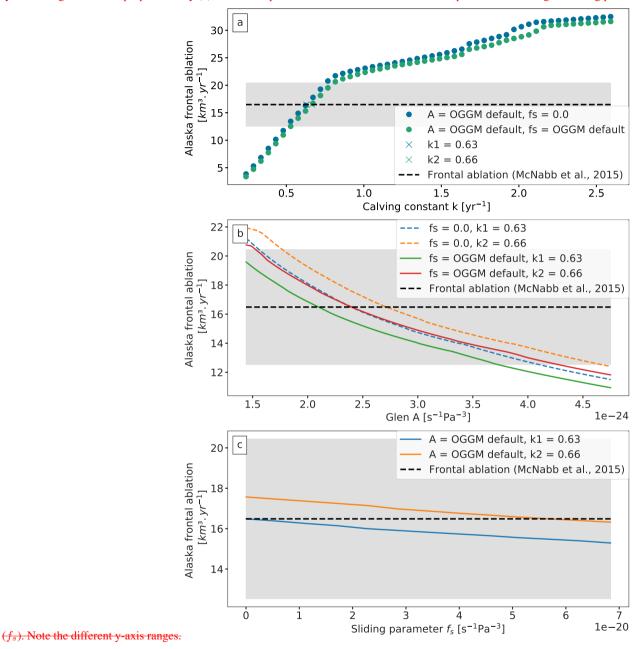


Figure 9. Total frontal ablation of Alaska marine-terminating glaciers computed with varying OGGM parameters. The dashed dark line indicates the Alaska regional frontal ablation calculated by McNabb et al. (2015), light gray shading indicating the standard errors as provided in the study. **a:** sensitivity on calving constant of proportionality (k); **b:** sensitivity on Glen's A parameter, the coloured dashed lines represent zero sliding; **c:** sensitivity on sliding parameter (f_s) . Note the different y-axis ranges.

Total volume of Alaskan marine-terminating glaciers before (blue) and after (green) accounting for frontal ablation and the total volume below sea level (red) before and after accounting for frontal ablation. The descriptions for each model configuration can be found in Table

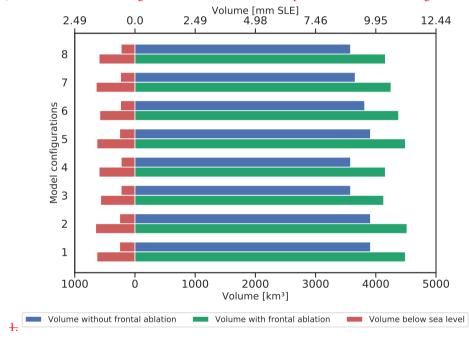


Figure 10. Total volume of Alaskan marine-terminating glaciers above sea level before (blue) and after (green) accounting for frontal ablation, and the total volume below sea level (red) before and after accounting for frontal ablation. The descriptions for each model configuration can be found in Table 1.

Comparison of OGGM F_a estimates (blue and green) to 36 frontal ablation estimates computed by (McNabb et al., 2015) (red). Both OGGM estimates were calculated using default values of k, A and f_s and correcting the width and water depth at the calving front (green). Hubbard Glacier (RGI60-01.14443) is off scales if no corrections are applied to the width and depth of the calving front

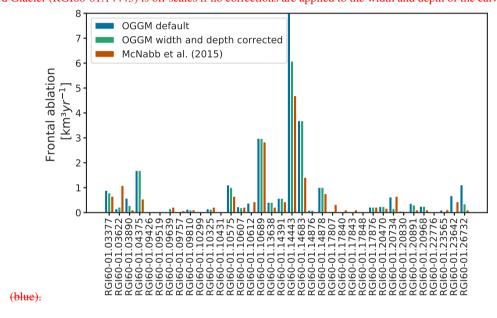


Figure 11. Comparison of OGGM F_a estimates (blue and green) to 36 frontal ablation estimates computed by (McNabb et al., 2015) (red). Both OGGM estimates were calculated using default values of k, A and f_s and correcting the width and water depth at the calving front (green). Hubbard Glacier (RGI60-01.14443) is off scales if no corrections are applied to the width and depth of the calving front (blue).

Table 1. Different model configurations applied to marine-terminating glaciers of Alaska.

Experiment number	Calving constant k [yr ⁻¹]	Glen A creep parameter $[s^{-1} Pa^{-3}]$	Sliding parameter f_s [s ⁻¹ Pa ⁻³]
1	0.61 -0.63	default	no sliding, $f_s = 0.0$
2	0.70 <u>0.66</u>	default	no sliding $f_s = 0.0$
3	0.61 -0.63	default	default
4	0.70 <u>0.66</u>	default	default
5	0.61-0.63	2.34 2.40 ×10 ^{−24}	no sliding, $f_s = 0.0$
6	0.70 0.66	$\frac{3.33}{2.72} \times 10^{-24}$	no sliding, $f_s = 0.0$
7	0.61-0.63	$\frac{1.61}{2.10} \times 10^{-24}$	default
8	0.70 <u>0.66</u>	$\frac{2.33}{2.40} \times 10^{-24}$	default

OGGM default values for Glen A = $2.4\times10^{-24}~\rm s^{-1}~Pa^{-3}$ and f_s = $5.7\times10^{-20}~\rm s^{-1}~Pa^{-3}$