



1 **A simple equation for the surface-elevation feedback of ice**
2 **sheets**

3 A. Levermann^{1,2,3*} & R. Winkelmann^{1,3}

4 ¹*Potsdam Institute for Climate Impact Research, Potsdam, Germany.*

5 ²*LDEO, Columbia University, NY, USA.*

6 ³*Institute of Physics, Potsdam University, Potsdam, Germany.*

7 *Correspondence to: anders.levermann@pik-potsdam.de



8 **Abstract:**

9 In recent decades, the Greenland Ice Sheet is been losing mass and thereby contributed to global
10 sea-level rise. The ice loss is likely to increase under future warming. Beyond a critical
11 temperature threshold, a meltdown of the Greenland Ice Sheet is induced by the self-enforcing
12 feedback between its lowering surface elevation and its increasing surface mass loss: The more
13 ice is lost, the lower the ice surface reaches into the atmosphere and the warmer the surrounding
14 air becomes which fosters melting and further ice loss. The rate of ice loss is highly relevant for
15 coastal protection worldwide. The computation of this rate so far relies on complex numerical
16 models as it should be. In order to contribute a little to the conceptual understanding, we derive
17 here a simple equation for the self-enforcing feedback and use it to estimate the melt time for
18 different levels of warming using three observable characteristics of the ice sheet itself and its
19 surroundings. When the volume loss is dominated by the feedback, the resulting logarithmic
20 equation unifies existing numerical simulations and shows that the melt time depends critically
21 on the level of warming with a critical slowing-down near the threshold: The median time to lose
22 10% of the present-day ice volume varies between about 3500 years for a temperature level of
23 0.5°C above the threshold and 500 years for 5°C. Unless future observations show a significantly
24 higher melting sensitivity than currently observed, a complete melt down is unlikely within the
25 next 2000 years without significant ice-dynamical contributions.



26 **1. Introduction**

27 Anthropogenic climate warming by expanding ocean waters and melting ice is raising global sea
28 level (IPCC, 2013). Over the two past decades, the Greenland Ice Sheet has lost mass at an
29 accelerating pace (Bamber et al., 2000; Box et al., 2012; van den Broeke et al., 2009; Fettweis et
30 al., 2013; Mernild et al., 2011; Nick et al., 2009; Rignot et al., 2008, 2011; Shepherd and
31 Wingham, 2007; Thomas et al., 2011). The ice loss is likely to increase under unabated
32 greenhouse-gas emissions (Clark et al., 2016; Fettweis et al., 2013; Goelzer et al., 2012;
33 Graversen et al., 2011; Harper et al., 2012; Huybrechts et al., 2011; Levermann et al., 2013;
34 Nowicki et al., 2013; Price et al., 2011). Numerical simulations suggest that a decline of the
35 Greenland Ice Sheet is inevitable once its surface temperature permanently exceeds a certain
36 threshold (Charbit et al., 2008; Greve, n.d.; Huybrechts and Wolde, 1999; Huybrechts et al.,
37 2011; Ridley et al., 2005, 2010; Robinson et al., 2012; Solgaard and Langen, 2012). If and when
38 this temperature threshold is passed, depends critically on past and future greenhouse-gas
39 emissions (Fettweis et al., 2013; Goelzer et al., 2013; Gregory et al., 2004a; Rae et al., 2012).
40 Even if emissions were reduced to zero, temperatures would not drop significantly for thousands
41 of years because of the long life-time of anthropogenic CO₂ in the atmosphere and reduced
42 oceanic heat uptake if oceanic convection is extenuated (Allen et al., 2009; Solomon et al., 2009;
43 Zickfeld et al., 2013). This implies a possible commitment of a melt-down of the Greenland Ice
44 Sheet in the near future which would eventually raise global sea-level by more than 7 meters
45 (Howat et al., 2014b). Whether this occurs on a multi-centennial or rather a multi-millennial time
46 scale is of relevance for coastal planning. The framework that we provide here can also be used
47 to include new physical processes that might be discovered in the future, e.g. potential changes
48 in surface albedo through melting (Box et al., 2012) or aerosol-induced surface melt or the lack
49 thereof (Polashenski et al., 2015).

50 Here we first recap the Vialov profile and add a simple representation of the surface-elevation
51 feedback towards a governing equation for a steady-state ice-sheet in zero dimension (section 1),
52 then we derive the critical warming threshold for the existence of an ice sheet in this simple
53 model (section 2). In section 3 we derive a simple time-evolution equation for the decay of the
54 ice sheet after surface temperatures have exceeded the threshold. Finally we use observational
55 estimates of the three parameters that enter the model to estimate the decay time of the ice sheet



56 under melting above the threshold. Here solid ice discharge is neglected as well as any other ice
57 sheet dynamics (Andresen et al., 2012; Howat and Eddy, 2012; Moon et al., 2012; Nick et al.,
58 2009; Price et al., 2011; Straneo et al., 2011; Walsh et al., 2012).



59 2. Governing equation for shallow-ice steady states under surface-elevation feedback

60 A nonlinear threshold behavior is generally associated with a fundamental self-enforcing
61 feedback and thereby an associated system memory e.g. (Levermann et al., 2012). For the
62 Greenland Ice Sheet, such a feedback is given by the interaction between surface elevation and
63 surface melting (Weertman, 1961). For illustration, we include this feedback in a well-
64 established highly idealized ice-profile of an ice-sheet in one dimension, the so-called Vialov-
65 profile (Vialov, 1958). We introduce the surface-elevation feedback in the simplest possible way
66 by assuming that the surface melt rate depends linearly on the surface temperature and that the
67 temperature decreases linearly with the height of the ice surface following a constant
68 atmospheric lapse rate.

69 We consider a highly simplified flowline model for an isothermal ice sheet grounded on a flat
70 and rigid bed. The solution of the shallow-ice approximation in one dimension for the ice-sheet
71 elevation under these simplifying assumptions is called the Vialov-profile:

$$72 \tilde{h}(x) = h_m \left(1 - (x/L)^{(n+1)/n}\right)^{n/(2n+2)} \quad (1)$$

73 where h_m is the maximum surface elevation and n is Glen's flow law exponent (Glen, 1955).
74 The inherent assumption of isothermal ice is a strong simplification, but we do not aim for a
75 realistic representation of the ice flow but will derive a measure for the average height of the ice
76 sheet and its dependence on changes in the surface mass balance. The surface mass balance is
77 considered to be homogeneous at a value, a , which will later be considered dependent on the
78 surface elevation. The overall horizontal extension of the ice sheet is set to L , and it is thereby
79 assumed that any ice flow across this point is calved off into ice bergs. This situation represents a
80 confined ice-bearing bedrock topography as in most of Greenland's interior (Howat et al.,
81 2014a).

82 The mean surface elevation can then be computed to be

$$83 \bar{h} = L^{-1} \int_0^L dx h(x) = \omega \cdot h_m \quad (2)$$

84 It is proportional to the maximum surface elevation h_m with a proportionality factor

$$85 \omega \equiv \int_0^1 d\xi \left(1 - \xi^{(n+1)/n}\right)^{n/(2n+2)} \quad (3)$$



86 which only depends on the flow law exponent.

87 The maximum surface elevation is determined by the surface mass balance \tilde{a} and the ice softness
 88 \tilde{A}

$$89 \quad h_m = 2^{(n-1)/(2n+2)} \cdot L^{1/2} \cdot \left(\frac{(n+2)\tilde{a}}{(\rho g)^n \tilde{A}} \right)^{1/(2n+2)} \quad (4)$$

90 with ρ being the ice density and g the gravity constant. We normalize all three quantities by
 91 defining $h \equiv \omega \cdot h_m / \bar{h}_0$, $a \equiv \tilde{a} / a_0$ and $A \equiv \tilde{A} / A_0$ where a_0 is the accumulation rate on the
 92 ground, i.e., in the absence of an ice-sheet, and $A_0 = a_0 / \left((\rho g)^n (\varepsilon \cdot L)^{(n+1)} \right)$ with $\varepsilon = H/L$ being
 93 the typical height-to-width ratio. \bar{h}_0 is the equilibrium line of the considered ice sheet in the
 94 initial equilibrium situation. Values for a_0 , \bar{h}_0 and L are later chosen to resemble the conditions
 95 of the Greenland Ice Sheet.

96 The non-dimensional surface elevation, h , of the ice sheet can then be expressed as

$$97 \quad h = \left(\frac{a}{A} \right)^{1/m} \quad (5)$$

98 For the Vialov profile $m=2(n+1)$ where n denotes the Glen flow-law exponent observed to be
 99 around $n=3$ which yields $m=8$. We introduce the surface elevation feedback in its simplest form
 100 through a dependency of the surface melt rate on the surface elevation:

$$101 \quad a = a_0 + \gamma \Gamma \cdot h \quad (6)$$

102 with the atmospheric lapse rate $\Gamma > 0$. γ denotes the melting sensitivity of the ice surface, i.e. the
 103 increase in surface melt-rate per degree of warming, which is regularly measured and comprises
 104 a large number of physical processes (e.g. (Box, 2013)). For simplicity we rescale the surface
 105 mass balance by the constant ice softness parameter, A , which is considered to be constant. The
 106 steady state solution for the surface elevation of the ice-sheet is thus governed by the following
 107 equation

$$108 \quad h^m - \gamma \Gamma \cdot h - a_0 = 0 \quad (7)$$

109 which has two positive solutions for h as long as the surface mass balance on the ground is
 110 negative, i.e., $a_0 < 0$. Note that the surface mass balance can be positive even if $a_0 < 0$. If the



111 ice-sheet is in an unstable configuration, a slight perturbation will either cause it to converge into
112 the stable state with a positive surface mass balance or to melt-down completely.

113 Our simple approach qualitatively captures the basic hysteresis behavior of the Greenland Ice
114 Sheet caused by the surface-elevation feedback (Fig. 1): For a given surface temperature a stable
115 state of the ice sheet (red line) annihilates an external perturbation in surface elevation by
116 changes in surface mass balance (grey arrows). The unstable solution branch defines the basin of
117 attraction for the stable state. A surface elevation that is lower than the unstable solution branch
118 cannot be sustained. In that case the melting reduces the surface elevation to practically zero
119 even without further external perturbation (grey arrows). Beyond a certain surface temperature
120 threshold (vertical dotted line) no ice sheet can be sustained.



121 **3. Critical surface mass balance in steady state**

122 As illustrated in Fig. 1, there is a critical temperature above which the ice-sheet is not
123 sustainable. Let us denote the corresponding surface elevation by h_c . The critical point (T_c, h_c)
124 has to fulfill two conditions. First, it has to be a solution of the governing equation and second it
125 has to be a minimum of the function

126
$$F(h) = h^m - \gamma \Gamma \cdot h - a_0 \tag{8}$$

127 which we can determine by setting the derivative of F to zero.

128 Consequently,

129
$$h_c = \left(\frac{\Gamma \cdot \gamma}{m}\right)^{1/(m-1)} \tag{9}.$$

130 Inserting this into the governing equation yields the critical surface mass balance at the ground

131
$$a_{0c} = -(m - 1) \cdot \left(\frac{\Gamma \cdot \gamma}{m}\right)^{m/(m-1)} \tag{10}.$$

132 For illustrative purposes we have assumed a_0 to decline linearly with the surrounding temperature
133 and plotted the solution of equation (7) against that temperature with an arbitrary off-set in Fig.

134 1.



135 **4. A simple temporal equation for the surface-elevation feedback**

136 Based on the governing equation, we can derive the critical surface mass balance and surface
 137 elevation below which a meltdown of the ice-sheet is inevitable. Let us define the time τ_α as the
 138 time it takes to melt a fraction α of the initial ice volume and the threshold temperature T_c as
 139 the temperature above the pre-industrial level at which the surface mass balance becomes
 140 negative. Robinson et al. (2012) find a range of 0.8 – 3.2°C for the threshold warming beyond
 141 which no ice sheet can be sustained on Greenland. Their best estimate for the threshold is 1.6°C
 142 above pre-industrial level. Ridley et al. (2010) find that in their model the ice sheet cannot be
 143 sustained for a warming of 2°C. Some studies assume that the threshold is associated with a
 144 mean negative surface mass balance (Gregory et al., 2004b; Ridley et al., 2005; Toniazzo et al.,
 145 2004). In Fig. 2 we use 1.6°C as a threshold value for both models. This number can be easily
 146 adjusted if new estimates are obtained.

147 For a fixed anomalous melt rate $\Delta a_0 = -\gamma \cdot \Delta T$ in response to an anomalous temperature increase
 148 ΔT above this threshold temperature, the decay time without any feedbacks would be

$$149 \quad \tau_0 = -\frac{h_0}{\Delta a_0} = \frac{h_0}{\gamma \cdot \Delta T} \quad (11)$$

150 Since the surface temperature increases with decreasing elevation, this zero-order estimate for
 151 the decay time is higher than the actual value. As a first-order correction to the situation of fixed
 152 melting, let us assume that the anomalous surface mass balance behaves as

$$153 \quad \Delta a = \Delta a_0 + \frac{1}{\tau_\gamma} \cdot (h - h_0) \quad (12)$$

154 where $\tau_\gamma = 1/(\gamma \cdot \Gamma)$.

155 From the relation $dh/dt = \Delta a$, we then obtain

$$156 \quad \frac{d\Delta h}{dt} = -\Delta a_0 + \frac{\Delta h}{\tau_\gamma}, \quad (13)$$

157 if $\Delta h \equiv h_0 - h$ is defined as the reduction in height. For a time-dependent melting induced by
 158 surface warming $\Delta a_0 = \gamma \cdot \Delta T$ the general solution of equation (13) is



$$159 \quad \Delta h(t) = \gamma \cdot \int_0^t dt' \Delta T(t') \cdot e^{(t-t')/\tau_\gamma} \quad (14)$$

160 This equation corresponds to a linear response theory with the melting $\gamma \cdot \Delta T$ as forcing and an
 161 exponential response function

$$162 \quad R(t') = e^{t'/\tau_\gamma} \quad (15)$$

163 Linear response theory states that the convolution of equation (14) yields the linear response of
 164 the system (Good et al., 2011; Winkelmann and Levermann, 2013). Note that generally linear
 165 response theory is used as an approximation of a non-linear system to relatively weak forcing. In
 166 these circumstances the response function has to decline with time because it represents the
 167 history of the system's response to past perturbation. For example, if the response function was
 168 a declining exponential $R(t') = e^{-t'}$ that would mean that the effect of forcing that occurred in
 169 the past, i.e. prior to the time t that is considered, becomes exponentially less relevant for the
 170 current system response. Here however the response function is increasing with time which
 171 means that the past deviation from the steady state is amplified which is exactly what an unstable
 172 situation should do. The exponent $1/\tau_\gamma$ can be considered the Lyapunov exponent of the system.

173 Given the boundary condition $\Delta h(t=0)=0$, for a constant temperature increase ΔT , equation (14)
 174 becomes

$$175 \quad \Delta h(t) = h_0 \cdot \left(\frac{\tau_\gamma}{\tau_0} - \frac{\tau_\gamma}{\tau_0} \cdot e^{t/\tau_\gamma} \right) - \frac{h_0}{\tau_0} - \frac{h_0}{\tau_\gamma} \quad (16).$$

176 The decay time for a relative volume reduction of α is then given by:

$$177 \quad \tau_\alpha = \frac{1}{\gamma\Gamma} \cdot \log \left(1 + \alpha \cdot \frac{\Gamma \cdot h_0}{\Delta T} \right) \quad (17),$$

178 where \log denotes the natural logarithm. Equation (17) is denoted the *decay-time equation*
 179 hereafter.



180 5. Estimating the Melt Time of the Greenland Ice Sheet from Observables

181 In this simplified approach, the collapse time is thus a function of three observable quantities: the
182 equilibrium-line altitude, h_0 , the atmospheric lapse rate, Γ , and the melting sensitivity to
183 temperature, γ . The average equilibrium-line altitude of the Greenland Ice Sheet is at about 1150
184 meters (Box & Steffen 2001)). The observed range for the atmospheric lapse rate is estimated to
185 be between 5 ± 2 °C/km (Fausto et al. 2009; Gardner & Sharp 2009), and current estimates for
186 the melting sensitivity scatter around 4.4 ± 2 cm/year/°C (Box 2013). In order to obtain an
187 estimate of the decay time and the uncertainty around this estimate we use equation (17) and
188 chose the lapse rate and melting sensitivity uniformly randomly from these observed intervals
189 (Tab. 1, Figs. 2 – 4).

190 Existing numerical simulations for a decay of the Greenland Ice Sheet (Ridley et al. 2010;
191 Robinson et al. 2012) differ in their trajectories for the total ice volume, but exhibit a
192 characteristic functional form when the relative ice volume is expressed as a function of the
193 temperature anomaly above the critical temperature threshold (Fig. 2). This characteristic
194 relation is captured by our first-order equation for the decay time, embedding the results from
195 process-based models into a simple analytical framework. This approach provides a good
196 approximation if, on the one hand, the volume loss is significantly large for the surface-elevation
197 feedback to become relevant and, on the other hand, the melting is dominating the ice loss
198 compared to the dynamic ice discharge.

199 Following the decay-time equation (17), the observational constraints for the atmospheric lapse
200 rate, Γ , and the melting sensitivity, γ , translates into an uncertainty range for the melt time of the
201 Greenland Ice Sheet, assuming uniform probability distributions for both Γ and γ within the
202 above intervals. Fig. 2 shows the histograms of the time until 10% of its present-day ice volume
203 (corresponding to 0.7 m global sea-level rise) are melted for different warming scenarios. The
204 melt time depends strongly on the level of warming beyond the temperature threshold: The
205 median estimate varies from more than 2000 years for a warming of +1°C to less than 500 years
206 for a warming of +5°C.

207 Since the melt time is a monotonically decreasing function of both the lapse rate and the melting
208 sensitivity, the upper and lower limits of the estimates can be directly computed from the



209 observed uncertainty interval of these quantities. However, the functional form of equation (17)
210 introduces a specific structure into the histogram of the melt time which is highly skewed
211 towards the low end (Tab. 1 and Fig. 4).

212 The simple equation provided here is clearly limited in its applicability. Since it does not account
213 for any dynamic discharge or even ice motion the results from equation (17) strongly deviate
214 from numerical simulations when the ice has time to adjust dynamically to the volume loss. This
215 can be seen for a stronger ice loss of 50% of the initial volume (Fig. 3). Also the role of the ice
216 material properties is comprised into one parameter, the melting sensitivity of the ice to a
217 temperature increase at the surface. This sensitivity will in general vary not only with time but
218 also spatially and due to the melting itself. Similarly the feedback role of the surrounding climate
219 is represented by only one parameter, the atmospheric lapse rate which will again vary spatially
220 but also with time as the ice surface declines.

221 The dynamic discharge from Greenland is strongly limited by the ice sheet's bottom topography,
222 for which estimates yield an upper bound of approximately 5-13 cm during the next century
223 (Graversen et al., 2010; Price et al., 2011). Over a period during which the ice loss is dominated
224 by the feedback and the ice-dynamic effect is limited, our approach provides a quantitative
225 estimate of the melt time based on observable quantities. Equation (17) can thus be used when
226 new observations suggest an altered melting sensitivity or changes in the atmospheric response
227 to Greenland ice loss.



228 **6. Discussion and conclusion**

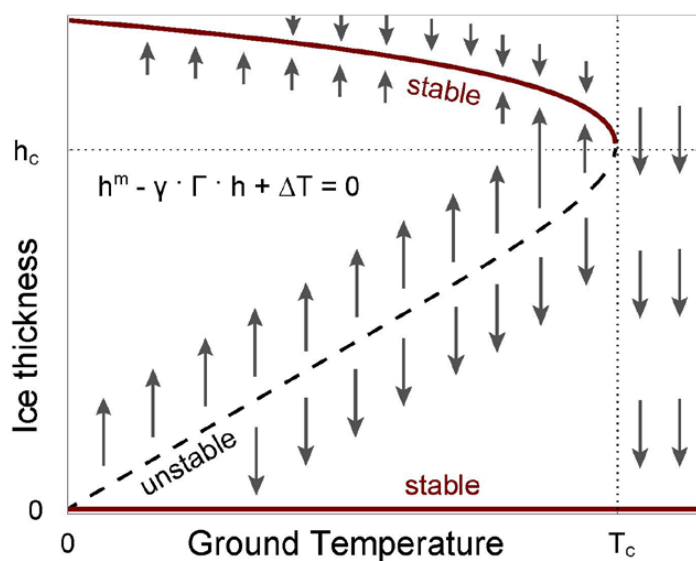
229 Our estimate for the decay time captures the characteristic slow-down near the critical threshold
230 as can be seen from the divergence of the decay time, τ_a , in the limit of vanishing warming above
231 the threshold (equation (17)). The simple equation of the decay time quantitatively reproduces
232 the range given by simulations with process-based models. The feedback becomes more
233 dominant near the threshold compared to larger temperature increase for which the external
234 climatic forcing is more relevant (Fig. 5). For these curves in this figure we used the central
235 values of the parameters, i.e. equilibrium-line altitude $h_0=1150\text{m}$, atmospheric lapse rate $\Gamma=5$
236 $^{\circ}\text{C}/\text{km}$ and melting sensitivity $\gamma=4.4\text{ cm}/\text{year}/^{\circ}\text{C}$.

237 For a temperature increase of 5°C , which could be reached within this century (IPCC, 2013), the
238 median rate of sea-level contribution is about 1.4 mm per year which is about four times that of
239 its current contribution (Rignot et al., 2011). Even for extremely high temperatures however, the
240 Greenland Ice Sheet cannot melt infinitely fast – our results show that a complete disintegration
241 within the next two millennia is highly unlikely unless ice dynamics effects become dominate or
242 the melting sensitivity is significantly higher than currently observed. For a global mean
243 temperature increase below two degrees, as agreed upon during the 1015 Paris UNFCCC climate
244 summit, the threshold temperature would only be exceeded mildly and the decay time of the
245 Greenland ice sheet would be multi-millennial.



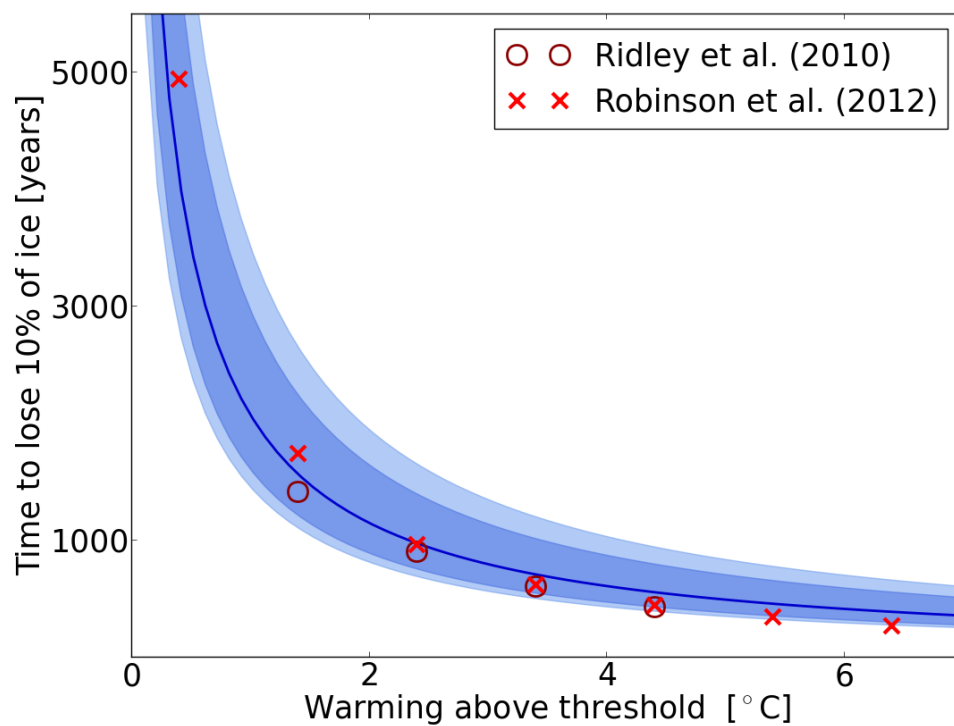
Volume loss		0.5°C	1°C	2°C	3°C	4°C	5°C
10%	Lower	2140 yr	1320 yr	760 yr	530 yr	410 yr	330 yr
	Median	3430 yr	2040 yr	1140 yr	790 yr	610 yr	500 yr
	Upper	7290 yr	4120 yr	2210 yr	1520 yr	1150 yr	930 yr
50%	Lower	4920 yr	3600 yr	2460 yr	1900 yr	1550 yr	1320 yr
	Median	8740 yr	6170 yr	4040 yr	3040 yr	2450 yr	2090 yr
	Upper	20740 yr	13920 yr	8640 yr	6310 yr	4980 yr	4120 yr
100%	Lower	6340 yr	4920 yr	3600 yr	2910 yr	2460 yr	2140 yr
	Median	11610 yr	8730 yr	6160 yr	4840 yr	4020 yr	3500 yr
	Upper	28710 yr	20740 yr	13920 yr	10630 yr	8640 yr	7290 yr

246 **Table 1: Decay time.** Time period after which different percentages of volume loss have
 247 occurred at different warming levels. Provided are the median values of the distributions from
 248 Figures 2 and 3 together with the lower and upper limit that are derived respectively from the
 249 upper and lower limits of the uncertainty range of the observed melting sensitivity and
 250 atmospheric lapse rate.



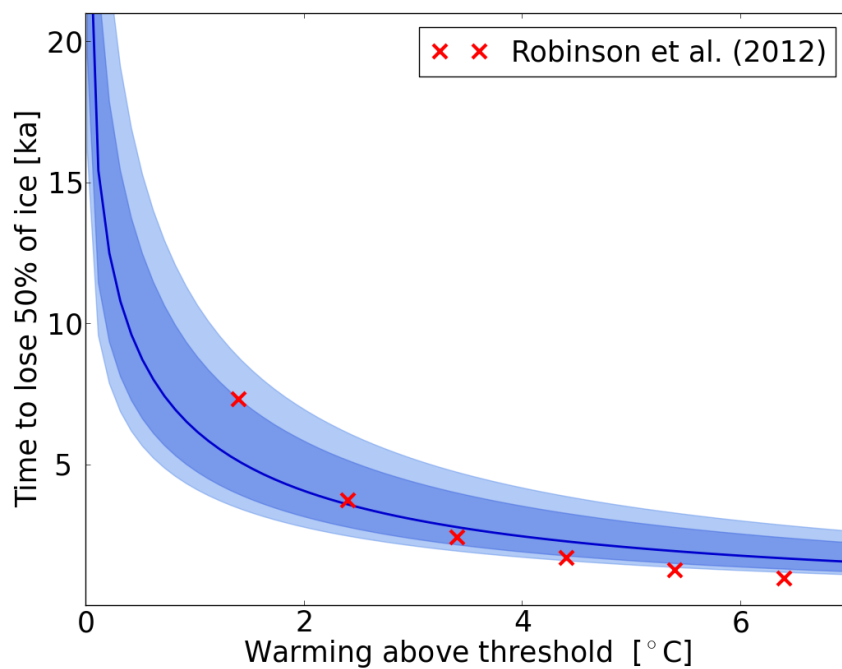
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252 **Figure 1: Ice-sheet hysteresis.** If the ice-sheet is in an unstable configuration (dashed black
 253 branch), a slight perturbation will either cause it to converge into the stable state (upper red
 254 branch) or to melt-down completely. For a given temperature, the dotted line gives the critical
 255 surface elevation (section 3). If the surface elevation is lower than h_c , a complete meltdown of
 256 the ice sheet is inevitable. Once the temperature threshold, T_c , is crossed, the time for a collapse
 257 of a certain fraction of the ice-sheet can be estimated via equation (17).



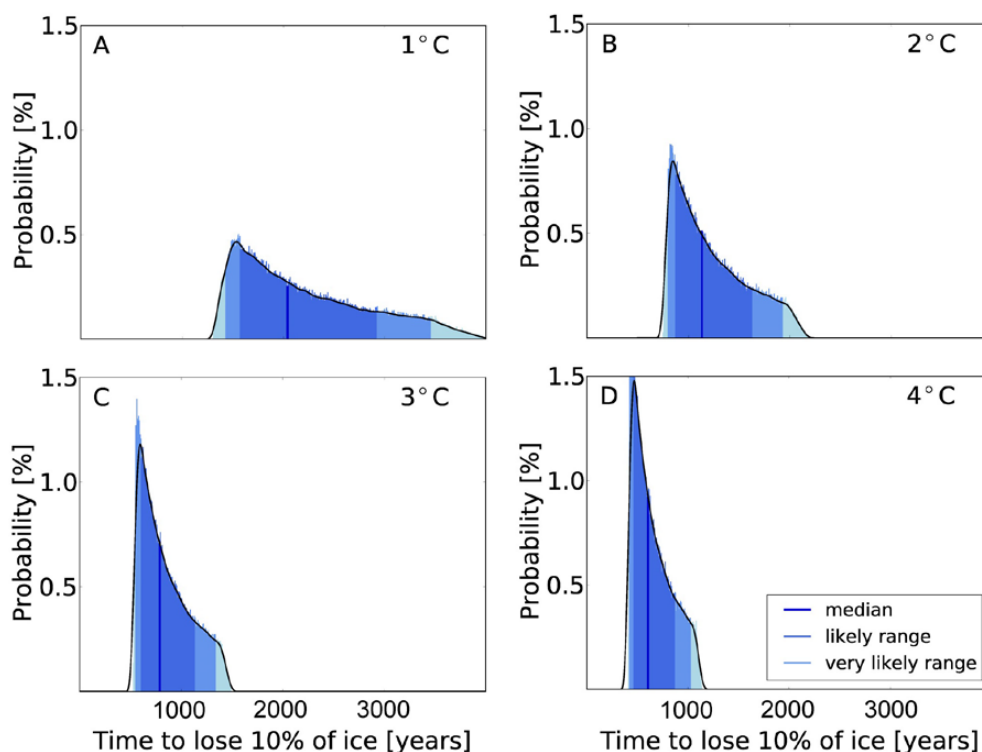
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259 **Figure 2. Decay-time of the Greenland Ice Sheet.** The decay time depends critically on the level
260 of warming above the temperature threshold. Shown are the median (black line) and the likely
261 (18% to 83% quantiles, dark blue shading) and very likely (5% to 95% quantiles, light blue
262 shading) ranges for the time to melt 10% of the present-day ice volume, estimated via equation
263 (17). The red circles and crosses indicate the results from process-based model simulations by
264 Ridley et al. (2010) and Robinson et al. (2012), respectively.



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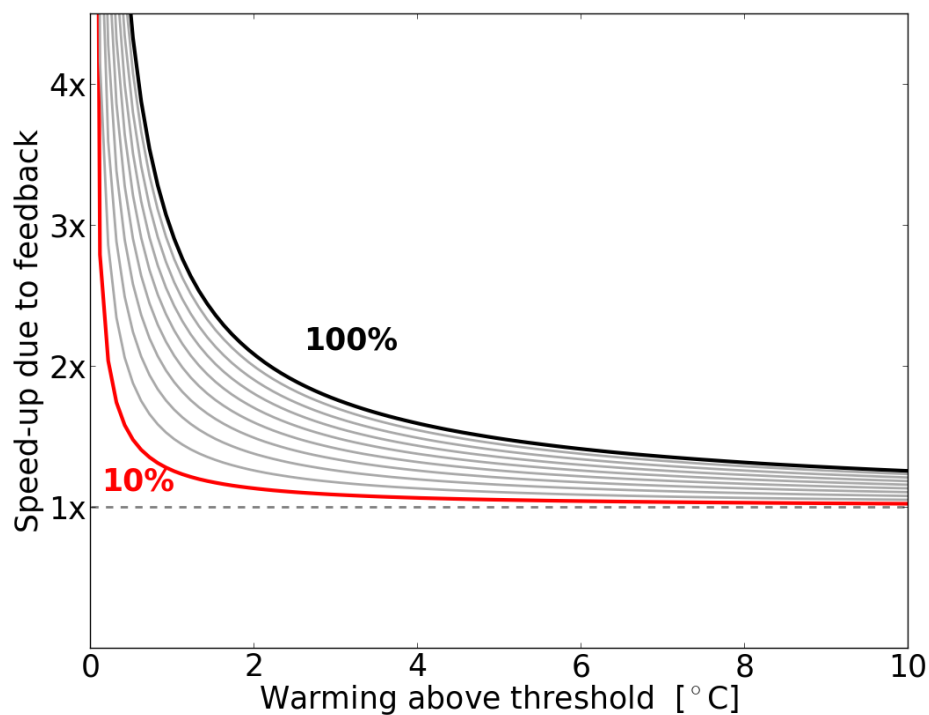
266 **Figure 3: Time until 50% of the Greenland Ice Sheet are melted.** Shown are the median (black
267 line) and the likely (18% to 83% percentiles, dark blue shading) and very likely (5% to 95%
268 percentiles, light blue shading) ranges for the time to melt 50% of the present-day ice volume,
269 estimated via the equation for the decay time τ_a . The red crosses indicate the results from
270 process-based model simulations by Robinson et al. (2012).



271

272 **Figure 4. Likelihood for 10%-decay of Greenland Ice Sheet.** Shown are the probabilities for the
273 ice-sheet to lose 10% of its initial ice volume in a certain time period for surface warming of
274 +1°C (A), +2°C (B), +3°C (C) and +4°C (D) above the threshold. The median is indicated by
275 the black line, and the likely and very likely ranges are shaded in dark and light blue,
276 respectively.

277



278

279 **Figure 5: Role of surface elevation feedback in melting of Greenland ice sheet declines with**
280 **increasing temperature.** Shown is the ratio of melting time with surface-elevation feedback over
281 melting time without the feedback τ_a/τ_0 . Each line represents the ratio for a loss of different
282 percent of the initial ice volume. The red line shows the ratio of the decay time with feedback
283 over the decay time without feedback for a 10% ice loss (corresponding to figures 2 and 4). The
284 influence of the feedback becomes less dominant with stronger warming above the critical
285 threshold (x-axis). Near the threshold the melting time without feedback diverges stronger
286 ($1/\Delta T$) than the melt time with feedback which declines logarithmically.



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