

## 1 General remarks

We would like to thank all reviewers for the reading of the manuscript and for their thoughtful and very constructive comments. In particular addressing the sensitivity of the model and questioning the individual parameter choices has led to some interesting results. In the following, reviewer comments are printed in blue and manuscript excerpts are printed in grey. A texdiff-file is also provided for the revised manuscript. Also, I provide all figures from the Supplement at the end of this document. I will answer all points individually further below, but before that I would like to introduce some modifications of the dEBM, which were a side product of the revision process.

1.) I realized, that the minimum solar elevation angle was based on an incorrect estimate of the solar flux density at the surface ( $\tau\widehat{S}_r = 600 \text{ W m}^{-2}$ .) Upon closer inspection I could identify the error in the calculation and corrected this to  $\tau\widehat{S}_r = 800 \text{ W m}^{-2}$ , which results in a smaller minimum elevation angle of  $\Phi = 17.5^\circ$ .

2.) Analysing hourly PROMICE data, I found that  $PDD_{\sigma=3.5}$  better represents melt period temperatures than  $PDD_{\sigma=5}$  (approximated with a constant standard deviation of  $\sigma = 3.5^\circ\text{C}$  instead of  $\sigma = 5^\circ\text{C}$ ).

All experiments and analyses have been repeated, using  $PDD_{\sigma=3.5}$  and minimum elevation angle  $\Phi = 17.5^\circ$ . We found that these corrections don't change the results qualitatively.

Furthermore we have included a section on the sensitivity of the scheme in the main manuscript. Depending on the editors decision this may as well be moved to the supplement:

## 2 Sensitivity to model parameters and boundary conditions

**Sensitivity to tuning parameters:** In the above application, the parameter  $\beta$  for sensible heat and the background melting condition  $T_{min}$  have served as tuning parameters. The parameter  $\beta = 10 \text{ W m}^{-2} \text{ K}^{-1}$  was determined by optimizing the scheme to MAR melt rates. This value agrees reasonably well with the moderate wind speeds found in PROMICE observations during melt periods (Fig. S2 in the supplement). Changing  $\beta$  by  $\pm 20\%$  changes the total annual Greenland surface melt by  $\pm 3\%$ . The choice of  $T_{min} = -6.5^\circ\text{C}$  is in good agreement with observations, which reveal no substantial melt for temperatures  $< -7^\circ\text{C}$  (e.g. Orvig, 1954). Increasing the background melting condition  $T_{min}$  particularly reduces the melt rates at high elevations, while reducing  $T_{min}$  results in a longer melting season and increases the annual surface melt. Using no background melting condition at all results in unrealistic melt rates at high elevations and would almost double the predicted total Greenland surface melt. Changing  $T_{min}$  by  $\pm 1 \text{ K}$  changes the predicted mean annual surface melt by  $\pm 8\%$  for the MAR simulation used in this study. Intense surface melt is usually accompanied by warm temperatures and is thus insensitive to the choice of  $T_{min}$ . As refreezing particularly suppresses the contribution of weak surface melt at low temperatures, the resulting runoff can be expected to be less sensitive to the choice of  $T_{min}$ .

**Sensitivity to diurnal cycle of solar radiation:** Melt schemes which do not include the diurnal cycle of radiation will predict the same melt rate for a given combination of insolation and temperature forcing, irrespective of latitude or season. By contrast, Fig. 4 indicates a strong sensitivity of the dEBM surface melt predictions to latitude in summer. According to the dEBM, a short melt period with intensive solar radiation is causing melt more effectively than a longer melt period with accordingly weaker solar radiation. This sensitivity is particularly prominent in high latitudes and may explain the latitudinal bias found in many studies which do not resolve radiation on sub-daily time scales (e.g. Plach et al., 2018; Krebs-Kanzow et al., 2018; Krapp et al., 2017).

**Sensitivity to orbital configuration and transmissivity of the atmosphere:** The TOA solar flux density  $\widehat{S}_r$  depends on the distance between Earth and Sun and due to the eccentricity of the Earth's orbit gradually varies by  $\pm 3.5\%$  from the solar constant from December to July respectively. On orbital time scales this seasonal deviation from the solar constant may amount to 10%. Transmissivity  $\tau$ , on the other hand, strongly depends on cloud cover and atmospheric composition and additionally increases with the solar elevation angle. In consequence the minimum elevation angle  $\Phi$  may be less than  $13^\circ$  ( $\tau\widehat{S}_r = 1150 \text{ W m}^{-2}$  for clear sky, intense summer insolation). For overcast sky and weak summer insolation, we can ultimately expect  $\tau\widehat{S}_r < 400 \text{ W m}^{-2}$ . In that case, however, it is not justified to use the clear sky emissivity in Eqs. 5 and 7. Consequently, the proposed scheme is no longer suitable, as net outgoing long wave radiation will vanish and the energy

balance will become very sensitive to turbulent heat fluxes. Applications aiming at continental ice sheets with climatological forcing will be however restricted to a much narrower range of scenarios. As one can expect that transmissivity decreases towards the morning and afternoon hours, it may be justified to reduce the estimate of  $\tau \widehat{S}_r$  by a few percent. Fig. 4 reveals that the scheme becomes very sensitive if the minimum elevation angle  $\Phi$  takes values close to or larger than the obliquity of the Earth. Under such conditions the duration of the melt period will vanish near the Pole. On the other hand the scheme is remarkably insensitive to intensified insolation (and accordingly reduced elevation angle  $\Phi$ ) or variations in the obliquity. Accordingly, estimating the elevation angle locally and for each month using Eq. ??, which is possible but computationally more expensive, does not improve the skill of the dEBM noticeably (not shown).

### 3 Response to first referee (Alexander Robinson)

10 – Major comments ————— ... However, the description of the alternative methods is not very precise, and I think the comparison with them could be more thorough and analytical.

We now distinguish between ETIM and ITM:

15 Introduction: “ Another empirical approach uses a linear function of solar radiation and temperature to predict surface melt. This approach was originally used to estimate ablation rates of glacial ice sheets (Pollard, 1980; Pollard et al., 1980). Formally similar schemes have been chosen, when the influence of solar radiation is changing over orbital time scales (the insolation temperature melt (ITM) equation designed to be used with monthly or seasonal forcing on long time scales, e.g. van den Berg et al., 2008; Robinson et al., 2010; de Boer et al., 2013), or for debris-covered glaciers, where surface albedo, and thereby the effect of insolation, is partly independent of air temperature (enhanced temperature index models (ETIM), consider sub-daily radiation and temperature of that period of a day, during which temperature exceeds a threshold temperature. Typically, this approach is used with sub-daily climate forcing from weather stations, e.g. Pellicciotti et al., 2005; Carenzo et al., 2016). The empirical schemes, however, incorporate parameters, which require a local calibration and which are not necessarily valid under different climate conditions.

25 - As pointed out by the editor, a distinction should be made when discussing a melt model alone (which is a somewhat artificial construct in isolation) versus an energy balance model, which may calculate many variables that are useful for ice-sheet modeling (ice temperature, albedo, refreezing, smb). Thus I see PDD, ETIMs, ITM (see next point) and the model presented here in a similar category – melt models that can be used as a subcomponent of smb models – while SEMIC and full EBMs are more wholistic solutions. A bit of clarity here on these definitions would improve the manuscript greatly.

We have included a more detailed description of SEMIC:

30 Introduction: Krapp et al. (2017) have formulated a complete surface mass balance model including accumulation, surface melt and refreezing (SEMIC) which can be used with daily or monthly forcing. SEMIC predicts the surface mass balance with a daily time step, but implicitly accounts for the sub-daily temperature variability in the surface layer of the ice to account for diurnal freeze-melt cycles.

35 -“ETIM” as used throughout the text seems to be the wrong term for the comparison being made here. ETIMs involve a “temperature index” such as PDD (Hock et al., 2003; Pellicciotti et al., 2005). This is why, in Robinson et al., 2010, we opted to create the name ITM for the model of Eq. 14, since we saw it simply as an “insolation-temperature melt model”.

40 - Equation 14 is not correct, in representing the approach of Pollard (1980) or Robinson et al. (2010). The second term should not contain PDDs, but the mean near-surface air temperature relative to the melting point:  $k_1 * (T_a - T_0)$

Admittedly, this was formulated too sloppy. Trying to correctly incorporate the ITM concept, I noticed that this method has problems to reproduce melt rates at low temperatures. In the context of a full SMB-model this would probably carry no weight as refreeze is usually balancing the surface melt at low temperatures. However, the calibration to MAR melt rates is hampered by the biased low temperature melt rates. In consequence, our calibration would yield parameters, which fail to skillfully reproduce the surface melt rates at warm temperatures. I have decided to stick to a scheme which incorporates PDD, but we now refer to this scheme as  $dEBM_{const}$ . Comparing to a dEBM version with constant parameters also meets your suggestion

further below. We have reformulated the first part of section

**First evaluation of the scheme:** The dEBM and two empirical schemes are calibrated and evaluated using the state-of-the-art regional climate and snow pack model MAR (Fettweis et al., 2017) as a reference.

5 The elevation angle used in the dEBM is estimated as  $\Phi = 17.5^\circ$ , applying Eq. (9) with a typical albedo of 0.7 and  $\tau \widehat{S}_r = 800 \text{ W m}^{-2}$  being roughly estimated from the summer insolation in the ablation regions (Eq. ??). This estimate corresponds to a transmissivity of  $\tau \approx 0.6$  which is in good agreement with Ettema et al. (2010). Further, the dEBM is optimized to reproduce the total annual Greenland surface melt averaged over the entire MAR-simulation by calibrating the background melting condition as  $\overline{T}_a > -6.5^\circ\text{C}$  and the parameter  $\beta = 10 \text{ W m}^{-2} \text{ K}^{-1}$ . We then apply the scheme to  $\overline{SW}_0$ ,  $PDD_{\sigma=3.5}(\overline{T}_a)$  and albedo  $A$  from a MAR-simulation of Greenland's climate (years 1948 to 2016) (Fettweis et al., 2017) and compare estimated melt rates with the respective MAR melt rates.

10 Two empirical schemes are considered in the same way: a PDD-scheme based on  $PDD_{\sigma=5}(\overline{T}_a)$ , as defined and calibrated in Krebs-Kanzow et al. (2018) and a scheme, in the following referred to as  $dEBM_{const}$ , which is a simplified variant of the dEBM where parameters are constant in time and space:

$$M = ((1 - A)\overline{SW}_0 + k_1 PDD_{\sigma=3.5}(\overline{T}_a) + k_2) \frac{1}{\rho L_f} \quad (1)$$

15 with  $k_1 = 10 \text{ W m}^{-2} \text{ K}^{-1}$  and  $k_2 = -55 \text{ W m}^{-2}$ . The  $dEBM_{const}$  is very similar to the ITM-scheme and also uses similar parameters as in Robinson et al. (2010), but includes PDD instead of temperature, which particularly yields different results for low temperatures. As in Robinson et al. (2010), we treat  $k_2$  as a tuning parameter to optimize the scheme and also use  $\overline{T}_a > -6.5^\circ\text{C}$  as a background melting condition.

20 The computational cost of the dEBM in this application is very similar to the other two schemes as parameters are computed only once prior to the application. All schemes reproduce the total annual Greenland surface melt averaged over the entire MAR-simulation of 489 Gt with a relative bias not exceeding 1% (the mean bias is 0.4 Gt for the PDD scheme, -0.6 Gt for the  $dEBM_{const}$  and -2.0 Gt for the dEBM). These calibrations are primarily conducted to facilitate a fair comparison between the different schemes and are not necessarily optimal for other applications.

25 - SEMIC also supports the input of monthly temperature data, although the model itself is calculated on daily time steps (from Krapp et al., 2017: "In principle, the use of monthly input data is also supported but would require interpolation to daily time steps."). I would additionally note that SEMIC is open source and prepared to run easily with MAR data as input, making its comparison with dEBM feasible if the authors wanted to be more thorough. It would certainly be convincing if it could be explicitly shown that dEBM can do a better job than SEMIC for a much lower cost. (This point is only a suggestion, and I would not consider it necessary for revision.)

30 I now discuss SEMIC more specifically in the Introduction (see above). I would also be very interested in this comparison. The intention behind the comparison of the different schemes in the presented paper, however, is not a complete intercomparison, but rather to demonstrate, that the latitudinal bias found in other schemes, might be reduced, if we account for the diurnal cycle of radiation.

35 I find the approach outlined here quite elegant and the physical derivation is nicely described. However, then I am surprised to see PDD pop up in Eq. 6 again. Would it not be simpler keep  $(T_a - T_0)$  here? The only reason to use PDDs is to incorporate a measure of variability in  $T_a$ . But it seems to me that if you want to include the variability around  $T_a$  in the melt model, it would be more appropriate to apply it to the whole equation rather than just to the temperature term (ie, calculate the average melt rate from the distribution of melt rates for the month).

40 We have added a few lines to

**The daily melt period and its energy balance:** Near surface air temperature measurements from PROMICE stations on the GrIS reveal a good agreement between monthly mean temperatures of the daily melt periods and the  $PDD_{\sigma=3.5}$  approximated as in Braithwaite (1985) from monthly mean near surface temperature  $\overline{T}_a$  and a constant standard deviation of  $\sigma = 3.5^\circ\text{C}$  (Fig.

45 S1 in the supplement).

And added the following to the

**Supplement: Mean surface temperature and wind speed of melt periods from observations**  $\overline{T}_a$  is the monthly mean tem-

perature and thus also includes temperatures outside of the daily melt period. The strategy in our paper is to only consider that part of the day, when the ice is warm enough to melt. We thus need to estimate the mean temperature during this melt period. To illuminate the relation between  $T_a$  and  $T_{MP}$ , we analyzed hourly climate data from PROMICE (Ahlstrom et al., 2008) weather stations: 2m air temperature  $T_a$ , surface temperature  $T_{surf}$ , albedo  $A$  and short wave radiation  $SW$ . In analogy to the dEBM, we determine the melt period for each month by identifying those hours which comply with the conditions

$$\overline{(1 - A)SW} > 71.9Wm^{-2}$$

and

$$\overline{T_{surf}} > -0.01^{\circ}C$$

The bars denotes hourly data taken from the monthly mean diurnal cycle. We analyzed 18 PROMICE stations which cover a period of up to ten years (2008-2017) and identified 390 monthly mean diurnal cycles which exhibit a melt period according to our above definition. We don't need to resort to a minimum elevation angle here, as hourly radiation is available. Likewise the background melting condition is replaced by the condition, that hourly surface temperature data must be near melting point. Indeed, the PROMICE data indicate that PDD is quite a good proxy for the monthly mean temperature of the melt period  $T_{MP}$ . Using a constant standard deviation of  $3.5^{\circ}C$  exhibits a particularly good fit (Fig. S1).

Furthermore analyzing the mean wind speed during the above melt periods, we find on average a wind speed of  $u_{MP} = 3.8m s^{-1}$  (Fig. S2).

Why PDD is such a good estimate of  $T_{MP}$  is not completely clear. It would be interesting to develop alternative estimates for  $T_{MP}$ .

Looking into the observational data, we also noticed that daily melt periods are considerably longer than in our original MAR-based study (up to 20 hours). In fact this is how I realized that the estimated minimum elevation angle must be incorrect. The newly estimated  $\Phi = 17.5^{\circ}$  yields longer melt periods and generally agrees with the PROMICE data.

If you follow the path above, this change would make Eq. 6 essentially equivalent to Eq. 14 (also without PDDs), and it maintains its physically-based origins and makes it obvious that the key differences are: - The term  $q_{\Phi}$ , which scales the insolation according to the time it is actually available. - The term  $dt_{\Phi}$ , which scales the melt according to the time when it is relevant. - The derivation of the constants  $c_1$  and  $c_2$ . I note that the used values of  $c_1 = 13.5$  and  $c_2 = -71.9$  are not too far from values used in Eq. 14 for  $k_1 = 10$  and  $k_2 = -60.5$ . It would be interesting to understand if this is systematic, that generally  $c_1 > k_1$  and  $k_2 > c_2$ , to compensate for the lack of  $q_{\Phi}$  and  $dt_{\Phi}$  terms. For example, if in Eq. 6, you set  $q_{\Phi} = 1$  and  $dt_{\Phi} = dt$ , how well does your model perform (after retuning the constants) – as well as before, or is the performance degraded? In other words, I would be happy to see an analysis that specifically shows the value of incorporating the diurnal terms to the model

I think with introducing  $dEBM_{const}$ , this suggestion is implemented now.  $dt_{\Phi} < dt$  in most places and accordingly  $c_1 > k_1$ . Understanding  $q_{\Phi}$  is more complicated. We have reformulated the part about the radiative contribution and hope this is more clear, now.

**First evaluation of the scheme:** The radiative contribution in the dEBM becomes less efficient for long melt periods, as the same insolation must balance the outgoing longwave radiation for a longer time. On the other hand, radiative contribution can also decrease towards short melt periods, if the sun only marginally rises above the minimum elevation angle at solar noon. This effect becomes important for higher estimates of the minimum elevation angles in high latitudes (Sect. 4).

#### — Minor comments —

We would like to comment on the following minor comments

: Page 2, line 1: “Another empirical approach, the enhanced temperature-index method, ETIM” => In addition to the fact that I believe ETIM is the wrong term here, as I already mentioned, ETIM refers to a class of models that can take many forms that generally extend PDD in various ways, not to a specific model formulation. Therefore, I would rephrase here. Alternatively, you can use the term “ITM”, which does refer to the formulation of Pollard (1980). Or, a more descriptive term for this model

would be “linearized EBM” (Pollard, 1980).

We now use  $dEBM_{const}$

5 Page 3, line 5 (Eq. 3): I see no reason why  $e_i$  should appear multiplied with  $LW_{down}$ . This is only relevant for  $LW_{up}$  (as in Eq. 4), correct?

To my understanding,  $e_i$  is also influencing, how much LW radiation is absorbed, as a good emitter is also a good absorber.

Page 4, line 23: What is the calculation of  $\Phi = 23.5$  used for later? As I understand all tests were using MAR albedo, etc. Is this just an example?

10 Actually  $\Phi$  is a crucial parameter, as  $\delta t_{\Phi}$  and  $q_{II}$  will change with  $\Phi$ .

Page 5, line 11: “Equations (6) and (14) appear formally similar, with the first and third term representing the radiative contribution and the second term representing the PDD contribution.” <= This sentence is contaminated by the mistake in Eq. 14, however, just thinking about it in terms of Eq. 6, it is clear from the derivation that the first term represents shortwave radiation and the second and third terms represent the net longwave radiation and heat fluxes from R combined. Please rephrase.

We rephrased:

20 Equations (6) and (14) appear formally similar, with the second term being temperature dependent (the “temperature contribution”) and the first and third term being independent of temperature and only depending on solar radiation (the “radiative contribution”).

Page 5, line 11-21: Generally, I find this paragraph difficult to follow. Is the “flat elliptic” referring to the orbital configuration of the Earth, or some pattern in the figure itself? Does “going along with” mean “causing”? I find that “PDD contribution” a not very convenient name for the second term in Eq. 6, since it is easily confused with the PDD melt model itself in this context. I would consider serious revision here for clarity.

We reformulated this paragraph (ecliptic was the wrong term):

30 Fig. 1a illustrates the radiative and Fig. 1b the temperature contributions as diagnosed from the MAR simulation in comparison to the respective contribution from the  $dEBM_{const}$ . On the GrIS the radiative contribution can exceed  $25 \text{ mm d}^{-1}$  in the summer months and the two schemes appear qualitatively similar. The radiative contribution in the dEBM becomes less efficient for long melt periods, as the same insolation must balance the outgoing longwave radiation for a longer time. On the other hand, radiative contribution can also decrease towards short melt periods, if the sun only marginally rises above the minimum elevation angle at solar noon. This effect becomes important for higher estimates of the minimum elevation angles in high latitudes (Sect. 4). The temperature contribution of the dEBM does not exceed  $15 \text{ mm d}^{-1}$  (Fig. 1b) and becomes more efficient with longer melt periods and would agree with the  $dEBM_{const}$  for a melt period of 18 hours.

35 Page 5, line 25: “defective input” <= I’m not quite sure what you want to say with this sentence, consider rephrasing somewhat. Wouldn’t it be possible to make your ideal input data “defective” for testing purposes, if that was your goal?

We slightly rephrased:

40 With respect to error propagation the PDD-scheme might be more robust and , as it only requires temperature as a forcing and only distinguishes between snow and ice but does not require albedo.

t does not seem appropriate to limit the comparison of dEBM to points that satisfy  $T_a > -6.5C$ . Either the value of  $T_{min} = -6.5C$  is adequate, or  $T_{min}$  should be set to a lower value. In either case, the correct choice of this threshold should be reflected by the comparison to MAR melt. Based on the horizontal line of dark blue points in Figs. 1 and 2, I have to guess that the threshold chosen here is too high, or for some reason the dEBM underestimates melt at low temperatures. This should be discussed in the paper clearly. The horizontal line of dark blue points in Fig. 2 was related to the incorrect estimate of minimum elevation angle. We removed the RMS part from the main text and included the root mean square errors of the mean 1948-2016 local yearly surface melt rates in Fig. 3. We did not use the background melting condition for this calculation. The idea to use  $T_{min}$  arose as I wanted to limit the analysis to the ablation region and melt season. I see now that this can bias the statistics (it

did not substantially, though)

Page 8, line 13: “This threshold temperature should be considered as a tuning parameter” => I had understood this  $T_{min}$  simply to be a cost-saving measure, to avoid calculating the melt model for points where melt would be zero. However, this sentence makes me believe that the parameter is more important than I realized. Please elaborate on the role of  $T_{min}$  more in the derivation section for clarity

This is now discussed in the sensitivity section (Sect. 4).

We fully followed the following minor comments and corrected the manuscript accordingly:

- 10 Units and variables: Please check the units carefully. For example,  $T_a$  is in Kelvin, but then  $T_{min} = (T_0 - 6.5)K$ , right? Also, in Eq. 14, is the first term “ $SW_0$ ” the same as “ $SWD_0$ ” defined earlier in the text? Please keep the same terms throughout
- . Page 1, line 14: information on => information about
- Page 1, line 15: refreeze => refreezing
- Page 1, line 23: computational => computationally
- 15 Page 1, line 24: temperatures. => temperatures as input.
- Page 1, line 25: or paleo-temperature => and paleo-temperature
- Page 2, line 1: aproach => approach
- Page 2, line 19: a surface melt rate => a non-zero/positive surface melt rate
- Page 3, line 7: Per definitionem => By definition
- 20 Page 3, line 23 (Eq. 7): It looks like  $c_1$  is missing the term  $e_a$ , following the current equation formulations.
- Page 4, Section 2.1: Please make sure to use the same variables and notation as in the rest of the text. I guess that the elevation angle  $\Phi$  in the previous section is the same as the elevation angle  $\Theta$  in Sect. 2.1.
- Page 4, Eq. 13: I would suggest adding the intermediate definition of  $q_\Phi$  here to remind readers of your previous definition:  $q_\Phi = SW_\Phi/SW_0$  = [full definition]. Also again be clear about SW versus SWD.
- 25 Page 5, line 11: Eqatons => Equations
- Page 5, line 23: derived => obtained?
- Page 5, line 27: due to => Given
- Page 7, line 1: biasses => biases
- Page 7, line 6: refreeze => refreezing
- 30 Page 7, line 6: used together with the enhanced temperature index method in => presented by
- Page 8, line 16: Depending on application => Depending on the application

#### 4 Response to second referee (anonymous)

- 35 Page 4 line 12 TOA is introduced for “top of the atmosphere” but only used once on line 15 then not used on line 16 (where there are hyphens between the words). Is an initialism really needed?
- It is now used more often

- 40 Page 4 line 21 “Choosing  $\beta = 10$  ...“. If that is a choice, i.e. if alternative values could have been chosen, then the reason for this specific choice should be given, e.g. cited or explained. If however it is the only reasonable value then it’s not a choice and “using “would be better than “choosing”

We now make clear that this is the outcome of an calibration: Further, the dEBM is optimized to reproduce the total annual Greenland surface melt averaged over the entire MAR-simulation by calibrating the background melting condition as  $\bar{T}_a > -6.5K$  and the parameter  $\beta = 10 W m^{-2} K^{-1}$

- 45 Page 4, bottom, section 3 Just a general comment that any further citations or justifications for the values of coefficients used that can be included would be useful

We now reference ? and Orvig (1954) which agrees well with our independently calibrated parameters.

In the introduction it is mentioned that the PDD scheme is computationally inexpensive (page 1 line 23) and that energy balance models could have their computational costs reduced (page 2 line 7) but the evaluation makes no mention of the computational costs of dEBM and the other schemes. I think it would be useful to include a brief comment on the relative computational costs in section 3.

We added the following line to section 3: The computational cost of the dEBM in this application is very similar to the other two schemes as parameters are computed only once prior to the application.

The following suggestions are obsolete after the modification of the manuscript: Page 5 line 16 “going along with .... “ would “corresponding to...” read better?

Page 5 line 30 This refers to the blue points in Fig 2 panel 3 at 0 on the y-axis. I think this should be stated in the text.

Page 8 line 16 This is a new paragraph, should it be

We fully followed the following recommendations: Page 1 line 23 “computational” should be “computationally”

Page 2 line 27 “Further, we define the ratio between .....” would “ $q_{\Phi}$  is the ratio between...” read better?

Page 2 line 27 and 28 “SW” is used for the mean solar radiation. I assume the S and W stand for Short Wave, so it would be better to state that here

Page 3 lines 24 and 26 and Page 4 line 10 These lines appear to have been indented /tabbed

Page 4 line 22 “-6.5K” °C not K

Page 5 line 11 Misspelling “eqations”

Page 5 line 15 “GrIS” is used without definition. Whilst it is a well known abbreviation, especially for this journal, it maybe better to define

Figure S1, caption “meltrates” should be 2 words. Misspelling “lenght”. Refers to PDD, ETIM and DEBM as a), b) and c) but they are not labelled as such in the figures. Also “Identity... black line” is not shown (I think perhaps the caption is for an earlier version of the figure?)

## 5 Response to third referee (Mario Krapp)

**Major comments** - Solar elevation angle and surface slope: Whereas large parts of the Greenland ice sheet are rather flat its margins, where most of the melt occurs) are not and glaciers are even more sensitive to the slope of the embedding terrain. I suspect that the daily solar elevation angle depends on how the ice surface faces the sun. How much of an effect would a surface slope have and could that be included in Sect. 2.1?

Indeed, the melt period may be extended/shortened by a southward/northward slope. If we would want to account for this, it would make it necessary to perform a projection of the solar radiation to the surface before estimating the minimum elevation angle locally. The slopes on the 20km grid of the MAR-simulation rarely exceed 1%, which could change the minimum elevation angles by  $\approx 1^\circ$ . Seeing that the manuscript is already quite lengthy, I decided to not include this into the manuscript.

- I expect the atmospheric transmissivity (Sect. 2.1) to decrease with increasing solar zenith angle. How much of an effect would that have?

This is a very good point, I would estimate that this effect may increase the elevation angle by up to  $2^\circ$  relative to an estimate using a constant transmissivity. It is difficult to account for this effect in an objective way, but luckily the scheme is quite insensitive to minor changes in the minimum elevation angle and it appears sufficient to only do a rough estimate. I added the

following sentence to the Sect. 4:

As one can expect, that transmissivity decreases towards the morning and afternoon hours, it may be justified to reduce the estimate of  $\tau_{\widehat{S}_r}$  by a few percent.

- 5 I think that using a single parameter for the emissivity of air ( $\epsilon_a$ ) is also too simplistic and the contribution of cloud cover is missing.  $LW_{down}$  is parameterised using  $\epsilon_a$ , which is the clear sky emissivity but how do you deal with cloudy skies? In fact,  $\epsilon_a$  can vary between 0.7 (clear sky) and 1.0 (fully overcast). Therefore, the value for  $c_2$  can vary between -90 and 0 W/m<sup>2</sup> if you account for varying  $\epsilon_a$ . That means that a full overcast sky would add about 90 W/m<sup>2</sup> to the surface energy uptake Q. A very valid point, I did not consider this originally. The dEBM concept propably comes to its limits here. I have added this point to the sensitivity section as given above. However for continental ice sheets (i.e. Greenland and Antarctica and, in cold climates, the North American and Fennoscandian ice sheets) the clear sky assumption appears justified.

I think in Eq. (7),  $\epsilon_a$  is missing in the term for  $c_1$ , ... If that is the case  $c_1$  also yields a different value in line 25 on page 4 and my above argument about varying  $\epsilon_a$  implies that  $c_1$  can vary 13 and 14.4 W/m<sup>2</sup>K

- 15 This is an error which was only in the text and not in my dEBM function. I corrected the text accordingly.

Sensitivity of model parameters:... We now include the section about sensitivity, as stated above

- 20 The PDD component of dEBM is in general smaller than in ETIM (Fig. 1b). Obviously, the PDD contribution of dEBM would be larger for a larger  $\beta$  which can range between 7 to 20 W/m<sup>2</sup>K as you said earlier

This has changed after correcting and modifying various details. Also citing ? we now provide better constraints for the choice of  $\beta$ .

- 25 I would like to see a plot showing the time series of monthly melt and different diagnostics (as is shown in the supplement). For example, melt rates and its individual components (the PDD and the ETIM-related term) in Eq. (6), or the parameterised short- and longwave radiation  $SW$  and  $LW_{down}$  would help the reader to understand what the model is doing internally. Specifically it would be nice to see how  $q_\Phi$ , which is the novel part of your melt scheme, changes over time.

Primarily,  $q_\Phi$  and  $\delta_\Phi$  affect surface melt latitudinally, and to some degree seasonally. Perhaps, the effects are sufficiently illustrated in the new Fig. 4. I am hesitant to add another figure on the seasonal effect, as the paper seems already quite long.

- 30 To me everything in the conclusion, except for the first paragraph, is more like a "summary and discussion" section than an actual conclusion. Please revise. We changed the title of the section accordingly.

- 35 I guess if you consider a revision as article you can easily move Figure S1 (which is the only item in the supplement) to the main text

This can be easily done, but I would leave this decision to the editor.

Out of curiosity (not needed for the revision): If the melt scheme just uses a few input parameters, is it possible to force it with atmospheric data from available observations of the GrIS? For example, GC-MET (<http://cires1.colorado.edu/steffen/>)

- 40 At least the PROMICE data have a high frequency, so that better estimates should be possible, if a full energy balance model is used. Nevertheless, I can imagine that the scheme could be modified in a way, so that distributed melt estimates could be derived from satellite data in combination with weather station data. Also it could be possible to estimate melt rates from glaciers where weather stations only exist below the glacier. In both cases I would think that the scheme would have to undergo considerable modification. I would be indeed interested to discuss this with people from the observational community.

- 45 **Minor comments**

p2 ll.27-29: It is not clear whether  $SW_0$  or  $SW_\Phi$  mean surface or TOA shortwave radiation.



We included the word surface.

p.5 122: Please, specify what the atmospheric forcing variables from the MAR model are

We did so.

- 5 Please add a table with model parameters and parameter values used in the main text and analysis.

We will do so, if this fits into the format (article or brief communication)

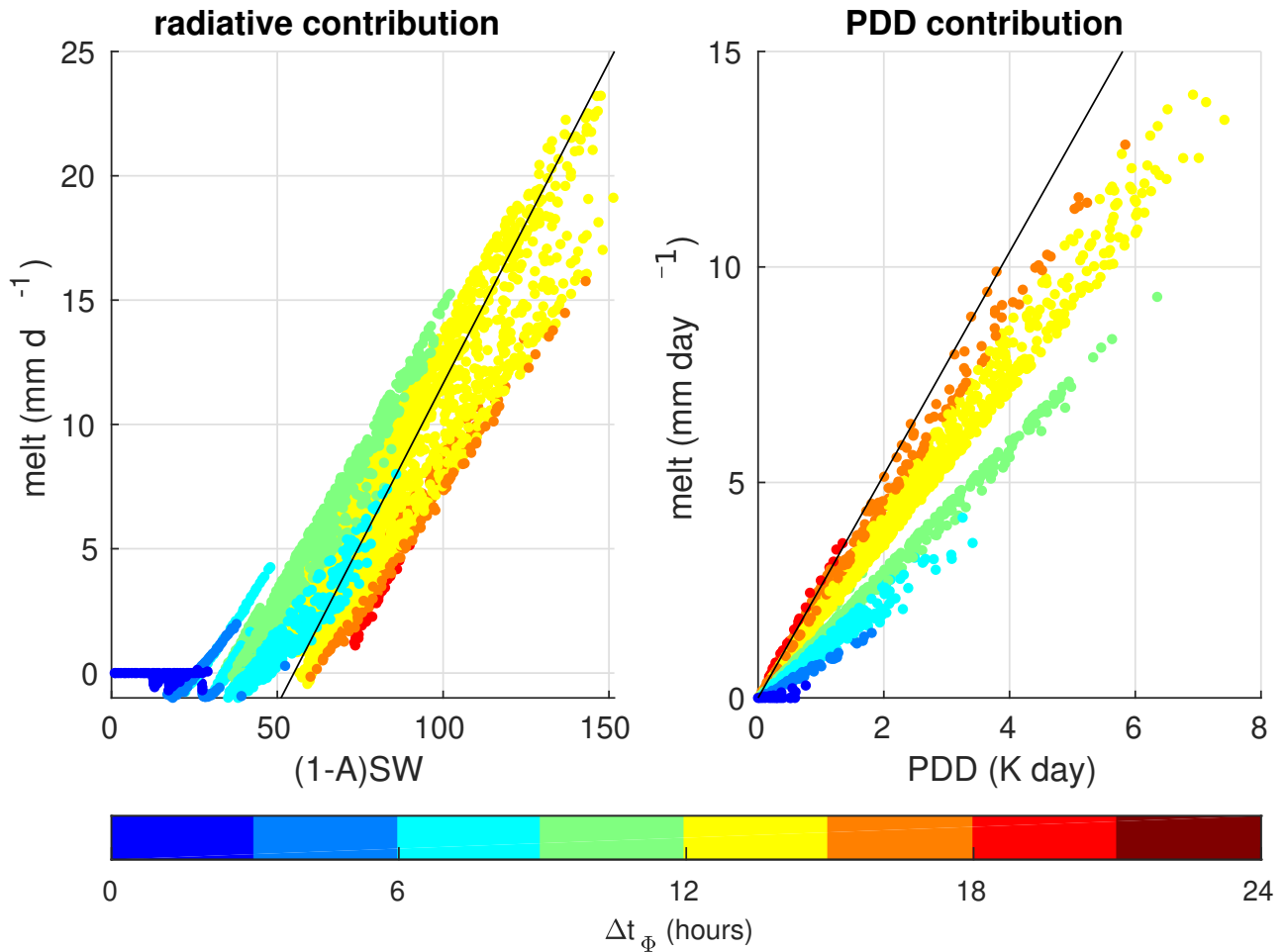
Fig. 2: add units to axis labels; duplicate y-axis labels ("PDD", "ETIM", and "dEBM")

We changed this.

10

Fig. 3: the min/max colors are really dark and hard to see

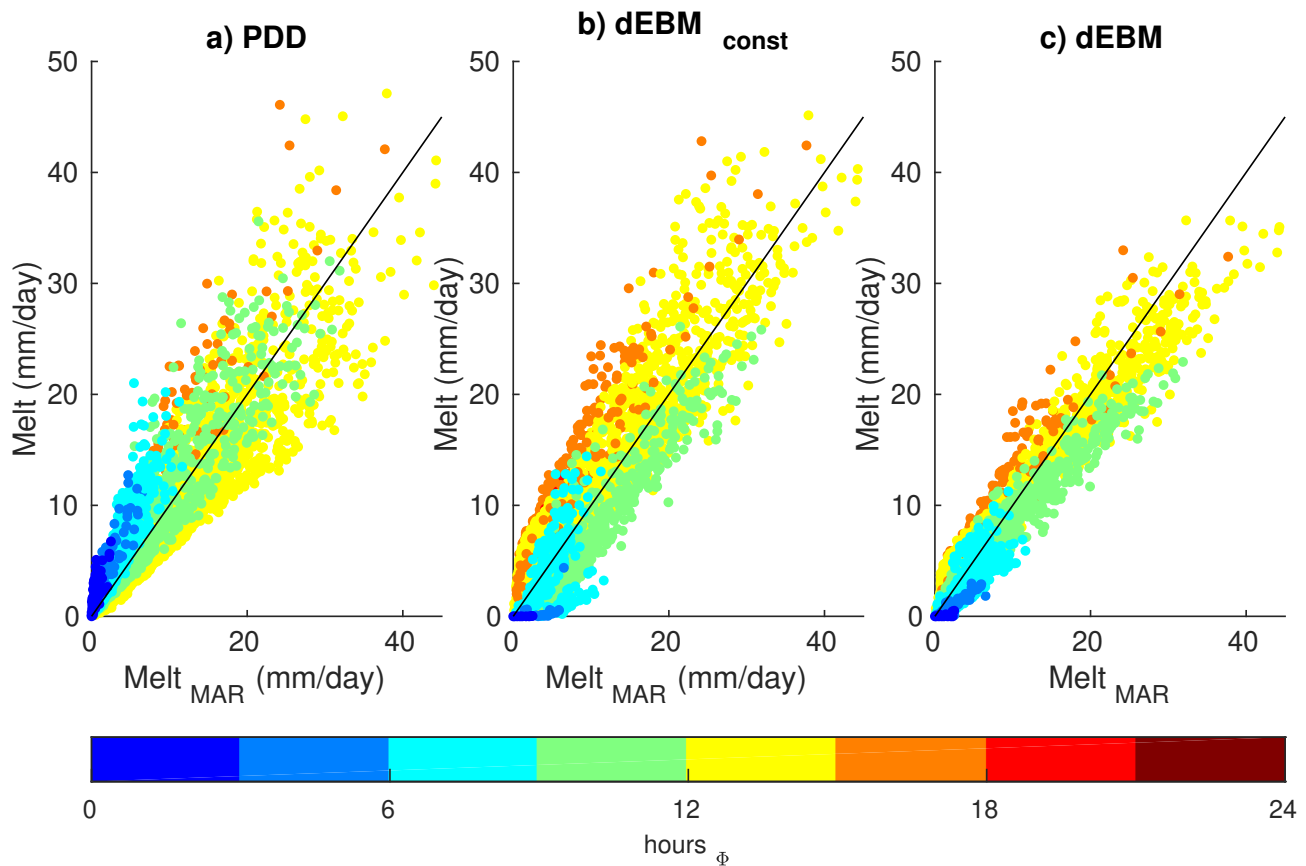
We tried to improve the colorbar.



**Figure 1.** a) Contribution of the first and third term (radiative contribution) and b) of the second term (temperature contribution) in Eq. (6) to monthly melt rates as diagnosed with climatological temperatures and solar radiation from the MAR simulation. Colors indicate length of melt period (h). The black lines represent the respective prediction of the  $dEBM_{const}$  according to Eq. (14)

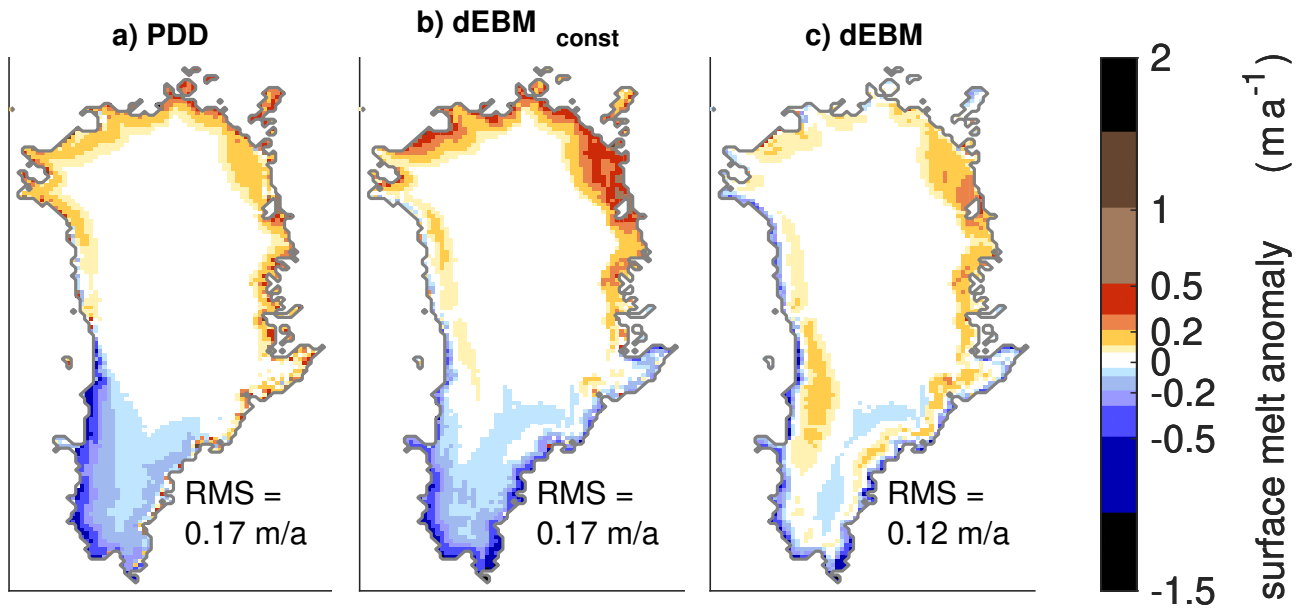
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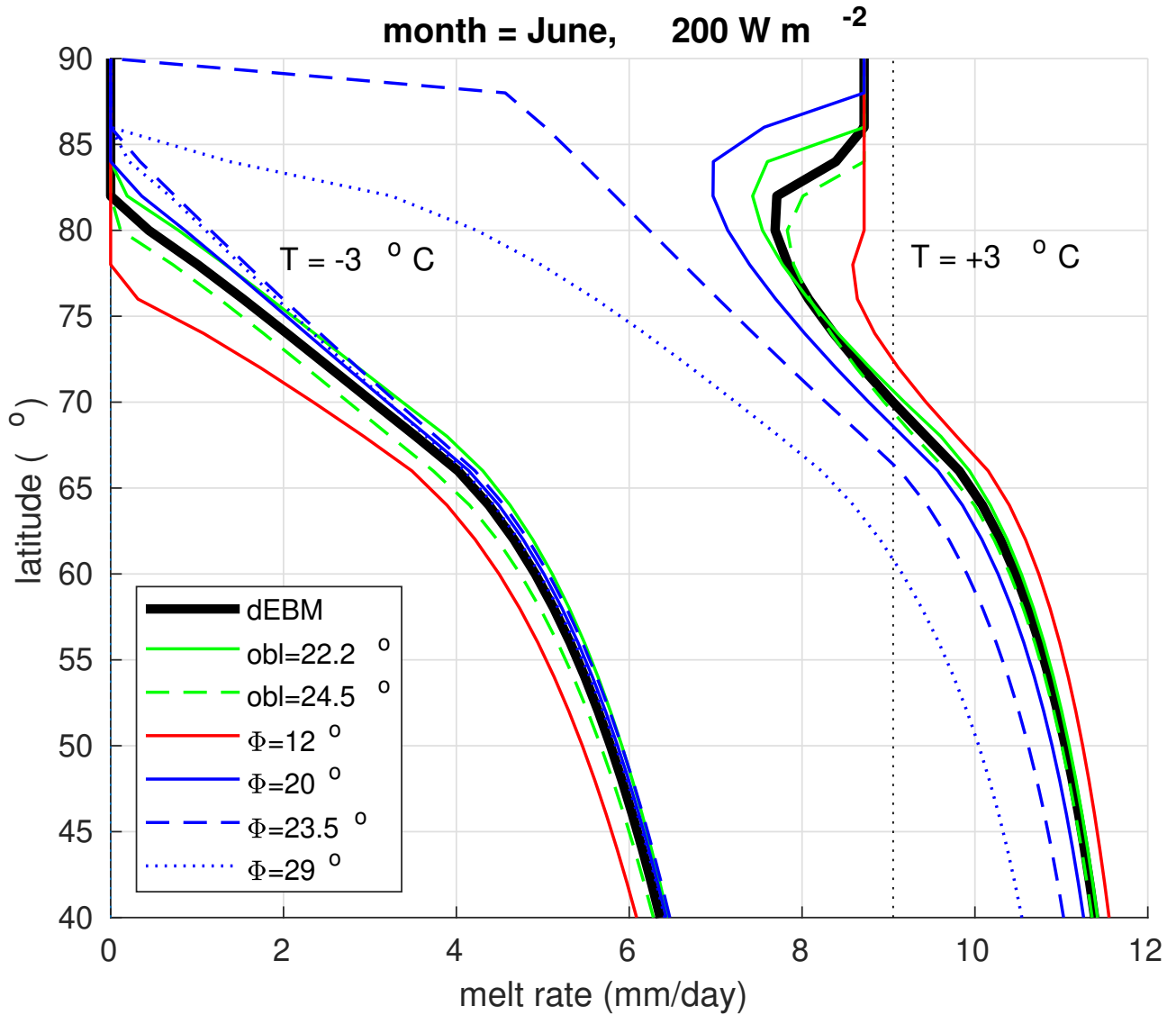
**Figure 2.** Multi-year monthly mean meltrates averaged of the years 1948-2016 as predicted by a) the PDD-scheme, b) the  $dEBM_{const}$  and c) the dEBM against respective MAR melt rates. Colors reflect the length of the daily melt period. Identity is displayed as a black line in all panels for comparison.

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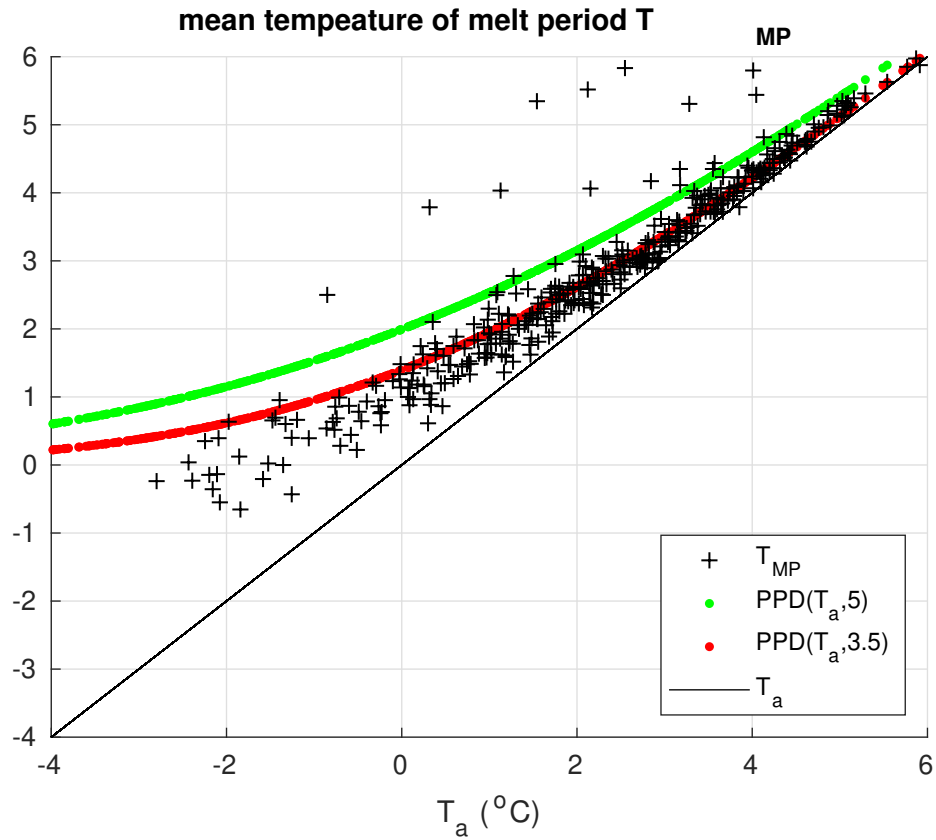


**Figure 3.** Bias between yearly melt rates as predicted by the individual schemes and as simulated by MAR, averaged over the whole simulation: a) PDD b)  $dEBM_{const}$  c) the proposed new scheme dEBM. The respective root mean square error (RMS) is given in the individual panels.

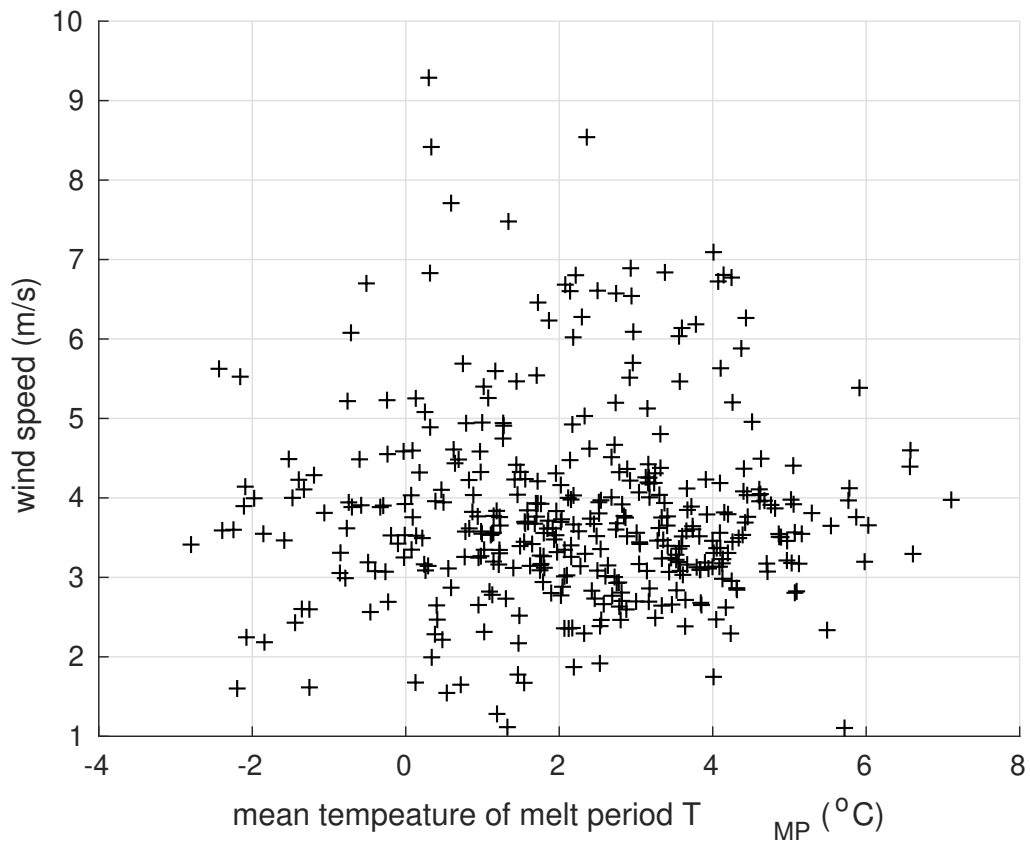
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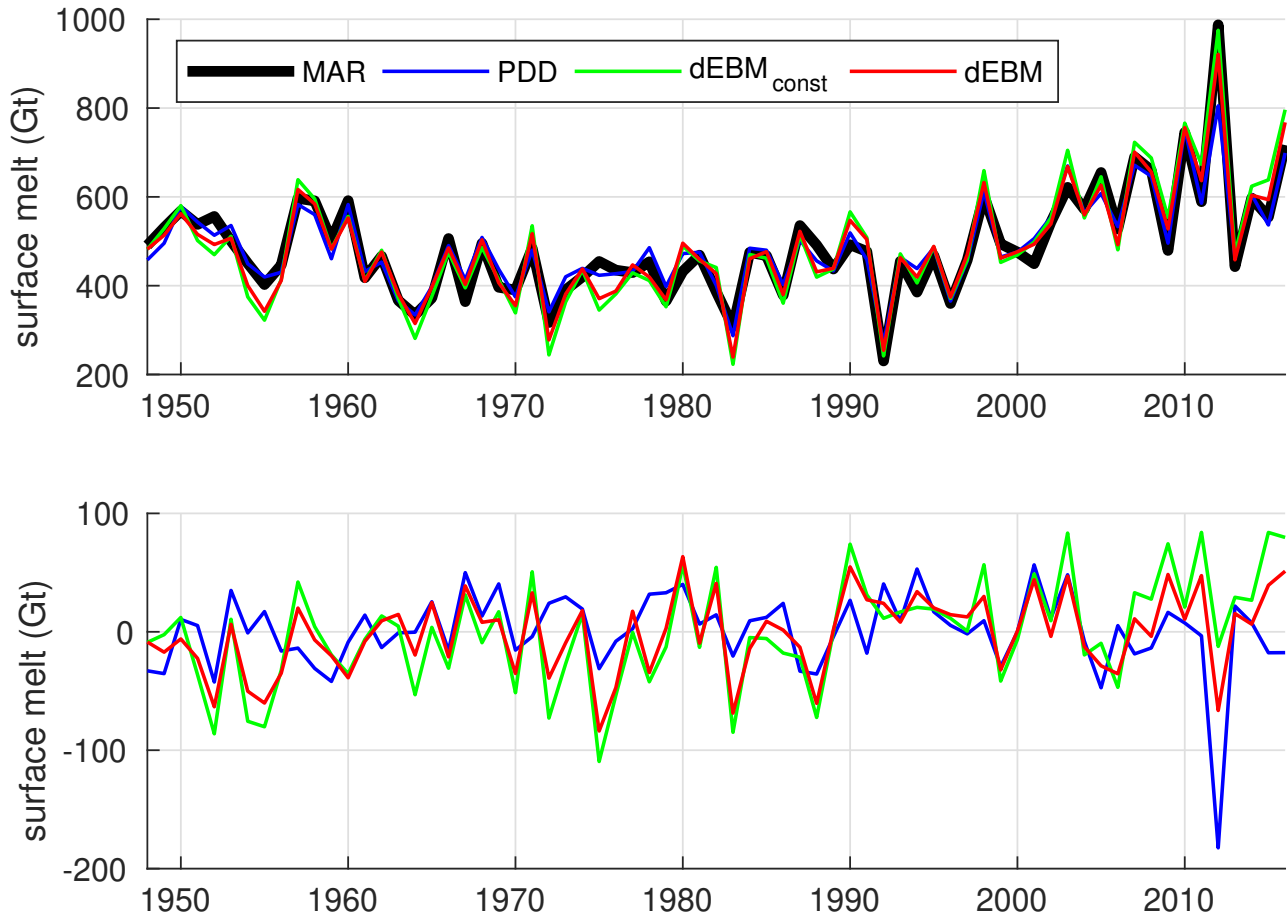
**Figure 4.** Sensitivity of the dEBM: June surface melt rate as predicted for  $SW_0 = 200 \text{ W m}^{-2}$ ,  $A = 0.7$ ,  $T_a = -3^\circ \text{C}$  (left curves) and  $T_a = 3^\circ \text{C}$  (right curves). Black: predictions with parameters as used for the presented simulation of Greenland’s surface melt. Green: parameters are recalculated using the minimum (solid) and maximum (dashed) obliquity of the last 1 million years. Blue: parameters are recalculated after the minimum elevation angle is adjusted to a reduced solar density flux at the surface of  $\tau \hat{S}_r = 700 \text{ W m}^{-2}$  (solid),  $\tau \hat{S}_r = 600 \text{ W m}^{-2}$  (dashed),  $\tau \hat{S}_r = 500 \text{ W m}^{-2}$  (dots). Red: parameters are recalculated after the minimum elevation angle is adjusted to an intensified solar density flux at the surface of  $\tau \hat{S}_r = 1150 \text{ W m}^{-2}$ . The  $dEBM_{const}$  predicts 0 mm/day for  $SW_0 = 200 \text{ W m}^{-2}$ ,  $A = 0.7$ ,  $T_a = -3^\circ \text{C}$  and 9 mm/day for  $SW_0 = 200 \text{ W m}^{-2}$ ,  $A = 0.7$ ,  $T_a = 3^\circ \text{C}$  (black dots).



**Figure S-5.** Monthly mean melt period temperature  $T_{MP}$  and PDDs as functions of monthly mean near surface air temperature  $T_a$ . Crosses reflect monthly mean  $T_{MP}$  as calculated from hourly near surface air temperature data of 18 PROMICE stations. Red and green points reflect PDD calculated from  $T_a$  assuming a constant standard deviation of  $3.5^{\circ}\text{C}$  and  $5^{\circ}\text{C}$  respectively.



**Figure S-6.** Monthly mean wind speed during melt periods  $u_{MP}$  as a function of monthly mean near surface air temperature  $T_a$ .



**Figure S-7.** Upper panel: total yearly surface melt of the years 1948-2016 from MAR (black) and as predicted a) Total Greenland surface melt from 1948 to 2016 as simulated by MAR (black) and predicted from PDD-scheme (blue),  $dEBM_{CONST}$  (green) and dEBM (red). Lower panel: yearly bias of total yearly surface melt predicted by PDD-scheme (blue),  $dEBM_{CONST}$  (green) and dEBM (red) for the 1948–2016 period relative to MAR.



# Brief communication: An Ice surface melt scheme including the diurnal cycle of solar radiation

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## Abstract.

We propose a surface melt scheme for glaciated land surfaces, which only requires monthly mean short wave radiation and temperature as inputs, yet implicitly accounts for the diurnal cycle of short wave radiation. The scheme is deduced from the energy balance of a daily melt period which is defined by a minimum solar elevation angle. The scheme yields a better spatial representation of melting than common empirical schemes when applied to the Greenland Ice Sheet, using a 1948-2016 regional climate and snow pack simulation as a reference. The scheme is physically constrained and can be adapted to other regions or time periods.

## 1 Introduction

The surface melt of ice sheets, ice caps and glaciers results in a freshwater runoff that represents an important freshwater source and directly influences the sea level on centennial to glacial-interglacial time scales. Surface melt rates can be determined from direct local measurements (e.g. Ahlstrom et al., 2008; Falk et al., 2018). On a larger scale, melt rates can be separated from integral observations such as the the World Glacier Monitoring Service (WGMS) (Zemp et al., 2015, and references therein) or the mass changes of ice sheets detected by the Gravity Recovery and Climate Experiment (GRACE) (Tapley et al., 2004; Wouters et al., 2014), which requires additional information ~~on~~ about other components of the mass balance, such as basal melting, accumulation, sublimation and ~~refreeze~~ refreezing (Sasgen et al., 2012; Tedesco and Fettweis, 2012). In principal, the surface melt rate can be deduced from the net heat flux into the surface layer, as soon as the ice surface has been warmed to the melting point. For low solar elevation angles, however, the net heat flux into the surface layer usually becomes negative, the ice surface cools below the melting point and melting ceases. Consequently, energy balance modelling provides reliable surface melt rates only if sub-daily changes in ice surface temperature and nocturnal freezing are taken into account. Where sub-daily energy balance modelling is not feasible, surface melt is often estimated from empirical schemes. A common approach is the positive degree-day method as formulated e.g. in Reeh (1989). This particularly simple approach linearly relates mean melt rates to positive degree-days, *PDD*, in which *PDD* refers to the temporal integral of near surface temperatures *T* exceeding the melting point. The *PDD*-scheme is ~~computational~~ computationally inexpensive and requires only seasonal or monthly near surface air temperatures as input. Consequently, it has been applied in the context of long climate simulations (e.g. Charbit et al., 2013; Ziemen et al., 2014; Heinemann et al., 2014; Roche et al., 2014; Gierz et al., 2015) ~~or~~ and paleo-

temperature reconstructions (e.g. Box, 2013; Wilton et al., 2017). Another empirical ~~approach, the enhanced temperature index method, ETIM (Pollard, 1980), additionally includes solar radiation~~. This approach is often chosen approach uses a linear function of solar radiation and temperature to predict surface melt. This approach was originally used to estimate ablation rates of glacial ice sheets (Pollard, 1980; Pollard et al., 1980). Formally similar schemes have been chosen, when the influence of solar radiation is changing over orbital time scales ~~(e.g. van den Berg et al., 2008; de Boer et al., 2013) or is enhanced over (the insolation temperature melt (ITM) equation designed to be used with monthly or seasonal forcing on long time scales, e.g. van den B~~ or for debris-covered glaciers ~~(e.g. Pelliotti et al., 2005; Carenzo et al., 2016). Both, the ETIM and the PDD-scheme, where surface albedo, and thereby the effect of insolation, is partly independent of air temperature (enhanced temperature index models (ETIM), c~~ The empirical schemes, however, incorporate parameters, which require a local calibration and which are not necessarily valid under different climate conditions. Additionally, Bauer and Ganopolski (2017) demonstrate that the PDD-scheme fails to drive glacial-interglacial ice volume changes as it cannot account for albedo feedbacks. An alternative ~~approach could be~~ approach could be, to modify and simplify energy balance models in a way that reduces their data requirements and computational costs. Krapp et al. (2017) have formulated ~~an energy balance model a complete surface mass balance model including accumulation, surface melt and refreezing (SEMIC) which can be used with daily forcing and which still is relatively complex. This model or~~ monthly forcing. SEMIC predicts the surface mass balance with a daily time step, but implicitly accounts for the sub-daily temperature ~~variations variability~~ in the surface layer of the ice ~~by making general assumptions about their shape and amplitude to account for diurnal freeze-melt cycles.~~

In the following, we deduce a more simplified scheme from the energy balance, which is formally similar to the ETIM and ITM-schemes but incorporates physically constrained parameters. This new scheme ~~implicitly resolves the diurnal cycle of radiation and~~ only requires monthly means of temperature and solar radiation as input but implicitly resolves the diurnal cycle of radiation. In a first application on the Greenland Ice Sheet, GrIS, we use a simulation of Greenland's climate of the years 1948 to 2016 with the state-of-the-art regional climate and snow pack model MAR (version 3.5.2 forced with reanalysis data from the National Centers for Environmental Prediction–National Center for Atmospheric Research (NCEP) for the years 1948-2016, Kalnay et al., 1996; Fettweis et al., 2017) as a reference.

## 25 **2 The daily melt period and its energy balance**

The temperature of a surface layer of ice  $T_i$  must rise to the melting point  $T_0$  before the net energy uptake  $Q$  of a surface layer can result in a positive surface melt rate  $M$ . In the following, we define background melt conditions on a monthly scale and melt periods on a daily scale.

The near surface air temperature  $T_a$  usually does not exceed  $T_0$  if (after winter) the ice is still too cold to approach  $T_0$  during daytime, so that, on a monthly scale surface air temperatures  $\overline{T}_a$  (with the bar denoting monthly means hereafter) can serve as an indicator for background melting conditions. In the following we assume that monthly mean melt rates  $\overline{M} > 0$  only occur if  $\overline{T}_a > T_{min}$ , where  $T_{min}$  is a typical threshold temperature to allow melt.

The daily melt period shall be that part of a day, during which  $T_i = T_0$  and  $Q \geq 0$ . Here, this period is assumed to be centered

around solar noon, so that it is also defined by the period  $\Delta t_\Phi$ , during which the sun is above a certain elevation angle  $\Phi$  (this minimum elevation angle will be estimated at the end of this section). Further, we define  $q_\Phi$  is the ratio between the mean solar radiation during the short wave radiation at the surface averaged over the daily melt period,  $SW_\Phi$ , and the mean daily solar radiation-short wave radiation at the surface averaged over the whole day,  $SW_0$ , as

$$5 \quad q_\Phi = \frac{SW_\Phi}{SW_0} \quad (1)$$

Both  $\Delta t_\Phi$  and  $q_\Phi$  depend on the diurnal cycle of short wave radiation and can be expressed as functions of latitude and time for any elevation angle  $\Phi$ , including parameters of the Earth's orbit around the sun.  $\Delta t_\Phi$  and  $q_\Phi$  will be derived in Sect. 2.1. During the melt period,  $Q_\Phi$  provides energy for fusion and results in a melt rate, which, averaged over a full day  $\Delta t$ , amounts to

$$10 \quad M = \frac{Q_\Phi \Delta t_\Phi}{\Delta t \rho L_f} \quad (2)$$

with latent heat of fusion  $L_f = 3.34 \times 10^5 \text{ J kg}^{-1}$  and the density of liquid water  $\rho = 1000 \text{ kg m}^{-3}$ . The energy uptake of the surface layer is

$$Q_\Phi = (1 - A)SW_\Phi + \epsilon_i LW \downarrow - LW \uparrow + R \quad (3)$$

with surface albedo  $A$ , long wave emissivity of ice  $\epsilon_i = 0.95$ , downward and upward longwave radiation  $LW \downarrow$  and  $LW \uparrow$  respectively and the sum of all non radiative heat fluxes  $R$ . Per definitionem By definition,

$$LW \uparrow = \epsilon_i \sigma T_0^4 \quad (4)$$

is valid during the melting period, with  $\sigma = 5.67 \times 10^{-8} \text{ W m}^{-2} \text{ K}^{-4}$  being the Stefan-Boltzmann constant. Further  $T_a - T_0$  will be small relative to  $T_0$  so that  $LW \downarrow$  can be linearized to

$$LW \downarrow = \epsilon_a \sigma T_a^4 \approx \epsilon_a \sigma (T_0^4 + 4T_0^3 (T_a - T_0)) \quad (5)$$

20 with  $\epsilon_a \epsilon_a = 0.76$  being the emissivity of air the near-surface air layer, if we neglect long wave radiation from upper atmospheric layers. Neglecting latent heat fluxes and heat fluxes to the subsurface and assuming  $R$  to be dominated by the turbulent sensible heat flux, we parameterize  $R = \beta (T_a - T_0)$ , with the turbulent heat transfer coefficient coefficient  $\beta$ . The turbulent heat transfer coefficient depends on representing the temperature sensitivity of the sensible heat flux. The coefficient  $\beta$  primarily is a function of wind speed and near surface temperature stratification and is estimated to be in the range of 7 to 20  $\text{W m}^{-2} \text{ K}^{-1}$  on  
 25 melting surfaces (Braithwaite, 1995, and references therein). Rewriting Eq. (3) for monthly means, we replace  $(T_a - T_0)$  with  $PDD(\bar{T}_a)$ .  $PDD(\bar{T}_a)$  serves here as an estimate for the temperatures effectively causing melt (Krebs-Kanzow et al., 2018) and is approximated according to Braithwaite (2009) can be estimated as  $\beta = \alpha u$  with  $\alpha \approx 4 \text{ W s m}^{-3} \text{ K}^{-1}$  at low altitudes. To find a formulation that is based on monthly climate forcing we need to estimate the mean melt period temperature from monthly mean temperatures. Near surface air temperature measurements from PROMICE stations on the GrIS reveal a good agreement

between monthly mean temperatures of the daily melt periods and the  $PDD_{\sigma=3.5}$  approximated as in Braithwaite (1985) from monthly mean near surface temperature  $\bar{T}_a$  and a constant standard deviation of  $5^\circ\text{C}$  as in Braithwaite (1985)  $\sigma = 3.5^\circ\text{C}$  (Fig. S1 in the supplement). Rewriting Eq. (3) for monthly means, we thus replace  $(T_a - T_0)$  with  $PDD_{\sigma=3.5}(\bar{T}_a)$ . The above approximations and assumptions then yield an implicitly diurnal Energy Balance Model (dEBM), which only requires monthly mean temperatures and solar radiation as atmospheric forcing, while albedo may be parameterized as in common surface mass balance schemes (e.g. Krapp et al., 2017):

$$\bar{M} \approx \left( q_\Phi (1 - A) \overline{SW}_0 + c_1 PDD_{\sigma=3.5}(\bar{T}_a) + c_2 \right) \frac{\Delta t_\Phi}{\Delta t \rho L_f} \quad (6)$$

where

$$\begin{aligned} c_1 &= \epsilon_i \epsilon_a \sigma 4 T_0^3 + \beta \\ &= 3.5 \text{ W m}^{-2} \text{ K}^{-1} + \beta \\ c_2 &= -\epsilon_i \sigma T_0^4 + \epsilon_a \epsilon_i \sigma (T_0^4) \\ &= -71.9 \text{ W m}^{-2} \end{aligned} \quad (7)$$

for any month that complies with the background melting condition  $\bar{T}_a > T_{min}$ .

The sensitivity of the scheme to the choices of  $\beta$  and to enhanced long wave radiation due to cloud cover or changed atmospheric composition is considered in sect. 4.

Both  $q_\Phi$  and  $\Delta t_\Phi$  strongly depend on latitude and month of the year. Thus, a given combination of insolation and temperature forcing yields different melt rates at different locations or seasons. The sensitivity of the dEBM to latitude is further investigated in sect. 4.

Finally, we use that  $M = 0$  in the moment when the sun passes  $\Phi$  and formulate the instantaneous energy balance analogously to Eq. (6) as

$$(1 - A) \tau \widehat{S}_r \sin \Phi \underline{S}_0 + c_1 (T_a(\Phi) - T_0) + c_2 = 0. \quad (8)$$

with  $\underline{S}_0$  being the irradiance normal to a surface at the bottom  $\tau$  representing the transmissivity of the atmosphere over the melting surface,  $\widehat{S}_0$  being the solar flux density at the top of the atmosphere and the instantaneous (TOA), and the instantaneous air temperature  $T_a(\Phi)$ . Assuming that  $T_a(\Phi) \approx T_0$  and using a typical  $\underline{S}_0$  one  $\tau \widehat{S}_r$  estimate for the melt season of the model domain, we can estimate

$$\Phi = \arcsin \frac{-c_2}{(1 - A) \underline{S}_0} \arcsin \frac{-c_2}{(1 - A) \tau \widehat{S}_r} \quad (9)$$

independent of time or location. The dEBM's sensitivity to the range of possible elevation angles is discussed in sect. 4.

## 25 2.1 Derivation of $\Delta t_\Phi$ and $q_\Phi$

The derivation of  $\Delta t_\Phi$  and  $q_\Phi$  is based on spherical trigonometry and fundamental astronomic considerations which, for instance, are discussed in detail in Liou (2002). The elevation angle  $\vartheta$  of the sun changes throughout a day according to

$$\sin \vartheta = \sin \phi \sin \delta + \cos \phi \cos \delta \cos h(\vartheta) \quad (10)$$

with the latitude  $\phi$ , the solar inclination angle  $\delta$  and the hour angle  $h$ .

5 The time which the sun spends above an elevation angle  $\vartheta$  then is

$$\Delta t_\vartheta = \frac{\Delta t}{\pi} h(\vartheta) = \frac{\Delta t}{\pi} \arccos \frac{\sin \vartheta - \sin \phi \sin \delta}{\cos \phi \cos \delta}. \quad (11)$$

~~At the top We assume that surface solar radiation is proportional to the TOA radiation  $\widehat{S}_r$  throughout a day (i.e. we neglect that transmissivity of the atmosphere (TOA)the mean  $\tau$  is usually increasing with elevation angle and assume that cloud cover does not exhibit a diurnal cycle). The solar radiation during the period which the sun spends above a certain elevation angle  $\vartheta$~~

10 is then

$$\underline{SW}_\vartheta = \frac{\widehat{S}}{\Delta t_\vartheta} \frac{\tau \widehat{S}_r}{\pi \Delta t_\vartheta} (h(\vartheta) \sin \phi \sin \delta + (\cos \phi \cos \delta \sin h(\vartheta))) \quad (12)$$

~~with  $\widehat{S}$  being the TOA solar radiation on a surface perpendicular to its rays.  $\widehat{S}$  is seasonally varying due to the eccentricity of the Earth's orbit. If we assume surface solar radiation to be proportional to the top-of-atmosphere radiation throughout a day (i.e. there is no diurnal cycle in the transmissivity of the atmosphere) Eq. 12 also allows to estimate  $\tau \widehat{S}_r$  from  $SW_0$ . Furthermore~~

15 we can calculate the ratio between the mean short wave radiation during the melt period  $\underline{SWD}_\Phi$  ~~also  $SW_0$~~  and the mean daily downward short wave radiation  ~~$SWD_0$  also  $SW_0$~~  at the surface ~~independent of  $\tau \widehat{S}_r$~~ :

$$q_\Phi = \frac{\underline{SW}_\Phi}{\underline{SW}_0} = \frac{h(\Phi) \sin \phi \sin \delta + \cos \phi \cos \delta \sin h(\Phi)}{h(0) \sin \phi \sin \delta + \cos \phi \cos \delta \sin h(0)} \frac{\Delta t}{\Delta t_\Phi}. \quad (13)$$

## 3 First evaluation of the scheme

~~Choosing  $\beta = 10 \text{ W m}^{-2} \text{ K}^{-1}$  and using  $\epsilon_a = 0.76$  for the present greenhouse gas concentration yields  $c_1 = 14.4 \text{ W m}^{-2} \text{ K}^{-1}$  and  $c_2 = -71.9 \text{ W m}^{-2}$ . As a background melting condition we here use  $\bar{T}_a > -6.5 \text{ K}$ . Further, assuming The dEBM and two empirical schemes are calibrated and evaluated using the state-of-the-art regional climate and snow pack model MAR (Fettweis et al., 2017) as a reference.~~

~~The elevation angle used in the dEBM is estimated as  $\Phi = 17.5^\circ$ , applying Eq. (9) with a typical albedo of 0.7 and  $S_0 = 600 \text{ W m}^{-2}$  in Eq.  $\widehat{S}_r = 800 \text{ W m}^{-2}$  being roughly estimated from the summer insolation in the ablation regions (Eq. 12). (9) yields~~

25  ~~$\Phi = 23.5^\circ$ . The new scheme is applied This estimate corresponds to a transmissivity of  $\tau \approx 0.6$  which is in good agreement with Ettema et al. (2010). Further, the dEBM is optimized to reproduce the total annual Greenland surface melt averaged over the~~

entire MAR-simulation by calibrating the background melting condition as  $\bar{T}_a > -6.5^\circ\text{C}$  and the parameter  $\beta = 10 \text{ W m}^{-2} \text{ K}^{-1}$ . We then apply the scheme to  $\overline{SW}_0$ ,  $PDD(\bar{T}_a)$   $PDD_{\sigma=3.5}(\bar{T}_a)$  and albedo  $A$  from a simulation-MAR-simulation of Greenland’s climate (years 1948 to 2016) with the state-of-the-art regional climate and snow pack model MAR (Fettweis et al., 2017). The (Fettweis et al., 2017) and compare estimated melt rates are then compared to with the respective MAR melt rates.

- 5 Two empirical schemes are tested and evaluated considered in the same way: a PDD-scheme based on  $PDD(\bar{T}_a)$   $PDD_{\sigma=5}(\bar{T}_a)$ , as defined and calibrated in Krebs-Kanzow et al. (2018) and a common-ETIM (Pollard, 1980), which estimates melt as-

$$M = \frac{((1 - A)\overline{SW}_0 + k_1 PDD(\bar{T}_a) + k_2) \frac{1}{\rho L_f}}$$

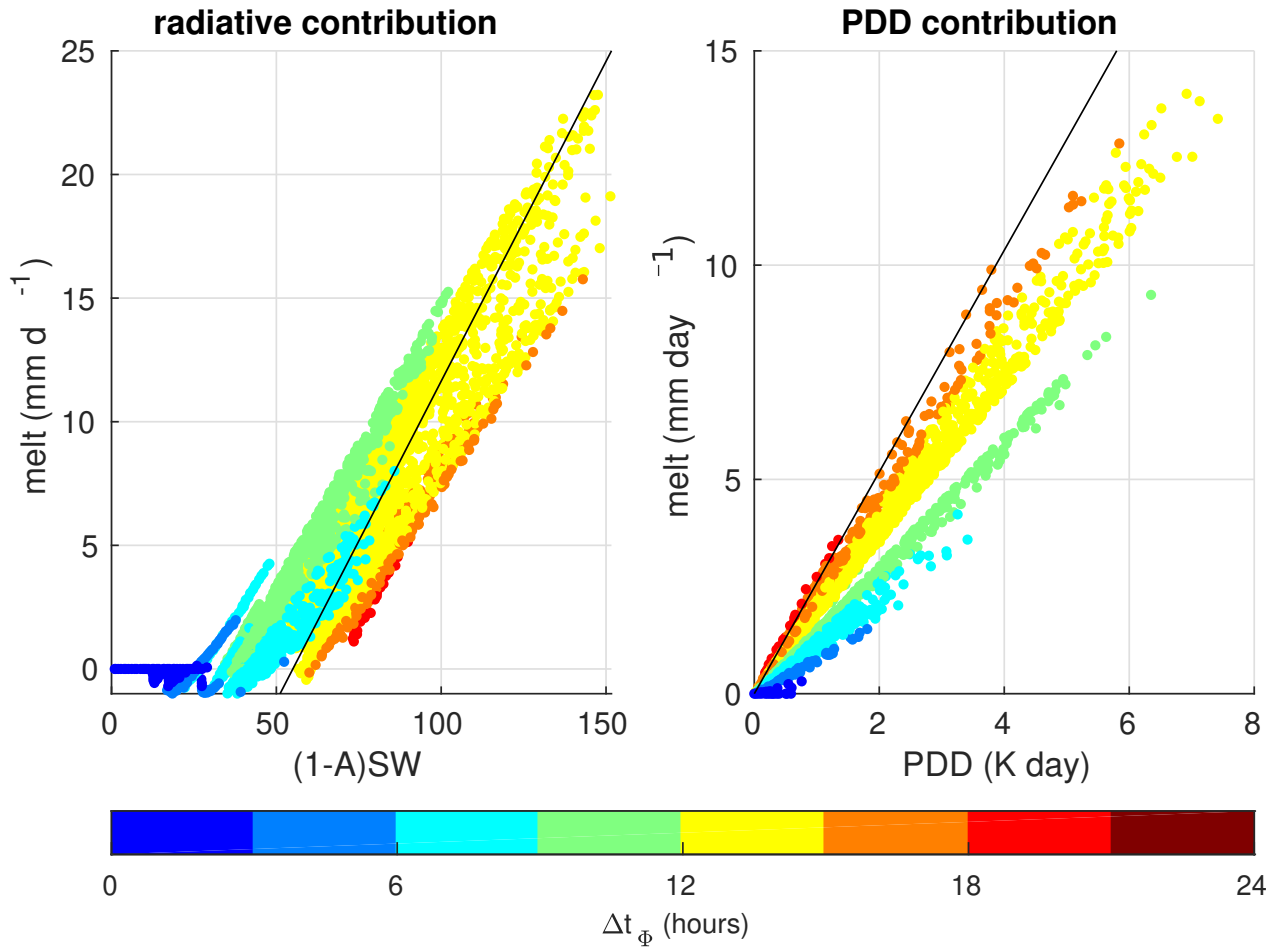
where scheme, in the following referred to as  $dEBM_{const}$ , which is a simplified variant of the dEBM where parameters are constant in time and space:

$$10 \quad M = \frac{((1 - A)\overline{SW}_0 + k_1 PDD_{\sigma=3.5}(\bar{T}_a) + k_2) \frac{1}{\rho L_f}}{\quad} \quad (14)$$

with  $k_1 = 10 \text{ W m}^{-2} \text{ K}^{-1}$  and  $k_2 = -60.5 \text{ W m}^{-2}$  chosen similar to Robinson et al. (2010). We here also use  $\bar{T}_a > -6.5 \text{ K}$   $k_2 = -55 \text{ W m}^{-2}$ . The  $dEBM_{const}$  is very similar to the ITM-scheme and also uses similar parameters as in Robinson et al. (2010), but includes PDD instead of temperature, which particularly yields different results for low temperatures. As in Robinson et al. (2010), we treat  $k_2$  as a tuning parameter to optimize the scheme and also use  $\bar{T}_a > -6.5^\circ\text{C}$  as a background melting condition. For

- 15 better comparison, all schemes have been optimized to-  
 The computational cost of the dEBM in this application is very similar to the other two schemes as parameters are computed only once prior to the application. All schemes reproduce the total annual Greenland surface melt averaged over the entire MAR-simulation of 489 Gt with a relative bias not exceeding 1% (the mean bias is  $-4.3 \text{ Gt}$   $0.4 \text{ Gt}$  for the PDD scheme,  $0.8 \text{ Gt}$  for the ETIM and  $-1.2 \text{ Gt}$   $-0.6 \text{ Gt}$  for the  $dEBM_{const}$  and  $-2.0 \text{ Gt}$  for the dEBM). For the PDD-scheme we use the calibrated parameters from Krebs-Kanzow et al. (2018), in the ETIM we optimized the background melting condition and  $k_2$  and in the dEBM we optimized the background melting condition and the turbulent heat transfer coefficient  $\beta$  within the range given in Braithwaite (1995) These calibrations are primarily conducted to facilitate a fair comparison between the different schemes and are not necessarily optimal for other applications.

- Equations Equations (6) and (14) appear formally similar, with the first and third term representing the radiative contribution and the second term representing the PDD contribution being temperature dependent (the “temperature contribution”) and the first and third term being independent of temperature and only depending on solar radiation (the “radiative contribution”). However, the respective parameters cannot be compared directly, as the  $\Delta t_\Phi$  and  $q_\Phi$  depend on latitude and month.  $\Delta t_\Phi$  and  $q_\Phi$  modulate the the radiative contribution and  $\Delta t_\Phi$  modulates the PDD-temperature contribution in Eq. (6). Fig. 1a illustrates the radiative and Fig. 1b the PDD-temperature contributions as diagnosed from the MAR simulation in comparison to the respective contribution from the ETIM  $dEBM_{const}$ . On the GrIS the radiative contribution can exceed  $40 \text{ mm d}^{-1}$   $25 \text{ mm d}^{-1}$  in the summer months and the two schemes appear qualitatively similar. However, a flat ecliptic (going along with The radiative



**Figure 1.** a) Contribution of the first and third term (radiative contribution) and b) of the second term (PDD-temperature contribution) in Eq. (6) to monthly melt rates as diagnosed with climatological temperatures and solar radiation from the MAR simulation. Colors indicate length of melt period ( $\Delta t_{\phi}$ ). The black lines represent the respective prediction of the  $ETIM-dEBM_{const}$  according to Eq. (14)

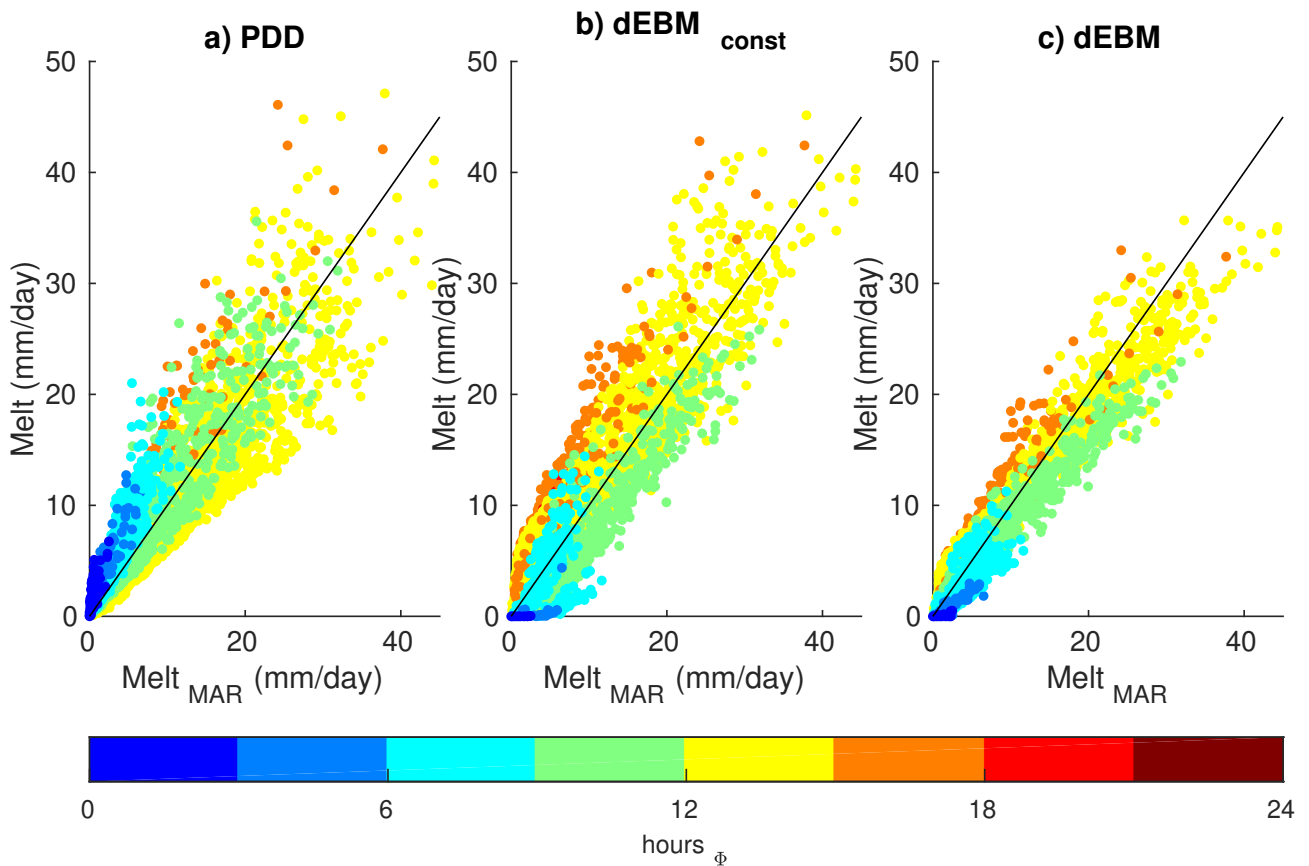
contribution in the dEBM becomes less efficient for long melt periods at high latitudes or with, as the same insolation must balance the outgoing longwave radiation for a longer time. On the other hand, radiative contribution can also decrease towards short melt periods in autumn and spring) reduces  $q_{\Phi}$  and consequently reduces the radiative contribution in the dEBM. As a result considerable difference between dEBM and ETIM are visible both for short and long melt periods. The PDD, if the sun only marginally rises above the minimum elevation angle at solar noon. This effect becomes important for higher estimates of the minimum elevation angles in high latitudes (Sect. 4). The temperature contribution of the dEBM appears reduced in comparison to the ETIM and does not exceed  $12 \text{ mm d}^{-1}$   $15 \text{ mm d}^{-1}$  (Fig. 1b). In the dEBM the PDD contribution and becomes more efficient with longer melt periods and would agree with the ETIM  $dEBM_{const}$  for a melt period of 16-18 hours.

Atmospheric forcing Atmospheric forcing (insolation and temperature) and albedo are here derived-obtained from MAR output, and are fully consistent with the MAR melt rates. Consequently, we can evaluate the skill of the considered schemes independent of the quality of the atmospheric forcing and the representation of albedo. On the other hand, we can not evaluate the performance of the schemes for defective input. In this respect With respect to error propagation the PDD-scheme might be more robust and, as it only requires temperature as a forcing and only distinguishes between snow and ice but does not require albedo. Due to Given the ideal input, all schemes reproduce the year-to-year evolution of the total Greenland surface melt of the MAR-simulation reasonably well (Fig. S1-S3 in the supplement). With The PDD-scheme yields increasing errors with intensifying surface melt rates, both, the PDD-scheme and the ETIM, yield increasing errors, which is not apparent for the  $dEBM_{const}$  and dEBM (Fig. 2). On the other hand, the dEBM cannot reproduce melt rates which may still occur even though the sun does not pass over the critical elevation angle and the duration of the melt period vanishes. The root mean square error of the predicted monthly, local melt rates relative to MAR melt rates is  $3.6 \text{ mm d}^{-1}$  for the PDD scheme,  $5.0 \text{ mm d}^{-1}$  for the ETIM and  $3.3 \text{ mm d}^{-1}$  for the dEBM, if we only consider grid points and months which comply with the background melting condition of  $\bar{T}_a > -6.5 \text{ K}$   $dEBM_{const}$  particularly overestimates (underestimates) melt rates for very short (long) melt periods. In comparison to the two empirical schemes, the dEBM produces smaller local errors with biases-biases being pronounced only in a narrow band along the ice sheet's margins (Fig.3).

#### 4 Sensitivity to model parameters and boundary conditions

Sensitivity to tuning parameters: In the above application, the parameter  $\beta$  for sensible heat and the background melting condition  $T_{min}$  have served as tuning parameters. The parameter  $\beta = 10 \text{ W m}^{-2} \text{ K}^{-1}$  was determined by optimizing the scheme to MAR melt rates. This value agrees reasonably well with the moderate wind speeds found in PROMICE observations during melt periods (Fig. S2 in the supplement). Changing  $\beta$  by  $\pm 20\%$  changes the total annual Greenland surface melt by  $\pm 3\%$ . The choice of  $T_{min} = -6.5^\circ \text{C}$  is in good agreement with observations, which reveal no substantial melt for temperatures  $< -7^\circ \text{C}$  (e.g. Orvig, 1954). Increasing the background melting condition  $T_{min}$  particularly reduces the melt rates at high elevations, while reducing  $T_{min}$  results in a longer melting season and increases the annual surface melt. Using no background melting condition at all results in unrealistic melt rates at high elevations and would almost double the predicted total Greenland

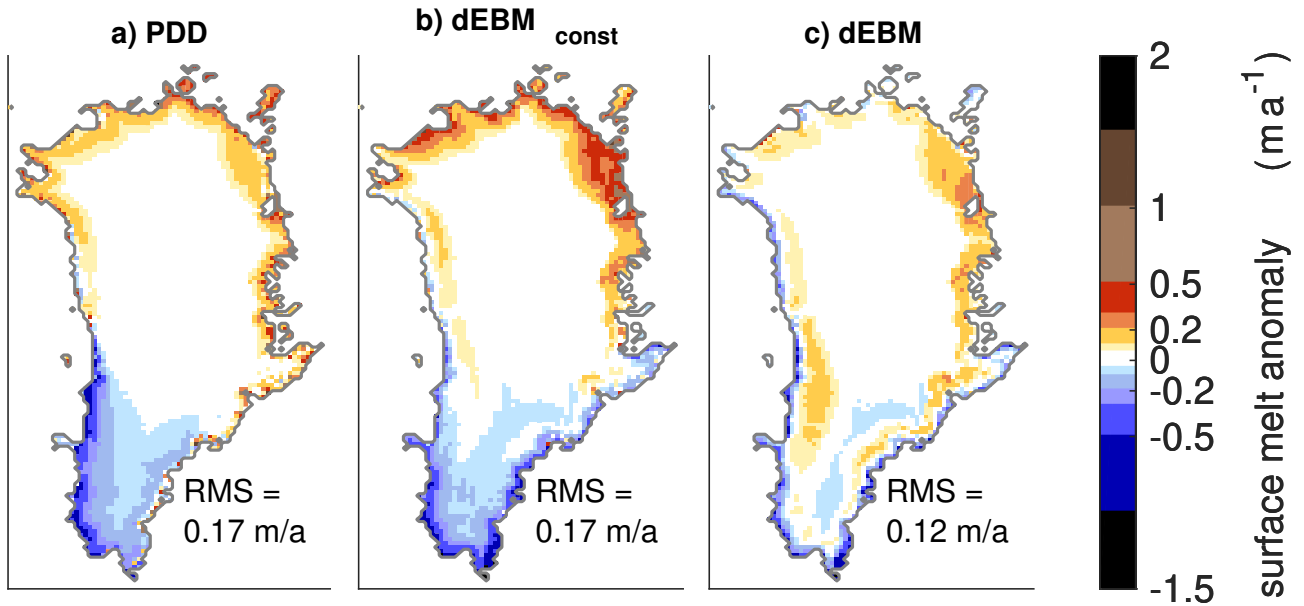




**Figure 2.** Multi-year monthly mean meltrates averaged of the years 1948-2016 as predicted by a) the PDD-scheme, b) the  $ETIM-dEBM_{const}$  and c) the dEBM against respective MAR melt rates. Colors reflect the  $\text{length-length}$  of the daily melt period. Identity is displayed as a black line in all panels for comparison.

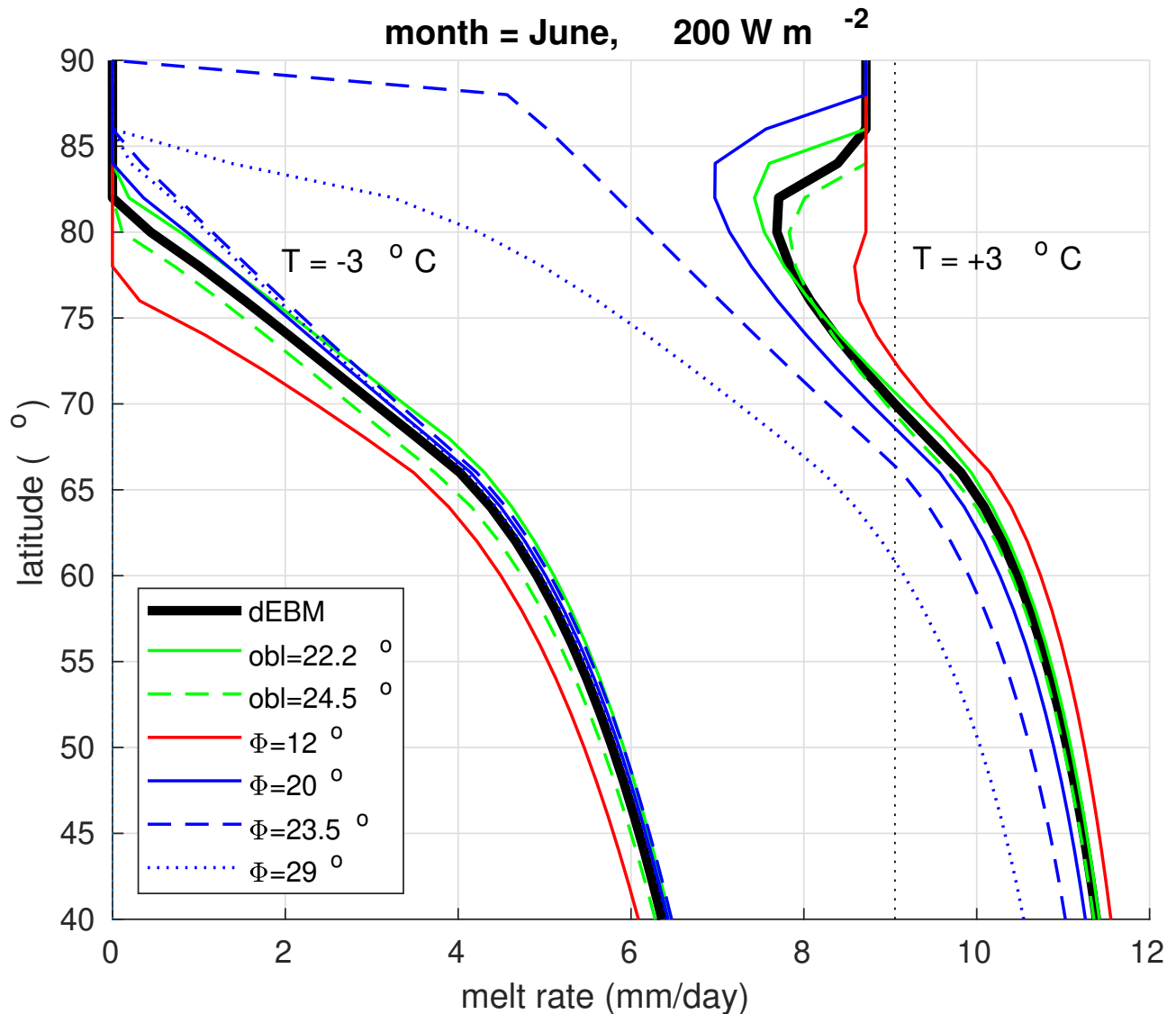
surface melt. Changing  $T_{min}$  by  $\pm 1K$  changes the predicted mean annual surface melt by  $\pm 8\%$  for the MAR simulation used in this study. Intense surface melt is usually accompanied by warm temperatures and is thus insensitive to the choice of  $T_{min}$ . As refreezing particularly suppresses the contribution of weak surface melt at low temperatures, the resulting runoff can be expected to be less sensitive to the choice of  $T_{min}$ .

- Sensitivity to diurnal cycle of solar radiation:** Melt schemes which do not include the diurnal cycle of radiation will predict the same melt rate for a given combination of insolation and temperature forcing, irrespective of latitude or season. By contrast, Fig. 4 indicates a strong sensitivity of the dEBM surface melt predictions to latitude in summer. According to the dEBM, a short melt period with intensive solar radiation is causing melt more effectively than a longer melt period with accordingly weaker solar radiation. This sensitivity is particularly prominent in high latitudes and may explain the latitudinal bias found in many studies which do not resolve radiation on sub-daily time scales (e.g. Plach et al., 2018; Krebs-Kanzow et al., 2018; Krapp et al., 2017).
- Sensitivity to orbital configuration and transmissivity of the atmosphere:** The TOA solar flux density  $\widehat{S}_r$  depends on



**Figure 3.** Bias between yearly melt rates as predicted by the individual schemes and as simulated by MAR, averaged over the whole simulation: a) PDD b) ~~ETIM~~-*dEBM<sub>const</sub>* c) the proposed new scheme dEBM. The respective root mean square error (RMS) is given in the individual panels.

the distance between Earth and Sun and due to the eccentricity of the Earth's orbit gradually varies by  $\pm 3.5\%$  from the solar constant from December to July respectively. On orbital time scales this seasonal deviation from the solar constant may amount to 10%. Transmissivity  $\tau$ , on the other hand, strongly depends on cloud cover and atmospheric composition and additionally increases with the solar elevation angle. In consequence the minimum elevation angle  $\Phi$  may be less than  $13^\circ$  ( $\tau \widehat{S}_r = 1150 \text{ W m}^{-2}$  for clear sky, intense summer insolation). For overcast sky and weak summer insolation, we can ultimately expect  $\tau \widehat{S}_r < 400 \text{ W m}^{-2}$ . In that case, however, it is not justified to use the clear sky emissivity in Eqs. 5 and 7. Consequently, the proposed scheme is no longer suitable, as net outgoing long wave radiation will vanish and the energy balance will become very sensitive to turbulent heat fluxes. Applications aiming at continental ice sheets with climatological forcing will be however restricted to a much narrower range of scenarios. As one can expect that transmissivity decreases towards the morning and afternoon hours, it may be justified to reduce the estimate of  $\tau \widehat{S}_r$  by a few percent. Fig. 4 reveals that the scheme becomes very sensitive if the minimum elevation angle  $\Phi$  takes values close to or larger than the obliquity of the Earth. Under such conditions the duration of the melt period will vanish near the Pole. On the other hand the scheme is remarkably insensitive to intensified insolation (and accordingly reduced elevation angle  $\Phi$ ) or variations in the obliquity. Accordingly, estimating the elevation angle locally and for each month using Eq. 12, which is possible but computationally more expensive, does not improve the skill of the dEBM noticeably (not shown).



**Figure 4.** Sensitivity of the dEBM: June surface melt rate as predicted for  $SW_0 = 200 \text{ W m}^{-2}$ ,  $A = 0.7$ ,  $T_a = -3^\circ \text{C}$  (left curves) and  $T_a = 3^\circ \text{C}$  (right curves). Black: predictions with parameters as used for the presented simulation of Greenland's surface melt. Green: parameters are recalculated using the minimum (solid) and maximum (dashed) obliquity of the last 1 million years. Blue: parameters are recalculated after the minimum elevation angle is adjusted to a reduced solar density flux at the surface of  $\tau \hat{S}_r = 700 \text{ W m}^{-2}$  (solid),  $\tau \hat{S}_r = 600 \text{ W m}^{-2}$  (dashed),  $\tau \hat{S}_r = 500 \text{ W m}^{-2}$  (dots). Red: parameters are recalculated after the minimum elevation angle is adjusted to an intensified solar density flux at the surface of  $\tau \hat{S}_r = 1150 \text{ W m}^{-2}$ . The  $dEBM_{const}$  predicts 0 mm/day for  $SW_0 = 200 \text{ W m}^{-2}$ ,  $A = 0.7$ ,  $T_a = -3^\circ \text{C}$  and 9 mm/day for  $SW_0 = 200 \text{ W m}^{-2}$ ,  $A = 0.7$ ,  $T_a = 3^\circ \text{C}$  (black dots).

## 15 5 Discussion and conclusion

The presented new scheme for surface melt (dEBM) requires, like ~~enhanced temperature index methods~~ the insolation temperature melt scheme (ITM), monthly mean air temperatures and insolation as input, but implicitly also includes the diurnal cycle. Together with suitable schemes for albedo and ~~refreeze (e.g. the parameterizations used together with the enhanced temperature index methods)~~ (e.g. the parameterizations presented in Robinson et al., 2010), it may replace empirical surface melt schemes which are commonly used in ice sheet modelling on long time scales.

An application to the Greenland Ice Sheet indicates, that the scheme may improve the spatial representation of surface melt in comparison to common empirical schemes. However, an evaluation to an independent data base is desirable. The most important advantage of the dEBM over empirical schemes may be, that it can be globally applied to other ice sheets and glaciers and under different climate conditions, as parameters in the scheme are physically constrained and implicitly account for the orbital configuration.

In the presented formulation a threshold temperature serves as a prerequisite for surface melt on monthly time scales. This threshold temperature should be considered as a tuning parameter, as the representation of the ice-atmosphere boundary layer in Earth system models may differ considerably from the MAR simulation, which here has served as a reference. Furthermore, long wave radiation and non-radiative heat fluxes are only crudely represented. Depending on the application, it may be advisable to adapt the parameterization of turbulent heat fluxes and long wave radiation to different climate regimes in order to account for changed wind speed, humidity, cloud cover or greenhouse gas concentration.

The daily melt period is defined by a minimum solar elevation angle. Together with the melt period, parameters in the dEBM depend on latitude and month of the year, but do not change from year to year if the minimum solar elevation angle is kept constant and the orbital configuration remains the same. For the Greenland Ice Sheet, a minimum solar elevation angle of ~~23.5°~~ 17.5° was roughly estimated from the mean summer insolation normal to a surface at the bottom of the atmosphere. ~~Since the normal summer insolation depends on the orbital configurations and atmospheric transmissivity, the minimum solar elevation angle should be readjusted for applications on the southern hemisphere, accounting for the stronger austral summer insolation. On long time scales the elevation angle may also change with~~ The dEBM is very sensitive if the intensity of solar radiation is substantially weaker than in the presented application (e.g. due to cloud cover or atmospheric water content). In this case it is necessary to carefully re-estimate the minimum elevation angle and to adjust the model parameters accordingly. The scheme appears to be relatively insensitive to changes in the orbital configuration and ~~atmospheric composition.~~ In the presented formulation a threshold temperature serves as a prerequisite for surface melt on monthly time scales. This threshold temperature should be considered as a tuning parameter, as the representation of the ice-atmosphere boundary layer in Earth system models may differ considerably from the MAR simulation, which here has served as a reference. Furthermore, non-radiative heat fluxes are only crudely represented. Depending on application, it may be advisable to adapt the heat transfer coefficient to different climate regimes or to include additional atmospheric variables, such as wind speed and humidity, for a better parameterisations of turbulent heat fluxes the parameters choices in this study may be valid in a wider range of settings.

The presented formulation has been designed for long Earth System Model applications, but it may be adapted to be also used

in the context of climate reconstructions or to be applied on regional or local scales. Furthermore, having defined the daily melt period by the minimum elevation angle, it should also be possible to estimate the amount of refreezing by considering the energy balance of the remainder of the day, following a similar approach as in Krapp et al. (2017).

*Competing interests.* The authors declare that they have no competing interests

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