

Brief communication: An Ice surface melt scheme including the diurnal cycle of solar radiation

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Abstract.

We propose a surface melt scheme for glaciated land surfaces, which only requires monthly mean short wave radiation and temperature as inputs, yet implicitly accounts for the diurnal cycle of short wave radiation. The scheme is deduced from the energy balance of a daily melt period which is defined by a minimum solar elevation angle. The scheme yields a better spatial representation of melting than common empirical schemes when applied to the Greenland Ice Sheet, using a 1948-2016 regional climate and snow pack simulation as a reference. The scheme is physically constrained and can be adapted to other regions or time periods.

1 Introduction

The surface melt of ice sheets, ice caps and glaciers results in a freshwater runoff that represents an important freshwater source and directly influences the sea level on centennial to glacial-interglacial time scales. Surface melt rates can be determined from direct local measurements (e.g. Ahlstrom et al., 2008; Falk et al., 2018). On a larger scale, melt rates can be separated from integral observations such as the the World Glacier Monitoring Service (WGMS) (Zemp et al., 2015, and references therein) or the mass changes of ice sheets detected by the Gravity Recovery and Climate Experiment (GRACE) (Tapley et al., 2004; Wouters et al., 2014), which requires additional information ~~on~~ about other components of the mass balance, such as basal melting, accumulation, sublimation and ~~refreeze~~ refreezing (Sasgen et al., 2012; Tedesco and Fettweis, 2012). In principal, the surface melt rate can be deduced from the net heat flux into the surface layer, as soon as the ice surface has been warmed to the melting point. For low solar elevation angles, however, the net heat flux into the surface layer usually becomes negative, the ice surface cools below the melting point and melting ceases. Consequently, energy balance modelling provides reliable surface melt rates only if sub-daily changes in ice surface temperature and nocturnal freezing are taken into account. Where sub-daily energy balance modelling is not feasible, surface melt is often estimated from empirical schemes. A common approach is the positive degree-day method as formulated e.g. in Reeh (1989). This particularly simple approach linearly relates mean melt rates to positive degree-days, *PDD*, in which *PDD* refers to the temporal integral of near surface temperatures *T* exceeding the melting point. The *PDD*-scheme is ~~computational~~ computationally inexpensive and requires only seasonal or monthly near surface air temperatures as input. Consequently, it has been applied in the context of long climate simulations (e.g. Charbit et al., 2013; Ziemen et al., 2014; Heinemann et al., 2014; Roche et al., 2014; Gierz et al., 2015) ~~or~~ and paleo-

temperature reconstructions (e.g. Box, 2013; Wilton et al., 2017). Another empirical ~~approach, the enhanced temperature index method, ETIM (Pollard, 1980), additionally includes solar radiation~~. This approach is often chosen approach uses a linear function of solar radiation and temperature to predict surface melt. This approach was originally used to estimate ablation rates of glacial ice sheets (Pollard, 1980; Pollard et al., 1980). Formally similar schemes have been chosen, when the influence of solar radiation is changing over orbital time scales ~~(e.g. van den Berg et al., 2008; de Boer et al., 2013) or is enhanced over (the insolation temperature melt (ITM) equation designed to be used with monthly or seasonal forcing on long time scales, e.g. van den B~~ or for debris-covered glaciers ~~(e.g. Pelliotti et al., 2005; Carenzo et al., 2016). Both, the ETIM and the PDD-scheme, where surface albedo, and thereby the effect of insolation, is partly independent of air temperature (enhanced temperature index models (ETIM), c~~ The empirical schemes, however, incorporate parameters, which require a local calibration and which are not necessarily valid under different climate conditions. Additionally, Bauer and Ganopolski (2017) demonstrate that the PDD-scheme fails to drive glacial-interglacial ice volume changes as it cannot account for albedo feedbacks. An alternative ~~approach could be~~ approach could be, to modify and simplify energy balance models in a way that reduces their data requirements and computational costs. Krapp et al. (2017) have formulated ~~an energy balance model a complete surface mass balance model including accumulation, surface melt and refreezing (SEMIC) which can be used with daily forcing and which still is relatively complex. This model or~~ monthly forcing. SEMIC predicts the surface mass balance with a daily time step, but implicitly accounts for the sub-daily temperature ~~variations variability~~ in the surface layer of the ice ~~by making general assumptions about their shape and amplitude to account for diurnal freeze-melt cycles.~~

In the following, we deduce a more simplified scheme from the energy balance, which is formally similar to the ETIM and ITM-schemes but incorporates physically constrained parameters. This new scheme ~~implicitly resolves the diurnal cycle of radiation and~~ only requires monthly means of temperature and solar radiation as input but implicitly resolves the diurnal cycle of radiation. In a first application on the Greenland Ice Sheet, GrIS, we use a simulation of Greenland's climate of the years 1948 to 2016 with the state-of-the-art regional climate and snow pack model MAR (version 3.5.2 forced with reanalysis data from the National Centers for Environmental Prediction–National Center for Atmospheric Research (NCEP) for the years 1948-2016, Kalnay et al., 1996; Fettweis et al., 2017) as a reference.

25 **2 The daily melt period and its energy balance**

The temperature of a surface layer of ice T_i must rise to the melting point T_0 before the net energy uptake Q of a surface layer can result in a positive surface melt rate M . In the following, we define background melt conditions on a monthly scale and melt periods on a daily scale.

The near surface air temperature T_a usually does not exceed T_0 if (after winter) the ice is still too cold to approach T_0 during daytime, so that, on a monthly scale surface air temperatures \overline{T}_a (with the bar denoting monthly means hereafter) can serve as an indicator for background melting conditions. In the following we assume that monthly mean melt rates $\overline{M} > 0$ only occur if $\overline{T}_a > T_{min}$, where T_{min} is a typical threshold temperature to allow melt.

The daily melt period shall be that part of a day, during which $T_i = T_0$ and $Q \geq 0$. Here, this period is assumed to be centered

around solar noon, so that it is also defined by the period Δt_Φ , during which the sun is above a certain elevation angle Φ (this minimum elevation angle will be estimated at the end of this section). Further, we define q_Φ is the ratio between the mean solar radiation during the short wave radiation at the surface averaged over the daily melt period, SW_Φ , and the mean daily solar radiation-short wave radiation at the surface averaged over the whole day, SW_0 , as

$$5 \quad q_\Phi = \frac{SW_\Phi}{SW_0} \quad (1)$$

Both Δt_Φ and q_Φ depend on the diurnal cycle of short wave radiation and can be expressed as functions of latitude and time for any elevation angle Φ , including parameters of the Earth's orbit around the sun. Δt_Φ and q_Φ will be derived in Sect. 2.1. During the melt period, Q_Φ provides energy for fusion and results in a melt rate, which, averaged over a full day Δt , amounts to

$$10 \quad M = \frac{Q_\Phi \Delta t_\Phi}{\Delta t \rho L_f} \quad (2)$$

with latent heat of fusion $L_f = 3.34 \times 10^5 \text{ J kg}^{-1}$ and the density of liquid water $\rho = 1000 \text{ kg m}^{-3}$. The energy uptake of the surface layer is

$$Q_\Phi = (1 - A)SW_\Phi + \epsilon_i LW \downarrow - LW \uparrow + R \quad (3)$$

with surface albedo A , long wave emissivity of ice $\epsilon_i = 0.95$, downward and upward longwave radiation $LW \downarrow$ and $LW \uparrow$ respectively and the sum of all non radiative heat fluxes R . Per definitionem By definition,

$$LW \uparrow = \epsilon_i \sigma T_0^4 \quad (4)$$

is valid during the melting period, with $\sigma = 5.67 \times 10^{-8} \text{ W m}^{-2} \text{ K}^{-4}$ being the Stefan-Boltzmann constant. Further $T_a - T_0$ will be small relative to T_0 so that $LW \downarrow$ can be linearized to

$$LW \downarrow = \epsilon_a \sigma T_a^4 \approx \epsilon_a \sigma (T_0^4 + 4T_0^3 (T_a - T_0)) \quad (5)$$

20 with $\epsilon_a \epsilon_a = 0.76$ being the emissivity of air the near-surface air layer, if we neglect long wave radiation from upper atmospheric layers. Neglecting latent heat fluxes and heat fluxes to the subsurface and assuming R to be dominated by the turbulent sensible heat flux, we parameterize $R = \beta (T_a - T_0)$, with the turbulent heat transfer coefficient coefficient β . The turbulent heat transfer coefficient depends on representing the temperature sensitivity of the sensible heat flux. The coefficient β primarily is a function of wind speed and near surface temperature stratification and is estimated to be in the range of 7 to 20 $\text{W m}^{-2} \text{ K}^{-1}$ on
 25 melting surfaces (Braithwaite, 1995, and references therein). Rewriting Eq. (3) for monthly means, we replace $(T_a - T_0)$ with $PDD(\bar{T}_a)$. $PDD(\bar{T}_a)$ serves here as an estimate for the temperatures effectively causing melt (Krebs-Kanzow et al., 2018) and is approximated according to Braithwaite (2009) can be estimated as $\beta = \alpha u$ with $\alpha \approx 4 \text{ W s m}^{-3} \text{ K}^{-1}$ at low altitudes. To find a formulation that is based on monthly climate forcing we need to estimate the mean melt period temperature from monthly mean temperatures. Near surface air temperature measurements from PROMICE stations on the GrIS reveal a good agreement

between monthly mean temperatures of the daily melt periods and the $PDD_{\sigma=3.5}$ approximated as in Braithwaite (1985) from monthly mean near surface temperature \bar{T}_a and a constant standard deviation of 5°C as in Braithwaite (1985) $\sigma = 3.5^\circ\text{C}$ (Fig. S1 in the supplement). Rewriting Eq. (3) for monthly means, we thus replace $(T_a - T_0)$ with $PDD_{\sigma=3.5}(\bar{T}_a)$. The above approximations and assumptions then yield an implicitly diurnal Energy Balance Model (dEBM), which only requires monthly mean temperatures and solar radiation as atmospheric forcing, while albedo may be parameterized as in common surface mass balance schemes (e.g. Krapp et al., 2017):

$$\bar{M} \approx \left(q_\Phi (1 - A) \overline{SW}_0 + c_1 PDD_{\sigma=3.5}(\bar{T}_a) + c_2 \right) \frac{\Delta t_\Phi}{\Delta t \rho L_f} \quad (6)$$

where

$$\begin{aligned} c_1 &= \epsilon_i \epsilon_a \sigma 4 T_0^3 + \beta \\ &= 3.5 \text{ W m}^{-2} \text{ K}^{-1} + \beta \\ c_2 &= -\epsilon_i \sigma T_0^4 + \epsilon_a \epsilon_i \sigma (T_0^4) \\ &= -71.9 \text{ W m}^{-2} \end{aligned} \quad (7)$$

for any month that complies with the background melting condition $\bar{T}_a > T_{min}$.

The sensitivity of the scheme to the choices of β and to enhanced long wave radiation due to cloud cover or changed atmospheric composition is considered in sect. 4.

Both q_Φ and Δt_Φ strongly depend on latitude and month of the year. Thus, a given combination of insolation and temperature forcing yields different melt rates at different locations or seasons. The sensitivity of the dEBM to latitude is further investigated in sect. 4.

Finally, we use that $M = 0$ in the moment when the sun passes Φ and formulate the instantaneous energy balance analogously to Eq. (6) as

$$(1 - A) \tau \widehat{S}_r \sin \Phi \underline{S}_0 + c_1 (T_a(\Phi) - T_0) + c_2 = 0. \quad (8)$$

with \underline{S}_0 being the irradiance normal to a surface at the bottom τ representing the transmissivity of the atmosphere over the melting surface, \widehat{S}_0 being the solar flux density at the top of the atmosphere and the instantaneous (TOA), and the instantaneous air temperature $T_a(\Phi)$. Assuming that $T_a(\Phi) \approx T_0$ and using a typical \underline{S}_0 one $\tau \widehat{S}_r$ estimate for the melt season of the model domain, we can estimate

$$\Phi = \arcsin \frac{-c_2}{(1 - A) \underline{S}_0} \arcsin \frac{-c_2}{(1 - A) \tau \widehat{S}_r} \quad (9)$$

independent of time or location. The dEBM's sensitivity to the range of possible elevation angles is discussed in sect. 4.

25 2.1 Derivation of Δt_Φ and q_Φ

The derivation of Δt_Φ and q_Φ is based on spherical trigonometry and fundamental astronomic considerations which, for instance, are discussed in detail in Liou (2002). The elevation angle ϑ of the sun changes throughout a day according to

$$\sin \vartheta = \sin \phi \sin \delta + \cos \phi \cos \delta \cos h(\vartheta) \quad (10)$$

with the latitude ϕ , the solar inclination angle δ and the hour angle h .

5 The time which the sun spends above an elevation angle ϑ then is

$$\Delta t_\vartheta = \frac{\Delta t}{\pi} h(\vartheta) = \frac{\Delta t}{\pi} \arccos \frac{\sin \vartheta - \sin \phi \sin \delta}{\cos \phi \cos \delta}. \quad (11)$$

~~At the top We assume that surface solar radiation is proportional to the TOA radiation \widehat{S}_r throughout a day (i.e. we neglect that transmissivity of the atmosphere (TOA)the mean τ is usually increasing with elevation angle and assume that cloud cover does not exhibit a diurnal cycle). The solar radiation during the period which the sun spends above a certain elevation angle ϑ~~

10 is then

$$\underline{SW}_\vartheta = \frac{\widehat{S}}{\Delta t_\vartheta} \frac{\tau \widehat{S}_r}{\pi \Delta t_\vartheta} (h(\vartheta) \sin \phi \sin \delta + (\cos \phi \cos \delta \sin h(\vartheta))) \quad (12)$$

~~with \widehat{S} being the TOA solar radiation on a surface perpendicular to its rays. \widehat{S} is seasonally varying due to the eccentricity of the Earth's orbit. If we assume surface solar radiation to be proportional to the top-of-atmosphere radiation throughout a day (i.e. there is no diurnal cycle in the transmissivity of the atmosphere) Eq. 12 also allows to estimate $\tau \widehat{S}_r$ from SW_0 . Furthermore~~

15 we can calculate the ratio between the mean short wave radiation during the melt period \underline{SWD}_Φ \underline{SW}_Φ and the mean daily downward short wave radiation \underline{SWD}_0 ~~also \underline{SW}_0~~ at the surface ~~: independent of $\tau \widehat{S}_r$:~~

$$q_\Phi = \frac{\underline{SW}_\Phi}{\underline{SW}_0} = \frac{h(\Phi) \sin \phi \sin \delta + \cos \phi \cos \delta \sin h(\Phi)}{h(0) \sin \phi \sin \delta + \cos \phi \cos \delta \sin h(0)} \frac{\Delta t}{\Delta t_\Phi}. \quad (13)$$

3 First evaluation of the scheme

~~Choosing $\beta = 10 \text{ W m}^{-2} \text{ K}^{-1}$ and using $\epsilon_a = 0.76$ for the present greenhouse gas concentration yields $c_1 = 14.4 \text{ W m}^{-2} \text{ K}^{-1}$ and $c_2 = -71.9 \text{ W m}^{-2}$. As a background melting condition we here use $\bar{T}_a > -6.5 \text{ K}$. Further, assuming The dEBM and two empirical schemes are calibrated and evaluated using the state-of-the-art regional climate and snow pack model MAR (Fettweis et al., 2017) as a reference.~~

~~The elevation angle used in the dEBM is estimated as $\Phi = 17.5^\circ$, applying Eq. (9) with a typical albedo of 0.7 and $S_0 = 600 \text{ W m}^{-2}$ in Eq. $\widehat{S}_r = 800 \text{ W m}^{-2}$ being roughly estimated from the summer insolation in the ablation regions (Eq. 12). (9) yields~~

25 ~~$\Phi = 23.5^\circ$. The new scheme is applied This estimate corresponds to a transmissivity of $\tau \approx 0.6$ which is in good agreement with Ettema et al. (2010). Further, the dEBM is optimized to reproduce the total annual Greenland surface melt averaged over the~~

entire MAR-simulation by calibrating the background melting condition as $\bar{T}_a > -6.5^\circ\text{C}$ and the parameter $\beta = 10 \text{ W m}^{-2} \text{ K}^{-1}$. We then apply the scheme to \overline{SW}_0 , $PDD(\bar{T}_a)$ $PDD_{\sigma=3.5}(\bar{T}_a)$ and albedo A from a simulation-MAR-simulation of Greenland's climate (years 1948 to 2016) with the state-of-the-art regional climate and snow pack model MAR (Fettweis et al., 2017). The (Fettweis et al., 2017) and compare estimated melt rates are then compared to with the respective MAR melt rates.

- 5 Two empirical schemes are tested and evaluated considered in the same way: a PDD-scheme based on $PDD(\bar{T}_a)$ $PDD_{\sigma=5}(\bar{T}_a)$, as defined and calibrated in Krebs-Kanzow et al. (2018) and a common-ETIM (Pollard, 1980), which estimates melt as-

$$M = \frac{((1 - A)\overline{SW}_0 + k_1 PDD(\bar{T}_a) + k_2) \frac{1}{\rho L_f}}$$

where scheme, in the following referred to as $dEBM_{const}$, which is a simplified variant of the dEBM where parameters are constant in time and space:

$$10 \quad M = \frac{((1 - A)\overline{SW}_0 + k_1 PDD_{\sigma=3.5}(\bar{T}_a) + k_2) \frac{1}{\rho L_f}}{\quad} \quad (14)$$

with $k_1 = 10 \text{ W m}^{-2} \text{ K}^{-1}$ and $k_2 = -60.5 \text{ W m}^{-2}$ chosen similar to Robinson et al. (2010). We here also use $\bar{T}_a > -6.5 \text{ K}$ $k_2 = -55 \text{ W m}^{-2}$. The $dEBM_{const}$ is very similar to the ITM-scheme and also uses similar parameters as in Robinson et al. (2010), but includes PDD instead of temperature, which particularly yields different results for low temperatures. As in Robinson et al. (2010), we treat k_2 as a tuning parameter to optimize the scheme and also use $\bar{T}_a > -6.5^\circ\text{C}$ as a background melting condition. For

- 15 better comparison, all schemes have been optimized to-

The computational cost of the dEBM in this application is very similar to the other two schemes as parameters are computed only once prior to the application. All schemes reproduce the total annual Greenland surface melt averaged over the entire MAR-simulation of 489 Gt with a relative bias not exceeding 1% (the mean bias is -4.3 Gt 0.4 Gt for the PDD scheme, 0.8 Gt for the ETIM and -1.2 Gt -0.6 Gt for the $dEBM_{const}$ and -2.0 Gt for the dEBM). For the PDD-scheme we use the calibrated parameters from Krebs-Kanzow et al. (2018), in the ETIM we optimized the background melting condition and k_2 and in the dEBM we optimized the background melting condition and the turbulent heat transfer coefficient β within the range given in Braithwaite (1995) These calibrations are primarily conducted to facilitate a fair comparison between the different schemes and are not necessarily optimal for other applications.

- Equations Equations (6) and (14) appear formally similar, with the first and third term representing the radiative contribution and the second term representing the PDD contribution being temperature dependent (the “temperature contribution”) and the first and third term being independent of temperature and only depending on solar radiation (the “radiative contribution”). However, the respective parameters cannot be compared directly, as the Δt_Φ and q_Φ depend on latitude and month. Δt_Φ and q_Φ modulate the the radiative contribution and Δt_Φ modulates the PDD-temperature contribution in Eq. (6). Fig. 1a illustrates the radiative and Fig. 1b the PDD-temperature contributions as diagnosed from the MAR simulation in comparison to the respective contribution from the ETIM $dEBM_{const}$. On the GrIS the radiative contribution can exceed 40 mm d^{-1} 25 mm d^{-1} in the summer months and the two schemes appear qualitatively similar. However, a flat-ecliptic (going along with The radiative

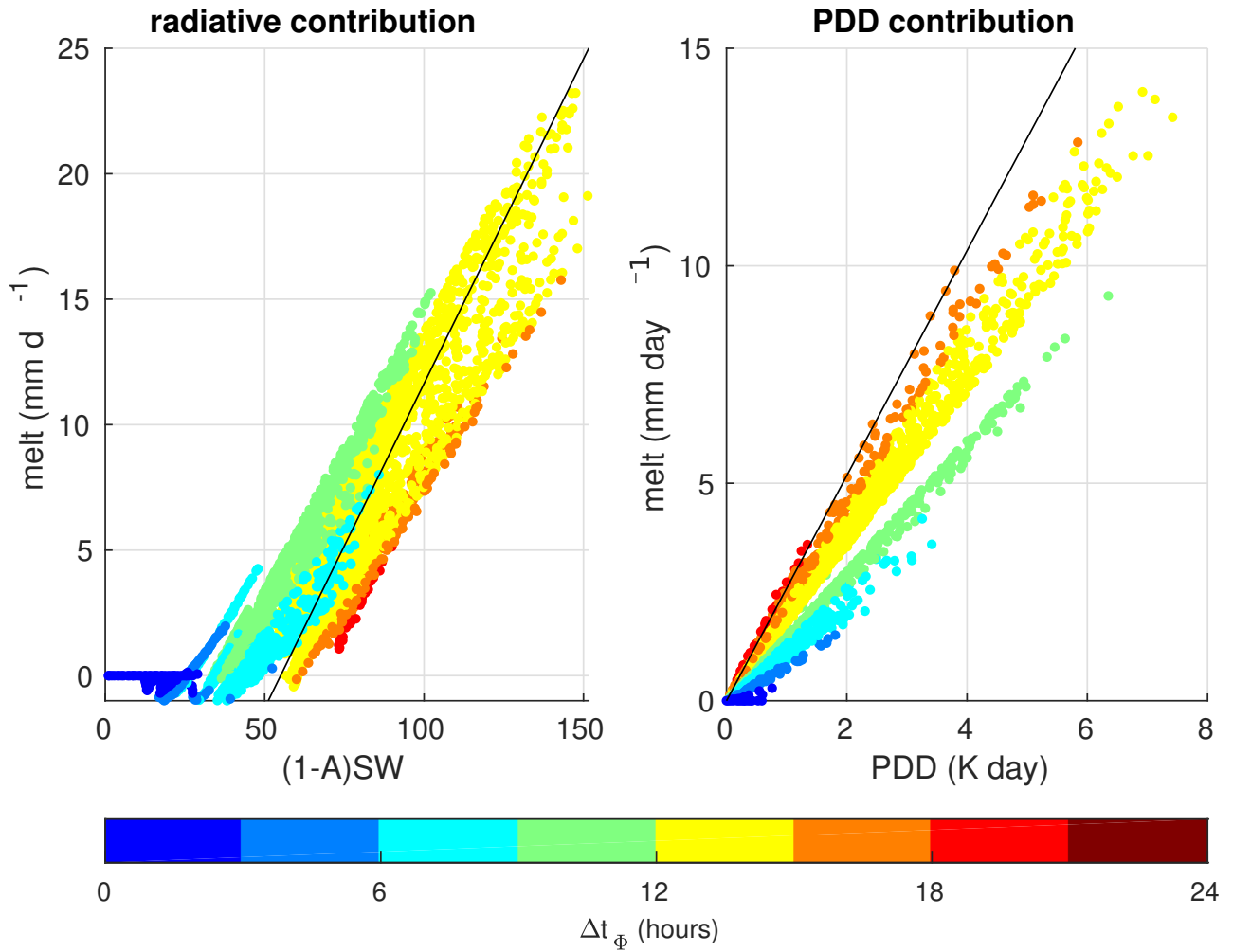


Figure 1. a) Contribution of the first and third term (radiative contribution) and b) of the second term (PDD-temperature contribution) in Eq. (6) to monthly melt rates as diagnosed with climatological temperatures and solar radiation from the MAR simulation. Colors indicate length of melt period (Δt_{Φ}). The black lines represent the respective prediction of the $ETIM-dEBM_{const}$ according to Eq. (14)

contribution in the dEBM becomes less efficient for long melt periods at high latitudes or with, as the same insolation must balance the outgoing longwave radiation for a longer time. On the other hand, radiative contribution can also decrease towards short melt periods in autumn and spring) reduces q_{Φ} and consequently reduces the radiative contribution in the dEBM. As a result considerable difference between dEBM and ETIM are visible both for short and long melt periods. The PDD, if the sun only marginally rises above the minimum elevation angle at solar noon. This effect becomes important for higher estimates of the minimum elevation angles in high latitudes (Sect. 4). The temperature contribution of the dEBM appears reduced in comparison to the ETIM and does not exceed 12 mm d^{-1} 15 mm d^{-1} (Fig. 1b). In the dEBM the PDD contribution and becomes more efficient with longer melt periods and would agree with the ETIM $dEBM_{const}$ for a melt period of 16-18 hours.

Atmospheric forcing Atmospheric forcing (insolation and temperature) and albedo are here derived-obtained from MAR output, and are fully consistent with the MAR melt rates. Consequently, we can evaluate the skill of the considered schemes independent of the quality of the atmospheric forcing and the representation of albedo. On the other hand, we can not evaluate the performance of the schemes for defective input. In this respect With respect to error propagation the PDD-scheme might be more robust and, as it only requires temperature as a forcing and only distinguishes between snow and ice but does not require albedo. Due to Given the ideal input, all schemes reproduce the year-to-year evolution of the total Greenland surface melt of the MAR-simulation reasonably well (Fig. S1-S3 in the supplement). With The PDD-scheme yields increasing errors with intensifying surface melt rates, both, the PDD-scheme and the ETIM, yield increasing errors, which is not apparent for the $dEBM_{const}$ and dEBM (Fig. 2). On the other hand, the dEBM cannot reproduce melt rates which may still occur even though the sun does not pass over the critical elevation angle and the duration of the melt period vanishes. The root mean square error of the predicted monthly, local melt rates relative to MAR melt rates is 3.6 mm d^{-1} for the PDD scheme, 5.0 mm d^{-1} for the ETIM and 3.3 mm d^{-1} for the dEBM, if we only consider grid points and months which comply with the background melting condition of $\bar{T}_a > -6.5 \text{ K}$ $dEBM_{const}$ particularly overestimates (underestimates) melt rates for very short (long) melt periods. In comparison to the two empirical schemes, the dEBM produces smaller local errors with biases-biases being pronounced only in a narrow band along the ice sheet's margins (Fig.3).

4 Sensitivity to model parameters and boundary conditions

Sensitivity to tuning parameters: In the above application, the parameter β for sensible heat and the background melting condition T_{min} have served as tuning parameters. The parameter $\beta = 10 \text{ W m}^{-2} \text{ K}^{-1}$ was determined by optimizing the scheme to MAR melt rates. This value agrees reasonably well with the moderate wind speeds found in PROMICE observations during melt periods (Fig. S2 in the supplement). Changing β by $\pm 20\%$ changes the total annual Greenland surface melt by $\pm 3\%$. The choice of $T_{min} = -6.5^\circ \text{C}$ is in good agreement with observations, which reveal no substantial melt for temperatures $< -7^\circ \text{C}$ (e.g. Orvig, 1954). Increasing the background melting condition T_{min} particularly reduces the melt rates at high elevations, while reducing T_{min} results in a longer melting season and increases the annual surface melt. Using no background melting condition at all results in unrealistic melt rates at high elevations and would almost double the predicted total Greenland

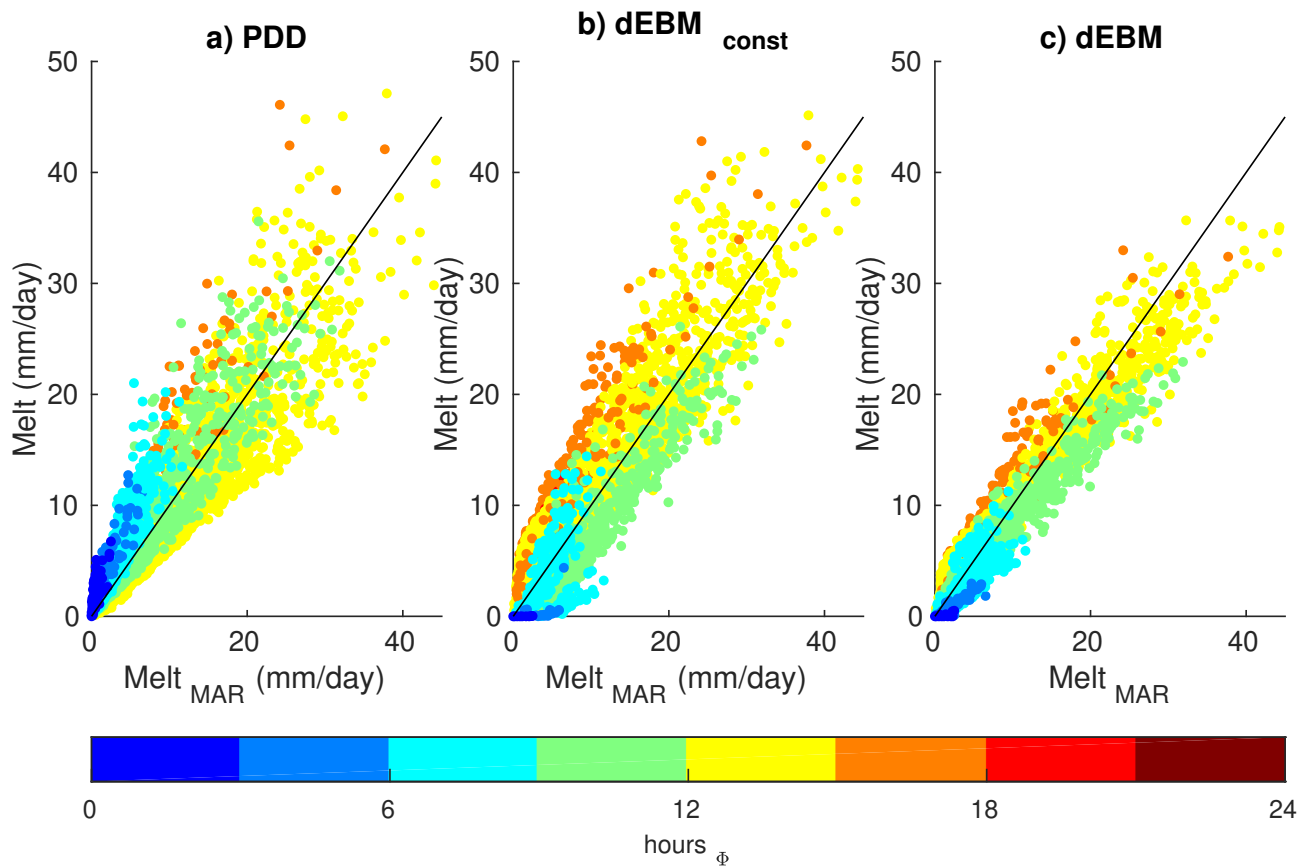


Figure 2. Multi-year monthly mean meltrates averaged of the years 1948-2016 as predicted by a) the PDD-scheme, b) the $ETIM-dEBM_{const}$ and c) the dEBM against respective MAR melt rates. Colors reflect the length-length of the daily melt period. Identity is displayed as a black line in all panels for comparison.

surface melt. Changing T_{min} by $\pm 1K$ changes the predicted mean annual surface melt by $\pm 8\%$ for the MAR simulation used in this study. Intense surface melt is usually accompanied by warm temperatures and is thus insensitive to the choice of T_{min} . As refreezing particularly suppresses the contribution of weak surface melt at low temperatures, the resulting runoff can be expected to be less sensitive to the choice of T_{min} .

- Sensitivity to diurnal cycle of solar radiation:** Melt schemes which do not include the diurnal cycle of radiation will predict the same melt rate for a given combination of insolation and temperature forcing, irrespective of latitude or season. By contrast, Fig. 4 indicates a strong sensitivity of the dEBM surface melt predictions to latitude in summer. According to the dEBM, a short melt period with intensive solar radiation is causing melt more effectively than a longer melt period with accordingly weaker solar radiation. This sensitivity is particularly prominent in high latitudes and may explain the latitudinal bias found in many studies which do not resolve radiation on sub-daily time scales (e.g. Plach et al., 2018; Krebs-Kanzow et al., 2018; Krapp et al., 2017).
- Sensitivity to orbital configuration and transmissivity of the atmosphere:** The TOA solar flux density \widehat{S}_r depends on

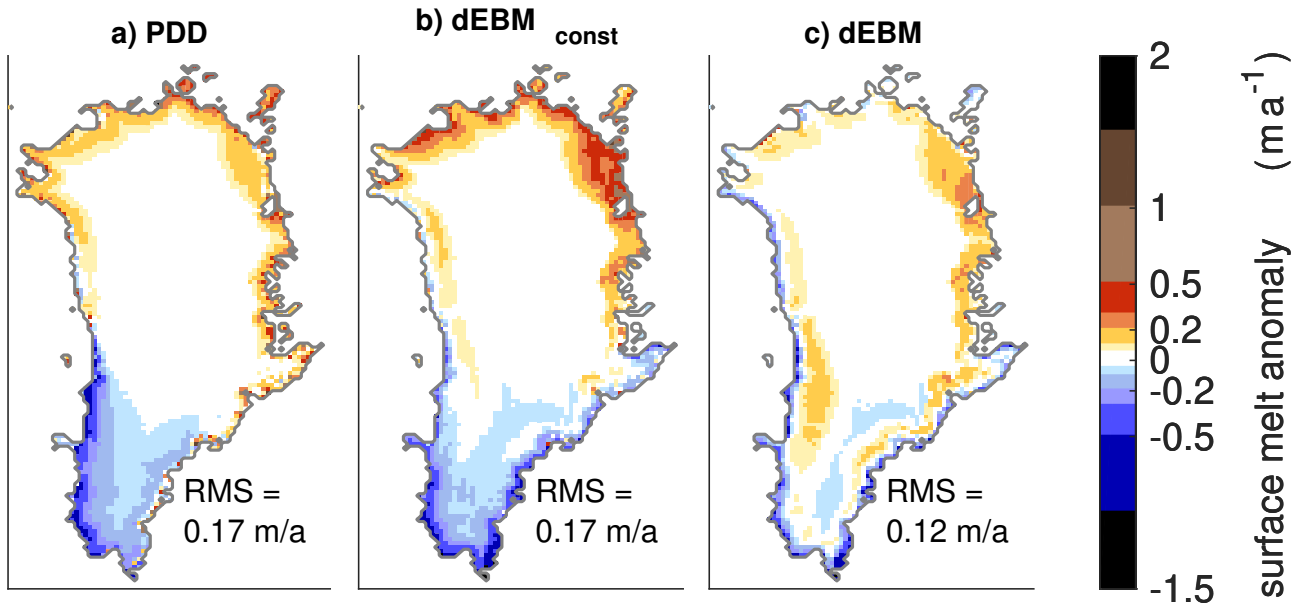


Figure 3. Bias between yearly melt rates as predicted by the individual schemes and as simulated by MAR, averaged over the whole simulation: a) PDD b) ~~ETM~~-*dEBM_{const}* c) the proposed new scheme dEBM. The respective root mean square error (RMS) is given in the individual panels.

the distance between Earth and Sun and due to the eccentricity of the Earth's orbit gradually varies by $\pm 3.5\%$ from the solar constant from December to July respectively. On orbital time scales this seasonal deviation from the solar constant may amount to 10%. Transmissivity τ , on the other hand, strongly depends on cloud cover and atmospheric composition and additionally increases with the solar elevation angle. In consequence the minimum elevation angle Φ may be less than 13° ($\tau \widehat{S}_r = 1150 \text{ W m}^{-2}$ for clear sky, intense summer insolation). For overcast sky and weak summer insolation, we can ultimately expect $\tau \widehat{S}_r < 400 \text{ W m}^{-2}$. In that case, however, it is not justified to use the clear sky emissivity in Eqs. 5 and 7. Consequently, the proposed scheme is no longer suitable, as net outgoing long wave radiation will vanish and the energy balance will become very sensitive to turbulent heat fluxes. Applications aiming at continental ice sheets with climatological forcing will be however restricted to a much narrower range of scenarios. As one can expect that transmissivity decreases towards the morning and afternoon hours, it may be justified to reduce the estimate of $\tau \widehat{S}_r$ by a few percent. Fig. 4 reveals that the scheme becomes very sensitive if the minimum elevation angle Φ takes values close to or larger than the obliquity of the Earth. Under such conditions the duration of the melt period will vanish near the Pole. On the other hand the scheme is remarkably insensitive to intensified insolation (and accordingly reduced elevation angle Φ) or variations in the obliquity. Accordingly, estimating the elevation angle locally and for each month using Eq. 12, which is possible but computationally more expensive, does not improve the skill of the dEBM noticeably (not shown).

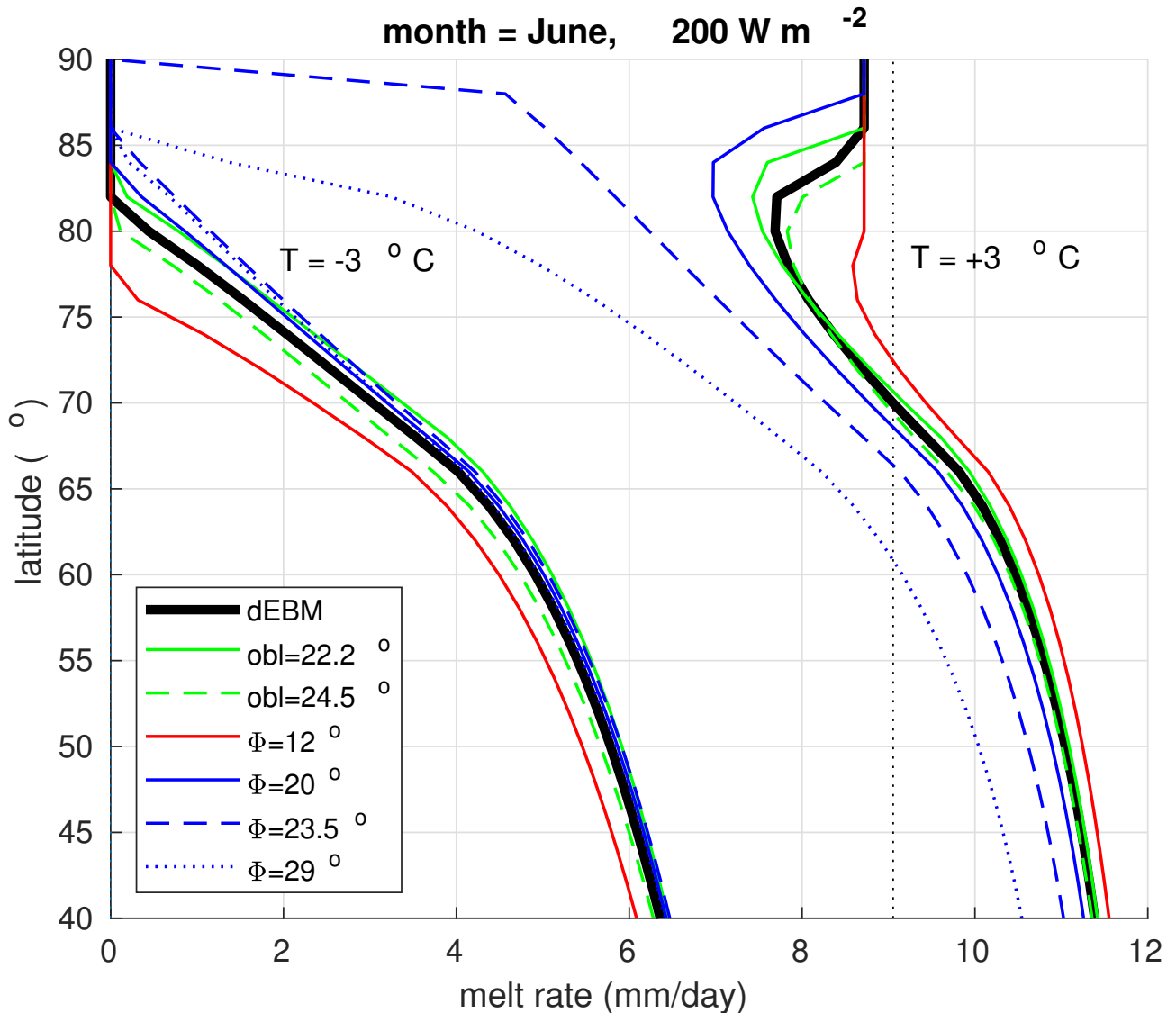


Figure 4. Sensitivity of the dEBM: June surface melt rate as predicted for $SW_0 = 200 \text{ W m}^{-2}$, $A = 0.7$, $T_a = -3^\circ \text{C}$ (left curves) and $T_a = 3^\circ \text{C}$ (right curves). Black: predictions with parameters as used for the presented simulation of Greenland's surface melt. Green: parameters are recalculated using the minimum (solid) and maximum (dashed) obliquity of the last 1 million years. Blue: parameters are recalculated after the minimum elevation angle is adjusted to a reduced solar density flux at the surface of $\tau \hat{S}_r = 700 \text{ W m}^{-2}$ (solid), $\tau \hat{S}_r = 600 \text{ W m}^{-2}$ (dashed), $\tau \hat{S}_r = 500 \text{ W m}^{-2}$ (dots). Red: parameters are recalculated after the minimum elevation angle is adjusted to an intensified solar density flux at the surface of $\tau \hat{S}_r = 1150 \text{ W m}^{-2}$. The $dEBM_{const}$ predicts 0 mm/day for $SW_0 = 200 \text{ W m}^{-2}$, $A = 0.7$, $T_a = -3^\circ \text{C}$ and 9 mm/day for $SW_0 = 200 \text{ W m}^{-2}$, $A = 0.7$, $T_a = 3^\circ \text{C}$ (black dots).

15 5 Discussion and conclusion

The presented new scheme for surface melt (dEBM) requires, like ~~enhanced temperature index methods~~ the insolation temperature melt scheme (ITM), monthly mean air temperatures and insolation as input, but implicitly also includes the diurnal cycle. Together with suitable schemes for albedo and ~~refreeze (e.g. the parameterizations used together with the enhanced temperature index methods)~~ (e.g. the parameterizations presented in Robinson et al., 2010), it may replace empirical surface melt schemes which are commonly used in ice sheet modelling on long time scales.

An application to the Greenland Ice Sheet indicates, that the scheme may improve the spatial representation of surface melt in comparison to common empirical schemes. However, an evaluation to an independent data base is desirable. The most important advantage of the dEBM over empirical schemes may be, that it can be globally applied to other ice sheets and glaciers and under different climate conditions, as parameters in the scheme are physically constrained and implicitly account for the orbital configuration.

In the presented formulation a threshold temperature serves as a prerequisite for surface melt on monthly time scales. This threshold temperature should be considered as a tuning parameter, as the representation of the ice-atmosphere boundary layer in Earth system models may differ considerably from the MAR simulation, which here has served as a reference. Furthermore, long wave radiation and non-radiative heat fluxes are only crudely represented. Depending on the application, it may be advisable to adapt the parameterization of turbulent heat fluxes and long wave radiation to different climate regimes in order to account for changed wind speed, humidity, cloud cover or greenhouse gas concentration.

The daily melt period is defined by a minimum solar elevation angle. Together with the melt period, parameters in the dEBM depend on latitude and month of the year, but do not change from year to year if the minimum solar elevation angle is kept constant and the orbital configuration remains the same. For the Greenland Ice Sheet, a minimum solar elevation angle of ~~23.5°~~ 17.5° was roughly estimated from the mean summer insolation normal to a surface at the bottom of the atmosphere. ~~Since the normal summer insolation depends on the orbital configurations and atmospheric transmissivity, the minimum solar elevation angle should be readjusted for applications on the southern hemisphere, accounting for the stronger austral summer insolation. On long time scales the elevation angle may also change with~~ The dEBM is very sensitive if the intensity of solar radiation is substantially weaker than in the presented application (e.g. due to cloud cover or atmospheric water content). In this case it is necessary to carefully re-estimate the minimum elevation angle and to adjust the model parameters accordingly. The scheme appears to be relatively insensitive to changes in the orbital configuration and ~~atmospheric composition.~~ In the presented formulation a threshold temperature serves as a prerequisite for surface melt on monthly time scales. This threshold temperature should be considered as a tuning parameter, as the representation of the ice-atmosphere boundary layer in Earth system models may differ considerably from the MAR simulation, which here has served as a reference. Furthermore, non-radiative heat fluxes are only crudely represented. Depending on application, it may be advisable to adapt the heat transfer coefficient to different climate regimes or to include additional atmospheric variables, such as wind speed and humidity, for a better parameterisations of turbulent heat fluxes the parameters choices in this study may be valid in a wider range of settings.

The presented formulation has been designed for long Earth System Model applications, but it may be adapted to be also used

in the context of climate reconstructions or to be applied on regional or local scales. Furthermore, having defined the daily melt period by the minimum elevation angle, it should also be possible to estimate the amount of refreezing by considering the energy balance of the remainder of the day, following a similar approach as in Krapp et al. (2017).

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