

We are grateful to Drs. Keith Makinson and Hartmut Hellmer for their thorough and thoughtful reviews. This manuscript will be much improved by their input. We have made changes to our document and are including below an overview of these changes.

Referee comments are in **bold**, responses are in *italics*, and corrected grammar indicated by ~~strikethrough~~.

## Hartmut Hellmer

### Specific comments:

**L032 – How can a paper published in 2006 cover the period 2002-2016? Actually, according to Monaghan et al. (2006), which covers the period 1955-2004, small changes in SA only occurred on the EAIS.** *Thank you for pointing out this oversight. We have rewritten this text and provided an updated ref. (Wang et al., 2016).*

**L055 – With regard to the direct flow of CDW into the ice shelf cavities of ABS Jenkins et al. (2010) is a more appropriate reference.** *Corrected (L67). We have also added a cite to Jacobs et al. (2013), since Jenkins et al. (2010) only discusses measurements for Pine Island Glacier ice shelf, while Jacobs et al. (2013) demonstrates CDW flows into Getz (also ABS) as well.*

**L081 – More precise: Hellmer et al. (2017) not just reversed the atmospheric conditions to a colder state but to 20th -century conditions.** *We have augmented this section to include this clarification.*

**L164 - Equation (4) must read  $w_b = QT_0/L \times \rho_0$ .** *And, somewhere it should be mentioned that heat flux through the ice shelf is ignored. Thank you for catching this typo! We have added a statement regarding the heat flux through the ice to the paragraph preceding Eqn. (1), and stated that we have ignored it for this study (reasonable for thick ice).*

**L216 – It comes as a surprise that open ocean wct = h has a maximum value of 1914m, though the model domain (Fig. 1) only covers the southern Weddell Sea continental shelf.** *Thanks. The value is now corrected, to 1211 m in Filchner Trough.*

**L283 – It is not clear whether the 'bulk dye' was added to the whole water column or just to the surface-sigma layer. The confusion starts when looking at Fig. 8a, which looks more like a 'bottom dye' distribution.** *The dye is added uniformly to all levels. We have amended the text to state "The bulk dye was initialized at a concentration of 100% over the entire water column but was not replenished after these simulations began.". We have included a couple of figures here to demonstrate the vertical structure of the bulk dye initialization (Figure 1) as well as the dye distribution in the surface and bottom layers.*

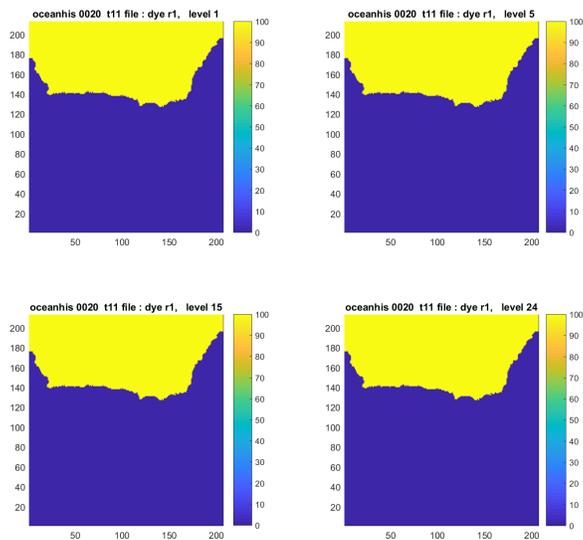


Figure 1 Dye concentration from 0-100% in sigma levels 1 (bottom), 5, 15, and 24 (surface)

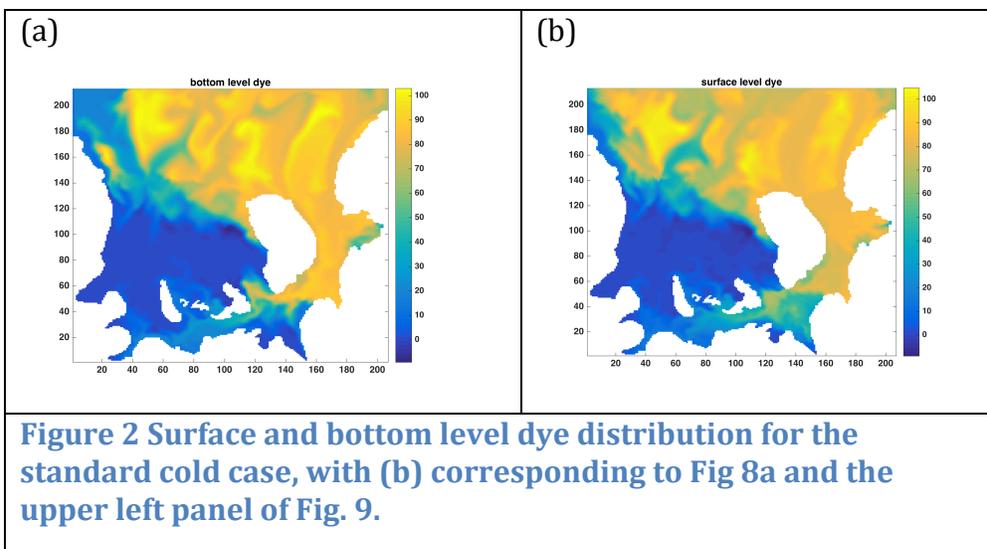


Figure 2 Surface and bottom level dye distribution for the standard cold case, with (b) corresponding to Fig 8a and the upper left panel of Fig. 9.

**L305 – It is not clear what is meant with 'outer/interior grounding line' – please explain.** *The labeling has been corrected using geographical referencing ("eastern", "southeastern", etc). We hope this helps to clarify the intended meaning.*

**L335 – Here, a serious deficit of the model becomes obvious, since the refreezing along the eastern coast of Berkner Island (e.g., Rignot et al. (2013)) is missing, certainly because the model exaggerates the flow into the Filchner cavity. We have clarified in the text how our lack of density gradient along the continental shelf yields a circulation bias with clockwise flow around Berkner Is., rather than the observed counterclockwise flow that is represented by models that include horizontal density gradients across the front.**

**L396 – A reduction of area-averaged melt rates due to adding tides also happens for Support Force.** *Support Force is now included in this statement.*

**L426 – The comparison with Hellmer et al. (2012) is risky because this kind of circulation only happens for the 'warm phase', while here the same circulation pattern exists for the 'standard cold case'. Such comparison might provoke a critical reader to question ROMS' performance in general.** *The intention of this phrasing was to highlight that in both these results and in the Hellmer et al. (2012) results the circulation within the FRIS cavity is clockwise, such that the primary ocean inflow is through FIS; but(!), we have decided to take a different approach in describing this circulation. The Discussion section now includes an overview of how our standard cold results are to be interpreted in the context of known present-day circulation. This addition also aims to address a comment by Keith Makinson.*

Our results show that tide forcing is important to FRIS ice-ocean interactions over a range of initial temperatures and with large variations in regional impacts. The aim of these simulations was to apply, uniformly, temperatures and salinities that approximate (1) present-day, inflow conditions and (2) a representative temperature of future, inflow conditions, reflecting a modest increase in temperature; however, the circulation within this particular ice shelf cavity is strongly affected by sea-ice formation on top of a general circulation that establish an east to west density gradient across the continental shelf (e.g. Foldvik et al., 1985; Nicholls et al., 2009). As such, our “present-day” scenario is a hypothetical one that forms the basis of this sensitivity study but that should not be interpreted to reflect the known circulation within the cavity. The known circulation within the cavity, setup by the east to west density gradient on the continental shelf, has inflow in the Ronne Depression and a counter clockwise circulation around Berkner Is. (Foldvik et al. 2001). Our simulations for both the present-day and melt-adjusted cases predict inflow through the FIS and a clockwise circulation around Berkner Is. This pattern of circulation reflects the future warming scenario presented in Hellmer et al. (2012). This sensitivity study, therefore, does not include changes that would occur from a shift in cavity circulation from a scenario that has the east to west density gradient along the continental shelf to one where that density gradient is relaxed to the degree that the sub-ice-shelf cavity circulation would change. Although these simplifications restrict the predictive capacity of this study, they do not much affect the results of our sensitivity analysis on ice-ocean interactions within FRIS and in particular the feedbacks found between tides and changing geometry and implications for further research.

**L714 – By summarizing important results I miss (5): The increase of refreezing in central RIS in the 'standard cold case', representing today's conditions. This is an important finding because refreezing in this area certainly changes the dynamics of the ice shelf by increasing the buttressing around Henry and Korff.** *This result has already been reported in Makinson et al. (2011) for present-day ocean conditions; we therefore added the contribution of our work, with appropriate attribution to Keith Makinson for his, We clarified our results in the context of previous work by introducing a new Discussion section that focuses on basal freezing beneath FRIS (Sect. 4.5)*

#### 4.5 Implications of regional freeze conditions on ice sheet mass balance

As described in **Sect. 3.2.1** and **Sect. 3.2.2**, refreezing occurs in our simulations throughout a large region of the central RIS. Refreezing in this region is qualitatively consistent with estimates of basal mass balance from satellite-based remote sensing (e.g., Joughin and Padman, 2003; Rignot et al., 2013; Moholdt et al., 2014). Persistent refreezing along ice flowlines can create a marine ice layer up to hundreds of meters thick, as observed in ice cores (Engelhardt and Determann, 1987; Oerter et al., 1992), and in radio-echo sounding and seismic measurements (Joughin and Vaughan, 2004; Lambrecht et al., 2007). These observations are important in the context of other studies which show that marine ice accretion supports ice shelf stability (Kulesa et al., 2014; McGrath et al., 2014; Li et al. (submitted)). Our standard cold tide-forced case produces local maxima in marine ice growth rates in the northwestern RIS, the region northeast and east of Korff Ice Rise, and the region to the north and west of Henry Ice Rise (**Fig. 5d**). The spatial pattern of these freeze conditions differs from observed patterns (Joughin and Padman, 2003; Rignot et al., 2013; Moholdt et al., 2014). We attribute this difference to the consequences of omitting the east to west density gradient along the continental shelf.

The regions of freezing are broadly consistent in all our model runs (**Fig. 5**) and the net mass increase in refreezing regions are increased when tide forcing is added (**Fig. 6**). Our standard cold tide-forced case has a ~4-fold mass gain compared to the standard cold no-tides case; this result is consistent with Makinson et al. (2011). In both warm cases, standard and modified geometry, adding tides increases net marine ice formation by a factor of two. That is, tides will continue to be important for marine ice accretion beneath FRIS if ocean temperatures rise as predicted by Hellmer et al. (2012, 2017) and will, therefore, continue to play a role in FRIS ice shelf stability.

*We also included the following statement as (3) in our list of conclusions:*

(3) Adding tide forcing increases the overall freezing conditions for all three cases including the two warm cases. Since freeze conditions lead to marine ice accretion, and marine ice strengthens the ice shelf, the tidal contribution to ice-shelf dynamics is expected to continue through future ocean warming, increasing grounding and associated contact stresses in the region near the Henry and Korff ice rises and Doake Ice Rumples

**L1044** – Please explain the difference between 'region' and 'inlet', used in **Fig. 8**. We have corrected the use of "inlet" as shorthand for "inlet region" by changing "inlet" to "region", while also changing the parenthetical statement "(see Fig. 4 for dye release regions)" in order to make this phrasing consistent.

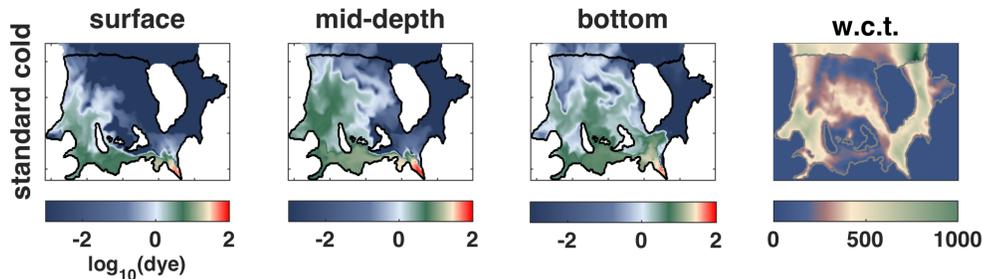
**L1061** – Please explain why Foundation shows a high dye concentration at the bottom. The signal cannot be advected from Support Force because there it does not exist, and highest

**melting beneath Foundation should stabilize the water column such that most, if not all, of the dye should concentrate at the base.** *We puzzled over this for a while. Based on the following figure (Fig. 3, below), and other analyses of  $T(z)$ ,  $S(z)$ , and FIS dye profiles, we conclude that FIS dye is present at depth in the S. Channel due to the combined influence of mixing within the Möller inlet region as well as a shoaling of bathymetry in both Möller and South Channel. FIS dye appears to circulate first into the Möller inlet region where additional freshwater is added to the “upper” branch of FIS-doped water and where mixing processes transport dye to depths that correspond to bottom level depths within the South Channel. Within South Channel, all water contains meltwater from different sources, including locally. The density stratification depends on the sum of freshwater from all sources, whereas a specific dye (e.g., FIS), depends only on meltwater from that region.*

*In order to clarify this influence, we have augmented section 4.3, to include the following statement:*

The presence of Foundation dye in the bottom level of the S. Channel transect reflects a shoaling of bathymetry (**Fig. 2c**) and mixing with the Möller region that allows the dye to be distributed to the bottom level within the Möller inlet region and then advected, at depth, through South Channel.

The evidence for this statement can be seen in Figure 3, below. Foundation dye is shown in the bottom, mid-depth and surface levels of the standard cold case. We attribute the circulation at this depth to be driven by changes in bathymetry, as shown in Fig. 2 of the main manuscript and here by w.c.t.



**Figure 3: Maps of Foundation dye taken at the bottom level (N=1), a mid-depth level (N=15) and the surface level (N = 24) for the standard cold cases with water column thickness on right (as a duplicate of Fig. 2c, in main manuscript).**

#### Technical corrections:

~~L031 – The dominant terms in the Antarctic ICE SHEET (AIS) mass budget...~~

~~L060 – We focus here ON...~~

~~L267 – ... over the LAST 30 days?~~

~~L298 – ... ice shelf frontal zone (ISFZ) of the RIS (here, front is redundant)~~

~~L337 – ...northWESTERN RIS.~~

~~L466 – ... from all upstream sources.~~

**L510 – Fig. 10e**

**L 833 – Hellmer, H. H.**

**L1000 – ~~.. the extent of the ice shelf...~~**

**L1017 – Locations of the six meltwater dye RELEASES.** *We have included this change together with an emphasis on “model dye”, which isn’t really “released” per se, though we agree with this choice in verb.*

## Keith Makinson

### Suggested minor revisions:

~~L39 remove 'the'~~

~~L58 change to 'over the observational record.'~~

~~L60 change 'the' to 'on'~~

~~L69 remove both 'the'~~

~~L71 Modified Warm Deep Water (MWDW)?~~

~~L73 MWDW also seen at Ronne Ice Front (Mooring R2 and CTD's Foldvik et al 2001 doi:10.1029/2000JC000217)~~

~~L90 change to 'pattern and magnitude of'~~

**L118 Are these temperatures and salinities restored throughout the model runs?** *Yes. We have augmented the text to explain: "Model hydrography is restored to these initial temperatures and salinity along the boundaries using a mixed radiation and nudging condition (Marchesiello et al., 2001) over a 20-day period."*

**L122 It would be worth mentioning the lack of an east to west density gradient and hence the reverse circulation in the cavity.** *We agree with the need to highlight this limitation in our model setup but feel that this information is best contained in the discussion section rather than the methodology section. We now use this information to introduce the discussion section and establish how our results can be interpreted in the context of other studies. The paragraph in question in our methodology section now reads:*

Our simulations were initialized with a homogeneous, stationary ocean that has a potential temperature of either  $\theta_{init} = -1.9^{\circ}\text{C}$  ("cold case") or  $\theta_{init} = -1.4^{\circ}\text{C}$  ("warm case"). Initial salinity is defined as  $S_{init} = 34.65$  for all cases. Model hydrography is restored to these initial temperatures and salinity at the boundaries using a mixed radiation and nudging condition (Marchesiello et al., 2001) over a 20-day period. The standard geometry cold case incorporates a uniform temperature and salinity that approximates conditions of the primary water mass entering the ice shelf cavity (Foldvik et al., 2001; Nicholls et al., 2001, 2009). The consequences to FRIS cavity circulation in choosing a uniform  $\theta_{init}$  and  $S_{init}$  are discussed in **Sect. 4**. The warm case represents a moderate ocean warming scenario with an increase of  $0.5^{\circ}\text{C}$  in the temperature of water being advected into the FRIS cavity. This change is much smaller than the  $2^{\circ}\text{C}$  temperature increase in the inflowing water by the end of this century predicted by Hellmer et al. (2012), but was chosen to investigate whether initial feedbacks due to melt-induced changes in cavity shape from initial warming might be positive or negative. Our idealized simulations do not include wind forcing, frazil ice, or sea-ice formation.

*The intro to the discussion section (Sect. 4) goes into more details as follows.*

Our results show that tide forcing is important to FRIS ice-ocean interactions over a range of initial temperatures and with large variations in regional impacts. The aim of these simulations was to apply temperatures and salinities that approximate (1) present-day inflow conditions and (2) a representative temperature of future inflow conditions, reflecting a modest increase in temperature. The choice of spatially constant initial temperature ( $\theta_{\text{init}}$ ) and salinity ( $S_{\text{init}}$ ) does, however, influence circulation into and under the FRIS cavity. In the real ocean, spatial structure of the wind stress and production of dense HSSW by sea ice formation over Ronne Depression establishes an east-west density gradient across the continental shelf (e.g. Foldvik et al., 1985; Nicholls et al., 2009) that leads to stronger flows into the cavity across the RIS front than our model generates. Our “present-day” scenario should, therefore, be regarded as the basis of this sensitivity study rather than a prediction of known circulation within the cavity. In particular, our standard cold case misses the inflow in the Ronne Depression and a counter-clockwise circulation around Berkner Island (Foldvik et al. 2001). In contrast, our simulations for both the present-day and melt-adjusted cases predict the primary inflow through the FIS and a clockwise circulation around Berkner Island; this pattern of circulation is, however, consistent with the future warming scenario presented in Hellmer et al. (2012). The fundamental conclusions of our sensitivity analysis of ice-ocean interactions within FRIS are, however, independent of these differences from the real-world modern circulation.

**L195-196 it would be useful to define what these numbers (Haney number and Beckmann and Haidvogel number), are if you are going to mention them.**

*The paragraph in question now includes the following description:*

The ice draft and bathymetry were each smoothed to minimize errors in the baroclinic pressure gradient that arises with the terrain-following coordinate system used in ROMS (Beckmann and Haidvogel, 1993; Haney, 1991). The two parameters used to quantify smoothing are the Beckmann and Haidvogel number,  $rx0 = |h(e) - h(e')| / (h(e) + h(e'))$  (Beckmann and Haidvogel, 1993), and the Haney number,  $rx1 = |h(e, k) - h(e', k) + h(e, k-1) - h(e', k-1)| / (h(e, k) + h(e', k) - h(e, k-1) - h(e', k-1))$  (Haney, 1991), where  $1 \leq k \leq N$  and  $e$  and  $e'$  represent two adjacent cells. Together, these parameters establish that the surface (ice) and bottom bathymetry slopes are sufficiently small to reduce or eliminate spurious flows due to a horizontal pressure gradient and ensures hydrostatic consistency throughout the water column at adjacent horizontal grid nodes. Our Beckman and Haidvogel number,  $rx0$ , is less than 0.045 along both surface and bottom topographies, and our Haney number,  $rx1$ , is less than 10 in both surface and bottom levels except for some areas along the ice shelf front, where  $rx1$  is larger and reaches a maximum value of 17.

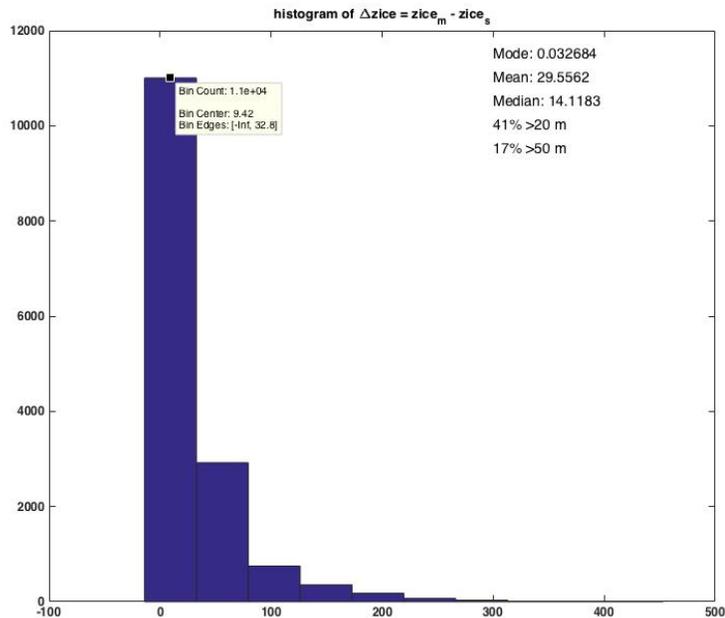
**L203 extreme stratification profile - a little more explanation maybe?** *The sentence now reads: “We initialized these models with horizontally uniform temperature and salinity fields taken from a standard warm case profile, in the vicinity north of Bjerkner Island, where the*

strongest stratification of all runs is represented.”

**L212** Mention that this is a known problem/limitation with this type of model. *We have included this information.*

**L216-1914 m. correct?**

**L233 .03 is this correct? Remove ‘below’.** *Yes. 0.03 is correct for the mode, but we agree that this number is a questionable asset to the discussion. We have changed the text to include information on the median: “...and a median of 14 m”. A graphic of the distribution is included below.*



**L234** remove ‘above freezing’

**L236** consider removing ‘Given...bathymetry.’

**L239-40** consider changing to ‘conditions and ran with and without...’

**L243** change to ‘tide-resolving with at temporal resolution of 2 hours and’

**L270** change ‘over’ to ‘after’

**L286** section label needed. *Indeed! We have corrected this and other Section label errors.*

**L298** change to ‘maximum tidal currents along’

**Para L327-330** consider adding a value or percentage for the ‘increased melt rates’ and ‘slightly modifies’. *We have modified the text to read:*

The pattern of  $w_b$  for the standard warm no-tides case (**Fig. 5b**) is generally similar to the standard cold no-tides case (**Fig. 5a**) but with a 3.5 fold increase in the shelf-averaged value. Changing cavity shape while imposing the same initial ocean

temperature in the modified warm case (**Fig. 5c**) only slightly reduces melt rates (by 10%) for the no-tides scenario (cf. **Fig. 5b and 5c**).

~~L336 it should be noted that there is very limited freezing north of Henry ice rise. L415 'southern' rather than 'innermost'~~

~~L441 'these' to 'the'~~

~~L466 sources~~

~~L510 Fig. 10e~~

~~L543 'is' to 'are'~~

~~L706 Ronne Ice Front~~

~~L759 Any bathymetry data from beneath ice shelves is useful as it will help better define the cavity geometry which you have demonstrated to be important for the whole system (tides and circulation).~~

~~Fig 1. Add W and S labels for lon and lat.~~

~~L1010 remove 'than the standard geometry'~~

~~L1012 change to 'barotropic tidal transport'~~

~~L1017 change to 'continuous dye release'~~

~~Fig8 and 9. Mention in caption that this is after 2 years.~~

**Fig12. Holland et al 2008 show similar melt figures over an extended range.**

**doi:10.1175/2007jcli1909.1** *This is an important paper to cite here, and we have done so as follows: "In general, our values are in range of those shown in Holland et al. (2008), (c.f. their Fig. 1 and our Fig. 12b),...."*

**Also Holland et al 2007 doi:10.1029/2006JC003915 show similar results to your dye tracer experiments.** *We have included a reference to this important paper in the first paragraph of section 2.11: "Our model excludes the influences of wind-driven circulation and sea-ice formation. As such, it is perhaps no surprise that these dye distributions are qualitatively similar to those shown by Holland et al. (2007)."*

1 **Tidal influences on a future evolution of the Filchner-Ronne**  
2 **Ice Shelf cavity in the Weddell Sea, Antarctica**

3 Rachael D. Mueller<sup>1</sup>, Tore Hattermann<sup>2,3</sup>, Susan L. Howard<sup>4</sup>, Laurence Padman<sup>5</sup>,

4 <sup>1</sup>Earth & Space Research, Bellingham, WA 98225, USA

5 <sup>2</sup>Akvaplan-niva, Tromsø, 9296, Norway

6 <sup>3</sup>Alfred Wegener Institute, Helmholtz Centre for Polar and Marine Research, 27570  
7 Bremerhaven, Germany

8 <sup>4</sup>Earth & Space Research, Seattle, WA 98121, USA

9 <sup>5</sup>Earth & Space Research, Corvallis, OR 97333, USA

10 *Correspondence to:* Rachael D. Mueller (mueller@esr.org)

11 **Abstract.** Recent modeling studies of ocean circulation in the southern Weddell Sea,  
12 Antarctica, project an increase over this century of ocean heat into the cavity beneath  
13 Filchner-Ronne Ice Shelf (FRIS). This increase in ocean heat would lead to more basal  
14 melting and a modification of the FRIS ice draft. The corresponding change in cavity shape  
15 will affect advective pathways and the spatial distribution of tidal currents, which play  
16 important roles in basal melting under FRIS. These feedbacks between heat flux, basal  
17 melting, and tides will affect the evolution of FRIS under the influence of a changing  
18 climate. We explore these feedbacks with a three-dimensional ocean model of the southern  
19 Weddell Sea that is forced by thermodynamic exchange beneath the ice shelf and tides along  
20 the open boundaries. Our results show regionally-dependent feedbacks that, in some areas,  
21 substantially modify the melt rates near the grounding lines of buttressed ice streams that  
22 flow into FRIS. These feedbacks are introduced by variations in meltwater production as  
23 well as the circulation of this meltwater within the FRIS cavity; they are influenced locally

24 by sensitivity of tidal currents to water column thickness and non-locally by changes in  
25 circulation pathways that transport an integrated history of mixing and meltwater  
26 entrainment along flow paths. Our results highlight the importance of including explicit tidal  
27 forcing in models of future mass loss from FRIS and from the adjacent grounded ice sheet as  
28 individual ice stream grounding zones experience different responses to warming of the  
29 ocean inflow.

## 30 **1 Introduction**

31 The dominant terms in the mass balance of the grounded portion of the Antarctic Ice Sheet  
32 are gains from snowfall and losses by gravity-driven flow of ice into the ocean. Around the  
33 ocean margins, the ice sheet thins sufficiently to float, forming ice shelves. Continuous  
34 gravity measurements from the GRACE satellite during 2002–2015 (Harig and Simons,  
35 2015; Groh and Horwath, 2016) show that grounded-ice mass decreased during this period.  
36 This loss, which is a significant contribution to current rates of global sea level rise (e.g.  
37 Shepherd et al., 2012), is attributed to recent acceleration of ice loss (e.g. Harig and Simons,  
38 2015), with little to no change in snowfall (Monaghan et al., 2006; Wang et al., 2016).

39 Most of this net mass loss is occurring in the Amundsen Sea sector (Sutterley et al.,  
40 2014), predominantly in glaciers flowing into Pine Island Bay (Mouginot et al., 2014;  
41 Khazendar et al., 2016), and is observed as glacier acceleration, ice-sheet thinning, and  
42 grounding-line retreat. Losses in this sector are correlated with observed thinning of the ice  
43 shelves (Pritchard et al., 2009, 2012), consistent with a reduction in back-stress  
44 (“buttressing”) that impedes the seaward flow of the grounded ice (e.g., Scambos et al.,  
45 2004; Dupont and Alley, 2005; Rignot et al., 2014; Joughin et al., 2014). These studies  
46 demonstrate a need for improving predictions of how the extent and thickness of ice shelves  
47 will evolve as climate changes.

48 | The mass budget for an ice shelf is the sum of mass gains from snow accumulation  
49 | and advection of ice across the grounding line, and mass losses from iceberg calving, basal  
50 | melting, surface runoff, and sublimation. Calving and melting each contribute roughly half  
51 | of the total Antarctic Ice Sheet mass loss (Rignot et al., 2013; Depoorter et al., 2013),  
52 | although this ratio varies substantially between ice shelves in different sectors. Surface  
53 | runoff and sublimation are insignificant for most Antarctic ice shelves. The ice shelves that  
54 | are currently experiencing the most rapid thinning are in the Amundsen and Bellingshausen  
55 | seas where relatively warm Circumpolar Deep Water (CDW) has direct access into the ice  
56 | shelf cavities (Jenkins and Jacobs, 2008; Padman et al., 2012; Jenkins et al., 2010b; Jacobs  
57 | et al., 2013; Schmidtko et al., 2014). The large ice shelves in other sectors that are not  
58 | directly influenced by CDW inflows are closer to steady state, suggesting that the transport  
59 | of ocean heat under these ice shelves has not changed significantly over the observational  
60 | record.

61 | We focus here on Filchner-Ronne Ice Shelf (FRIS) in the southern Weddell Sea  
62 | (**Fig. 1**). The FRIS is a large ice shelf (~430,000 km<sup>2</sup>) that accounts for 30% of the total area  
63 | of Antarctic ice shelves; however, it currently contributes only 10% of the total ice shelf  
64 | mass loss. For comparison, Pine Island Glacier accounts for 0.4% of total area of Antarctic  
65 | ice shelves but contributes 7% of total ice shelf mass loss (Rignot et al., 2013). The  
66 | disproportionately small melt contribution from FRIS may change, however, in the coming  
67 | century. Models suggest a large and persistent increase in ocean temperatures beneath FRIS  
68 | in response to atmospheric changes in a warmer, future climate (Hellmer et al., 2012;  
69 | Timmermann and Hellmer, 2013), ~~and these conditions persisted even when atmospheric~~  
70 | ~~conditions were reversed to those of the 20<sup>th</sup> century (Hellmer et al., 2017).~~ In the modern  
71 | state, most of the water entering the ocean cavity under Filchner Ice Shelf (FIS) and Ronne  
72 | Ice Shelf (RIS) is derived from High Salinity Shelf Water with a temperature close to the  
73 | surface freezing point of -1.9°C (Nicholls et al., 2009). Traces of Modified Warm Deep

74 | Water (MWDW) with temperature up to about -1.4°C are found in Filchner Trough near the  
75 | FIS ice front (Darelius et al., 2016) and at the RIS front (Foldvik et al., 2001); however,  
76 | MWDW does not appear to be a major heat source for melting beneath the ice shelf. In the  
77 | warming scenarios of Hellmer et al. (2012), however, almost the entire FRIS cavity is  
78 | flooded by WDW with above-zero temperatures by the end of the 21<sup>st</sup> century, leading  
79 | to basal melt rates an order of magnitude higher than present. In this warm state, the  
80 | associated rapid thinning of the ice shelf would reduce the buttressing of the large marine-  
81 | based grounded ice sheet surrounding FRIS (Ross et al., 2012), significantly accelerating  
82 | future sea level rise (Mengel et al., 2016). Furthermore, simulations by Hellmer et al. (2017)  
83 | show that the increased meltwater production will sustain the warm inflow even if  
84 | atmospheric conditions were reversed to a colder state, suggesting the existence of an  
85 | irreversible tipping point once melting increases past a certain threshold.

86 | These estimates of increased melt, however, assume that cavity geometry does not  
87 | change in a way that alters the access of ocean heat to the FRIS base. Studies of Larsen C  
88 | Ice Shelf (Mueller et al., 2012) and Pine Island Glacier ice shelf (Schodlok et al., 2012)  
89 | showed that changes to the ice shelf cavity shape can significantly alter the spatial pattern of  
90 | basal melt rate, particularly in regions where tidal currents contribute substantially to the  
91 | total turbulent kinetic energy near the ice base. Tides were not explicitly included in the  
92 | forcing for the Hellmer et al. (2012) study. However, tidal currents often play a critical role  
93 | in setting the pattern and magnitude of basal melt rates under cold water ice shelves  
94 | (MacAyeal, 1984; Padman et al., in press) including FRIS (Makinson et al., 2011), which  
95 | leads us to hypothesize that tides would influence changes in meltwater production from a  
96 | warming ocean.

97 | We explore this hypothesis using a suite of numerical model simulations that  
98 | incorporate variations in tide forcing, initial temperature, and cavity geometry together with  
99 | thermohaline interactions at the interface between the ocean and ice shelf. We then use these

100 models to describe how feedbacks between ice shelf thinning and predicted tidal currents in  
101 the ice shelf cavity influence the evolution of a tide-dominated ice shelf environment under  
102 the condition of increased influx of ocean heat. Lastly, we consider the role of tides on basal  
103 mass loss near the grounding lines of each of the major ice streams supplying ice to FRIS, as  
104 a guide to how individual ice stream grounding zones might respond to the projected  
105 increase in ocean heat flux to the FRIS cavity.

## 106 **2 Methods**

### 107 **2.1 Model overview and thermodynamic parameterization**

108 Our simulations were carried out with a version of the Regional Ocean Modeling System  
109 (ROMS 3.6; Shchepetkin and McWilliams, 2009) that has been modified to include  
110 pressure, friction, and surface fluxes of heat and salt imposed at the base of the ice shelf  
111 (Dinniman et al., 2007, 2011; McPhee et al., 2008; Mueller et al., 2012). ROMS is a  
112 hydrostatic, 3D primitive equation model with a terrain-following ( $\sigma$ -level) coordinate  
113 system and Arakawa-C staggered grid. Our model domain (**Fig. 1**) covers a portion of the  
114 southern Weddell Sea, Antarctica including FRIS. The grid spacing is 5 km with  $N = 24$   
115 vertical levels. A full description of model parameter choices and processing options is  
116 given in a supplementary document.

117 Two model geometries were used in our set of simulations, one representing the modern  
118 state (standard geometry) and the other representing a possible future state (modified  
119 geometry). Model geometry consists of a land mask (including grounded ice sheet), seabed  
120 bathymetry ( $h$ ), and ice draft ( $z_{ice}$ ). These grids are described in **Sect. 2.2**.

121 Our simulations were initialized with a homogeneous, stationary ocean that has a  
122 potential temperature of either  $\theta_{init} = -1.9^{\circ}\text{C}$  (“cold case”) or  $\theta_{init} = -1.4^{\circ}\text{C}$  (“warm case”).  
123 Initial salinity was set as  $S_{init} = 34.65$  for all cases. Model hydrography was restored to  $\theta_{init}$

124 and  $S_{init}$  at the boundaries using a mixed radiation and nudging condition (Marchesiello *et*  
 125 *al.*, 2001) with a 20-day time scale. Values of  $\theta_{init}$  and  $S_{init}$  for the standard geometry cold  
 126 case were chosen to approximate the primary water mass entering the ice shelf cavity at  
 127 present (Foldvik *et al.*, 2001; Nicholls *et al.*, 2001, 2009). The consequences to FRIS cavity  
 128 circulation in choosing a uniform  $\theta_{init}$  and  $S_{init}$  are discussed in **Sect. 4**. The warm case  
 129 represents a moderate ocean warming scenario with an increase of 0.5°C in the temperature  
 130 of water entering the FRIS cavity. This change is much smaller than the 2°C temperature  
 131 increase in the inflowing water by the end of this century predicted by Hellmer *et al.* (2012),  
 132 but was chosen to investigate whether initial feedbacks due to melt-induced changes in  
 133 cavity shape from initial warming might be positive or negative. Our idealized simulations  
 134 do not include wind forcing, frazil ice, or sea-ice formation.

135 Circulation develops through buoyancy forcing caused by thermodynamic exchange at  
 136 the base of the ice shelves and, for tide-forced cases, by boundary conditions of tidal depth-  
 137 integrated velocity and sea surface height. The thermodynamically-driven component of the  
 138 circulation was introduced by scalar fluxes at the ice-ocean interface beneath FRIS. These  
 139 fluxes are based on a simplified version of the 3-equation parameterization that assumes that  
 140 the heat flux through the ice shelf is negligible (Hellmer and Olbers, 1989; Holland and  
 141 Jenkins, 1999):

$$Q_T^o = \rho_o c_{po} (\alpha_h u_* + m) \Delta T \text{ [W m}^{-2}\text{]}, \quad (1)$$

$$Q_S^o = \rho_o (\alpha_s u_* + m) \Delta S \text{ [kg m}^2 \text{ s]}, \text{ and} \quad (2)$$

$$T_b = T_f = 0.0939 - 0.057 S_b + 7.6410 \times 10^{-4} z_{ice} \text{ [}^\circ\text{C]}. \quad (3)$$

142 In Eq. (1), the surface heat flux ( $Q_T^o$ ) is determined by the combined effect of thermal forcing  
 143 and turbulent heat exchange. The thermal forcing is represented as  $\Delta T = (T_b - T_o)$ , where  
 144  $T_b$  is the temperature at the ice-ocean interface and  $T_o$  is the temperature of the ocean mixed  
 145 layer under the ice base. The value of  $T_b$  is assumed to be the freezing point temperature,  $T_f$ ,  
 146 and depends on the salinity at the ice-ocean interface,  $S_b$ , as well as the ice draft,  $z_{ice} < 0$

147 (Foldvik and Kvinge, 1974; Dinniman et al., 2007). For  $T_o$ , we follow a common approach  
 148 of using the temperature of the surface  $\sigma$ -layer in place of mixed layer values, with the  
 149 thickness of the surface  $\sigma$ -layer beneath the ice shelf cavity in our standard grid ranging  
 150 from 2 to 24 m and with 72% of points between 5 and 15 m. The turbulent heat exchange at  
 151 the ice-ocean interface is represented by a thermal transfer coefficient,  $\alpha_h$ , scaled by a  
 152 friction velocity,  $u_*$ . This turbulent heat exchange is then adjusted by a meltwater advection  
 153 term,  $m$ , that corrects the scalar fluxes for a computational drift that is introduced as an  
 154 artifact of assumptions made in the numerical representation of the ice shelf as a material  
 155 boundary (Jenkins et al., 2001). We define  $m = -\alpha_s u_* (1 - S_o/S_b)$  where  $S_b < S_s$  and  $m = 0$   
 156 elsewhere. The friction velocity is calculated from the surface quadratic stress of the upper  
 157 sigma level as  $u_* = C_d^{1/2} |\mathbf{u}|$ , where  $C_d = 2.5 \times 10^{-3}$  is a constant drag coefficient and  $|\mathbf{u}|$  is  
 158 the magnitude of the surface layer current. The potential density of seawater,  $\rho_o(x, y, z, t)$ , is  
 159 evaluated for the uppermost layer, with the heat capacity of the ocean,  $c_{po}$ , assumed constant  
 160 at  $3985 \text{ J kg}^{-1} \text{ }^\circ\text{C}^{-1}$ .  $\Delta S$  is the salinity equivalent to  $\Delta T$  and is defined as  $\Delta S = (S_b - S_o)$ ,  
 161 with  $S_b$  solved by quadratic formula from combining Eq. 1, 2, and 3 (without the meltwater  
 162 advection term,  $m$ ) and  $S_o$  representing the salinity of the surface  $\sigma$ -layer.

163 These heat and salt fluxes ( $Q_T^o, Q_S^o$ ) depend on scalar transfer coefficients ( $\alpha_h, \alpha_s$ ) that are  
 164 proportional to each other by a “double diffusive” parameter,  $R = \alpha_h/\alpha_s$  (McPhee et al.,  
 165 2008). Chapter 2 in Mueller (2014) provides a more detailed explanation of the background  
 166 and motivation for this parameterization. Here, we used scalar transfer coefficients based on  
 167 observations of the RIS sub-ice-shelf cavity (Jenkins et al., 2010a), with  $\alpha_h = 1.1 \times 10^{-2}$  and  
 168  $R = 35.5$ . The meltwater-equivalent melt\_rate term is derived by scaling the heat flux,  $Q_o^T$ , by  
 169 latent heat,  $L = 3.34 \times 10^5 \text{ J kg}^{-1}$ , and the density of ice,  $\rho_i = 918 \text{ kg m}^{-3}$ , such that

$$171 \quad w_b = -Q_o^T / (L \rho_i) \text{ [m s}^{-1}\text{]}. \quad \text{_____ (4)}$$

172 Melting ice is indicated by  $w_b > 0$  and represents the thickness of freshwater added to the  
173 ocean surface, per second. These equations highlight that basal melting is driven by ocean  
174 heat and motion, the latter being influenced by thermohaline circulation and tides.

175 A set of 12 model simulations was performed and is summarized in Table 1. A detailed  
176 description of the different simulations is given in **Sect. 2.3**. Each case involves a  
177 combination of standard or modified geometry, cold or warm ocean, and tidal forcing  
178 switched off or on. For tide-forced simulations, tide heights and barotropic currents were  
179 specified along the domain’s open-ocean boundaries (see **Fig. 1**). The tidal boundary  
180 conditions were obtained for the four most energetic tidal constituents ( $K_1$ ,  $O_1$ ,  $M_2$ , and  $S_2$ )  
181 from the CATS2008 barotropic inverse tide model, an updated version of the circum-  
182 Antarctic model described by Padman et al. (2002). These four constituents account for 94%  
183 of the total tidal kinetic energy for this region, based on CATS2008 estimates. Flather  
184 (1976) boundary conditions were used for the barotropic velocity with free surface  
185 conditions following Chapman (1985). Radiation conditions for baroclinic velocities were  
186 applied following Raymond and Kuo (1984). Tracer equations were radiated across the open  
187 boundaries (Marchesiello et al., 2001) and nudged to initial conditions over a 20-day time  
188 scale.

## 189 **2.2 Geometries**

190 The grid of seabed bathymetry ( $h$ ) over the entire domain (**Fig. 2a**) was derived from the  
191 RTOPO-1 gridded dataset (Timmerman et al., 2010). The ice shelf is represented by a non-  
192 evolving, although freely floating, surface boundary based on an ice draft ( $z_{ice}$ , **Fig. 2b**) that  
193 was also derived from RTOPO-1. The land mask was adjusted around the ice rises and  
194 rumples in the southern RIS to follow the grounding line provided by Moholdt et al. (2014).  
195 Values of  $h$  and  $z_{ice}$  in regions of the ice sheet that are grounded in the RTOPO-1 mask but  
196 floating (i.e., ice shelf) in the mask obtained from the Moholdt et al. (2014) data were

197 computed by linear interpolation and a nearest-neighbor extrapolation to ice shelf points in  
198 the original RTOPO-1 grids.

199 The ice draft and bathymetry were each smoothed to minimize errors in the baroclinic  
200 pressure gradient that arises with the terrain-following coordinate system used in ROMS  
201 (Beckmann and Haidvogel, 1993; Haney, 1991). The two parameters used to quantify  
202 smoothing are the Beckmann and Haidvogel number,  $rx0 = |h(e) - h(e')| / (h(e) + h(e'))$   
203 (Beckmann and Haidvogel, 1993), and the Haney number,  $rx1 = |h(e, k) - h(e', k) + h(e, k-$   
204  $1) - h(e', k-1)| / (h(e, k) + h(e', k) - h(e, k-1) - h(e', k-1))$  (Haney, 1991), where  $1 \leq k \leq N$   
205 and  $e$  and  $e'$  represent two adjacent cells. Together, these parameters establish that the  
206 surface (ice) and bottom bathymetry slopes are sufficiently small to reduce or eliminate  
207 spurious flows due to a horizontal pressure gradient and ensures hydrostatic consistency  
208 throughout the water column at adjacent horizontal grid nodes. Our Beckman and Haidvogel  
209 number,  $rx0$ , is less than 0.045 along both surface and bottom topographies, and our Haney  
210 number,  $rx1$ , is less than 10 in both surface and bottom levels except for some areas along  
211 the ice shelf front, where  $rx1$  is larger and reaches a maximum value of 17.

212 Our maximum values of  $rx1$  are larger than typically recommended for ROMS. To test  
213 whether large values lead to significant circulation from resulting errors in the baroclinic  
214 pressure gradient, we ran unforced models for each of the standard and modified grids. We  
215 initialized these models with horizontally uniform temperature and salinity fields, using an  
216 extreme density profile in order to get an upper bound on the grid errors. We chose a profile  
217 from a location just north of the eastern side of Berkner Island. The  $T$  and  $S$  profiles in this  
218 region yielded a relatively large pycnocline with potential density changing from 1027.67 to  
219  $1027.77 \text{ kg m}^{-3}$  between 0 and 400 m, a depth range where the change in ice draft along the  
220 ice shelf front is most likely to cause spurious flows. This profile was extrapolated in depth  
221 and horizontally to yield the uniformly stratified test hydrography. The resulting velocities in  
222 these unforced runs are representative of maximum grid errors that may occur in the full

223 | simulations. We [quantified](#) grid error by comparing the currents generated by these  
224 | uniformly stratified, unforced model runs to the [30-day averaged current speeds in the](#)  
225 | standard warm tide-forced and modified warm tide-forced cases. [The maximum fractional](#)  
226 | error in our velocity fields is 10% for the standard grid and 5% for the modified grid. [Large](#)  
227 | [errors were limited](#) to a very [small region](#) north and northwest of Berkner Island; [the relative](#)  
228 | error over most of the domain is negligible.

229 |       In the smoothed standard geometry, the ice draft beneath FRIS ranges from 1537 m at  
230 | the deepest part of the grounding line to 11 m at the shallowest point of the ice shelf front.  
231 | Small values of ice draft near the ice front are unrealistic, but are a consequence of necessary  
232 | smoothing [in models that use terrain-following vertical coordinates](#). The region of thinned  
233 | ice shelf represented by these small values is a narrow band along the ice front (**Fig. 2b and**  
234 | **2c**). The water column thickness,  $wct = h + z_{ice}$ , ranges from 50 m (a specified minimum  
235 | value, chosen for numerical stability) to 1111 m under FRIS. In the open ocean,  $wct = h$  and  
236 | has a maximum value of [1211 m, in the Filchner Trough](#).

237 |       Using this standard geometry, we conducted simulations for both the cold and warm  
238 | cases described in **Sect. 2.1**, with and without tides. The modified geometry was then  
239 | created from the output [of](#) the two 20-year tide-forced simulations of the standard cold and  
240 | standard warm cases ([see Sect. 2.3.2](#)). In creating this grid, we assumed that the RIS and FIS  
241 | are both in steady state under present-day conditions (Rignot et al., 2013; Depoorter et al.,  
242 | 2013; Moholdt et al., 2014) represented by our standard cold case, and that the most accurate  
243 | simulations of basal melting will be those with tidal forcing included (Makinson et al.,  
244 | 2011). Steady state requires that mass input from lateral ice transport across the grounding  
245 | line plus snowfall onto the ice shelf is balanced by basal melting and iceberg calving that  
246 | maintains a constant ice-front position. The difference in local melt between the standard  
247 | warm and standard cold cases, neglecting any ice dynamical feedbacks, would then be

248 equivalent to the rate of change in thickness of the ice shelf, provided the change in melt rate  
249 is not offset by changes in mass inputs to the ice shelf.

250 We applied the melt-rate imbalance for a period of 50 years to provide a sufficiently  
251 large change in  $z_{ice}$  to significantly alter the general circulation and tidal currents in the  
252 cavity. The resulting modified geometry thins  $z_{ice}$  by an average across the ice shelf of 30 m  
253 and a median of 14 m. The ice shelf thickens in the freezing (mid-shelf) regions by a  
254 maximum of 14 m and thins in the melt regions by a maximum of 453 m, although about  
255 99% of all thinning values are less than 200 m (Fig. 2c and 2d). The combined area where  
256 the ice shelf thickens is only 0.1% of the total ice shelf area and is characterized by an  
257 average increase of 5 m. The modified-case bathymetry is the same as the standard case  
258 bathymetry, so these changes in  $z_{ice}$  cause an equal magnitude change in  $wct$ . We chose to  
259 only run the modified geometry as a warm case because it is designed to represent the FRIS  
260 cavity under warm conditions, with and without the influence of tidal forcing along the open  
261 boundaries.

## 262 **2.3 Model Simulations**

263 Three types of simulations were run: (1) tide-resolving with time-averaged output every two  
264 hours and no thermodynamic exchange; (2) simulations with ice/ocean thermodynamics,  
265 with and without tide forcing; and (3) passive dye tracer simulations to explore circulation  
266 patterns. These runs are more fully described in the following sections.

### 267 **2.3.1 Tide-resolving simulations with no thermodynamic exchange**

268 We performed two 40-day simulations with 2-hr-averaged output, one with standard  
269 geometry and the other with modified geometry, to predict tidal current speeds. These  
270 simulations (“tides-only cases”) did not include thermodynamic interactions at the ice-ocean  
271 boundary, so that the ocean remained unstratified at its initial homogeneous state. Absent

272 stratification, the resulting currents are barotropic in nature, although some depth-  
273 dependence arises from the friction at the seabed and ice base (see, e.g., Makinson et al.,  
274 2006).

275 The spatial characteristics of time-averaged tidal currents (**Fig. 3a,b**) were calculated as  
276 the time- and depth-averaged tidal current speed  $|\mathbf{u}|_{tide}$ , given by:

277

$$278 \quad |\mathbf{u}|_{tide} = \langle \sqrt{u_b^2 + v_b^2} \rangle_t \text{ [m s}^{-1}\text{]}, \quad (5)$$

279

280 where  $u_b(x, y, t)$  and  $v_b(x, y, t)$  are orthogonal components of modeled, depth-averaged  
281 current and  $\langle \rangle_t$  represents temporal averaging over the last  $t = 30$  days of the model run,  
282 which characterizes two cycles of the 15-day spring-neap cycles generated by the  $M_2$ ,  $S_2$ ,  $K_1$ ,  
283 and  $O_1$  tides. The maximum tidal speed at spring tides is, typically, about  $2 \times |\mathbf{u}|_{tide}$ .

### 284 2.3.2 Base simulations

285 Six simulations, each 20-30 years long, were conducted with thermodynamic exchanges of  
286 heat and freshwater at the ocean/ice-shelf interface. Output for each of these simulations was  
287 averaged over the last 30 days. Three of these were run with tidal forcing, two standard  
288 geometry cases, one with  $\theta_{init} = -1.9^\circ\text{C}$  (cold) and one with  $\theta_{init} = -1.4^\circ\text{C}$  (warm), and one  
289 modified geometry case with  $\theta_{init} = -1.4^\circ\text{C}$  (warm). We refer to these runs as: standard cold  
290 tide-forced, standard warm tide-forced, and modified warm tide-forced (Table 1). These  
291 three simulations all reached steady state solutions by 20 years. We then used the last 30-day  
292 averaged output grids in these tide-forced solutions as initial conditions for three “restart”  
293 simulations without tidal forcing, each of which reached a new steady state over 10 model  
294 years. We refer to these runs as: standard cold no-tides, standard warm no-tides, and  
295 modified warm no-tides.

### 296 2.3.3 Passive dye tracer simulations

297 Three simulations were run with passive dye tracers to investigate the advection and  
298 diffusion of water from different regions. These simulations were initialized with the steady-  
299 state solutions of the standard cold, standard warm, and modified warm tide-forced cases.  
300 They were run for 2 years each, with 30-day averaged output. Two types of dyes were used.  
301 Passive “meltwater” dyes were continuously added to the model’s surface sigma layer at a  
302 rate of  $1 \times 10^4 w_b$  in six regions, the grounding zones of five tributary glaciers plus “South  
303 Channel”, [the region of ice shelf south of Henry Ice Rise \(Fig. 4\)](#). A “bulk” dye was added  
304 to the open ocean region shown in **Fig. 4**. The bulk dye was initialized at a concentration of  
305 100%, [over the entire water column](#), but was not replenished after these simulations began.

## 306 3 Results

307 The main result of our study is that melt-induced changes in cavity shape introduce regional  
308 variations in tide current speeds and advection pathways that result in [spatial variations in](#)  
309 feedbacks to basal melting. We explain these insights in the following subsections through  
310 analyses of: tidal currents, spatial patterns of  $w_b$ , ice-shelf-averaged  $w_b$  and its sensitivity to  
311 model setup, regionally-averaged  $w_b$  and its sensitivity to model setup, and ocean circulation  
312 patterns shown by maps of dye tracer distribution.

### 313 3.1 Tidal currents in tide-resolving simulations

314 The maps of  $|\mathbf{u}|_{\text{tide}}$  defined by [Eq. \(5\)](#) (**Fig. 3a and 3b**) highlight the spatial variability of  
315 tidal currents beneath FRIS. In particular, they show negligible tidal currents in the inlets of  
316 the major ice streams that feed into the RIS and FIS, and local maxima along the  
317 northeastern RIS front and South Channel.

318 The maximum [tidal currents](#) along the northeastern ice shelf frontal zone of the RIS [are](#)  
319 consistent with previous tide models (e.g., Robertson et al., 1998; Makinson and Nicholls,

1999). This region has a relatively small  $wct$  (Fig. 2c), so a larger tidal current here is expected. The melt-induced geometry change in the modified case (Fig. 3c) has the overall effect of increasing the water depth in this region and reducing these tidal currents (Fig. 3d).

Tidal currents in South Channel are not as strong as those in the northeastern ice shelf frontal zone, but the melt-induced change in  $wct$  and  $|\mathbf{u}|_{tide}$  is larger than in that region (Fig. 3c and 3d). The melt-induced change in  $wct$  is also large along the southeastern grounding line of FIS (Fig. 3c). These changes in  $wct$  and  $|\mathbf{u}|_{tide}$  enhance barotropic tidal transport ( $|\mathbf{u}|_{tide} \times wct$ ) along the southern edge of South Channel, the eastern grounding line of FIS, and along the northeast boundary of RIS with Berkner Island (Fig. 3e). These comparisons show that melt-induced ice shelf thinning generally reduces the local tidal currents (Figs. 3c,d). However, larger-scale reorganization of the barotropic tidal energy fluxes under FRIS also occurs (see, e.g., Rosier et al. (2014) and Padman et al. (in press)), so that simple scaling of modern tidal currents by the change in  $wct$  is not possible.

### 3.2 Spatial pattern of melt rates ( $w_b$ ) in the base simulations

We analyzed the six base simulations described in Sect. 2.3.2 to quantify the sensitivity of the spatial pattern of basal melt rates ( $w_b$ ) to  $\theta_{mit}$ , tides, and geometry.

#### 3.2.1 Base simulation “no-tides” cases

The pattern of  $w_b$  in the standard cold no-tides case (Fig. 5a) is generally consistent with the increase in thermal forcing at the ice base ( $\Delta T = (T_f - T_o)$ ) due to the depression of the in situ freezing point temperature of seawater ( $T_f$ ) as pressure increases. The greatest values of  $w_b$  occur along the deepest grounding lines (see Fig. 2 for geometry), notably in the Support Force, Foundation, and Rutford inlets. This pattern of pressure-dependent melt fuels the ice pump mechanism that drives thermohaline circulation within the cavity and causes refreezing conditions ( $w_b < 0$ ) as melt water ascends to the mid-ice-shelf regions, as can be

344 seen under the central RIS and near the RIS ice front. Since our model does not include a  
345 mechanism for frazil-ice formation, these regions represent where ice would form by direct  
346 freezing onto the ice base.

347 The pattern of  $w_b$  for the standard warm no-tides case (Fig. 5b) is generally similar to the  
348 standard cold no-tides case (Fig. 5a) but with an increase, by a factor of about 3.5, in the  
349 shelf-averaged value. Changing cavity shape while imposing the same initial ocean  
350 temperature in the modified warm case (Fig. 5c) only slightly reduces melt rates (by 10%)  
351 for the no-tides scenario (compare Figs. 5b and 5c).

### 352 3.2.2 Base simulation “tide-forced” cases

353 Adding tide forcing to the standard cold case changes the magnitude and pattern of  $w_b$   
354 (compare Figs. 5a and 5d). Melt rates increase around the grounding line and in South  
355 Channel, (Fig. 5g). The increase in  $w_b$  in South Channel, where tidal currents are relatively  
356 strong, from the standard no-tides to tide-forced cases exceeds 2 m a<sup>-1</sup>. Adding tides also  
357 increases refreezing in portions of RIS, including north of Korff Ice Rise and along the coast  
358 of the northwestern RIS, with more limited refreezing north of Henry Ice Rise. This increase  
359 in refreezing with tides can be explained by the increased production of cold, buoyant  
360 meltwater from the deeper parts of the ice shelf near the grounding line, and is qualitatively  
361 consistent with the effects of adding tides reported by Makinson et al. (2011).

362 In the standard warm case,  $w_b$  also increases around the deep grounding lines when tides  
363 are added (compare Figs. 5b and 5e). In this case, however, this increased melt doesn't  
364 enhance mid-shelf basal freeze conditions as much as in the standard cold case.  
365 Consequently, the increase of refreezing under the RIS is less pronounced than for the  
366 standard cold tide-forced case (compare Figs. 5e and Fig. 5d). There are two possible  
367 factors contributing to this result. First, the meltwater product at the deepest grounding lines  
368 in the warm case is warmer than in the cold case and, hence, has a smaller potential for

369 supercooling when reaching shallower parts of the ice base. Second, the rising meltwater  
370 may continue to warm on its ascent due to admixture of warmer ambient water in the ice  
371 shelf cavity. Both factors are consistent with an increase in thermohaline circulation in  
372 response to warmer ocean temperatures.

373 The modified warm tide-forced case (Fig. 5f) also exhibits a similar amplification of  
374 basal melt by tides as the standard warm tide-forced case, although with regional differences  
375 (compare **Figs. 5i and 5h**).

376 The differences between the tide-forced and no-tides cases for all three model setups  
377 (**Fig. 5g-5i**) show that the principal effect of tides is to increase  $w_b$  under FIS and South  
378 Channel.

### 379 **3.3 Sensitivity of $w_b$ to tides, $\theta_{init}$ and geometry in the base simulations**

380 We summarize the effect of  $\theta_{init}$  and geometry through values averaged over the ice shelf  
381 area. Net mass change ( $M_b$ : Gt a<sup>-1</sup>) and averaged values of  $w_b$  were calculated for three  
382 regions: (1) all of FRIS, (2) areas for which melting conditions are predicted ( $w_b > 0$ ), and  
383 (3) areas where freezing conditions are predicted ( $w_b < 0$ ). The ratio of  $M_b$  and  $w_b$  for the  
384 freeze-only and melt-only calculations of mass change are not constant, since  $M_b$  is  
385 influenced by the extent of melting and freezing regions as well as by the mean magnitude  
386 of  $w_b$ .

387 Ocean temperature is the dominant control on total ice-shelf-integrated  $M_b$  and ice-shelf  
388 averaged  $w_b$  (**Fig. 6; Table 2**). Regardless of tides and geometry, warming the ocean inflow  
389 by 0.5°C increases net mass loss by a factor of ~3-5. The integrated mass gain due to  
390 freezing (marine ice formation) is insensitive to temperature for the no-tide cases but  
391 sensitive to temperature for the tide-forced cases (**Fig. 6a**), suggesting that accurate  
392 predictions of marine ice formation requires accurate representation of tidal currents in  
393 simulations.

394 | Tides change the effect of ocean heat on [distributions of  \$M\_b\$](#)  and  $w_b$ . In particular, the  
395 | addition of tides to the standard cold case (our approximation to the modern state) increases  
396 | net freezing by a factor of four, almost exactly offsetting a factor of  $\sim 2$  increase in [mass loss](#)  
397 | in melt-only regions. For the warm cases, tides increase total mass loss in melting regions by  
398 | about 20–40%, with most of this increase occurring in South Channel and under FIS (see  
399 | **Fig. 5**). In contrast to the cold case, the increases in net freezing in the warm cases is small  
400 | compared with the increased mass loss, so that the total basal mass loss for FRIS increases  
401 | significantly when tides are added to a warm ocean. ~~We attribute this result to production of~~  
402 | ~~a warmer plume near the deep grounding lines as a result of heat in the mixed layer that isn't~~  
403 | ~~fully utilized to fuel melting.~~

404 | Changing geometry has a much smaller but still significant effect on ice-shelf-  
405 | integrated  $M_b$  and averaged  $w_b$ . In the no-tides simulations, the change from standard to  
406 | modified geometry causes net mass loss to increase slightly, ~~suggesting a weak positive~~  
407 | ~~feedback,~~ while the tide-forced cases show a slight decrease, ~~or negative feedback~~ (**Fig. 6**).  
408 | This change in sign in the mass loss anomaly is driven primarily by the anomalous behavior  
409 | of South Channel, and will be discussed in greater detail in [Sects. 3.4 and 4.2](#).

### 410 | **3.4 Regional sensitivity of $w_b$ in the base simulations**

411 | Regional averages of  $w_b$  (**Fig. 7**) indicate that basal mass loss near [the](#) grounding lines of  
412 | major inflowing ice streams varies by an order of magnitude within a given simulation.  
413 | Support Force, Foundation, and Rutford ice streams show the largest values, exceeding 2 m  
414 |  $\text{a}^{-1}$  for the standard cold cases with and without tide forcing. In contrast, modeled melt rates  
415 | for Möller and Institute ice streams are in the range of 0.28–0.44  $\text{m a}^{-1}$  for the standard cold  
416 | case runs.

417 | For each ice stream inlet,  $\theta_{init}$  is the primary control on melt rate near the grounding line,  
418 | with mean melt rate approximately doubling from the standard cold case to the standard

419 warm case. Tidal forcing is a secondary control that leads to either an increase or decrease in  
420  $w_b$  near grounding lines. For [Support Force, Foundation](#), and Rutford ice streams, adding  
421 tides reduces area-averaged melt rates, with the relative change being larger for the warm  
422 cases with both standard and modified geometry. The largest fractional change in melt rate  
423 due to tides occurs near the Rutford Ice Stream grounding line in the modified-geometry  
424 warm case, where adding tides reduces mean melt rate by 40% from  $7.7 \text{ m a}^{-1}$  to  $4.6 \text{ m a}^{-1}$ .

425 South Channel is an exception to the general result that regional sensitivity of  $w_b$  is  
426 more strongly affected by changes in  $\theta_{init}$  than tidal forcing. In this region,  $w_b$  increases by  
427 roughly an order of magnitude between the no-tide and tide-forced simulations, whereas the  
428 fractional change due to  $\theta_{init}$  is much smaller, about a factor of  $\sim 2$  (**Fig. 7**). South Channel  
429 also experiences a large reduction ( $\sim 30\%$ ) in regionally-averaged  $w_b$  in the modified warm  
430 tide-forced run compared with the standard warm tide-forced run. We attribute this change  
431 in  $w_b$  to the reduction in tidal currents as geometry is changed (**Fig. 3**).

### 432 **3.5 Ocean circulation within the FRIS cavity in the passive-dye tracer simulations**

433 General patterns of water mass circulation into and under FRIS are demonstrated by output  
434 from the two-year simulations with passive-tracer dyes (see **Sect. 2.3.3**). We focus only on  
435 tide-forced simulations because, as discussed in **Sect. 3.3** and by Makinson et al. (2011),  
436 tidal currents are known to be critical to patterns of basal melting beneath FRIS.

#### 437 **3.5.1 Dye tracer circulation in standard cold tide-forced case**

438 The concentration of the open ocean bulk dye tracer in the upper  $\sigma$ -layer (**Fig 8a**) reveals  
439 that the FRIS cavity has two different sources of heat inflow. The FIS and innermost RIS  
440 cavities are flooded by a southward transport of the open continental shelf waters across the  
441 FIS front, whereas the cavity circulation in the northeastern portion of RIS is dominated by  
442 incursions of water from across the RIS front. The latter inflow does not penetrate deep into

443 the central and southern RIS within two years of simulation, although this is likely to be an  
444 artefact of the omission of the [High Salinity Shelf Water](#) that is known to be formed at the  
445 RIS front and is assumed to fuel gravity currents that reach the deep western grounding lines  
446 of the RIS. In our simulations, the water entering through FIS circulates clockwise along the  
447 deep grounding line. After two years, some dye has reached as far west as Carlson inlet;  
448 however, very little of this dye is found under the central RIS north of the ice rises and  
449 rumples. [The most direct impact of changes in open ocean inflow is observed in](#) Support  
450 Force [and](#) Foundation [inlets](#), and [in](#) South Channel.

451 Meltwater produced near Foundation Ice Stream grounding line (**Fig. 8b**) reveals  
452 similar clockwise circulation. This water reaches the western RIS ice front in about two  
453 years. Meltwater from Foundation inlet flows into all ice stream inlets to the west of  
454 Foundation. The flow of this meltwater through South Channel is limited to the southern  
455 side of the channel.

456 Meltwater produced in South Channel also reaches all of the western RIS within two  
457 years (**Fig. 8c**), including much of the central region where refreezing occurs. Meltwater  
458 produced in Rutford inlet flows northward to the west of Korff Ice Rise (**Fig. 8d**).

459 These dye maps demonstrate that water found in the uppermost layer, in contact with  
460 the ice shelf base, in a specific ice stream inlet is a mixture of the incoming high-salinity  
461 ocean water and meltwater that was produced at other inlets further upstream. As an  
462 important consequence, changes in meltwater production in different regions will alter the  
463 meltwater plume characteristics (e.g., temperature) experienced by downstream ice stream  
464 grounding zones. In the following, it will be shown that the interactions [within](#) different  
465 grounding zone [regions](#) lead to non-local feedbacks of the melting response to changes in  
466 ocean temperatures and ice shelf geometry, ~~for modeling of which an explicit inclusion of~~  
467 ~~tidal currents is one of the key ingredients.~~

468 **3.5.2 FRIS cavity dye tracer distribution for tide-forced cases**

469 Comparisons of dye concentration maps after two years of integration for the three tide-  
470 forced simulations (**Fig. 9**) show differences that can be attributed both to  $\theta_{init}$  (comparing  
471 standard cold and standard warm cases) and to geometry (comparing standard warm and  
472 modified warm cases).

473 The stronger cavity circulation introduced by the amplification of net basal melting for  
474 the warmer ocean,  $\theta_{init} = -1.4^\circ\text{C}$ , increases inflow through the FIS and into the RIS cavity  
475 (upper row of **Fig. 9**). Open-ocean water is present under most of RIS after two years in the  
476 standard warm case. The dye concentration of open-ocean water under the northern portion  
477 of RIS decreases as  $\theta_{init}$  increases, indicating that the stronger northward flow of meltwater  
478 in the warm case reduces the contribution of the direct open-ocean inflow to the northern  
479 RIS. This influence of  $\theta_{init}$  on strengthening the sub-ice-shelf cavity circulation decreases  
480 slightly in the modified warm case, which shows less open water dye penetrating into the  
481 innermost RIS than the standard warm case solution (compare the two upper right subplots  
482 of **Fig. 9**).

483 Comparisons of meltwater dyes from ice stream inlets and South Channel (lower six  
484 rows in **Fig. 9**) show, in all cases, more rapid ventilation of downstream regions when  $\theta_{init}$  is  
485 warmer. In these simulations, meltwater dyes are injected continuously at a rate that is  
486 scaled to the basal melt rate (**Sect. 2.3.3**). Relative dye concentrations at specific locations  
487 can, therefore, be interpreted as the relative values of meltwater from different sources with  
488 total meltwater plume concentration being an integration of the contributions from all  
489 upstream sources. Changes in the different runs reflect the response of the cavity circulation  
490 and changes in meltwater production rate in the respective grounding zones. Meltwater from  
491 South Channel dominates the central RIS, although melting in Foundation and Rutford inlets  
492 provides a substantial freshwater flux to the western RIS.

493 The changes in upper-ocean circulation caused by changes in geometry, seen by  
494 comparing the two warm cases in the last two columns of **Fig. 9**, are less obvious than the  
495 effect of changing temperature. Nevertheless, changing geometry has a significant regional  
496 effect. Foundation inlet meltwater spreads out more in the modified warm case than in the  
497 standard warm case as a result of increased dye transport through the channel between  
498 Henry Ice Rise and Berkner Island. South Channel meltwater concentrations are reduced in  
499 the modified warm case, which is consistent with the reduced melt rates in the region  
500 (**Fig. 5**). Similar to South Channel, Rutford inlet meltwater in the surface layer is also  
501 reduced for the modified geometry case.

### 502 **3.5.3 Regional meltwater dye comparison, for tide-forced cases**

503 Regional meltwater dye production and advection is evaluated from the surface levels of  
504 Foundation, Möller, and South Channel inlet regions (as in **Fig. 4**). **Fig. 10** shows the  
505 integrated values over these regions for the standard cold, standard warm and modified  
506 warm tide-forced cases. As described in **Sect 2.3.3**, meltwater dye from a particular region is  
507 a scaled quantity of  $w_b$  that reflects the magnitude of meltwater produced in that region. The  
508 resulting passive dye is then transported through the domain through a combination of  
509 advection and mixing and acts as a proxy for the meltwater plume. In this section, we use the  
510 quantity of these meltwater tracers to demonstrate how meltwater circulation is affected by  
511 changes in  $\theta_{init}$  and geometry.

512 Foundation inlet shows an increase in integrated meltwater dye with the  $0.5^\circ\text{C}$  increase  
513 in  $\theta_{init}$  between the standard cold and standard warm cases (**Fig. 10a**). This increase in  
514 integrated meltwater dye is not sustained with the change in cavity geometry. Instead, the  
515 net amount of dye is reduced in the modified warm case such that the value of integrated dye  
516 in the surface level more closely matches that of the standard cold case. This reduction in  
517 integrated meltwater dye between the standard warm and modified warm case carries

518 forward into the Möller region, where the reduction of Foundation dye between the two  
519 cases is even greater than in Foundation [inlet](#) (compare **Fig. 10a** and **10b**). At the same time,  
520 the reduction in Foundation dye in the Möller region is somewhat compensated by the  
521 Möller meltwater dye, which is consistent between the two warm cases (**Fig. 10b**). Overall,  
522 the Möller region appears to be less affected by the change in geometry than the Foundation  
523 region. Within South Channel, the influence of geometry on the quantity of meltwater dye is  
524 compensated by changes in circulation that allow for more Foundation dye in the surface  
525 level of South Channel in the modified warm case than the standard warm case (**Fig. 10c**).  
526 This increase in surface level Foundation dye in South Channel is caused by changes in  
527 circulation that distribute the dye more evenly across South Channel in the modified warm  
528 case than in the standard warm case (**Fig. 9**).

529 These results highlight that the regional sensitivities of meltwater dye to  $\theta_{init}$  and  
530 geometry may influence but not necessarily determine the quantity and [temperature](#) of  
531 meltwater in downstream regions. This result reveals the degree to which  $\theta_{init}$  and cavity  
532 shape precondition the quantity and origin of meltwater in any given region. For example,  
533 the FRIS-integrated surface dye quantity (**Fig. 10e**) for Foundation and Support Force is  
534 equivalent between the standard warm and modified warm cases, even though there are  
535 strong regional variations in these cases (**Fig. 10 a-c**). In addition, the FRIS-integrated  
536 values of meltwater dyes from the ice front regions (RIS west, RIS east, and FIS) are similar  
537 among all cases while they differ among regions, showing greater amounts of dye in  
538 Foundation, Möller, and South Channel regions for the warm cases than in the cold case.  
539 These regional and integrated changes demonstrate that the FRIS meltwater product is a  
540 result of regional feedbacks that are affected by a combination of production, mixing, and  
541 advection.

542 **4 Discussion**

543 Our results confirm an earlier study (Makinson et al., 2011) demonstrating that adding tide  
544 forcing to numerical models substantially increases basal melting along the deep grounding  
545 lines of FRIS and increases marine ice formation rates under RIS. By carrying out  
546 simulations with different temperatures of water entering the sub-ice-shelf cavity, and  
547 investigating potential changes to ice draft in a scenario with a warmer ocean, we have also  
548 shown that the spatial patterns of melting and refreezing are sensitive to complex feedbacks  
549 between basal melting, tidal currents, advection and mixing.

550 The simplified forcing of our models, however, prevents the development of some sub-  
551 ice-shelf circulation features observed to be present in the modern state. The circulation  
552 under RIS is strongly affected by winter sea-ice formation and the associated production of  
553 High Salinity Shelf Water over the southern Weddell Sea continental shelf. Combined with  
554 larger-scale atmospheric forcing, these processes establish an east-to-west density gradient  
555 across the continental shelf (e.g. Foldvik et al., 1985; Nicholls et al., 2009) that drives a  
556 counter-clockwise circulation with inflow in the Ronne Depression and a counter-clockwise  
557 circulation around Berkner Is. (Foldvik et al. 2001). Our idealized model also lack the  
558 seasonal warming of the upper ocean near the ice front that leads to significant summer  
559 melting and rapid basal melting of the ice shelf frontal zone (e.g., Makinson and Nicholls,  
560 1999; Joughin and Padman, 2003; Moholdt et al., 2014). Since we omit these forcings, our  
561 simulations do not capture these components of sub-ice-shelf circulation. As a result, our  
562 cold-case simulations are “present-day” in terms of ocean thermal forcing but with  
563 circulation that is more representative of the future-warming scenario presented by Hellmer  
564 et al. (2012). These simplifications restrict the predictive capacity of our simulations but  
565 help us clarify the importance of tidal currents and tide-related feedbacks that affect future  
566 mass loss from FRIS and the adjacent buttressed, grounded ice.

#### 567 4.1 Comparison of modeled, ice shelf averaged basal melt estimates with observations

568 The melt rate averaged over the area of an ice shelf is a common metric for evaluating  
569 ice shelf mass balance (e.g., Rignot et al., 2013; Depoorter et al., 2013). Our estimate of melt  
570 rate averaged over FRIS for the standard case is  $0.14 \text{ m a}^{-1}$  freshwater equivalent, equal to  
571  $\sim 48 \text{ Gt a}^{-1}$  of net mass loss (**Fig. 6** and **Table 2**). The range of values reported by other  
572 studies extends from  $0.03 \text{ m a}^{-1}$ , the lower bound in Depoorter et al. (2013), to  $0.55 \text{ m a}^{-1}$   
573 from the first oceanographically-derived estimates (Jenkins, 1991; Jacobs et al., 1992); see  
574 **Fig. 11** and **Table 3**. The range in estimates of  $w_b$  is a result of variations in observation type  
575 and model choices. Estimating  $w_b$  from observations typically requires averaging other ice  
576 shelf mass budget terms, derived from satellite observations and atmospheric models, over  
577 several years. Estimates from models are affected by model setup.

578 Compared with the three most recent satellite-constrained estimates, our value is near  
579 the central estimate of  $0.12 \text{ m a}^{-1}$  of Depoorter et al. (2013), and near the lower limit of the  
580 ranges reported by Rignot et al. (2013) and Moholdt et al. (2014). Given the model  
581 simplifications discussed above, we regard the general agreement between our integrated  
582 mass loss and prior studies as evidence that our simulations are sufficiently realistic for  
583 further sensitivity studies and interpretation of the role of tides in FRIS evolution for future  
584 climate states.

585

#### 586 4.2 Sensitivity of $w_b$ to $\Delta T$ and surface currents

587 We explore the regional variations of thermal forcing ( $\Delta T$ ) and turbulent exchange ( $u_*$ ) on  
588  $w_b$  using the 30-day averaged values from the end of each simulation to calculate  $\Delta T$  and  $|u|$ .  
589 Note that  $w_b$  in the 30-day averaged model output is based on the average of instantaneous  
590 heat fluxes and, therefore, includes the model's knowledge of covariances between  $\Delta T$  and  
591  $|u|$  on much shorter time scales. In contrast,  $|u|$  is calculated from 30-day averaged u- and v-

592 | velocity components. We use a linear combination of non-tidal and tidal currents,  $\mathbf{U}$ , given  
593 | by

594

$$595 \quad \mathbf{U} = |\mathbf{u}|_{\text{tide}} + |\mathbf{u}| \text{ [m s}^{-1}\text{]}, \quad (6)$$

596

597 | where  $|\mathbf{u}|_{\text{tide}}$  is from Eq. (5), to represent the local forcing for turbulent exchange. For the no-  
598 | tides cases,  $|\mathbf{u}|_{\text{tide}}$  is zero and  $\mathbf{U}_{\text{no tides}} = |\mathbf{u}|$ . We include  $|\mathbf{u}|_{\text{tide}}$  in the tide-forced cases to more  
599 | closely approximate the non-time-averaged relationship described by Eq. (1), because the  
600 | 30-day average removes the tidal signal in  $\Delta T$  and  $|\mathbf{u}|$  in the tide-forced cases.

601 | Comparisons of the six base simulations show that  $w_b$  generally follows the expected  
602 | functional dependence on  $\Delta T$  and  $\mathbf{U}$  (**Fig. 12a**): in all six cases, values of  $w_b$  increase with  
603 | stronger currents and more thermal forcing, with values roughly falling along lines of  
604 | constant  $\Delta T \cdot \mathbf{U}$ . In general, our values are in range of those shown in Holland et al. (2008),  
605 | (compare their Fig. 1 with our Fig. 12b), although regional differences can be seen in the  
606 | bivariate relationships between  $w_b$  and either  $\Delta T$  or  $\mathbf{U}$  (**Fig. 12b and 12c**). Most ice-stream  
607 | inlet averages show a similar increase in  $w_b$  with respect to  $\Delta T$  (**Fig. 12b**), suggesting that  
608 | reasonable estimates of melt rate in the ice-stream inlets could be obtained from variability  
609 | of  $\Delta T$  and a constant, assumed low, value of  $\mathbf{U}$ . South Channel and, to some degree, Institute  
610 | inlet diverge from this relationship, demonstrating a larger variability in  $w_b$  in relation to  $\Delta T$   
611 | than is seen in other inlets (**Fig. 12b**). This larger variability in  $w_b$  in South Channel arises  
612 | because changes in modeled melt in this area are controlled primarily by changes in  $\mathbf{U}$  (**Fig.**  
613 | **12b**).

614 | Comparisons of the ratios for  $\Delta T$ ,  $\mathbf{U}$ , and  $w_b$  at each site between simulations without  
615 | and with tides (**Fig. 12d-f**) show how each region responds to the combined effects of tide-  
616 | induced changes in ocean conditions. With the exception of South Channel, adding tides  
617 | always cools (decreases  $\Delta T$ ) the upper layer of ocean water adjacent to the ice base (**Fig.**

618 **12d**). On average, the largest reductions occur for the RIS ice stream inlets. We attribute this  
619 result to cooling of water entering the RIS inlets by inclusion of meltwater from upstream  
620 freshwater sources, with RIS inlets being influenced by rapid melting in Support Force and  
621 Foundation inlets, and in South Channel (**Figs. 8 and 9**).

622 The differences between the tide-forced and no-tide cases show up more strongly in the  
623 regionally-averaged comparison of  $U$  (**Eq. (6), Fig. 12e**). In all regions, the effect of adding  
624 tides is greater for the cold standard cases than for warm standard cases. Since the value of  
625  $|u|_{\text{tide}}$  in **Eq. (5)** is the same for the standard geometry runs, this difference represents the  
626 increase in the thermohaline-driven  $|u|$  from the cold to warm cases.

627 The largest differences in  $|u|$  amongst all three model runs are in Möller, South Channel,  
628 and Institute inlets. For the warm cases, modifying the geometry increases the ratio of  $U_{\text{tide-}}$   
629  $\text{forced} / U_{\text{no tides}}$  for these three regions even though tidal currents decrease (**Fig. 3**) as  $wct$   
630 increases. This response implies that  $U_{\text{no tides}}$  also declines in the modified geometry case. A  
631 decline in  $U_{\text{no tides}}$  in the modified geometry is consistent with a reduction in  $z_{\text{ice}}$  in the inlet  
632 regions, which would reduce the thermal forcing and, hence, reducing the ice pump  
633 circulation. If true, this feedback is an artefact of our model geometry, which excludes the  
634 possibility of deeper ice that could be exposed when the grounding line migrates due to the  
635 imposed thinning. Corollary evidence for this reduction in ice pump circulation is seen in the  
636 top row of **Fig. 9**.

637 The role of South Channel melt on cooling downstream ice stream inlets, its sensitivity  
638 to tides, and tidal sensitivity to changing  $z_{\text{ice}}$  suggest that reliable predictions of change in  
639 modeled  $w_b$  in the southern RIS ice streams for future climate scenarios depends on the  
640 correct representation of changes to South Channel geometry.

641 **4.3 Role of advection through South Channel**

642 As the maps of surface-layer dye tracers (**Fig. 8 and 9**) show, most water entering the FRIS  
643 cavity in our simulations flows southward under the FIS front and then circulates clockwise  
644 around the FIS and RIS grounding lines. A water parcel takes about two years to travel from  
645 the FIS front to the southwestern RIS region of Rutford inlet. During that time, each water  
646 parcel is subjected to mixing with meltwater, so that the properties of water entering each  
647 inlet depend on the processes along the entire upstream path. Meltwater produced along each  
648 flow path continues to circulate clockwise with the inflowing warmer and saltier water that  
649 originated north of the ice front; see, e.g., dye distribution representing meltwater from  
650 Foundation inlet (Fig. 8b).

651 Water near the ice base in South Channel contains significant freshwater contributions  
652 from Support Force and Foundation inlets, with a smaller contribution from Möller inlet  
653 (Fig. 9). ~~Since circulation in our simulations is driven only by thermohaline circulation~~  
654 ~~modified by tides, these pathways. Our model excludes the influences of wind-driven~~  
655 ~~circulation and sea-ice formation, so these dye distributions are qualitatively similar to those~~  
656 ~~shown by Holland et al. (2007).~~ A north-south transect across the western end of South  
657 Channel (Fig. 13), shows that all water within that transect is colder (and fresher; not shown)  
658 than  $\theta_{mit}$ ; i.e., some meltwater from upstream is present at all depths, with the path-  
659 integrated volume of added meltwater setting the buoyancy that drives stratification. Further,  
660 distributions of meltwater contributions from individual regional sources also vary in the  
661 vertical (Fig. 13). The standard geometry simulations show a core of open water dye along  
662 the bottom and northeastern slope of the trough under South Channel. Support Force dye is  
663 concentrated near the ice base, toward the southwestern end of the transect. Foundation dye  
664 appears in both the surface and deep model layers, concentrated on the southern side of  
665 South Channel (see, also, Fig. 8b). The bifurcation of Foundation dye in South Channel  
666 reflects two sources; one in which fairly pure inflow water melts ice in Foundation inlet and

667 | then flows directly into deeper portions of South Channel, and one stream that then  
668 | experiences further cooling and freshening near the ice base from interactions with the ice in  
669 | Möller inlet and South Channel to the east of the transect. As expected, South Channel dye  
670 | has the highest concentration in the surface waters of this transect.

671 |       The spatial pattern in dye distribution is fairly consistent between the warm and cold  
672 | standard geometry cases, although much more open water dye from north of the ice front is  
673 | present in the warm case. This quantitative difference is consistent with the overall  
674 | understanding that warmer  $\theta_{init}$  drives a stronger thermohaline circulation that enhances  
675 | cavity circulation and leads to a shorter residence time (**Fig. 9**).

676 |       More qualitative differences between simulations arise from the change in cavity shape.  
677 | Except for South Channel dye, the modified geometry shows more laterally uniform dye  
678 | concentrations across the channel. Dye distribution remains vertically stratified in all three  
679 | cases with the depth of the upper layer being similar in the standard warm and modified  
680 | warm cases. However, even though the averaged  $w_b$  in South Channel is similar between the  
681 | standard cold and modified warm cases (**Fig. 7**), the South Channel meltwater product does  
682 | not mix down as far in the modified warm case as it does in the standard cold case (**Fig. 13**),  
683 | which we attribute to the much weaker tidal currents in this region (**Fig. 3**) for modified  
684 | geometry.

685 |       Transects for dye tracers are only provided for the tide-forced cases. However, a  
686 | comparison of temperature transects for the no-tides and tide-forced cases (**Fig. 13**) show  
687 | that the thermocline is deeper in the standard geometry tide-forced cases, with the  
688 | thermocline most affected in the standard cold case. As shown in **Fig. 12d**, tides increase the  
689 | thermal forcing in South Channel in the standard geometry by a factor of  $\sim 3$  while having a  
690 | negligible effect on  $\Delta T$  in the modified geometry. These results suggest that the lowered  
691 | thermocline in this region is caused by tide-induced mixing rather than advection, so that its  
692 | depth responds to the reduced tidal currents in the modified warm case.

#### 693 4.4 Implications of regional melt on ice sheet mass balance

694 Walker et al. (2008) showed that the spatial distribution of ice shelf melt rates was critical to  
695 the behavior of the buttressed grounded-ice streams; for the same integrated mass loss from  
696 an ice shelf, grounded-ice loss was significantly faster when the melting was concentrated  
697 near the grounding line. Gagliardini et al. (2010) confirmed this analysis and also noted that  
698 a grounded-ice stream could thicken, and its grounding line could advance even when net  
699 melting increased, if the melt rate decreased near the grounding line. In the context of our  
700 study the implication is that, even when the change in the ice-shelf area-averaged melt rate is  
701 small, substantial variability in melt rates near ice-stream grounding lines could still have a  
702 large impact on loss (or gain) of grounded ice.

703 In addition to being affected by the spatial distribution of  $w_b$ , dynamic mass loss of  
704 grounded ice is also affected by bedrock slope and ice sheet topography. These factors  
705 introduce additional spatial heterogeneity in the influence of basal melting on overall mass  
706 loss from the grounded ice streams flowing into FRIS. Wright et al. (2014) used the  
707 BISICLES ice sheet model to test the sensitivity of the grounded ice sheet to changes in  
708 FRIS mass loss at the grounding line. They found that Institute and Möller ice streams are  
709 the most sensitive to changes in basal mass balance that might be caused by a warming  
710 ocean inflow. This result was confirmed by Martin et al. (2015) using the Parallel Ice Sheet  
711 Model (PISM). These two ice streams rest on top of steep reverse bed slopes with low basal  
712 roughness, conditions which have been shown to contribute to grounding line instability and  
713 retreat (Schoof, 2007). Furthermore, these ice streams are also sensitive to changes in the  
714 buttressing effect from ice shelf mass change around Henry and Korff ice rises and the  
715 associated change in basal sliding over these ice rises. Our results indicate that tides  
716 currently exert a strong influence on basal mass balance in the area around Henry and Korff  
717 ice rises (**Fig. 5**), by increasing melting in South Channel and increasing marine ice  
718 accretion north of the ice rises and Doake Ice Rumples.

719 Möller and Institute are among the lowest meltwater producing regions (**Fig. 7**) and  
720 receive the largest fraction of meltwater product from Foundation inlet basal melt (**Fig. 10**).  
721 The relative quantities of these meltwater products are sensitive to changes in advection and  
722 mixing imposed by changes in  $\theta_{init}$  and geometry (**Sec. 3.5**). As shown in **Fig. 7**, the 0.5°C  
723 increase in  $\theta_{init}$  increases the Möller grounding-line region  $w_b$  to 1.03 m a<sup>-1</sup> (an increase of  
724 134%) and Institute grounding-line region  $w_b$  to 1.30 m a<sup>-1</sup> (an increase of 100%), for the  
725 tide-forced cases. The grounding lines in these regions appear to be very sensitive to changes  
726 in  $\theta_{init}$  and less sensitive to changes in the cavity ocean circulation imposed by a change in  
727 model geometry. Even with Möller and Institute’s sensitivity to  $\theta_{init}$ , however, these inlets  
728 are buffered from variations in open ocean heat due to the combined influence of circulation  
729 pathways and inflowing meltwater derivatives (**Fig. 10**).

730 Of the nine grounding-line regions explored in this study, Foundation inlet has the  
731 highest averaged melt rate of 2.76 m a<sup>-1</sup> for the standard cold case (**Fig. 7**), a rate which  
732 more than doubles to 6.01 m a<sup>-1</sup> when  $\theta_{init}$  increases from -1.9°C to -1.4°C. However,  
733 grounded-ice mass flux from Foundation Ice Stream is less sensitive to changes in basal  
734 melting than Möller and Institute (Wright et al., 2014). According to the results presented in  
735 Wright et al. (2014), even the higher melt rate with the warmed ocean in our study is  
736 insufficient to drive grounding line retreat and significant acceleration of grounded-ice loss  
737 through Foundation inlet. Therefore, it is possible that the dominant effect on the grounded-  
738 ice mass budget of large  $w_b$  at Foundation is through the effect of Foundation inlet meltwater  
739 on downstream inlets, particularly Möller. As shown in the dye results presented in **Sect.**  
740 **3.5**, Möller is somewhat isolated from FIS inflow but flooded by Foundation meltwater.

#### 741 4.5 Implications of regional freeze conditions on ice sheet mass balance

742 As described in Sect. 3.2.1 and Sect. 3.2.2, refreezing occurs in our simulations throughout a  
743 large region of the central RIS. Refreezing in this region is qualitatively consistent with

744 estimates of basal mass balance from satellite-based remote sensing (e.g., Joughin and  
745 Padman, 2003; Rignot et al., 2013; Moholdt et al., 2014). The extent of freezing conditions  
746 is important because marine ice accretion supports ice shelf stability through its effect on the  
747 mechanical properties of ice (Kulesa et al., 2014; McGrath et al., 2014; Li et al., submitted)  
748 and by altering the extent of grounding on topographic highs such as ice rises and rumples.

749 Our standard cold tide-forced case produces local maxima in marine ice growth rates in  
750 the northwestern RIS, the region northeast and east of Korff Ice Rise, and the region to the  
751 north and west of Henry Ice Rise (Fig. 5d). These regions of freezing are broadly consistent  
752 in all our model runs (Fig. 5) and the net mass increase in refreezing regions are increased  
753 when tide forcing is added (Fig. 6). Our standard cold tide-forced case has roughly four  
754 times more mass gain than the standard cold no-tides case, generally consistent with  
755 Makinson et al. (2011). In both warm cases, standard and modified geometry, adding tides  
756 increases net marine ice formation by a factor of two. That is, tides will continue to be  
757 important for marine ice accretion beneath FRIS if ocean temperatures rise as predicted by  
758 Hellmer et al. (2012, 2017) and will, therefore, continue to play a role in FRIS ice shelf  
759 stability.

## 760 **5 Conclusions**

761 The idealized modeling results presented here on the basal melting of FRIS, combined with  
762 ice-sheet model results reported by Wright et al. (2014), indicate that the response of the  
763 Antarctic Ice Sheet in the Weddell Sea sector to large-scale ocean circulation changes  
764 depends on several regional and local processes that combine to determine ocean state in  
765 individual ice-stream inlets. These processes include the tidal contribution to ocean mixing,  
766 advection of meltwater products into downstream inlets, and feedbacks between advection,  
767 tides and melting as ice shelf draft evolves.

768 In general, tides increase the area-integrated mass loss from the entire FRIS, consistent  
769 with the findings of Makinson et al. (2011); however, for our cold case ocean representing  
770 the modern state, increased basal melting with tides is completely offset by a factor-of-four  
771 increase in freezing (marine ice formation) in the central Ronne Ice Shelf.

772 As proposed by Hellmer et al. (2012), warming of water entering the cavity under FRIS,  
773 primarily as an inflow under the FIS front, leads to a large increase in ice-shelf-integrated  
774 mass loss. In our simulations, warming of 0.5°C increased total FRIS mass loss by a factor  
775 of ~3.6 for the no-tides simulations (cf. Hellmer et al., 2012) and by a factor of ~5.1 when  
776 tidal forcing was included.

777 The large-scale sub-ice-shelf circulation in our idealized model is dominated by a  
778 southward inflow of open-ocean water across the Filchner Ice Shelf front, and clockwise  
779 circulation of this water along the southern grounding line. This clockwise sub-ice-shelf  
780 circulation is, in part, a consequence of our simplified model forcing, which excludes some  
781 inflows that would be forced by realistic spatial and seasonal variability in the open ocean  
782 north of the ice shelf. Under this circulation regime, a water parcel takes about two years to  
783 travel from the Filchner ice front to the southwestern Ronne Ice Shelf.

784 At the regional scale, complex feedbacks occur between local processes such as tide-  
785 induced mixing and advection, so that the temperature of a water parcel represents the  
786 upstream integrated history of mixing between the inflowing source water and basal  
787 meltwater. The temperature of the upper ocean layer adjacent to the ice shelf base is cooler  
788 when tide forcing is included, especially in the southwestern Ronne ice stream inlets  
789 (Rutford, Carlson and Evans). We attribute this cooling to incorporation of meltwater from  
790 upstream sources, notably Foundation inlet and South Channel.

791 Our results show regionally variable responses to changes in tides,  $\theta_{init}$ , and cavity  
792 geometry that can be summarized as follows.

- 793 (1) Meltwater plumes from basal melting introduce non-local feedbacks, within the  
794 same cavity, in response to variations of inflowing ocean heat and melt-induced  
795 changes in ice draft.
- 796 (2) Adding tide forcing to models increases  $w_b$  under the FIS and portions of the  
797 RIS, with the largest increase within South Channel.
- 798 (3) Adding tide forcing increases integrated marine ice formation for all three cases  
799 including the two warm cases. The tidal contribution to ice-shelf dynamics will  
800 persist through future ocean warming of at least 0.5°C and may increase ice  
801 sheet grounding and associated contact stresses in the region near Henry and  
802 Korff ice rises and Doake Ice Rumples.
- 803 (4) In some regions (e.g. South Channel), tides influence  $w_b$  directly by changing  
804 the friction velocity; in other regions (e.g., Rutford), tides influence meltwater  
805 production through changes in  $\theta$  by mixing along the upstream flow path. ~~Tides~~  
806 ~~affect how  $w_b$  changes in response to  $\theta_{\text{mix}}$  and cavity geometry by these direct~~  
807 ~~and indirect influences.~~
- 808 (5) The greatest fraction of meltwater in the Möller and Institute inlets are  
809 contributed by basal melting in Foundation inlet, indicating that increased  
810 meltwater production in one inlet may reduce melting in a downstream inlet.
- 811 The regional distributions of meltwater and  $w_b$  are sensitive to the accuracy of our grids  
812 of seabed depth and  $w_{ct}$ , which are based on few passive seismic measurements in regions  
813 of strong model sensitivity (**Fig. 3f**). Distributions are also affected by the model  
814 configuration, including neglect of atmospheric and sea-ice forcing, the choice of mixing  
815 schemes and the thermodynamic exchange coefficients for the ice-ocean boundary layer  
816 parameterization. Nevertheless, our analysis shows that the interplay of tides, far-field  
817 thermal forcing and the oceanic response to ice shelf geometry changes leads to complex

818 and sometimes non-local interactions that alter the overall basal mass balance that effects  
819 melting near the grounding lines, thereby controlling the dynamical response of adjacent  
820 grounded ice streams.

821 Estimates of the future mass loss through the ice streams draining the West Antarctic  
822 Ice Sheet into Ronne Ice Shelf, in climate scenarios where the heat flux into the cavity under  
823 FRIS increases, are sensitive to how the ice draft in South Channel evolves. Under modern  
824 conditions and with the seabed and ice draft represented by the RTOPO-1 database, tides are  
825 a critical contributor to basal melting in that region. A warmer ocean will increase mass loss  
826 by basal melting that will lead to ice shelf thinning unless it is offset by increased inputs  
827 from ice advection and snowfall. However, this thinning then causes regional feedbacks that  
828 include a reduction in basal melting in South Channel, as tidal currents weaken, a change in  
829 circulation pathways with consequences for heat and meltwater transport and, possibly, a  
830 dynamic response of the grounded ice that may offset ocean-driven thinning of the ice shelf.

831 We conclude that it is not possible to predict the true effect of oceanic warming on ice  
832 thinning near individual ice stream grounding lines without a better understanding of the  
833 feedbacks introduced by tidal forcing and circulation as a result of changes in *w<sub>ct</sub>*. That is, as  
834 coupled ocean/ice-sheet models become a standard tool for projecting ice sheet response to  
835 changing climate, tides must be either explicitly modeled, or represented by a  
836 parameterization that itself can evolve with time at a rate set by the evolution of the cavity.  
837 Furthermore, potential bottlenecks in sub-ice-shelf circulation of ocean heat must be  
838 identified through improved surveys of seabed bathymetry which, when combined with the  
839 better-known ice shelf draft, determines both the tidal current speeds and the mean ocean  
840 circulation towards downstream sites including ice-stream inlets. While FRIS is presently in  
841 approximate steady state, the potential for future ocean warming, increased *w<sub>b</sub>*, and a  
842 corresponding mass loss causing a ~1 m sea-level rise supports the need to augment

843 | measurements of the seabed bathymetry [beneath FRIS, particularly within](#) the ice stream  
844 | inlet [regions](#) and under South Channel.

#### 845 | **Author contribution**

846 | R.D.M. led the study. The simulations were designed by R.D.M. and L.P., implemented by  
847 | R.D.M. and S.L.H., and analyzed by R.D.M., L.P. and T.H. The paper was written  
848 | by R.D.M., L.P. and T.H.

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**Table 1** An overview of the eight model runs presented in this paper and the case name that is used to reference them. The three runs that were used as the spin-up solutions to initialize other runs are marked and referenced as b1, b2, and b3. The four runs that include passive dye tracers are shaded in grey. All run intervals provide steady state solutions as determined by the transient solutions of shelf-averaged basal melt.

#	Case Name	Run length	Averaged output period	Cavity geometry	$\theta_{init}$ (°C)	min $z_{ice}$ (m)	max $z_{ice}$ (m)	min $wct$ (m)	max $wct$ (m)
1	standard cold tide-forced	20-years	30-day	present-day	-1.9	-11	-1537	50	1210
2	standard cold no-tides	10-years	30-day	present-day	-1.9	“	“	“	“
3	standard warm tide-forced	20-years	30-day	present-day	-1.4	“	“	“	“
4	standard warm no-tides	10-years	30-day	present-day	-1.4	“	“	“	“
5	standard tides-only	30-days	2-hour	present-day	NA	“	“	“	“
6	standard cold dye (restart #1)	2-year	30-day	present-day	-1.9	“	“	“	“
8	standard warm dye (restart #3)	2-year	30-day	present-day	-1.4	“	“	“	“
9	modified warm tide-forced	20-year	30-day	melt-adjusted	-1.4	-25	-1442	52	1180
10	modified warm no-tides	10-year	30-day	melt-adjusted	-1.4	“	“	“	“
11	modified tides-only	30-days	2-hour	melt-adjusted	NA	“	“	“	“
12	modified warm dye (restart #9)	2-year	30-day	melt-adjusted	-1.4	“	“	“	“

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1104 **Table 2 Values for integrated mass transport ( $M_b$ , Gt a<sup>-1</sup>) and FRIS-averaged basal melt rate ( $w_b$ , m a<sup>-1</sup>) for**  
 1105 **runs shown in Fig. 6: Standard cold no-tides (S -1.9 ☉), Standard cold tides-forced (S -1.9), Standard warm r**  
 1106 **(S -1.4 ☉), Standard warm tides-forced (S -1.4), Modified warm no-tides (M -1.4 ☉), Modified warm tides**  
 1107 **(M -1.4).**

		S -1.9 ☉	S -1.9	S -1.4 ☉	S -1.4	M -1.4 ☉	M -1.4
$M_b$ (Gt a <sup>-1</sup> )	Net	48	47	171	239	188	221
	Melt	62	104	182	262	200	246
	Freeze	-14	-57	-11	-23	-12	-25
$w_b$ (ma <sup>-1</sup> )	Net	0.14	0.14	0.49	0.69	0.54	0.63
	Melt	0.27	0.46	0.66	0.95	0.69	0.86
	Freeze	-0.12	-0.44	-0.14	-0.29	-0.20	-0.37

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1110 **Table 3 Publication sources and abbreviations used in Fig. 3. Method of calculating melt rates is summarized as Ocean Model (OM), Standard Glaciological Method**  
 1111 **(GM), Ocean Observation (OO), Geophysical Tracer (GT), following the nomenclature used in Table S2 of Rignot et al. (2013) supplementary document. The time**  
 1112 **period of observation(s) or forcing files are listed together with source of data or model output.**

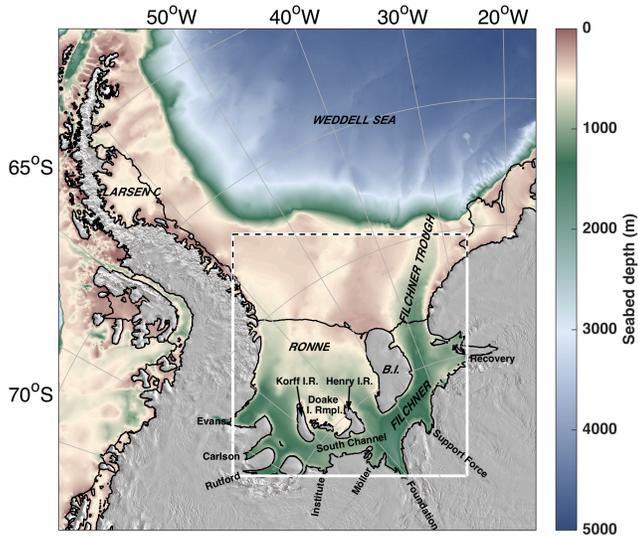
Pub. Abbr.	method	reference	time period	estimate source
TS	OM	this study	NA	numerical model
M14	GM	Moholdt et al. (2014)	2003-2009	
R13	GM	Rignot et al. (2013)	2003-2009	ICESat
			2007-2008	ALOS PALSAR
				InSAR
			1979-2010	RACMO2
				Operation IceBridge
				BEDMAP
D13	GM	Depoorter et al. (2013)	2003-2009	ICESat
			1994-2002	ERS-1
			2007-2009	ERS-2
			2007-2009	InSAR
			1979-2010	RACMO2
T12	OM	Timmermann et al. (2012)	1958-2010	FESOM model, NCEP winds (1958-2010)
M11	OM	Makinson et al. (2011)	NA	
M14	OM	Moholdt et al. (2014)	1979-2007	NCEP 10 m winds

				2-m air temperature
				specific humidity
				cloudiness
				and net precipitation
JP03	GM	Joughin and Padman (2003)	1997	RADARSAT InSAR
N03	OO	Nicholls et al. (2003)	1995-1999	CTD
F01	OO	Foldvik et al. (2001)	1992-1993	CTD & mooring
G99	OM	Gerdes et al. (1999)	NA	
G94	GT	Gammelsrød et al. (1994)	Feb. 1993	CFC-11, CFC-12, O <sub>2</sub> , Si
J92	GM	Jacobs et al. (1992)		
JD91	GM	Jenkins (1991)	1985-1988	Radar echo sounding
S90	GT	Schlosser et al. (1990)	Jan-Mar. 1985	$\delta_{18}\text{O}$ , He

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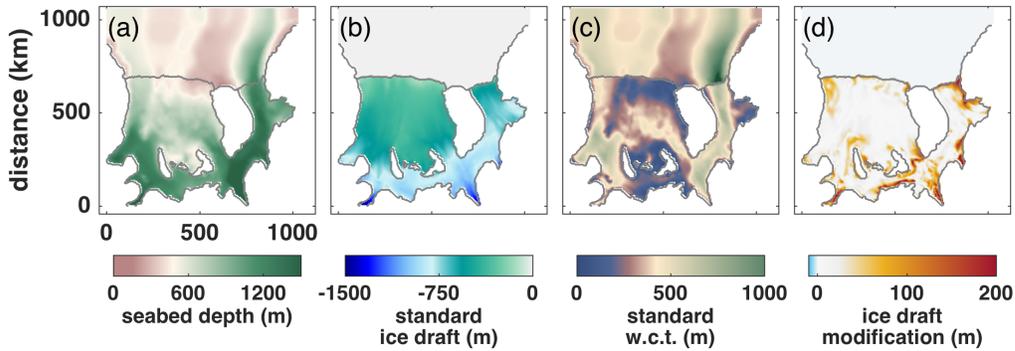
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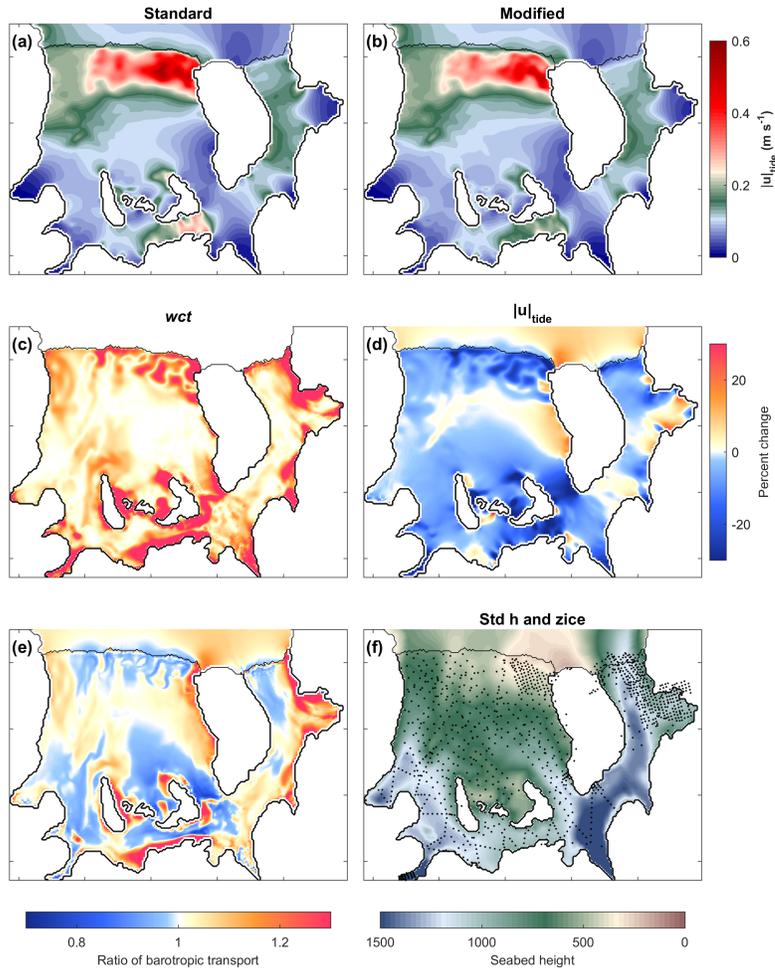
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1117 Figure 1: Weddell Sea region of study with model domain outlined by white box. Dashed black lines highlight the  
 1118 open boundaries. The labels on land indicate the names of the tributary glaciers used for regional analyses in this  
 1119 study. Black lines over seabed indicate the extend of the ice shelf and black lines around the grey mask indicate the  
 1120 ice sheet grounding line and/or transition between ocean and land.



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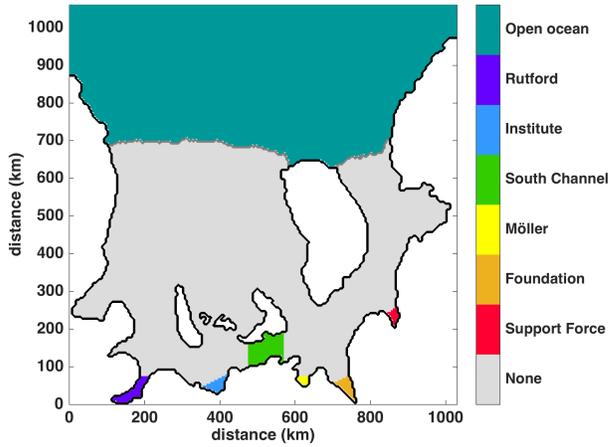
1122 Figure 2: Bathymetry ( $h$ ) and ice draft ( $z_{ice}$ ) for the standard and modified geometries: (a)  $h$  for both the standard  
 1123 and modified cases; (b)  $z_{ice}$  for the standard case; (c)  $w.c.t.$  for the standard case; (d) Difference between standard  $z_{ice}$   
 1124 and modified  $z_{ice}$ , where difference  $> 0$  indicates regions of melting and a corresponding decrease in  $z_{ice}$  in the  
 1125 modified geometry when compared to the standard geometry.



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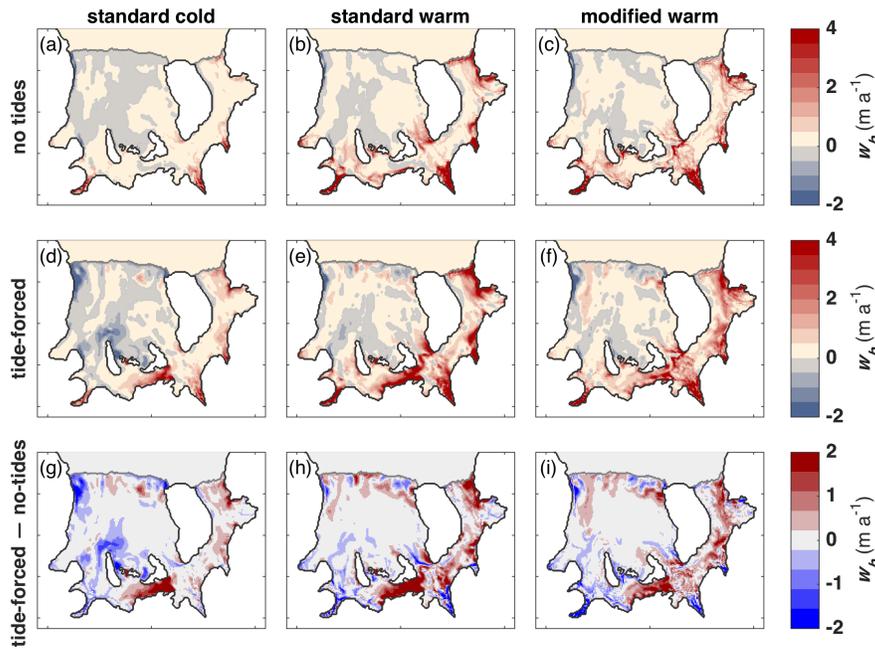
1127 | Figure 3: (a) Barotropic current ( $|u|_{tides}$  Eq. (5)) for the standard tides-only run. (b) Same as (a) but for the modified  
 1128 | tides-only run. (c) Percent change in  $wct$  between the standard and modified cases with positive values indicating  
 1129 | where the  $wct$  is greater in the modified geometry. (d) Change in  $|u|_{tide}$  between (a) and (b) where Percent change  $> 0$   
 1130 | indicates locations where the standard case  $|u|_{tide}$  is greater than the modified case  $|u|_{tide}$ . (e) Ratio of barotropic tidal  
 1131 | transport ( $wct \times |u|_{tide}$ ) shown here as modified/standard, with values  $> 0$  showing where there is increased  
 1132 | transport for the modified case. (f) Seabed depth (as in Figure 2a) with existing seismic observation locations shown  
 1133 | as black dots.

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1136 | Figure 4: Locations of the six, continuous, modeled meltwater dye releases and the open ocean bulk dye explained in  
 1137 | Sec. 2.3.3.

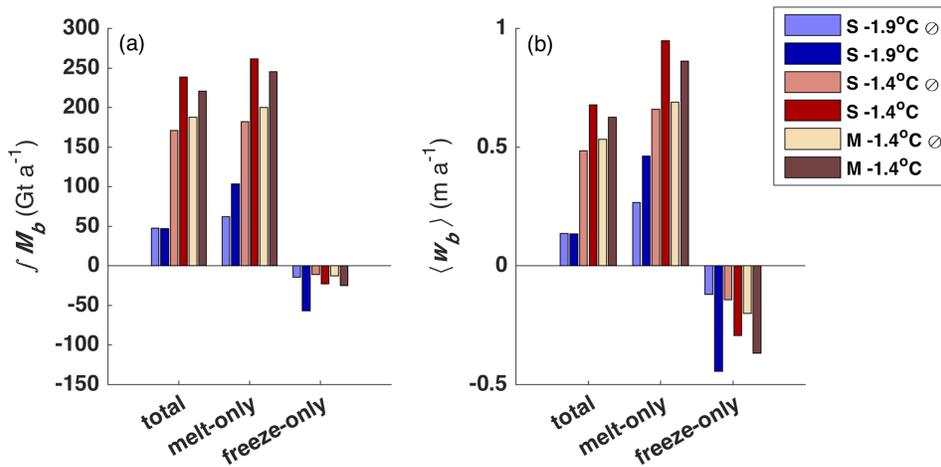


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1139 | Figure 5: Melt rates averaged over 1-year of steady state solutions for (top) no tides runs, (middle) tide-forced runs,  
 1140 | and (bottom) the difference between the tide-forced and no-tides melt solutions. Positive values in the bottom  
 1141 | subplots show where there is more basal melting in the solutions that include tidal forcing (middle subplots). The left

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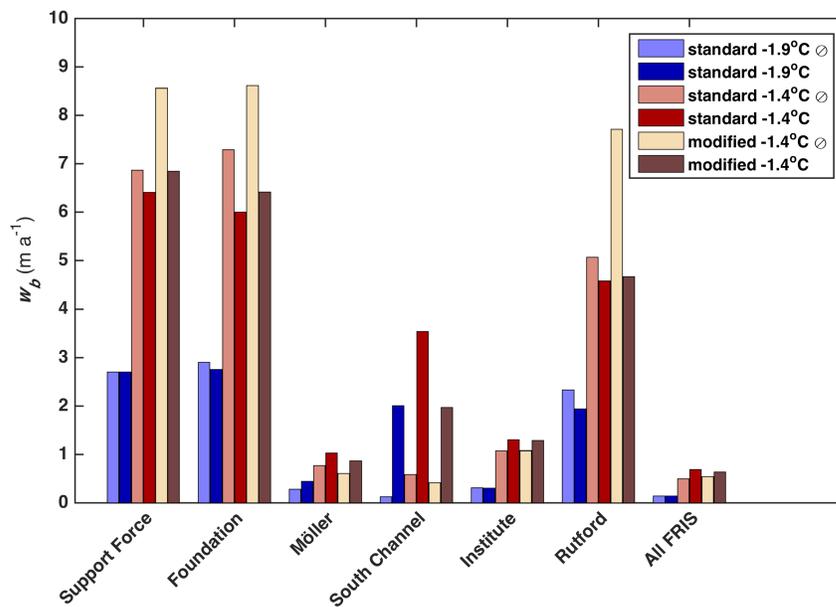
column (a, d, g) shows results for the standard cold case; the middle column (b, e, h) shows results for the standard warm case; and the right column (c, f, i) shows results for the modified warm case.



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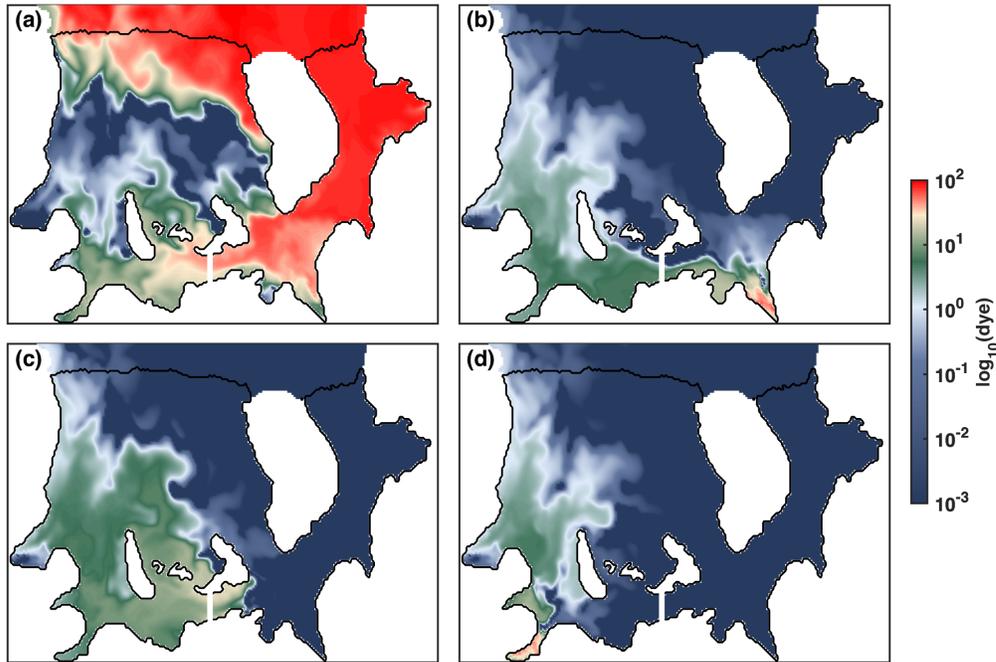
Figure 6: (a) integrated mass flux over “total” FRIS area, “melt-only” regions, and “freeze-only” regions for both no-tide (⊙) and tide-forced cases. (b) Same regions and runs as in (a) but showing FRIS-averaged basal melting.



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Figure 7: Melt rates averaged over last 12 months of steady state solutions in the standard cold, standard warm, and modified warm cases for some of the regions shown in Fig. 4 and for both no-tides (⊙) and tide-forced simulations. “All FRIS” duplicates the information shown by “total” in Fig. 6b.



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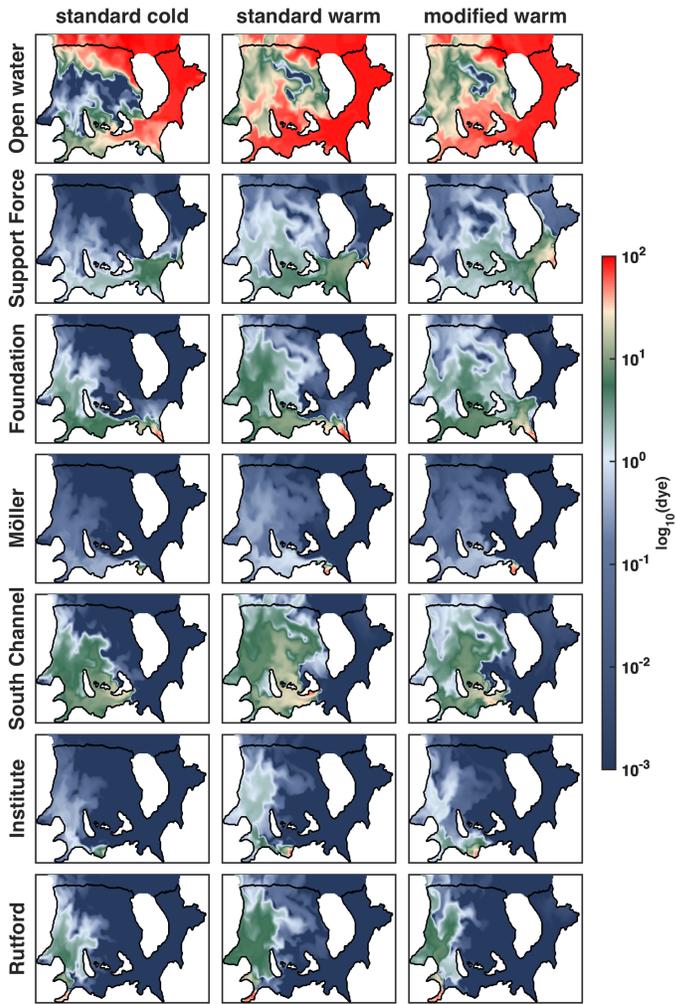
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Figure 8: Distribution of dye concentration from the last time step and the upper model layer of the standard cold, tide-forced case described in Sect. 2.3.3. These distributions are from 2-years after the initiation of model dye releases following 20-year of model circulation spin-up time. (a) bulk dye representing penetration of water initially north of the FRIS ice front. (b-d) meltwater dyes with sources in Foundation, South Channel, and Rutford regions, respectively (see Fig. 4 for dye release regions). The white line across South Channel represents the location of the transects in Fig. 13.



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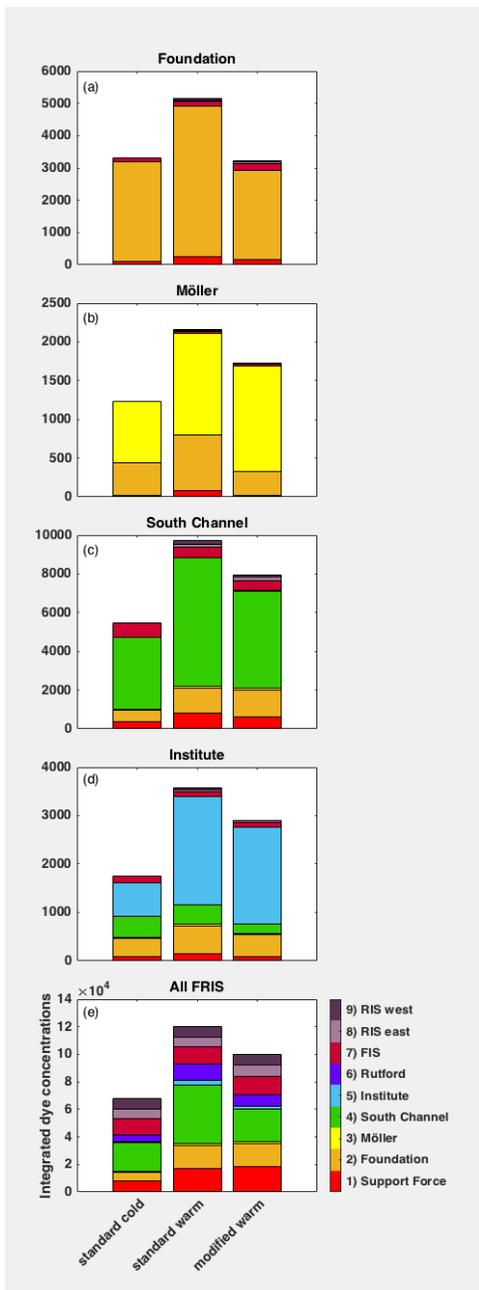
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Figure 9: An expanded distribution of dye concentration than that shown in Fig. 8 to include all meltwater dyes in the three tide-forced base simulations. As in Fig. 8, dye concentrations are from the last 30-day average of upper model layer solutions from the runs described in Sect. 2.3.3. **These distributions are from 2-years after initializing dye release following 20-years of model circulation spin-up time.** The left hand column of this graphic includes the same four regional plots as shown in Fig. 8.

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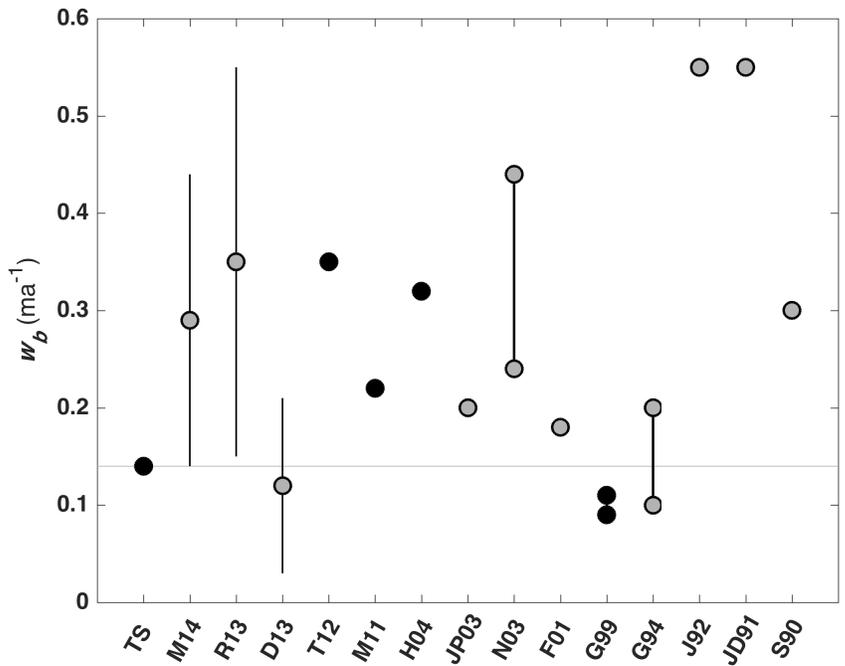
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Figure 10 Integrated meltwater dye (Sect. 2.3.3) by region for the tide-forced, base simulations, showing: (a) Foundation region, (b) Möller region, (c) South Channel region, (d) InSTITUTE region, and (e) all of FRIS. Regions are shown in Fig. 4.



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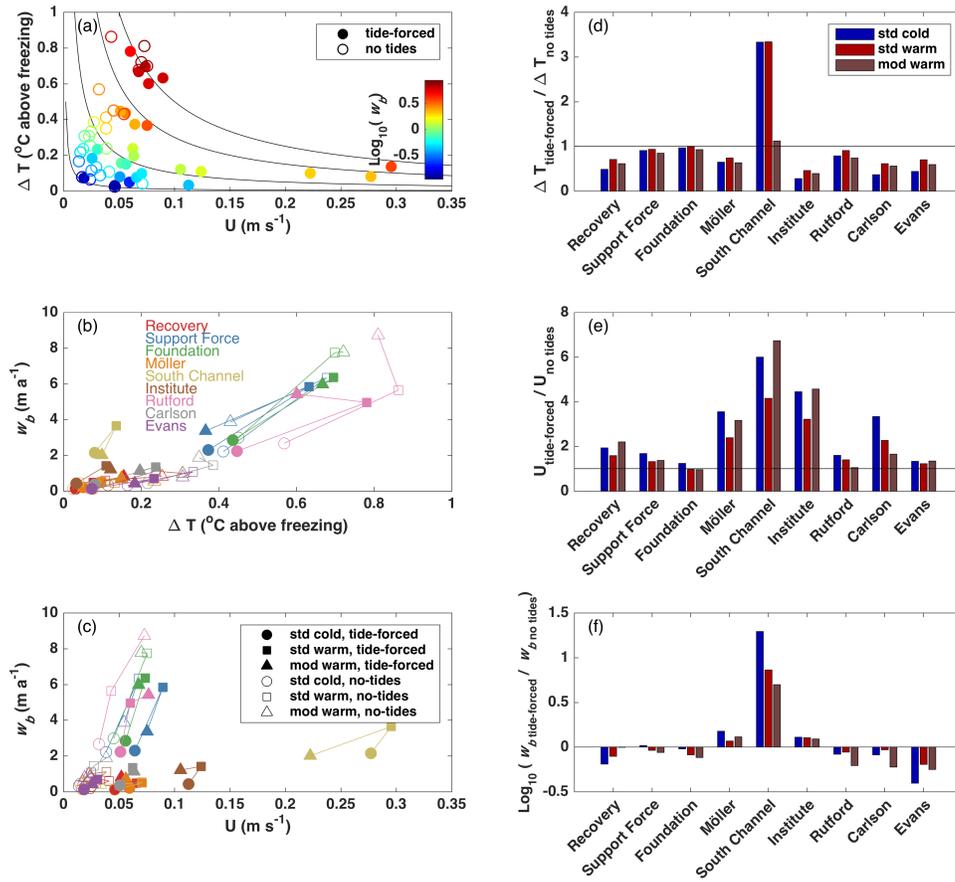
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Figure 11 FRIS-averaged basal melt rate comparison between this study [TS] and others. Model results are shown as black dots while observations are shown as grey dots. Error bars for remote sensing observations are shown as black lines for M14 (Moholdt et al., 2014), R13 (Rignot et al., 2013) and D13 (Depoorter et al., 2013). Min and max values are connected by thick, solid, black lines to show the range of values reported by N03 (Nicholls et al., 2003) and G94 (Gammelsrød et al., 1994). A summary of the studies presented here and their abbreviations is provided in Table 2.



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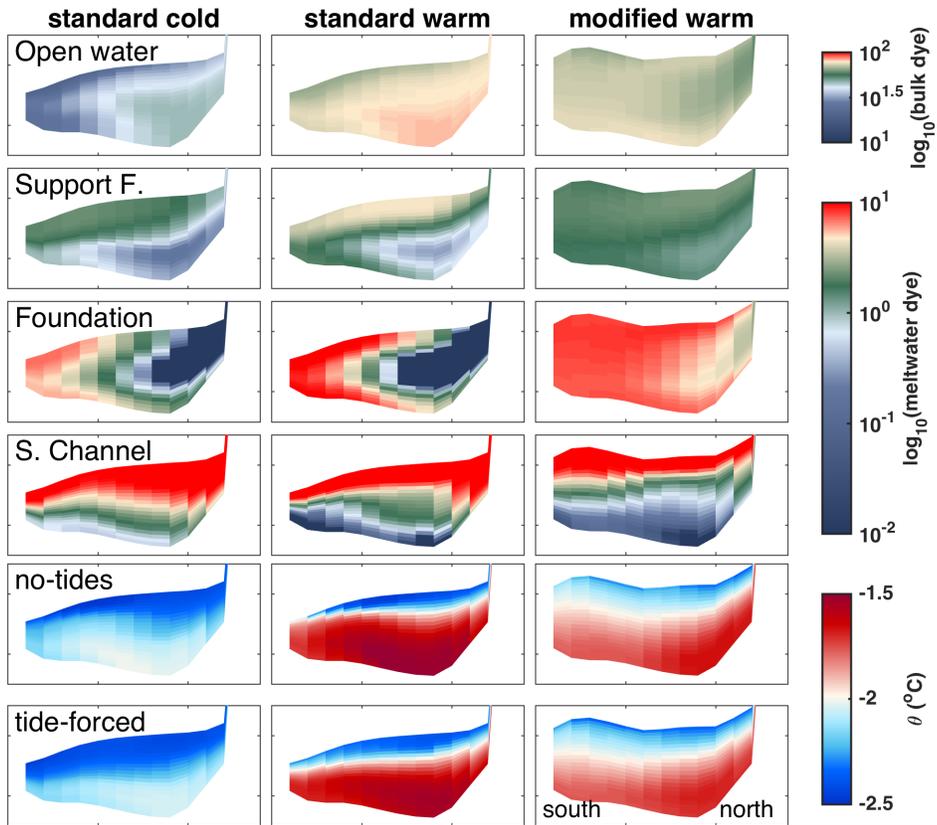
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Figure 12: Regional influences of  $\Delta T$  and current speed on melt rates. Tide-forced cases are plotted using solid marker style, e.g. “■”, and no-tide cases are plotted using open marker style, e.g. “□”. (a) Current speed ( $U$ , Eq. (6)) vs. thermal forcing ( $\Delta T$ ), color-coded according to melt rate ( $w_b$ ). Black contours follow  $\Delta T = c/U$  (with  $c$  being a set of different scalars), along which constant values of  $w_b$  (as in Sect. 3.2) are expected to be found. (b)  $\Delta T$  vs.  $w_b$  for each region. (c)  $U$  vs.  $w_b$  for each region. (d)  $\Delta T$  difference between no-tides and tide-forced cases such that positive values show where thermal forcing is stronger in the no-tides cases, (e) current speed difference between tide-forced ( $U_{\text{tides}}$ ) and no-tides ( $U_{\text{no tides}}$ ) cases, and (f)  $w_b$  difference between tide-forced and no-tides cases.



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Figure 13: Transects of dyes (upper four rows) and potential temperature ( $\theta$ , lower two rows) across South Channel at the western tip of Henry Ice Rise. The upper four panels are for tide-forced runs only. Transect location is shown in Fig. 8.