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2 **The ~~characteristics of gravelly soil~~ physical properties of**
3 **coarse soil fragment and their effects on permafrost**
4 **dynamics: A case study on the central Qinghai-Tibetan**
5 **Plateau**

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29 **Abstract.** Soils on the Qinghai-Tibetan Plateau (QTP) have distinct physical properties from
30 agricultural soils due to weak weathering and strong erosion. These properties might affect
31 permafrost dynamics. However, few studies have investigated both quantitatively. In this
32 study, we selected a permafrost site on the central region of the QTP and excavated soil
33 samples ~~from 20 cm down~~ to 200 cm. We measured soil porosity, thermal conductivity,
34 saturated hydraulic conductivity and matric potential in the laboratory. Finally, we ran a
35 simulation model replacing default sand or ~~silty clay loam~~ parameters with different

1 | combinations of these measured parameters. Results showed that ~~gravel-coarse soil fragment~~
2 | content (diameter >2 mm) was ~55% on average in soil profile; soil porosity was less than 0.3;
3 | saturated hydraulic conductivity ranged from 0.004-0.03 mm s⁻¹; saturated matric potential
4 | ranged from -14 to -604 mm. When default sand or ~~silty-clayloam~~ parameters were
5 | substituted with these measured values, the model errors of soil temperature, soil liquid water
6 | content, active layer depth and permafrost lower boundary were reduced. The root mean
7 | squared errors of active layer depths simulated using measured parameters, and the default
8 | sand and ~~silty-clayloam~~ parameters were about 0.28, 1.06, 1.83 m, respectively. Among these
9 | measured parameters, porosities, which were much smaller than soil textures used in land
10 | surface models, played a dominant role in reducing model errors. We also demonstrated that
11 | soil water dynamic processes should be considered, rather than using static properties under
12 | frozen and unfrozen soil states as in most permafrost models. We concluded that it is
13 | necessary to consider the distinct physical properties of soil and water dynamics on the QTP
14 | when simulating dynamics of permafrost ~~in this region~~. It is important to develop methods for
15 | systematic measuring physical properties of ~~gravelly soil~~~~coarse soil fragment~~ and to develop a
16 | spatial dataset for porosity because of its importance in simulating permafrost dynamics in
17 | this region.

18 | **Key words:** Terrestrial Ecosystem Model; Active Layer; Sensitivity Test; Soil Temperature;
19 | Soil Water Content; Gravel

20 | 1 Introduction

21 | Permafrost covers 25% of the earth surface. Degradation of permafrost has been reported
22 | extensively in Alaska, Siberia and the Qinghai-Tibetan Plateau (QTP; Boike et al., 2013;
23 | Jorgenson et al., 2006; Wu and Zhang, 2010). It has global impacts by releasing large
24 | quantities of soil carbon previously preserved in a frozen state and enhancing concentrations
25 | of atmospheric greenhouse gases, which will promote further atmospheric warming and
26 | degradation of permafrost (Anisimov, 2007; McGuire et al., 2009). Permafrost dynamics also
27 | have local to regional impacts on ecosystems by altering soil thermal and hydrological
28 | regimes (Salmon et al., 2015; Wang et al., 2008; Wright et al., 2009; Ye et al., 2009; Yi et al.,
29 | 2014a). In addition, degradation of permafrost affects infrastructure, e.g. QTP railways and
30 | roads (Wu et al., 2004), and the Trans-Alaska Pipeline System in Alaska (Nelson et al., 2001).
31 | Therefore, it is critical to develop mitigation and adaptation strategies in permafrost regions

1 for ongoing climate change. Accurate projection of the degree of permafrost degradation is a
2 prerequisite for developing these strategies.

3 Significant effort has been made to improve modeling accuracy and efficiency of
4 permafrost dynamics along two primary lines of inquiry. One is to create suitable freezing and
5 thawing algorithms for different applications, including land surface models (Chen et al.,
6 2015; Oleson et al., 2010; Wang et al., 2017), permafrost models (Goodrich, 1978; Langer et
7 al., 2013; Qin et al., 2017) and other related models (Fox, 1992; Woo et al., 2004). The other
8 line of inquiry is focused on schemes of soil physical properties (Chen et al., 2012; Zhang et
9 al., 2011), which play a critical role in permafrost dynamics. For example, thermal diffusivity
10 (thermal conductivity/heat capacity) directly determines how quickly energy can be
11 conducted into and out of permafrost from the top and from the bottom of the permafrost
12 horizon. Porosity determines the maximum amount of water that can be contained in a soil
13 layer, and hydraulic properties determine the exchange of soil water between soil layers. The
14 amount of water then affects not only soil thermal properties, but also determines the large
15 amount of latent heat loss/gain for freezing/thawing. On the QTP, soil is coarse due to weak
16 weathering and strong erosion (Arocena et al., 2012). Soils with gravel content (particle
17 diameter >2 mm) has been reported in several studies (Wang et al., 2011; Wu et al., 2016;
18 Yang et al., 2009; Qin et al., 2015; Chen et al., 2017; Du et al., 2017). These gravelly soil
19 properties are different from those used in current modeling studies (Wang et al., 2013). For
20 example, Soil properties in Community Land Model are calculated from fractions of sand, silt
21 and clay based on measurements of agriculture soils (Oleson et al., 2010). However, those of
22 gravelly soil on the QTP and their effects on permafrost dynamics are under studied (Pan et
23 al., 2017).

24 In this study we investigated the characteristics of soil physical properties at a site on the
25 central QTP and its effects on permafrost dynamics. We first measured soil physical properties
26 of excavated soil samples in laboratory. We then conducted sensitivity analyses with an
27 ecosystem model by substituting the default soil physical properties by those that we
28 measured. We aimed to emphasize the effects of gravel content on soil physical properties and
29 on permafrost dynamics. It is not our purpose to develop general schemes of soil physical
30 properties for using in modeling studies on the QTP.

2 Methods

2.1 Site description

The site (34°49'46.2" N, 92°55'56.58" E, 4,628ma.s.l.) is located in the Beiluhe basin. This basin is in the continuous permafrost region of the central QTP (Figure 1a, Zou et al. 2017). Based on the soil map of Li et al. (2015), soil of this region belongs to Gelisols and Inceptisols, which occupy 34% and 28% of the total area of permafrost region of the QTP, respectively. Land surface types include alpine meadow, alpine steppe, barren surface and thermokarst lakes (Figure 1b; Lin et al., 2011).

The site is on top of upland plain landforms, which are formed with fluvial and deluvial sediments. The surficial sediments are dominated by fine to gravelly sands and stones (Figure 2; Yin et al., 2017). Soil of this site belongs to Inceptisols (Dr. Li, Wangping, personal communication). Mudstone is common beneath soil. The plant community type is mainly alpine meadow which is dominated by monocotyledonous species, primarily Poaceae and Cyperaceae. The dominant species are *Kobresia pygmaea*, accompanied *Elymus nutans*, *Carex moorcroftii*, *Oxytropis pusilla*, *Tibetia himalaica*, *Leontopodium nanum* and *Androsace tapete* (Figure 2c-e).

A weather station was set up in 2002 (Figure 2a). Air temperature and relative humidity (2.2m, HMP45C - L11 /L36, Campbell Scientific Inc.), solar radiation (MS-102, EKO), precipitation (QMR102, Vaisala Company) were measured. Soil temperatures were measured at depths of 5, 10, 20, 40, 80 and 160 cm using PT-100 (EKO); soil moistures were measured at depths of 20, 40, 80 and 160 cm using CS616-L50 (EKO). CR3000 data logger (Campbell Scientific Inc., USA) was used to store these data at an interval of 30 minutes. These halfhour values were averaged or summed (e.g. precipitation) into monthly values for model driving and validation. Based on measurements, multi-year mean annual air temperature, precipitation, downward solar radiation and relative humidity were -3.61 °C, 365.7 mm, 206.3 W/m² and 51.1%, respectively (Figure 3). The multi-year mean summer (June to August)/winter (December to February) air temperature and precipitation were 5.27/-12.44 °C and 248.3/5.3 mm, respectively. The multi-year mean annual, summer, winter soil temperature at 40/80 cm were 0.17/0.11, 6.65/4.32 and -7.15/-4.86 °C, respectively.

A borehole was drilled in 2002. Temperature thermistors made by the State Key Laboratory of Frozen Soil Engineering, Chinese Academy of Sciences (ref) were installed at depths between 0.5 m and 10 m with interval of 0.5 m; at depths between 12 m and 30 m with

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1 interval of 2 m; at depths between 34 m and 50 m with interval of 4 m; and at 55 and 60 m.
2 Temperature accuracy of this type of thermistor is 0.05 °C (Wu et al., 2016). The
3 temperatures were recorded on the 5th and 20th days of each month using CR3000 data
4 logger (Campbell Scientific Inc., USA). Based on measurement, active layer depth is ~3.3 m
5 and the lower boundary of permafrost is at a depth of ~20 m. The multi-year mean ground
6 temperatures at 0.5, 12, and 60 m are about -0.52, -0.29 and 1.81 °C, respectively.
7 ~~, it is in flat terrain with most slopes <10°. Fluvial and deluvial sediments formed the upland~~
8 ~~plain landforms. The surficial sediments are dominated by fine to gravelly sands. (Yin, et al.,~~
9 ~~2017). The site is located in the continuous permafrost region of the central QTP (Figure 1a,~~
10 ~~Zou et al., 2017). Based on the soil map of Li et al. (2015), soil of this region belongs to~~
11 ~~Gelisols and Inceptisols, which occupy 34% and 28% of the total area of permafrost region of~~
12 ~~the QTP, respectively. Meteorological variables (air temperature, radiation, precipitation and~~
13 ~~humidity), soil variables (soil temperature and moisture) down to 1.6 m, and borehole~~
14 ~~temperatures down to 60 m have been measured at this site since 2002. The meteorological~~
15 ~~station and borehole are located on a gentle slope with sparse vegetation (Figure 1b). Based~~
16 ~~on measurements, the mean annual precipitation and air temperature are 366 mm yr⁻¹ and 3.6~~
17 ~~°C, respectively. Active layer depth is ~3.3 m and the lower boundary of permafrost is at a~~
18 ~~depth of ~20 m. Details of meteorological and borehole variables can be found in Qin et al.~~
19 ~~(2013).~~
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21 2.2 Soil sampling and measurement

22 ~~Permafrost dynamics are affected by atmosphere, vegetation and soil textures, therefore, We we~~
23 ~~excavated soil outside of the fence of the close to meteorological weather station and borehole~~
24 ~~(Figure 1b2a) down to 2 m (Figure 1e2b) in August 2014. We used cut rings (10 cm diameter,~~
25 ~~6.37 cm height and 500 cm³) to take soil samples at depth ranges of 0-10, 10-20, 20-30, 40-50,~~
26 ~~70-80, 110-120, 150-160, and 190-200 cm. At each depth, three replicates were sampled from~~
27 ~~the top of each depth range and sealed for analysis in the laboratory. Above 120 cm in the soil~~
28 ~~pit, coarse soil material was small enough to be fitted in cut rings. Below 150 cm, there exists~~
29 ~~weathered mudstone, which could also be sampled with our cut rings.~~

30 We used the KD2 Pro (Decagon, US) to measure thermal conductivity of soil samples. The
31 steps were: 1) soil samples were dried in oven and weighed (0.001g precision) to calculate bulk

1 density; 2) soil samples were exposed to a constant temperature (20°C) over 24 h, a certain
 2 volume of water was injected into the soil samples, and the KD2 was used to measure the
 3 thermal conductivity of the soil samples. ~~samples were then saturated with water (20°C)~~
 4 weighed (0.001g precision), and the KD2 probe (SH 1) was then inserted into soil samples to
 5 measure thermal conductivity; 3) samples and the KD2 probe were then put into a refrigerator
 6 (0~26°C) at -15°C over 12 h, at which time thermal conductivity was then measured; 4)-Steps
 7 2 and 3 were repeated at different levels of soil volumetric water content until soil samples
 8 were about to be saturated.- 45) Finally, soil samples were immersed into water over 24 h and
 9 weighed to calculate porosity; and the saturated unfrozen and frozen thermal conductivity were
 10 then measured, accordingly. The bulk density (BD), porosity (PORO) and volumetric water
 11 content (VWC) were calculated with the following equations.

$$12 \quad BD = \frac{W_{dry} - W_{cr}}{V_{ar}}$$

$$13 \quad PORO = \frac{W_{sat} - W_{dry}}{V_{cr}} / \rho$$

$$14 \quad VWC = \frac{W_{all} - W_{dry}}{V_{cr}} / \rho$$

15 Where W_{dry} , W_{sat} , W_{all} , W_{cr} are weight of over dried sample, saturated sample, sample with
 16 some water with cut ring, and empty cut ring (g), respectively. ρ is density of water (1 g/cm³).

17 We used pressure membrane instruments (1500F1, Soilmoisture Equipment Corp, US) to
 18 measure matric potential of soil samples (Azam et al., 2014; Wang et al., 2007). In this study
 19 we used both 15 bar and 5 bar pressure chamber. Pressure values were set at 0, 10, 20, 40, 60,
 20 80, 100, 150, 200, 300, and 400 kpa. It usually took 3-4 days to finish one measurement at one
 21 pressure level. We used soil permeability meter (TST-70, China) to measure saturated hydraulic
 22 conductivity of soil samples (Gwenzi et al., 2011). Finally, soil samples were sieved through
 23 meshes with diameters of 2.0, ~~1.0, 0.5 and 0.25~~ mm, and soil particle size distribution was
 24 determined with a Malvern laser diffraction analyzer (Malvern-2000, Instruments Inc.
 25 Worcestershire, UK), in a sequence and weighted to calculate fractions.

26 2.3 Model description

27 The model used in this study is dynamic organic soil version of Terrestrial Ecosystem Model
 28 (DOS-TEM). Models of TEM family simulate the carbon and nitrogen pools of vegetation
 29 and soil, and their fluxes among atmosphere, vegetation and soil (McGuire et al., 1992). They

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1 have been widely used in studies of cold region ecosystems (e.g. McGuire et al., 2000; Yuan
2 et al., 2012; Zhuang et al., 2004; 2010) The DOS-TEM consists of four modules, these being
3 the environmental, ecological, fire disturbance, and dynamic organic soil modules (Yi et al.,
4 2010). The environmental module operates on a daily time interval using mean daily air
5 temperature, surface solar radiation, precipitation, and vapor pressure, which are downscaled
6 from monthly input data (Yi et al., 2009b). The module takes into account radiation and water
7 fluxes among the atmosphere, canopy, snow pack, and soil.

8 **2.3.1 Implementation of soil thermal processes**

9 Earlier versions of TEM did not simulate soil temperature (McGuire et al., 1992). Zhuang et
10 al. (2001) incorporated Goodrich permafrost model into TEM. Yi et al. (2009a) incorporated a
11 two-directional Stefan algorithm to simulate soil freezing and thawing for complex soil
12 situation with changes of organic soil and moisture. Soil temperatures of all soil layers in the
13 DOS-TEM are updated daily. Phase change is calculated first before heat conduction. A two-
14 directional Stefan algorithm is used to predict the depths of freezing or thawing fronts within
15 the soil (Woo et al., 2004). It first simulates the depth of the front in the soil column from the
16 top downward, using soil surface temperature as the driving temperature. It then simulates the
17 front from the bottom upward using the soil temperature at a specified depth beneath a front
18 as the driving temperature (bottom-up forcing). The latent heat used for phase change is
19 recorded for each soil layer. If a layer contains n freezing or thawing fronts, this layer is then
20 explicitly divided into $n+1$ soil layers All soil layers are grouped into 3 parts: 1) the soil layers
21 above the uppermost freezing or thawing front; 2) the soil layers below the lowermost
22 freezing or thawing front; and 3) the soil layers between the uppermost and lowermost fronts.
23 Soil temperatures are then updated by solving finite difference equations of each part with
24 phase change latent heat as energy source or sink (Yi et al., 2014a). Soil surface temperature,
25 which is used as a boundary condition, is calculated using daily air maximum, air minimum,
26 radiation, and leaf area index (Yi et al., 2013).

27 The version of the DOS-TEM in this study uses the Côté and Konard (2005) scheme to
28 calculate thermal conductivity (Yi et al., 2013; Pan et al., 2017), which is also used by other
29 studies on the QTP (e.g. Chen et al., 2012, Luo et al., 2009).

$$\lambda = \begin{cases} k_e \lambda_{sat} + (1 - k_e) \lambda_{dry} & s > 10^{-5} \\ \lambda_{dry} & s \leq 10^{-5} \end{cases}$$

(14)

where λ , λ_{sat} , λ_{dry} are soil thermal conductivity, saturated soil thermal conductivity, and dry soil thermal conductivity ($\text{W m}^{-1} \text{K}^{-1}$), respectively. k_e is Kersten number (Côté and Konrad, 2005).

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$$\lambda_{dry} = \chi 10^{-\eta \phi}$$

(25)

where χ ($\text{W m}^{-1} \text{K}^{-1}$) and η (no unit) are parameters accounting for particle shape effects, which are specified for gravel, fine mineral and organic soil (Côté and Konard, 2005). ϕ is porosity.

$$\lambda_{sat} = \begin{cases} \lambda_s^{1-\phi} \lambda_{liq}^{\phi} & T \leq T_f \\ \lambda_s^{1-\phi} \lambda_{ice}^{\phi} & T > T_f \end{cases}$$

(36)

where λ_{liq} , λ_{ice} , λ_s are thermal conductivity of liquid water, ice and solid ($\text{W m}^{-1} \text{K}^{-1}$), which are all constant values. T and T_f are temperature of soil and freezing point temperature of soil ($^{\circ}\text{C}$), respectively.

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2.3.2 Implementation of soil hydrological processes

Surface runoff, infiltration, and water redistribution among soil layers are simulated in a similar way as Community Land Model 4 (Oleson et al 2010). Soil matric potential (Ψ) determines the direction of water movement. And hydraulic conductivity ~~determines~~ describes the ease with which water can move through soil pore. ~~the rate of water movement.~~

$$\Psi = \Psi_{sat} \left(\frac{\theta_{liq}}{\phi} \right)^{-B}$$

(47)

where Ψ_{sat} is saturated soil matric potential (mm H_2O , hereafter mm), θ_{liq} is volumetric liquid water content ($\text{m}^3 \text{m}^{-3}$), and B is pore size distribution parameter.

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$$K = K_{sat} \left(\frac{\theta_{liq}}{\phi} \right)^{2B+3}$$

(58)

1 where K is soil hydraulic conductivity, and K_{sat} is saturated soil hydraulic conductivity (mm s^{-1}).
2

3 Several important features relating to permafrost have been considered in the DOS-TEM
4 (see Yi et al., 2014b), e.g. runoff from perched saturated zone and exchanges of water
5 between soil and a water reservoir. Runoff from the perched saturated zone above the
6 permafrost is implemented following Swenson et al. (2013),

$$7 \quad Q_{\text{perch}} = \alpha k_p (z_{\text{frost}} - z_{\text{perched}}) \sin\left(\frac{\theta}{180} \pi\right)$$

8 ~~(69)~~

9 Where α is an adjustable parameter (0.6 m^{-1}), K_p is the mean saturated hydraulic conductivity
10 within perched saturated zone (mm s^{-1}), z_{frost} and z_{perched} are the depths to permafrost table and
11 perched water table (m), respectively, and θ is slope ($^\circ$).

12 The DOS-TEM has been verified against the Neumann Equation for water, mineral and
13 organic soil under an idealized condition (Yi et al., 2014b), and validated against field
14 measurements for various locations in Alaska, the Arctic, and the QTP (Yi et al., 2009b, Yi et
15 al., 2013, Yi et al., 2014a).

16 2.4 Model inputs and initialization

17 We used the measured air temperature, downward radiation, precipitation and humidity
18 (monthly) as input to drive the DOS-TEM. Leaf area index, ~~one half of the total one-sided~~
19 green leaf area per unit ground surface area, was specified to be $0.6 \text{ m}^2 \text{ m}^{-2}$ in July and August,
20 $0.1 \text{ m}^2 \text{ m}^{-2}$ in April and October, ~~0 m²m⁻² between November and March,~~ and interpolated
21 linearly in other months. It is used in the DOS-TEM to calculate ground surface temperature
22 in combination with other meteorological variables (Yi et al., 2013). ~~Its value is unchanged~~
23 ~~within each month.~~

24 Soil temperature and moisture were initialized at $-1 \text{ }^\circ\text{C}$ and saturation. ~~Sand and silty clay~~
25 ~~were used in testing to represent coarse and fine soil textures, respectively, on the QTP~~
26 ~~(FAO/HASA/ISRIC/ISSCAS/JRC, 2009).~~ The temperature gradient at the bottom of bedrock
27 was set to be $0.06 \text{ }^\circ\text{C cm}^{-1}$ based on borehole observations. Volumetric unfrozen liquid water
28 in winter was set to be 0.1 based on observations. ~~The DOS TEM was the spun up using the~~
29 ~~Multi-year mean driving data from (2003-2012) monthly driving data were used for spun up~~

1 for 100 yr. In this way, proper initial values of soil moisture, temperature and rock
2 temperature of each layer can be generated for the beginning of 2003. Finally, monthly
3 driving data were used to drive DOS-TEM over the period of 2003-2012.

4 2.5 Sensitivity analyses

5 ~~We considered two soil textures in the DOS-TEM, i.e. silty clay and sand. The former is~~
6 ~~considered as the major soil type of this region (Lin et al., 2011), and the latter is the coarsest~~
7 ~~soil type considered in land surface modeling (Oleson et al., 2010). The soil textures on the~~
8 ~~QTP mainly consist of loam, sand and gravel (Wu and Nan, 2016). We used sand and loam in~~
9 ~~whole soil profile uniformly to represent coarse and fine soil textures, respectively. The~~
10 ~~parameters of gravel are not considered in most of the modeling studies (e.g. Oleson et al.,~~
11 ~~2010). Therefore, we used our measured parameters to substitute the parameters of sand and~~
12 ~~loam to investigate the effects of soil parameters on permafrost dynamics.~~ We first ran the
13 DOS-TEM using the default porosity, soil thermal conductivity (Equation 14), hydraulic
14 conductivity (Equation 58) and matric potential schemes of these two soil ~~types-textures~~
15 (Equation 74). The default parameters Φ , Ψ_{sat} , K_{sat} and B were calculated based on soil texture
16 used in Community Land Model (Equation 4-7 and 58; Oleson et al., 2010). We then
17 substituted the ~~original- default~~ values of Φ , Ψ_{sat} , K_{sat} and B based on laboratory
18 measurements and calibration. Saturated matric potential and B were fitted with measured
19 matric potential data using Isqucurvefit tools of Matlab. We did not calibrate soil thermal
20 conductivity to retrieve parameters of Equation 2-5 and 36. Instead, we interpolated measured
21 thermal conductivity over a range of the degree of saturation (0 to 1), which was used as a
22 lookup table by the DOS-TEM. Therefore, our sensitivity analyses considered a set of 4
23 factors, i.e. porosity, matric potential (Ψ_{sat} and B), hydraulic conductivity (K_{sat} and B) and
24 thermal conductivity. We also analyzed 3 different slopes (0, 5 and 10°) and 3 different soil
25 thicknesses (3.25, 4.25 and 5.25 m) above 56 m of bed rock. There are 11 soil layers with the
26 top 9 layers being 0.05, 0.1, 0.1, 0.2, 0.2, 0.2, 0.3, 0.3 and 0.3 m thick. The thicknesses of the
27 bottom 2 soil layers are 0.5 and 1 m, 0.5 and 2 m, and 1.5 and 2 m for the 3.25, 4.25 and 5.25
28 m cases, respectively. There are 6 rock layers with thicknesses of 2, 2, 4, 8, 16 and 20 m.
29 Since the site is on the top of upland plain landforms, we did not further test the effects of
30 aspect on radiation on ground surface. We considered the effects of slope on surface runoff. In

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1 summary, our sensitivity analyses with the DOS-TEM involved 288 different combinations of
2 parameter values.

3 We did not measure the heat capacity of gravelly soil. The maximum and minimum heat
4 capacities of mineral soil types considered in land surface model are 2.355 and 2.136 MJ m⁻³,
5 respectively. The relative difference is less than 10%. Therefore, in this study, we did not
6 make sensitivity tests using thermal diffusivity (the ratio between thermal conductivity and
7 heat capacity).

8 3 Results

9 3.1 Soil physical properties

10 3.1.1 Soil porosity, particle size and bulk density

11 The mean weight fraction of gravel (particle size diameter > 2 mm) of different soil layers
12 ranged from 0.38 to 0.65 with a mean of 0.55 (Table 1). ~~The weight fraction of soil with~~
13 ~~particle size diameter > 0.25 mm ranged from 0.77 to 0.86 with a mean of 0.84 among~~
14 ~~layers. According to the USDA classification system (clay (<2 μ m), silt (2 -50 μ m, in this~~
15 ~~study 2-63 μ m) and sand (50 μ m -2.0 mm, in this study 63 μ m -2.0 mm)), the major soil~~
16 ~~texture of this site was loamy sand, with the exception of sandy loam at depth of 20-30 cm~~
17 ~~(Table 1).~~ The default porosities of sand and ~~silty clayloam~~ were 37.3% and 43.58.1%,
18 respectively. The mean porosity of samples in 2 m depth ranged from 21% to 30% with a
19 mean of 27%. The mean bulk density ranged from 1.61 to 1.86 g cm⁻³ with a mean of 1.74 g
20 cm⁻³. No significant relationships were found among soil porosity, bulk density and the
21 fraction of gravel.

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22 3.1.2 Thermal conductivity

23 The mean unfrozen dry soil thermal conductivity of different soil layers ranged from 0.24 to
24 0.40 W m⁻¹ K⁻¹W-m⁻² with a mean of 0.36 W m⁻¹ K⁻¹W-m⁻² (Table 2). The mean frozen dry
25 soil thermal conductivity ranged from 0.25 to 0.41 W m⁻¹ K⁻¹W-m⁻² with a mean of 0.35 W m⁻¹
26 K⁻¹W-m⁻². The difference of dry thermal conductivity between frozen and unfrozen states
27 was small. The mean unfrozen saturated soil thermal conductivity of different soil layers
28 ranged from 2.15 to 2.74 W m⁻¹ K⁻¹W-m⁻² with a mean of 2.48 W m⁻¹ K⁻¹W-m⁻² (Table 2).

1 The mean frozen saturated soil thermal conductivity ranged from 3.06 to 3.72 $\text{W m}^{-1} \text{K}^{-1} \text{W m}^{-2}$
2 ² with a mean of 3.33 $\text{W m}^{-1} \text{K}^{-1} \text{W m}^{-2}$. The difference of saturated thermal conductivity
3 between frozen and unfrozen states was about 0.85 $\text{W m}^{-1} \text{K}^{-1} \text{W m}^{-2}$. There existed a
4 threshold of soil wetness, below which frozen soil thermal conductivity was slightly smaller
5 than unfrozen soil (Figure 2a4a).

6 The default dry frozen and unfrozen thermal conductivities using Côté and Konard (2005)
7 scheme of sand and silty clay loam were about 0.42 and 0.22-24 $\text{W m}^{-1} \text{K}^{-1} \text{W m}^{-2}$, respectively.
8 The saturated frozen and unfrozen thermal conductivities of sand were 3.11 and 1.90 W m^{-1}
9 $\text{K}^{-1} \text{W m}^{-2}$, respectively. Those of silty clay loam were about 2.35-36 and 1.24-33 $\text{W m}^{-1} \text{K}^{-1} \text{W}$
10 m^{-2} , respectively (Figure 2b4b). The default dry frozen and unfrozen thermal conductivities
11 using Farouki scheme of sand and silty clay loam were about 0.97 and 0.33-63 $\text{W m}^{-1} \text{K}^{-1} \text{W m}^{-2}$
12 ², respectively. The saturated frozen and unfrozen thermal conductivities of sand were 5.21
13 and 3.18 $\text{W m}^{-1} \text{K}^{-1} \text{W m}^{-2}$, respectively. Those of silty clay loam were about 2.874.49 and
14 4.522.52 $\text{W m}^{-1} \text{K}^{-1} \text{W m}^{-2}$, respectively (Figure 2e4c).

15 3.1.3 Saturated hydraulic conductivity

16 The mean saturated hydraulic conductivity of soil layers ranged from 0.0036 to 0.0315 mm s^{-1} .
17 The maximum saturated hydraulic conductivity was about 8.7 times larger than the minimum
18 (Table 3). The saturated hydraulic conductivity tended to be larger with increasing proportion
19 of gravel content coarse fragment in the soil samples (Figure 3a5a), and was about 0.03-0.06
20 mm s^{-1} for some samples with gravel content coarse fragment greater than 70%. The default
21 saturated hydraulic conductivities of sand and silty clay loam were 0.024 and 0.0011-0042 mm
22 s^{-1} , respectively.

23 3.1.4 Matric potential

24 ~~Saturated matric potential and B were fitted using measured matric potential values.~~ The
25 correlation coefficients between calculated and fitted matric potential were all greater than
26 0.96. The mean absolute value of saturated matric potential of soil layers ranged from 27.02
27 to 603.7 mm, and those of B ranged from 5.22 to 1.89 (Table 3 and Figure 3b5b). The default
28 absolute value of saturated matric potential of sand and silty clay loam were 47.29 and
29 632.99-207.34 mm, respectively, and the B values 3.39 and 40.385.77, respectively.

1 3.2 Comparisons between simulations using default vs. measured parameters

2 3.2.1 Soil temperature

3 The mean root mean squared errors (RMSEs) between monthly measured soil temperatures
4 and model runs with measured parameters using different combination of soil thicknesses
5 (3.25, 4.25 and 5.25 m) and slopes (0, 5 and 10°) were about 1.07 °C at 20 cm (Figure 4e6c).
6 The mean RMSEs for all model runs with default sand and ~~silty-clayloam~~ parameters were
7 about 0.97 and ~~1.37~~1.18 °C, respectively. For other soil layers, the RMSEs of model runs with
8 measured parameters were much smaller than those with default sand and ~~silty-clayloam~~
9 parameters (Figure 4d6d-l). The simulated soil temperatures using default sand and ~~silty~~
10 ~~clayloam~~ parameters were all lower than measured ones in summer at 100 and 200 cm; and in
11 winter at 400 cm. The RMSEs can be as large as ~~2.91~~53 °C (Figure 4e6e).

12 The standard deviations of soil temperatures among different slopes and soil thicknesses
13 using measured parameters were larger than those using the default parameters (Figure-46);
14 and they increased from 0.40 °C at 100 cm to 0.61 °C at 200 cm (Figure 4f-6f and i). The
15 standard deviations using default ~~silty-clayloam~~ parameters were smaller (<0.06-15 °C at all
16 depths) than those using default sand parameters.

17 3.2.2 Soil liquid water

18 The mean RMSEs between monthly measured liquid soil volumetric water content (VWC)
19 and model simulations with measured parameters ranged from 0.03 to 0.09, which were
20 smaller than RMSEs for sand and ~~silty-clayloam~~ parameters (Figure 57). The model
21 simulations for ~~silty-clayloam~~ parameters have larger RMSEs than those for sand parameters.
22 VWCs were always overestimated in warm seasons at depths of 10, 40 and 80 cm. VWCs
23 were underestimated at a depth of 160 cm, where the simulated soil was frozen. All model
24 simulations overestimated VWC at 40 cm, where the maximum measured VWCs were about
25 0.1 (Figure 5d7d-f).

26 The standard deviations of VWC among different slopes and soil thicknesses using sand
27 parameters were about 0.077, which were larger than those using measured parameters
28 (~0.062). The standard deviations of VWC using ~~silty-clayloam~~ parameters (<0.011032) were
29 less than those using measured parameters.

1 3.2.3 Active layer depth (ALD)

2 The mean RMSEs between measured ALDs (derived from linear interpolation of soil
3 temperatures) and modelled ALDs (simulated explicitly) were about 1.06, ~~1.83-72~~ and 0.28 m
4 for model runs with sand, ~~silty-clayloam~~ and measured parameters (Figure ~~6a8a~~). The mean
5 standard deviations were about 0.088, ~~0.0070.026~~ and 0.28 m. All simulations using sand and
6 ~~silty-clayloam~~ parameters underestimated ALDs.

7 3.2.4 Permafrost lower boundary (PLB)

8 The mean RMSEs between measured PLBs (derived from linear interpolation of temperatures)
9 and modelled PLBs (derived from linear interpolation of simulated bed rock temperatures)
10 were about 10.25, ~~7.9610.23~~ and 6.71 m for model runs with sand, ~~silty-clayloam~~ and
11 measured parameters (Figure 6b). The mean standard deviations were about 1.89, ~~0.291.51~~
12 and 6.62 m. All simulations using sand and ~~silty-clayloam~~ parameters overestimated PLBs.
13

14 3.3 Model sensitivity analyses

15 Deep soil layers used in models are usually specified as being thick. For example, a 1 m thick
16 soil layer was used in our simulations starting around 3 m soil depth. Soil temperatures at this
17 depth are usually close to 0°C. Therefore, the RMSEs of deep soil layers were small and did
18 not facilitate evaluation of model sensitivities. In the following subsections, we used 20 and
19 100 cm soil temperatures, ALDs and PLBs for sensitivity analysis.

20 3.3.1 Effects of single parameter sensitivity analyses

21 Porosity

22 Replacing default sand or ~~silty-clayloam~~ porosity with measured porosities changed mean
23 RMSEs of soil temperatures (model runs with 3 different slopes and 3 different soil
24 thicknesses at 2 different soil depths) from 1.18 or ~~2.111.84~~ °C to 1.25 or ~~1.08-09~~ °C,
25 respectively (Figure ~~7-9~~ and ~~810~~). Mean RMSEs of ALD were reduced from 1.06 or ~~1.84-72~~
26 m to 0.22 or ~~0.83-85~~ m, respectively. Mean RMSEs of PLB were changed from 10.26 or
27 ~~7.9610.24~~ m to 6.61 or ~~10.26-97~~ m. Mean RMSEs of VWC were reduced from 0.074 or ~~0.20~~

1 | ~~14~~ to 0.06 or ~~0.073-062~~ when measured porosities were used for replacing default sand or
2 | ~~silty-clayloam~~ porosity, respectively (Figure ~~9-11~~ and ~~1012~~).

3 | **Thermal conductivity**

4 | Replacing default sand or ~~silty-clayloam~~ thermal conductivity with measured thermal
5 | conductivity reduced mean RMSEs of soil temperatures from 1.18 or ~~2.11~~1.84°C to 1.02 or
6 | ~~1.33~~1.15°C, respectively (Figure ~~7-9~~ and ~~810~~). Mean RMSEs of ALD were reduced from
7 | 1.06 or ~~1.84-72~~ m to 0.56 or ~~1.18-04~~ m, respectively. Mean RMSEs of PLB were changed
8 | from 10.26 or ~~7.96~~10.24 m to 4.18 or ~~2.54~~1.27 m, respectively. Mean RMSEs of VWC
9 | changed very slightly (Figure ~~9-11~~ and ~~1012~~).

10 | **Hydraulic conductivity/Matric potential**

11 | Replacing default sand or ~~silty-clayloam~~ hydraulic conductivity with measured parameters
12 | had very small effects on mean RMSEs of soil temperatures and ALDs (Figure ~~7-9~~ and ~~810~~).
13 | The same was true for matric potential. When hydraulic conductivity of default sand or ~~silty~~
14 | ~~clayloam~~ was substituted, mean RMSEs of PLB were decreased or increased, however, when
15 | matric potential was substituted, mean RMSEs of PLBs were increased or decreased,
16 | respectively. When hydraulic conductivity or matric potential parameters were substituted in
17 | default sand or ~~silty-clayloam~~ parameters, mean RMSEs of VWC changed slightly (Figure ~~9~~
18 | ~~11~~ and ~~1012~~).

19 | **3.3.2 Effects of combined parameters**

20 | We compared model simulations with different combinations of measured parameters
21 | (porosity, thermal conductivity, hydraulic conductivity and matric potential) with those with
22 | one substituted measured parameter. We ~~selected-ranked~~ those model runs with less RMSEs
23 | than any of model runs with one substituted measured parameter (Table 4 and 5). We didn't
24 | consider the 10 cm soil temperature, which were similar among all model runs.

25 | For sand, model simulations with porosity and thermal conductivity or hydraulic
26 | conductivity substituted had 4 outcomes with lower RMSEs (Table 4 and Figures ~~7-9~~ and
27 | ~~911~~). Only 2 out of 7 outcomes had lower RMSEs with all 4 parameters were substituted.
28 | Among all the 18 cases with RMSEs less than the individual "best" RMSE, porosity was
29 | included 18 times, followed by thermal conductivity and hydraulic conductivity with 10 times.

1 For ~~silty clay loam~~, model simulations with porosity and thermal conductivity ~~and/or matric~~
2 ~~potential~~ substituted had 5 outcomes with lower RMSEs (Table 5 and Figures ~~8-10~~ and ~~1012~~).
3 Among all the ~~29-27~~ cases with RMSEs less than the individual “best” RMSE, porosity was
4 included ~~279~~ times, followed by thermal conductivity with ~~20-16~~ times and matric potential
5 with ~~16-14~~ times.

6 3.3.3 Effects of slope and soil thickness

7 Changes of slope alone had small effects on simulated soil temperatures and ALDs (Figures ~~7~~
8 ~~9~~ and ~~810~~). An increase of slope generally reduced RMSEs of VWCs (Figures ~~9-11~~ and ~~1012~~).
9 Model simulations with porosity substituted had smaller difference of VWC RMSE between
10 different cases of slopes. For example, the mean RMSEs of model simulations with slope of
11 0° or 5° and porosity substituted in default sand parameters were 0.078 or 0.048, respectively.
12 While those with porosity not substituted were 0.141 or 0.055, respectively. Similarly, the
13 mean RMSEs of model simulations using default ~~silty clay loam~~ parameters with porosity
14 substituted were 0.084 or 0.0605 for slope of 0° or 5°, respectively. The mean RMSEs were
15 0.2118 or 0.138 with porosity not substituted, respectively. For a further increase of slope to
16 10°, changes of RMSEs of VWCs at depths of 10-160 cm were small.

17 Soil thickness had small effects on 20 and 100 cm soil temperatures and 10-160 cm VWCs,
18 and it had prominent effects on PLB for a few cases only with a slope of 10° (Figures ~~7-9~~ and
19 ~~810~~).

20 4 Discussion

21 4.1 Characteristics of soil physical properties

22 Although the effects of ~~gravelly coarse fragment~~ soil on permafrost dynamics have been
23 considered in a few modelling studies, the thermal and hydraulic properties of ~~gravelly coarse~~
24 ~~fragment~~ soil were calculated without validation or ~~calibrated calibration~~ (Pan et al., 2017;
25 Wu et al., 2018). To our knowledge, this is the first study measuring physical properties of
26 ~~gravelly coarse fragment~~ soil samples from permafrost region of the QTP.

27 The weight fraction of ~~gravel coarse fragment~~ (diameter > 2mm, ~~including gravel~~) in the
28 soil samples we analysed was greater than 55% on average. While the typical soil types
29 considered in land surface models and other models usually have much smaller diameter. For

1 comparison, the fractions of gravel considered in Pan et al. (2017) ranges from 5% to 33%
2 and from 10% to 28% for the Madoi and Naqu sites, respectively. The Beiluhe site and the
3 aforementioned sites are located in regions with Gelisols and Inceptisols, which occupy ~62%
4 of the permafrost regions of the QTP (Li et al., 2015). It is possible that ~~gravelly-coarse~~
5 ~~fragment~~ soil commonly exists on the QTP. The dataset of Wu and Nan (2016) indicated that
6 gravel content widely exists on the middle and west part of the QTP. The saturated hydraulic
7 conductivity and matric potential of soil samples measured in this study were more similar to
8 sand than to ~~silty-clayloam~~ (see Section 3.1). It is consistent with the study of Wang et al.
9 (2013) that coarse soil material has poor water holding capability.

10 The measured ~~saturated~~ thermal conductivities of saturated soil samples were relatively
11 close to those estimated by the C α é and Konard (2005) scheme. But they were much less
12 than those estimated by the Farouki scheme (Figure 24). Several other studies also found that
13 Farouki scheme overestimated soil thermal conductivity (Chen et al. 2012; Luo et al., 2009).

14 One important finding of this study is the relatively small value of porosity. The measured
15 porosity ranged from 0.206 to 0.302, which is less than those of soil types considered in land
16 surface models. For example, the porosities of mineral soil types considered in Community
17 Land Model range from 0.37 to 0.48 (Oleson et al., 2010). Porosity determines the maximum
18 water stored in a soil layer, and affects soil thermal conductivity, hydraulic conductivity and
19 matric potential (Equation 25-58). It plays a more important role than other parameters in
20 simulated soil thermal and hydrological dynamics (Table 4 and 5; Figure 79-1012). It is
21 noteworthy that it is easy and efficient to measure porosity.

22 4.2 Effects of soil water on permafrost dynamics

23 Soil water not only affects soil thermal properties, e.g. thermal conductivity and heat capacity,
24 but also affects the amount of latent heat lost or gained, for freezing or thawing, respectively
25 (Goodrich, 1978; Farouki, 1986). Soil water is determined by infiltration, evapotranspiration,
26 water movement among soil layers, subsurface runoff and exchange with a water reservoir.
27 Therefore, processes or parameters that affect soil water dynamics will also affect permafrost
28 dynamics. This study quantitatively assessed the effects of soil water on permafrost dynamics.
29 For example, when default ~~silty-clayloam~~ parameters with high porosity and low saturated
30 hydraulic conductivity were used, soil layers were almost saturated (Figure 57). The
31 simulated ALDs were about 1.47-58 m, which was less than half of measured ALDs (Figure

1 | ~~6a8a~~). When the slope was 0° , subsurface runoff didn't happen in saturated zone above the
2 bottom of the active layer. The simulated soil water content was generally higher in the active
3 layer. However, when the slope was 5° , the simulated soil water content was less and the
4 RMSE was smaller (Figure ~~9-11~~ and ~~1012~~). These patterns were especially obvious when
5 both porosity and saturated hydraulic conductivity were large (Equation ~~96~~; Figure ~~9-11~~ and
6 ~~1012~~). Other studies have also emphasized the importance of subsurface runoff above the
7 bottom of the active layer (Frey and McClelland, 2009; Walvoord and Striegl, 2007). The
8 effects of soil water content on soil thermal dynamics increased with soil and rock depth
9 (Figure ~~7-9~~ and ~~810~~). The biggest effects were on PLB, which became manifest during long-
10 term spinup procedures.

11 Land surface models generally represent soil water dynamics (e.g. Chen et al., 2015;
12 Oleson et al., 2010; Wang et al., 2017). However the ~~permafrost-thermal~~ processes in ~~these~~
13 ~~permafrost~~ models usually use specified thermal properties, which were static during model
14 simulations (Li et al., 2009; Nan et al., 2005; Qin et al., 2017; Zou et al., 2017). As shown in
15 this study, when permafrost degraded, the thermal and hydrological regimes of soil also
16 changed. It is critical to simulate soil water dynamics to properly project permafrost dynamics
17 in the future.

18 **4.3 Limitations and Outlook**

19 **4.3.1 Sampling and laboratory measurement**

20 We used cut rings with 10 cm diameter to take soil samples. There are weathered mudstones
21 in our study site, which can be sampled in cut rings. However, it is very likely that there are
22 soil samples with much bigger ~~gravel~~coarse soil fragment. Therefore, larger containers
23 should be used to take samples for further laboratory analysis in the future.

24 During our laboratory work, we found two phenomena. First, we originally used the QL-
25 30 thermophysical instrument to measure thermal conductivity. It worked properly under
26 unfrozen condition. However, when frozen, surface of soil samples was uneven due to frost
27 heave. The contact between plate of QL-30 and soil sample surface was not ideal. The
28 measured frozen thermal conductivities were smaller than unfrozen thermal conductivity even
29 for the case of saturation, which were definitely wrong. The second phenomenon -was that
30 there seems to be a threshold of soil wetness, below which unfrozen soil thermal conductivity

1 | is greater than frozen soil thermal conductivity (Figure [2e4a](#)). This pattern was somewhat
2 | exhibited in estimates of the Côté and Konard (2005) scheme, but not in the estimates of the
3 | Farouki scheme (Figure [2e4c](#)). More measurements using instruments with higher accuracy
4 | should be made in the future.

5 | **4.3.2 Model simulation**

6 | Although the DOS-TEM using measured parameters provided satisfactory results, there are
7 | some aspects requiring further improvement in the future. For example, the measured soil
8 | moistures at 40 cm depth were less than $0.1 \text{ m}^3/\text{m}^3$. However, the simulated soil moistures
9 | were always much greater (Figure [5f7f](#)). There were spikes of measured soil moistures at 80
10 | and 160 cm depths, which were not presented in simulation (Figure [5-7](#) i and l). In the DOS-
11 | TEM, the unfrozen soil water content, or supercold water, was prescribed to be $0.1 \text{ m}^3/\text{m}^3$.
12 | When soil is freezing, if soil liquid water content is less than this value, no phase change will
13 | happen (Figure [5k7k](#)). It is ideal to simulate the dynamics of unfrozen soil water content
14 | (Romanovsky and Osterkamp, 2000).

15 | Field studies have shown that [gravel-coarse soil fragment](#) content in root zone affects
16 | vegetation growth (Qin et al., 2015), which affects ground surface temperature (Yi et al.,
17 | 2013). In the current study, we used specified leaf area index. The fractions of [gravel-coarse](#)
18 | [fragment](#) content in soil are also dynamic. For example, Chen et al. (2017) found that plateau
19 | pika excavated subsurface soil with gravel on to surface. Fine soil particles were carried away
20 | by wind and water erosion, which resulted in gravel remaining at the surface. Our ongoing
21 | research is working towards representing the coupling of vegetation growth, small mammal
22 | disturbances, and soil erosion on permafrost dynamics of the QTP in the future.

23 | **4.3.3 Regional applications**

24 | Soil texture plays an important role in permafrost dynamics (Figure [68](#)). However, the
25 | dominant soil texture on the QTP from [FAO/IIASA/ISRIC/ISSCAS/JRC Wu and Nan](#)
26 | [\(2009/2016\)](#) is [silty-clayloam, sand and gravel](#). The specification of [silty-clayloam](#) in
27 | simulations results in estimates of ALD that are much smaller than measurements (Yi et al.,
28 | 2014a). To properly simulate the distribution and dynamics of permafrost on the QTP under
29 | climate change scenarios, it is important to develop proper schemes of soil physical properties

1 | in relation to ~~gravel-coarse fragment~~ content (including gravel) and to develop regional
2 | datasets of soil texture for input.

3 | ~~Gravel-Coarse fragment~~ content affects soil physical properties. For example, soil porosity
4 | and saturated hydraulic conductivity are determined by the fraction of gravel, diameter and
5 | degree of mixture (Zhang et al., 2011). Organic soil carbon content in mineral soil on the QTP
6 | affects soil porosity and thermal conductivity (Chen et al., 2012). Alpine swamp meadow,
7 | alpine meadow, alpine steppe and alpine desert are the major vegetation types on the QTP
8 | (Wang et al., 2016; see also Figure 1b). Alpine swamp meadow and alpine meadow usually
9 | contain fine soil particles and high organic carbon density; while the other two types usually
10 | contain coarse soil particle and low organic carbon density (Qin et al., 2015). We only
11 | measured physical properties of soil samples from one site on the QTP in this study. The
12 | mean gravel fraction was about 0.55, which is definitely not suitable for direct use in regional
13 | simulations. More laboratory work is needed to develop proper schemes for representing
14 | mixed soil with fine mineral, coarse fragment (including gravel) and organic carbon in
15 | permafrost models. It is the first priority to develop schemes that make use of porosity data
16 | sets, due to its importance and simplicity of measurement.

17 | The development of a spatially explicit dataset of soil texture is also required for regional
18 | applications of projecting permafrost changes on the QTP. One way is to collect relevant data
19 | through extensive field campaigns (e.g., Li et al., 2015). Currently, gravelly soil has only been
20 | mentioned in scientific literature on the QTP (Chen et al., 2015; Wang et al., 2011; Yang et al.,
21 | 2009), ~~and no systematic analysis of gravelly soils exists across the QTP. Only recently, an~~
22 | preliminary dataset considering gravel has been created (Wu and Nan, 2016). Ground
23 | penetrating radar is a feasible tool to retrieve soil thickness above ~~gravel-coarse soil fragment~~
24 | layer (Han et al., 2016). Unmanned aerial vehicles has been used recently (Yi, 2017), and
25 | ~~gravel-coarse soil fragment~~ on the ground surface can be identified easily in aerial photos
26 | (Chen et al., 2017). In combination with ancillary datasets, e.g. geomorphology, topography,
27 | vegetation, it is possible to ~~generate-improve the accuracy of~~ spatial datasets of soil texture on
28 | the QTP (Li et al., 2015; Wu et al., 2016). Another way is to retrieve soil physical properties
29 | using data assimilation technology, e.g. Yang et al. (2016) assimilated porosity using a land
30 | surface model and microwave data.

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1 5 Conclusions

2 In this study, we excavated soil samples from a permafrost site on the central QTP and
3 measured soil physical properties in laboratory. ~~Gravel~~Coarse soil fragment content was
4 common in the soil profile and porosity was much smaller than the typical soil types used in
5 land surface models. We then performed sensitivity analysis of these parameters on soil
6 thermal and hydrological processes within a terrestrial ecosystem model. When default sand
7 or silty clay loam parameters were substituted with measured soil properties, the model errors
8 of soil temperature, soil liquid water content, active layer depth and permafrost low boundary
9 were generally reduced. Sensitivity analyses showed that porosity played a more important
10 role in reducing model errors than other soil properties examined. Though it is unclear how
11 representative this soil is in the QTP, it is clear that soil physical properties specific to the
12 QTP should be used to properly project permafrost dynamics into the future.

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28

带格式的: 行距: 1.5 倍行距

1 **Table 1.** The mean (standard deviation) of measured soil bulk density, porosity, and particle
2 size diameter fractions (>2 mm means the weight fraction between soil particles greater than
3 2 mm and total soil sample; while other fraction means the ratio between soil sample weight
4 of a size range and the weight of particles < 2mm) and soil texture (based on USDA
5 classification) of different layers based on soil samples in this study.

<u>Layer</u> <u>(cm)</u>	<u>Bulk</u> <u>density</u> <u>(g cm⁻³)</u>	<u>Porosity</u> <u>(%)</u>	<u>Fractions of particle in each diameter range</u>				<u>Texture</u>
			<u>>2 mm</u>	<u><2 μ m</u>	<u>2-63 μ m</u>	<u>>63 μ m</u>	
<u>0—10</u>	<u>1.74</u> <u>(0.21)</u>	<u>28.4</u> <u>(0.03)</u>	<u>0.38</u> <u>(0.07)</u>	<u>0.05</u> <u>(0.02)</u>	<u>0.18</u> <u>(0.04)</u>	<u>0.77</u> <u>(0.07)</u>	<u>Loamy</u> <u>sand</u>
<u>10—20</u>	<u>1.81</u> <u>(0.11)</u>	<u>27.7</u> <u>(0.02)</u>	<u>0.52</u> <u>(0.14)</u>	<u>0.07</u> <u>(0.05)</u>	<u>0.20</u> <u>(0.05)</u>	<u>0.72</u> <u>(0.11)</u>	<u>Loamy</u> <u>sand</u>
<u>20—30</u>	<u>1.86</u> <u>(0.32)</u>	<u>30.2</u> <u>(0.05)</u>	<u>0.55</u> <u>(0.17)</u>	<u>0.07</u> <u>(0.01)</u>	<u>0.24</u> <u>(0.08)</u>	<u>0.69</u> <u>(0.09)</u>	<u>Sandy</u> <u>loam</u>
<u>40—50</u>	<u>1.61</u> <u>(0.23)</u>	<u>29.6</u> <u>(0.02)</u>	<u>0.55</u> <u>(0.19)</u>	<u>0.04</u> <u>(0.02)</u>	<u>0.26</u> <u>(0.11)</u>	<u>0.70</u> <u>(0.13)</u>	<u>Loamy</u> <u>sand</u>
<u>70—80</u>	<u>1.62</u> <u>(0.20)</u>	<u>20.6</u> <u>(0.11)</u>	<u>0.65</u> <u>(0.16)</u>	<u>0.04</u> <u>(0.02)</u>	<u>0.25</u> <u>(0.07)</u>	<u>0.71</u> <u>(0.09)</u>	<u>Loamy</u> <u>sand</u>
<u>110—120</u>	<u>1.75</u> <u>(0.09)</u>	<u>27.7</u> <u>(0.01)</u>	<u>0.63</u> <u>(0.05)</u>	<u>0.03</u> <u>(0.02)</u>	<u>0.19</u> <u>(0.08)</u>	<u>0.79</u> <u>(0.09)</u>	<u>Loamy</u> <u>sand</u>
<u>150—160</u>	<u>1.70</u> <u>(0.15)</u>	<u>26.3</u> <u>(0.02)</u>	<u>0.63</u> <u>(0.09)</u>	<u>0.02</u> <u>(0.01)</u>	<u>0.13</u> <u>(0.03)</u>	<u>0.85</u> <u>(0.04)</u>	<u>Loamy</u> <u>sand</u>
<u>190—200</u>	<u>1.81</u> <u>(0.09)</u>	<u>27.1</u> <u>(0.02)</u>	<u>0.50</u> <u>(0.19)</u>	<u>0.05</u> <u>(0.05)</u>	<u>0.24</u> <u>(0.14)</u>	<u>0.71</u> <u>(0.19)</u>	<u>Loam</u> <u>y</u> <u>sand</u>

7

1 **Table 2.** The mean (standard deviation) of the measured frozen and unfrozen dry and
 2 saturated soil thermal conductivity ($\text{W m}^{-1} \text{K}^{-1}$) of different soil layers.
 3

Layer (cm)	Dry		Saturated	
	Unfrozen	Frozen	Unfrozen	Frozen
0-10	0.238 (0.09)	0.414 (0.09)	2.322 (0.17)	3.122 (0.48)
10~20	0.340 (0.04)	0.365 (0.23)	2.147 (0.47)	3.193 (0.55)
20-30	0.395 (0.07)	0.420 (0.11)	2.743 (0.38)	3.059 (0.29)
40-50	0.346 (0.00)	0.388 (0.14)	2.539 (0.30)	3.184 (0.33)
70-80	0.340 (0.03)	0.289 (0.12)	2.589 (0.16)	3.362 (0.38)
110-120	0.400 (0.06)	0.271 (0.07)	2.616 (0.11)	3.721 (0.05)
150-160	0.401 (0.01)	0.248 (0.07)	2.246 (0.19)	3.647 (0.48)
190-200	0.399 (0.26)	0.392 (0.14)	2.609 (0.12)	3.329 (0.19)

4
5

1 **Table 3.** The mean (standard deviation) of measured saturated hydraulic conductivity (K_{sat} ;
 2 mm s^{-1}) and fitted absolute value of saturated matric potential (Ψ_{sat} ; mm), fitted pore size
 3 distribution parameter (B) and the correlation coefficients (R^2) between calculated matric
 4 potential using fitted equations and measured.

5

Layer (cm)	K_{sat}	Matric potential		
		Ψ_{sat}	B	R^2
0-10	0.0285 (0.0274)	49.14	4.03	0.991
10~20	0.0056 (0.0036)	70.66	4.49	0.996
20-30	0.0047 (0.0027)	27.02	5.22	0.994
40-50	0.0078 (0.0043)	143.4	3.59	0.994
70-80	0.0072 (0.0054)	179.6	3.22	0.993
110-120	0.0315 (0.0054)	603.7	1.89	0.969
150-160	0.0053 (0.0028)	49.17	2.97	0.993
190-200	0.0036 (0.0023)	14.47	4.565	0.989

6

7

1 **Table 4.** Model performance of substituting default sand parameters with measured porosity
 2 (I), thermal conductivity (II), hydraulic conductivity (III) and matric potential (IV) .

	Best	I+II	I+ III	I+ IV	II+ III	II+ IV	III+ IV	I+ II+	I+ II+	I+ III +IV	II +III +IV	All
100 cm ST	II											
ALD	I		1									
PLB	II	1	2									
10 cm SM	I	7	2	4				1	5	6		3
40 cm SM	I											
80 cm SM	I	7	1	4				2	6	5		3
160 cm SM	I	1										

3 **Note:** Best column showed the model simulations (individual parameter substitution) with the
 4 smallest root mean squared error (RMSE) for 100 cm soil temperature (ST, °C), active layer
 5 depth (ALD, m), permafrost low boundary (PLB, m), 10, 40, 80 and 160 cm soil liquid water
 6 content (SM, -); Number indicated the combination of parameters (+) had smaller RMSE
 7 than the best model run using individual parameter substitution. All indicated the combination
 8 of all 4 parameters. The smallest number indicated the smallest RMSE.

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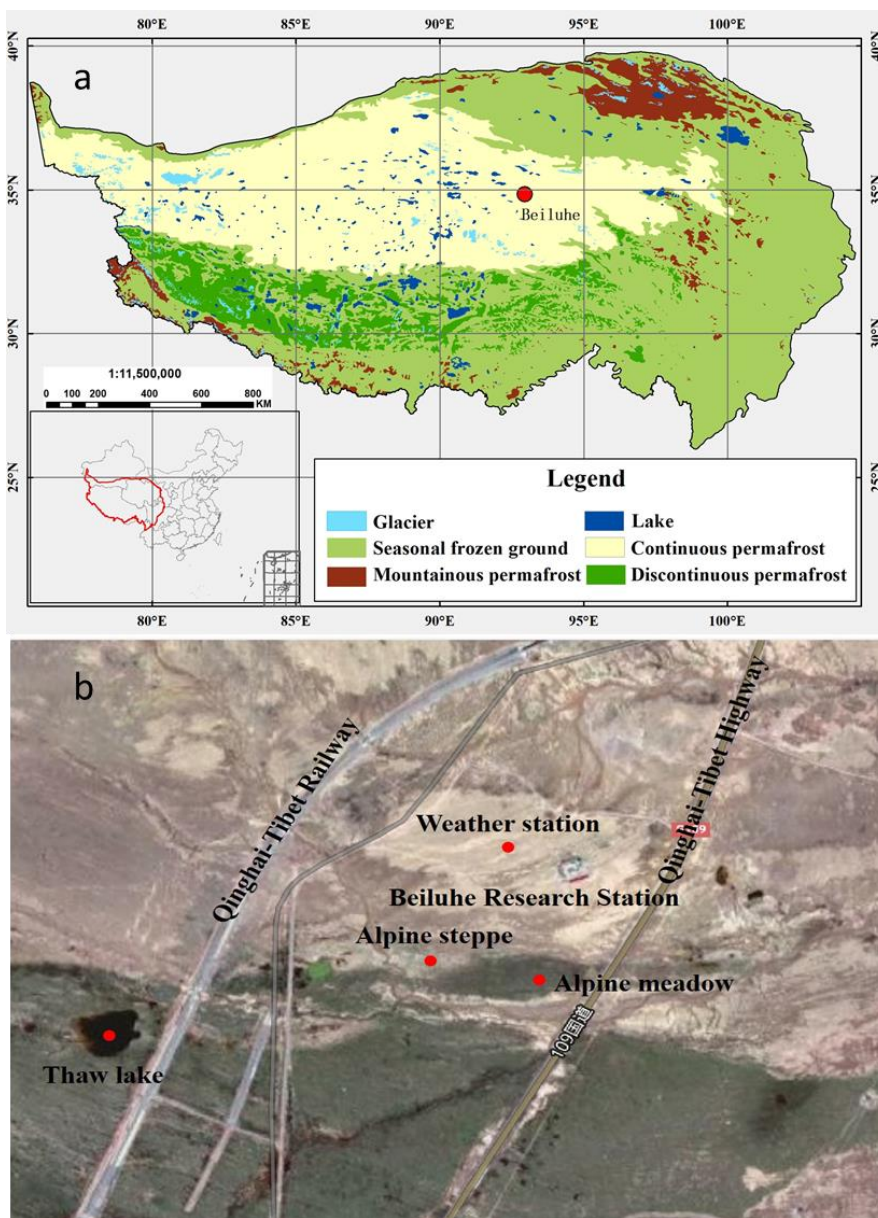
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1 **Table 5** Model performance of substituting default loam parameters with measured porosity
 2 (I), thermal conductivity (II), hydraulic conductivity (III) and matric potential (IV). ~~Same as~~
 3 Table 4, but for silty clay.
 4

	Best	I+	I+	I+	II+	II+	III+	I+	I+	I+	II	All
		II	III	IV	III	IV	IV	II+	II+	III	+III	
								III	IV	+IV	+IV	
100 cm ST	I	<u>2</u> ₁		<u>1</u> ₂					3			
ALD	I	<u>4</u> ₃	5	<u>7</u>				1	2	6		<u>3</u> ₄
PLB	II											
10 cm SM	I	7	<u>5</u> ₆	<u>6</u> ₁				<u>4</u> ₅	<u>3</u> ₂	<u>1</u> ₄		<u>2</u> ₃
40 cm SM	I	<u>7</u> ₅	<u>6</u> ₇	<u>4</u> ₁				<u>5</u> ₆	3	<u>2</u> ₄		<u>1</u> ₂
80 cm SM	I											
160 cm SM	I	1	3	<u>4</u>				2	<u>5</u>			

5
 6 **Note:** Best column showed the model simulations (individual parameter substitution) with the
 7 smallest root mean squared error (RMSE) for 100 cm soil temperature (ST, °C), active layer
 8 depth (ALD, m), permafrost low boundary (PLB, m), 10, 40, 80 and 160 cm soil liquid water
 9 content (SM, -); Number indicated the combination of parameters (+) had smaller RMSE
 10 than the best model run using individual parameter substitution. All indicated the combination
 11 of all 4 parameters. The smallest number indicated the smallest RMSE.

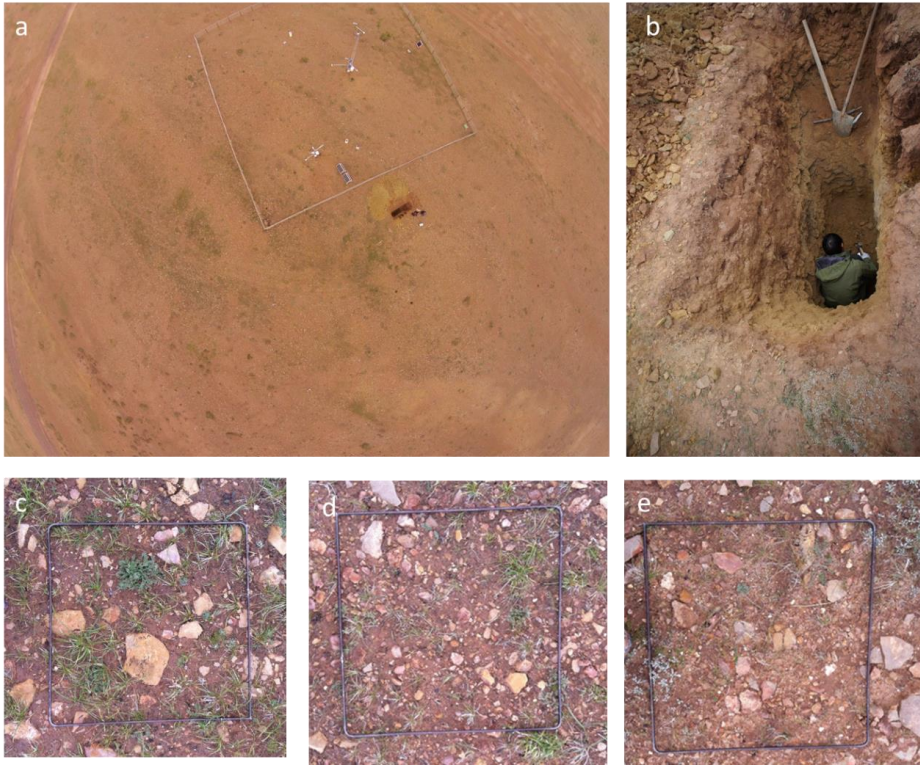
1 **Figure 1. a)** The location of Beiluhe permafrost station on the Qinghai-Tibetan Plateau
 2 (Permafrost type is from Li and Cheng, 1996); **b)** the [aerial view googlemap](#) of the
 3 [meteorological weather station](#) and [the excavated soil pit](#); and **c)** the detailed view of the
 4 [excavated soil pit](#) [the surrounding environment](#).



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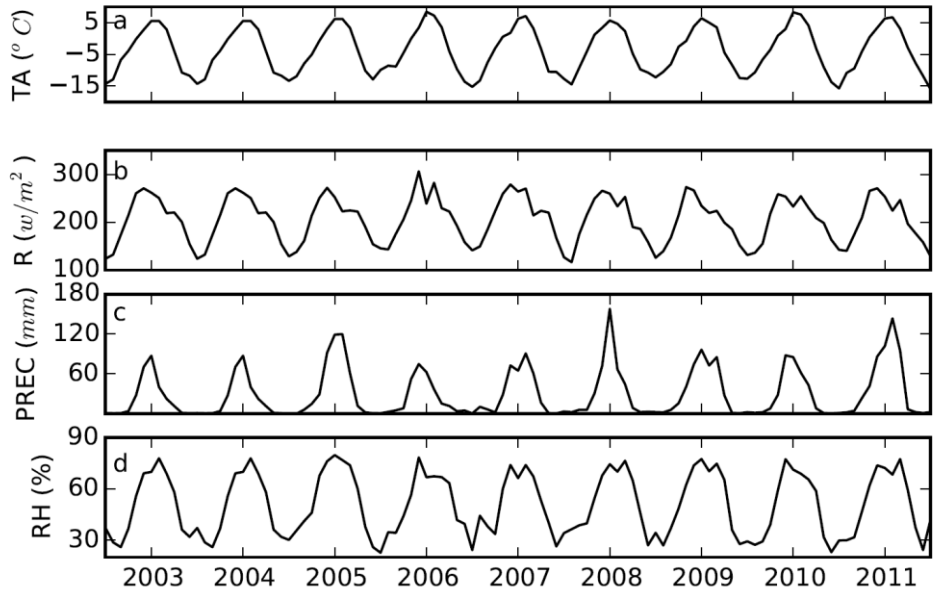
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6

1 Figure 2. a) the aerial view of the weather station and the excavated soil pit; the borehole is
2 located in the lower left corner of white fence; b) the detailed view of the excavated soil pit;
3 and c)-e) examples of vegetation, gravel and stones (iron frame is about 0.5 m×0.5 m).



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1 Figure 3. a) air temperature (TA, °C); b) downward solar radiation (R, w/m²); c) precipitation
2 (PREC, mm) and d) relative humidity (RH, %) measured on Beiluhe weather station on the
3 Qinghai-Tibet Plateau from 2003 to 2011.



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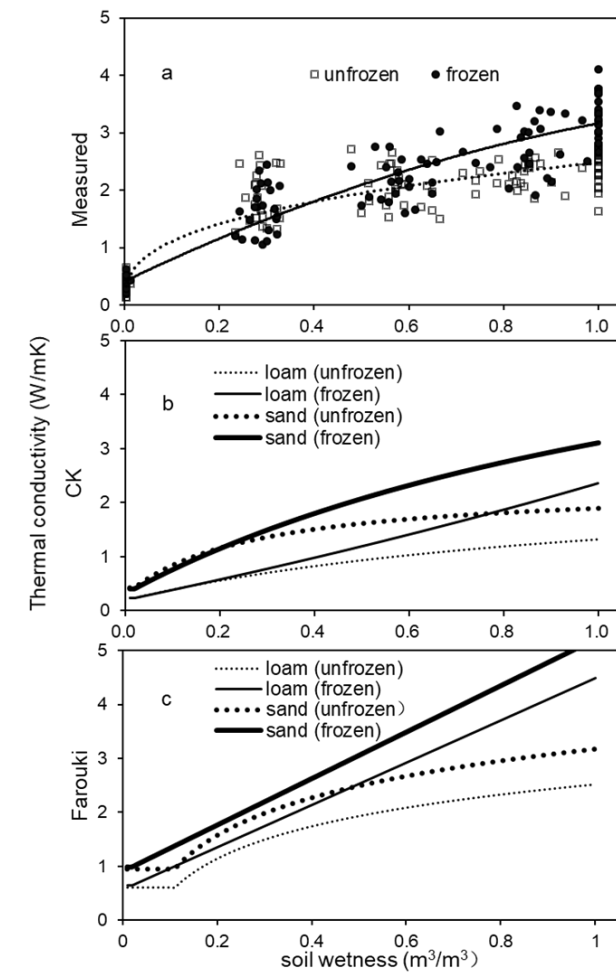
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1 **Figure 24.** The relationship between soil wetness (solid and dotted lines represent frozen and
 2 unfrozen cases) and soil thermal conductivity ($W/m^{\circ}CmK$) from **a)** measured values
 3 (Measured; dots and empty diamonds represent measured frozen and unfrozen soil thermal
 4 conductivities, respectively), **b)** using the C \acute{e} and Konard (2005) scheme (CK); and **c)** using
 5 the Farouki (1986) scheme (Farouki). Thick and thin lines represent relationships for sand and
 6 silty clayloam, respectively.



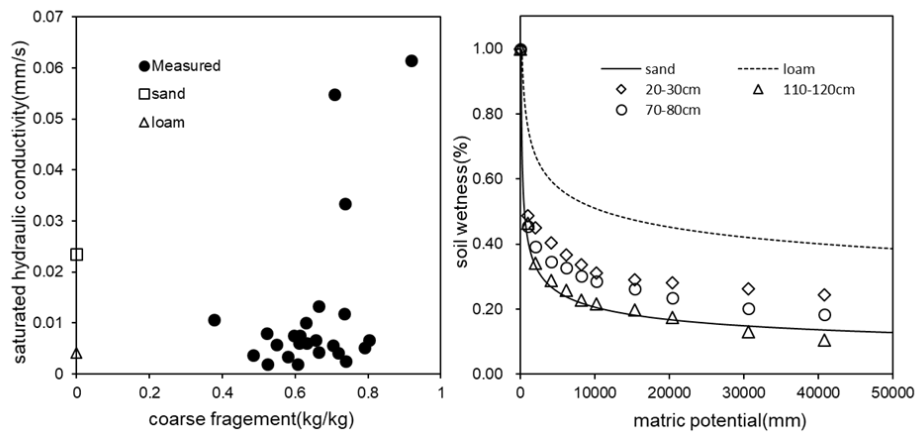
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1 **Figure 35. a)** the relationship between saturated hydraulic conductivity (mm s^{-1}) and **gravel**
 2 **content** **coarse fragment** fraction (Solid dots represent measured value; empty circle and
 3 empty triangle represent the corresponding values of sand and **silty clay loam** used in
 4 Community Land Model, respectively) ; **b)** the relationship between soil wetness (lines) and
 5 absolute value of matric potential ($\text{mm H}_2\text{O}$) at three representative depths. Solid and dashed
 6 lines represent default values of sand and **silty clay loam**, respectively (Oleson et al., 2010).



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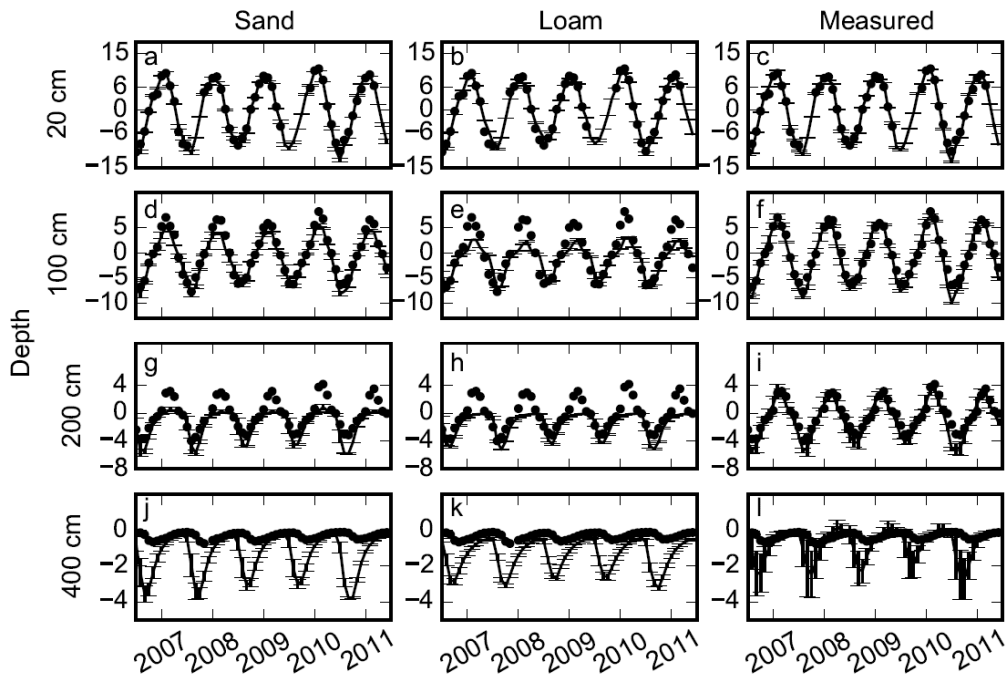
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1 **Figure-4_6.** Comparisons of soil temperatures simulated using default parameters of sand,
2 silty clay loam, and measured parameters (lines) with measured soil temperatures (dots) at 20,
3 100, 200 and 400 cm depths. Error bars showed the standard deviation calculated based on 9
4 simulations with 3 different slopes and 3 different soil thicknesses.

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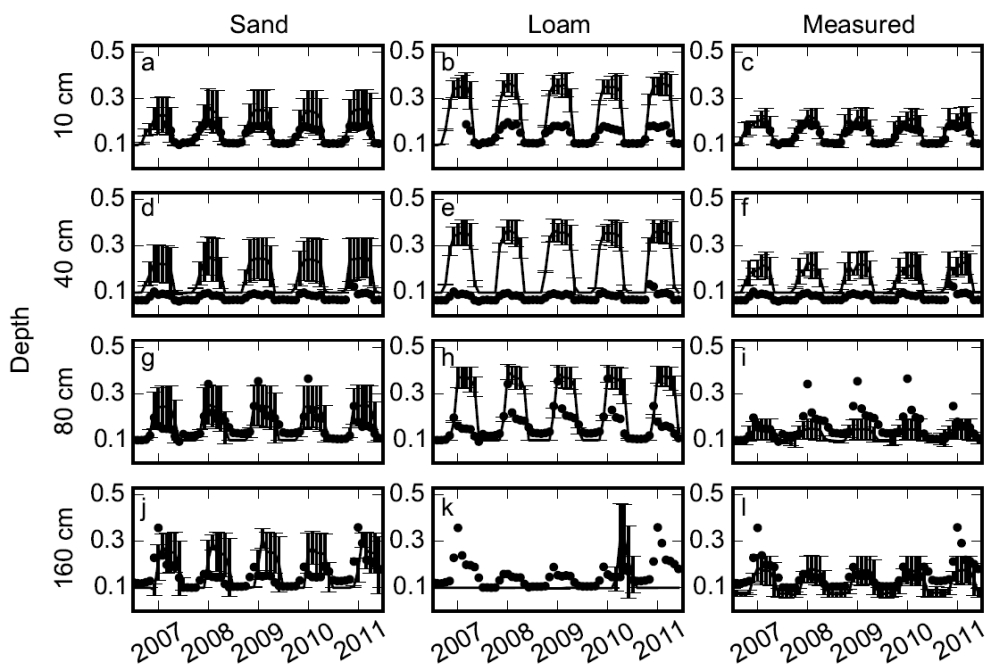
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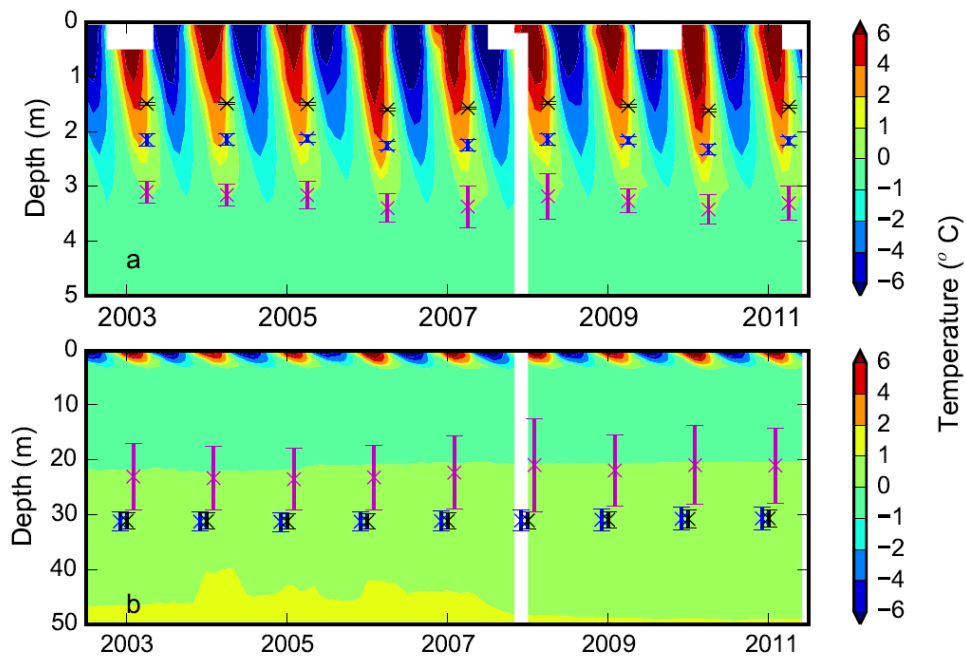
1 **Figure 57.** Comparisons of soil volumetric liquid water content simulated using default
2 parameters sand, default ~~silty clay loam~~, and measured parameters (lines) with measured soil
3 moistures (dots) at 10, 40, 80 and 160 cm depths. Error bars showed the standard deviation
4 calculated based on 9 simulations with 3 different slopes and 3 different soil thicknesses.



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1 | **Figure 68.** **a)** Contours of measured soil temperature ($^{\circ}\text{C}$) from borehole measurements down
2 | to 5 m and simulated active layer depth over the period of 2003-2011; and **b)** same as a) but
3 | down to 50 m and for simulated permafrost low boundary. Black, blue and magenta represent
4 | simulations with silty clay loam, sand and measured parameters, respectively. Error bars show
5 | the standard deviation calculated based on 9 simulations with 3 different slopes and 3
6 | different soil thicknesses.

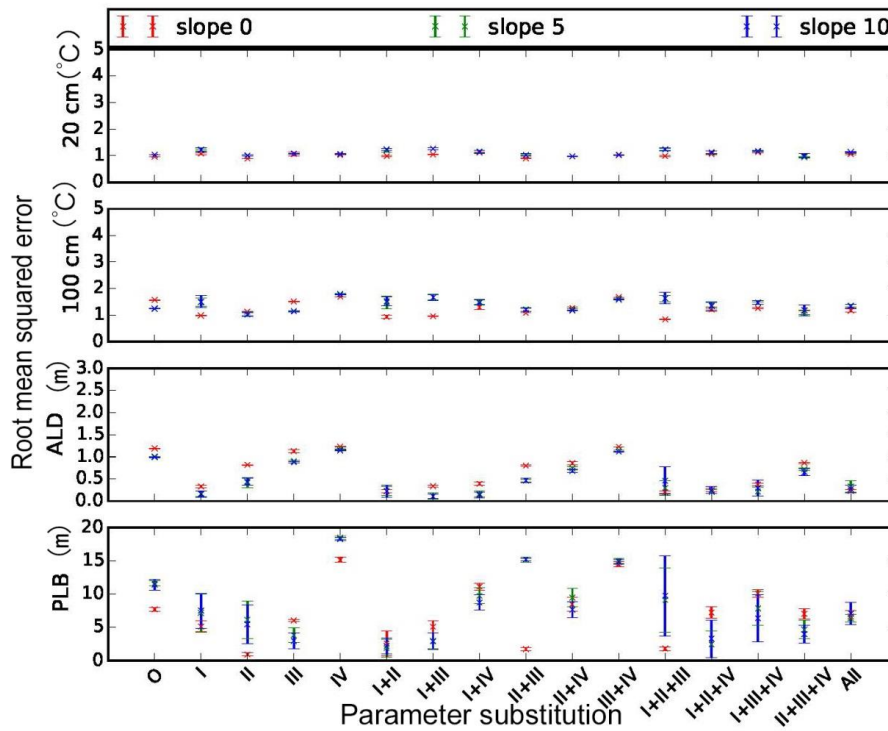


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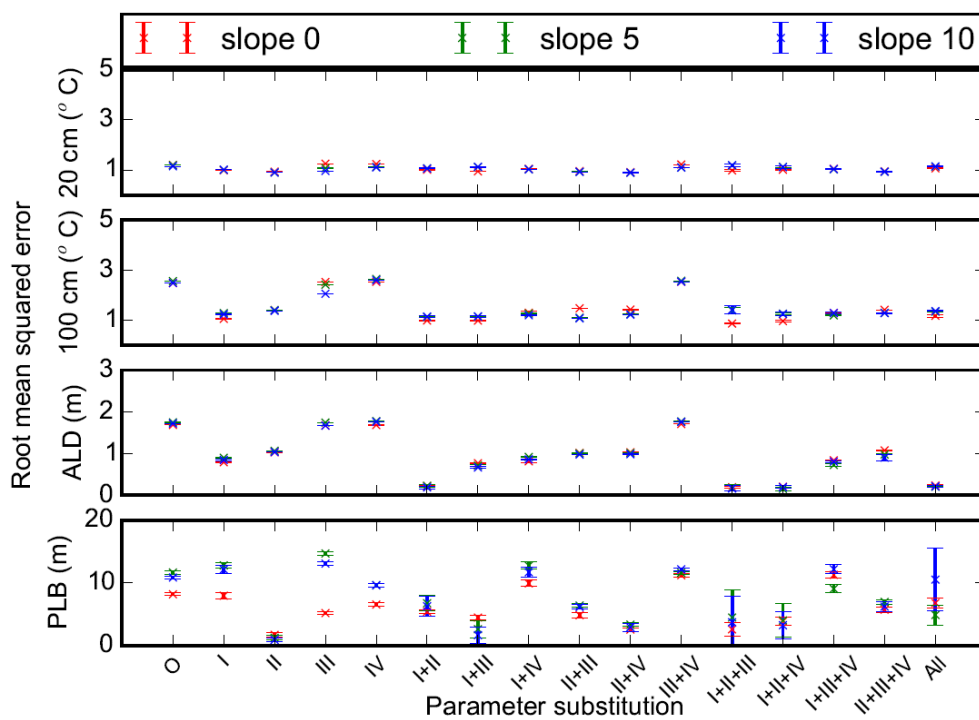
1 | **Figure 79.** Root mean squared errors between measurements and model simulations (with
 2 | different combinations of measured porosity (I), thermal conductivity (II), hydraulic
 3 | conductivity (III) and matric potential (IV) of default sand parameters) for a) 20 and b) 100
 4 | cm soil temperatures ($^{\circ}\text{C}$), c) active layer depth (ALD, m) and d) permafrost low boundary
 5 | (PLB, m). O and All represent model runs without substitution of default parameters and with
 6 | all 4 parameters substituted, respectively. Mean and standard deviation of model simulations
 7 | with 3 different soil thicknesses at each slope (slope 0: 0° ; slope 5: 5° ; slope 10: 10°) are
 8 | shown.

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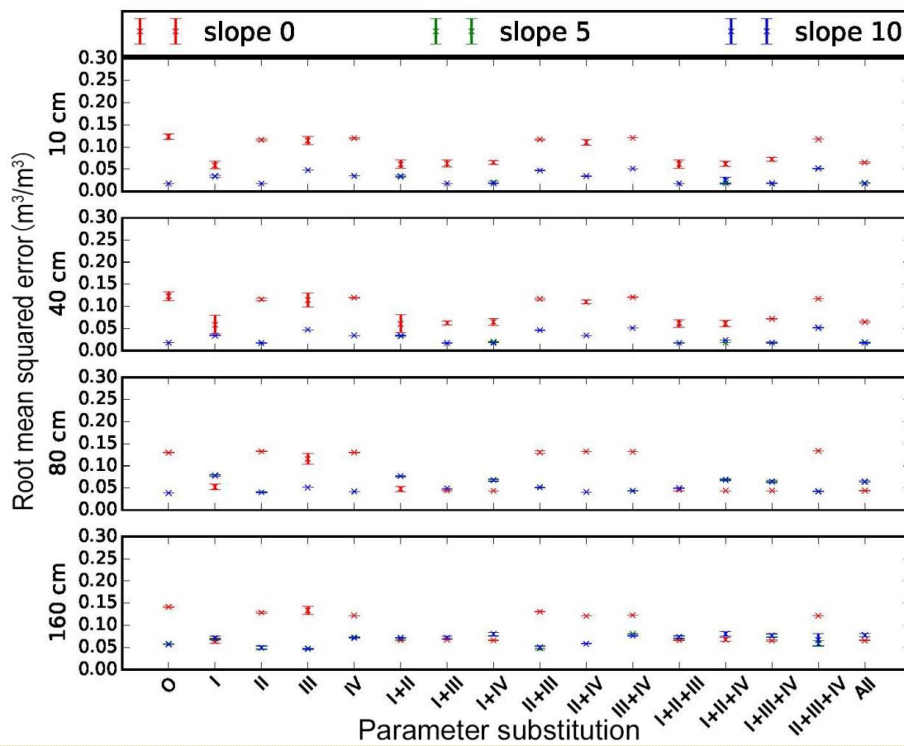
1 **Figure 810.** Root mean squared errors between measurements and model simulations (with
 2 different combinations of measured porosity (I), thermal conductivity (II), hydraulic
 3 conductivity (III) and matric potential (IV) of default loam parameters) for a) 20 and b) 100
 4 cm soil temperatures (°C), c) active layer depth (ALD, m) and d) permafrost low boundary
 5 (PLB, m). O and All represent model runs without substitution of default parameters and with
 6 all 4 parameters substituted, respectively. Mean and standard deviation of model simulations
 7 with 3 different soil thicknesses at each slope (slope 0: 0°; slope 5: 5°; slope 10: 10°) are
 8 shown. Same as Figure 7 but for default silty clay parameters.



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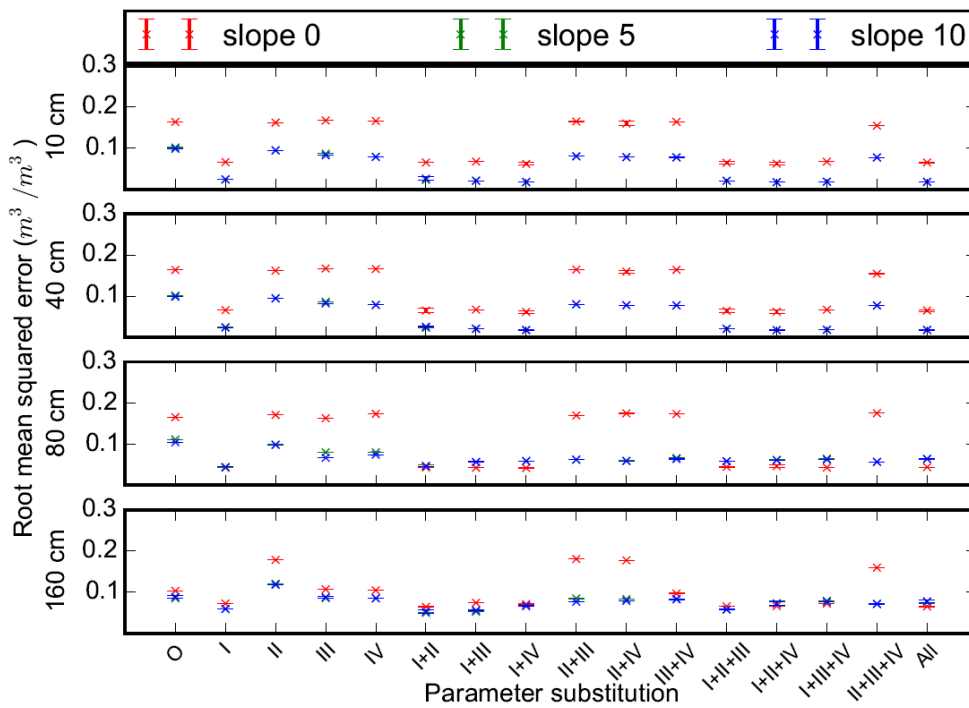
1 **Figure 911.** Root mean squared errors between measurements and model simulations (with
 2 different combinations of measured porosity (I), thermal conductivity (II), hydraulic
 3 conductivity (III) and matric potential (IV) of default sand parameters) for a) 10 cm, b) 40 cm,
 4 c) 80 cm and d) 160 cm soil volumetric liquid water content. O and All represent model runs
 5 without substitution of default parameters and with all 4 parameters substituted, respectively.
 6 Mean and standard deviation of model simulations with 3 different soil thicknesses at each
 7 slope (slope 0: 0°; slope 5: 5°; slope 10: 10°) are shown. Same as Figure 7 but for a) 10 cm, b)
 8 40 cm, c) 80 cm and d) 160 cm soil liquid water content.



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1 **Figure 1012.** Root mean squared errors between measurements and model simulations (with
 2 different combinations of measured porosity (I), thermal conductivity (II), hydraulic
 3 conductivity (III) and matric potential (IV) of default loam parameters) for a) 10 cm, b) 40 cm,
 4 c) 80 cm and d) 160 cm soil volumetric liquid water content. O and All represent model runs
 5 without substitution of default parameters and with all 4 parameters substituted, respectively.
 6 Mean and standard deviation of model simulations with 3 different soil thicknesses at each
 7 slope (slope 0: 0°; slope 5: 5°; slope 10: 10°) are shown. Same as Figure 9 but for default silty
 8 clay parameters.



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