

A simple equation for the melt-elevation feedback of ice sheets

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Abstract:

In recent decades, the Greenland Ice Sheet has been losing mass and thereby contributed to global sea-level rise. The rate of ice loss is highly relevant for coastal protection worldwide. The ice loss is likely to increase under future warming. Beyond a critical temperature threshold, a meltdown of the Greenland Ice Sheet is induced by the self-enforcing feedback between its lowering surface elevation and its increasing surface mass loss: the more ice is lost, the lower the ice surface and the warmer the surface air temperature which fosters further melting and ice loss. The computation of this rate so far relies on complex numerical models which are the appropriate tools to capture the complexity of the problem. By contrast we aim here at gaining conceptual understanding by deriving a purposefully simple equation for the self-enforcing feedback which is then used to estimate the melt time for different levels of warming using three observable characteristics of the ice sheet itself and its surroundings. The analysis is purely conceptual in nature and is missing important processes like ice dynamics to be useful for applications to sea-level rise on centennial time scales, but when the volume loss is dominated by the feedback, the resulting logarithmic equation unifies existing numerical simulations and shows that the melt time depends strongly on the level of warming with a critical slowing-down near the threshold: the median time to lose 10% of the present-day ice volume varies between about 3500 years for a temperature level of 0.5°C above the threshold and 500 years for 5°C . Unless future observations show a significantly higher melting sensitivity than currently observed, a complete meltdown is unlikely within the next 2000 years without significant ice-dynamical contributions.

1. Introduction

In past decades global mean sea level has been rising mainly by expansion of ocean waters and melting of ice on land (Church et al., 2013). Over the past two decades, the Greenland Ice Sheet has lost mass at an accelerating pace (Bamber et al., 2000; Box et al., 2012; van den Broeke et al., 2009; Fettweis et al., 2013; Mernild et al., 2011; Nick et al., 2009; Rignot et al., 2008, 2011; Shepherd and Wingham, 2007; Thomas et al., 2011). The ice loss is likely to increase under unabated greenhouse-gas emissions (Clark et al., 2016; Fettweis et al., 2013; Goelzer et al., 2012; Graverson et al., 2011; Harper et al., 2012; Huybrechts et al., 2011; Levermann et al., 2013; Nowicki et al., 2013; Price et al., 2011).

Numerical simulations suggest that a decline of the Greenland Ice Sheet is inevitable once its surface temperature permanently exceeds a certain threshold (Charbit et al., 2008; Greve, 2000; Huybrechts and Wolde, 1999; Huybrechts et al., 2011; Ridley et al., 2005, 2010; Robinson et al., 2012; Solgaard and Langen, 2012). If and when this temperature threshold is passed, depends critically on past and future greenhouse-gas emissions (Fettweis et al., 2013; Goelzer et al., 2013; Gregory et al., 2004a; Rae et al., 2012). Even if emissions were reduced to zero, temperatures would not drop significantly for thousands of years because of the long life-time of anthropogenic CO_2 in the atmosphere and reduced oceanic heat uptake if oceanic convection is extenuated (Allen et al., 2009; Solomon et al., 2009; Zickfeld et al., 2013). This implies a possible commitment of a melt-down of the Greenland Ice Sheet in the near future which would eventually raise global sea-level by more than 7 meters (Gregory et al., 2004a). Whether this occurs on a multi-centennial or rather a multi-millennial time scale is of relevance for coastal planning.

In this article we first recap the Vialov profile and add a simple representation of the melt-elevation feedback towards a governing equation for a steady-state ice-sheet in one dimensions, then we derive the critical warming threshold for the existence of an ice sheet in this simple model (Section 2). In Section 3 we derive a simple time-evolution equation for the decay of the ice sheet after surface temperatures have exceeded the threshold. Finally we use observational estimates of the three characteristics that enter the model to estimate the decay time of the ice sheet under melting above the threshold (Section 4). Here solid ice discharge is neglected as well as any other ice sheet dynamics (Andresen et al., 2012; Howat and Eddy, 2012; Moon et al.,

59 2012; Nick et al., 2009; Price et al., 2011; Straneo et al., 2011; Walsh et al., 2012). The
60 framework that we introduce here can be used to include new physical processes that might be
61 discovered in the future, e.g. potential changes in surface albedo through melting (Box et al.,
62 2012) or aerosol-induced surface melt or the lack thereof (Polashenski et al., 2015).

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2. Governing equation for shallow-ice steady states under melt-elevation feedback

A nonlinear threshold behaviour is generally associated with a fundamental self-enforcing feedback and thereby an associated system memory (Levermann et al., 2012). For the Greenland Ice Sheet, such a feedback is given by the interaction between surface elevation and surface melting (Weertman, 1961). For illustration, we include this feedback in a well-established highly idealized ice-profile of an ice-sheet in one dimension, the so-called Vialov-profile (Vialov, 1958). We introduce the melt-elevation feedback in the simplest possible way by assuming that the surface melt rate depends linearly on the surface temperature and that the temperature decreases linearly with the height of the ice surface following a constant atmospheric lapse rate.

2.1 Governing equation

We consider a highly simplified flowline model for an isothermal ice sheet grounded on a flat and rigid bed. The solution of the shallow-ice approximation in one dimension for the ice-sheet elevation under these simplifying assumptions is the Vialov-profile:

$$\tilde{h}(x) = h_m \left(1 - (x/L)^{(n+1)/n}\right)^{n/(2n+2)} \quad (1)$$

where h_m is the maximum surface elevation and n is Glen's flow law exponent (Glen, 1955). x denotes the horizontal position and L the horizontal limit of the ice sheet. The inherent assumption of isothermal ice is a strong simplification, which needs to be kept in mind when interpreting the results. The aim of this derivation is purposefully not a comprehensive representation of the ice flow but to derive a measure for the average height of the ice sheet and its dependence on changes in the surface mass balance. The surface mass balance is considered to be spatially and temporally constant at a value, a , which will later be considered dependent on the surface elevation and thereby temporally variable. The overall horizontal extension of the ice sheet is set to L , and it is thereby assumed that any ice flow across this point is calved off into icebergs. This situation represents a confined ice-bearing bedrock topography as in most of Greenland's interior (Howat et al., 2014).

The mean surface elevation can then be computed to be

$$\bar{h} = L^{-1} \int_0^L dx h(x) = \omega \cdot h_m \quad (2)$$

It is proportional to the maximum surface elevation h_m with a proportionality factor

$$\omega \equiv \int_0^1 d\xi \left(1 - \xi^{(n+1)/n}\right)^{n/(2n+2)} \quad (3)$$

which only depends on the flow law exponent.

The maximum surface elevation is determined by the surface mass balance \tilde{a} and the ice softness \tilde{A}

$$h_m = 2^{(n-1)/(2n+2)} \cdot L^{1/2} \cdot \left(\frac{(n+2)\tilde{a}}{(\rho g)^n \tilde{A}}\right)^{1/(2n+2)} \quad (4)$$

with ρ being the ice density and g the gravity constant. We normalize all three quantities by defining $h \equiv \omega \cdot h_m / \bar{h}_0$, $a \equiv \tilde{a} / a_0$ and $A \equiv \tilde{A} / A_0$ where a_0 is the accumulation rate on the ground, i.e., in the absence of an ice-sheet, and $A_0 = a_0 / \left((\rho g)^n (\varepsilon \cdot L)^{(n+1)}\right)$ with $\varepsilon = \bar{h}_0 / L$ being the typical height-to-width ratio. \bar{h}_0 is the equilibrium-line altitude of the considered ice sheet in the initial equilibrium situation. Values for a_0 , \bar{h}_0 and L are later chosen to resemble the conditions of the Greenland Ice Sheet.

The non-dimensional surface elevation, h , of the ice sheet can then be expressed as

$$h = \left(\frac{a}{A}\right)^{1/m} \quad (5)$$

For the Vialov profile, $m=2(n+1)$ where the Glen flow-law exponent is commonly chosen to be around $n=3$ which yields $m=8$.

We introduce the melt-elevation feedback in its simplest form through a dependency of the surface melt rate on the surface elevation:

$$a = a_0 + \gamma \Gamma \cdot h \quad (6)$$

with the atmospheric lapse rate $\Gamma > 0$. γ denotes the melting sensitivity of the ice surface, i.e. the increase in surface melt-rate per degree of warming, which is regularly measured and comprises a large number of physical processes (e.g. (Box, 2013)). For simplicity we rescale the surface mass balance by the constant ice softness parameter, A to obtain $h = (a_0 + \gamma \Gamma \cdot h)^{1/m}$. The steady state solution for the surface elevation of the ice-sheet is thus governed by the following equation

$$h^m - \gamma \Gamma \cdot h - a_0 = 0 \quad (7)$$

which has two positive solutions for h as long as the surface mass balance on the ground is negative, i.e., $a_0 < 0$. Note that the surface mass balance can be positive even if $a_0 < 0$. If the ice-sheet is in an unstable configuration, a slight perturbation will either cause it to converge into the stable state with a positive surface mass balance or to melt completely.

Our simple approach qualitatively captures the basic hysteresis behavior of the Greenland Ice Sheet caused by the melt-elevation feedback (Fig. 1, in which we have assumed the surface mass balance to depend linearly on temperature): For a given surface temperature, a stable state of the ice sheet (red line) annihilates an external perturbation in surface elevation by changes in surface mass balance (grey arrows). The unstable solution branch defines the basin of attraction for the stable state. A surface elevation that is lower than the unstable solution branch cannot be sustained. In that case the melting reduces the surface elevation to practically zero even without further external perturbation (grey arrows). Beyond a certain surface temperature threshold (vertical dotted line) no ice sheet can be sustained.

2.2. Critical surface mass balance in steady state

As illustrated in Fig. 1, there is a critical temperature above which the ice sheet is not sustainable. Let us denote the corresponding surface elevation by h_c . The critical point (T_c, h_c) has to fulfill two conditions, i.e. being a solution of the governing Equation 7 and minimum of the function

$$F(h) = h^m - \gamma \Gamma \cdot h - a_0 \quad (8)$$

which we can determine by setting the derivative of F to zero.

Consequently,

$$h_c = \left(\frac{\Gamma \cdot \gamma}{m} \right)^{1/(m-1)} \quad (9).$$

Inserting this into the governing equation yields the critical surface mass balance at the ground

$$a_{0c} = -(m-1) \cdot \left(\frac{\Gamma \cdot \gamma}{m} \right)^{m/(m-1)} \quad (10).$$

For illustrative purposes we have assumed a_0 to decline linearly with the surrounding temperature and plotted the solution of Equation 7 against that temperature with an arbitrary offset in Fig. 1.

3. A simple temporal equation for the melt-elevation feedback

Once the critical surface-mass balance and surface elevation threshold (as derived in the previous section 2) is transgressed, a meltdown of the ice-sheet is inevitable in our conceptual model. Let us define the time τ_α as the time it takes to melt a fraction α of the initial ice volume and the threshold temperature T_c as the temperature above the pre-industrial level at which the surface mass balance becomes negative. Robinson et al. (2012) find a range of $0.8 - 3.2^\circ\text{C}$ for the threshold warming beyond which no ice sheet can be sustained on Greenland. Their best estimate for the threshold is 1.6°C above pre-industrial level. The study uses a regional climate model of intermediate complexity (Robinson et al., 2009) coupled to the SICOPOLIS ice sheet model (Greve, 1997). Using a different model combination, Ridley et al. (2010) find that in their model the ice sheet cannot be sustained for a warming of 2°C . They combine the HadCM3 Atmosphere-Ocean-General Circulation Model (Gordon et al., 2000) with an atmospheric resolution of $2.5^\circ \times 3.75^\circ$ (Pope et al., 2000) to an ice sheet model of 20 km horizontal resolution (Huybrechts and Wolde, 1999).

Some studies assume that the threshold is associated with a mean negative surface mass balance (Gregory et al., 2004b; Ridley et al., 2005; Toniazzi et al., 2004). In Fig. 2 we use 1.6°C as a threshold value for both models because this value is given by Robinson et al. (2012) and consistent with Ridley et al. (2010) and thus a simple and transparent choice. This number can be easily adjusted if new estimates are obtained. For the translation from percentage ice thickness change to percentage ice volume change a constant horizontal ice surface area was assumed which renders the analysis conceptual in nature. Thus the quantitative interpretation of the melt times are subject to this additional simplification.

For a fixed anomalous melt rate $\Delta a_0 = -\gamma \cdot \Delta T$ in response to an anomalous temperature increase $\Delta T = T - T_c$ above this threshold temperature, T_c , the decay time without any feedbacks would be

$$\tau_0 = -\frac{h_0}{\Delta a_0} = \frac{h_0}{\gamma \cdot \Delta T} \quad (11)$$

Since the surface temperature increases with decreasing elevation, this zero-order estimate for the decay time is higher than the actual value. As a first-order correction to the situation of fixed melting, let us assume that the anomalous surface mass balance behaves as

$$\Delta a = \Delta a_0 + \frac{1}{\tau_\gamma} \cdot (h - h_0) \quad (12)$$

where $\tau_\gamma = 1 / (\gamma \cdot \Gamma)$.

From the relation $dh / dt = \Delta a$, we then obtain

$$\frac{d\Delta h}{dt} = -\Delta a_0 + \frac{\Delta h}{\tau_\gamma}, \quad (13)$$

if $\Delta h \equiv h_0 - h$ is defined as the reduction in height. For a time-dependent melting induced by surface warming $\Delta a_0 = -\gamma \cdot \Delta T$ the general solution of Equation 13 is

$$\Delta h(t) = \gamma \cdot \int_0^t dt' \Delta T(t') \cdot e^{(t-t')/\tau_\gamma} \quad (14)$$

This equation corresponds to a linear response theory with the melting $-\gamma \cdot \Delta T$ as forcing and an exponential response function

$$R(t') = e^{t'/\tau_\gamma} \quad (15)$$

Linear response theory states that the convolution of Equation 14 yields the linear response of the system (Good et al., 2011; Winkelmann and Levermann, 2013). Note that generally linear response theory is used as an approximation of a non-linear system to relatively weak forcing. In these circumstances the response function has to decline with time because it represents the history of the system's response to past perturbation. For example, if the response function was a declining exponential $(t') = e^{-t'}$, this would mean that the effect of forcing that occurred in the past, i.e. prior to the time t that is considered, becomes exponentially less relevant for the current system response. Here, however, the response function is *increasing* with time, which means that the past deviation from the steady state is amplified as expected near an unstable fixed point. The exponent $1/\tau_\gamma$ can be considered the Lyapunov exponent of the system.

Given the boundary condition $\Delta h(t=0)=0$, for a constant temperature increase ΔT , Equation 14 becomes

$$\Delta h(t) = h_0 \cdot \left(\frac{\tau_\gamma}{\tau_0} - \frac{\tau_\gamma}{\tau_0} \cdot e^{t/\tau_\gamma} \right) - \frac{h_0}{\tau_0} - \frac{h_0}{\tau_\gamma} \quad (16).$$

The decay time for a relative volume reduction of α is then given by:

$$\tau_\alpha = \frac{1}{\gamma \Gamma} \cdot \log \left(1 + \alpha \cdot \frac{\Gamma \cdot h_0}{\Delta T} \right) \quad (17),$$

where \log denotes the natural logarithm. Equation 17 is denoted the *decay-time equation* hereafter.

3. Estimating the Melt Time of the Greenland Ice Sheet from Observables

In this simplified approach, the collapse time is thus a function of three observable quantities: the equilibrium-line altitude, h_0 , the atmospheric lapse rate, Γ , and the melting sensitivity to temperature, γ . The average equilibrium-line altitude of the Greenland Ice Sheet is at about 1150 meters (Box & Steffen 2001)). The observed range for the atmospheric lapse rate is estimated to be between 5 ± 2 °C/km (Fausto et al. 2009; Gardner & Sharp 2009), and current estimates for the melting sensitivity scatter around 4.4 ± 2 cm/year/°C (Box 2013). In order to obtain an estimate of the decay time and the uncertainty around this estimate we use Equation 17 and choose the lapse rate and melting sensitivity uniformly randomly from these observed intervals (Tab. 1, Figs. 2 – 4).

Following the decay-time Equation 17, the observational constraints for the atmospheric lapse rate, Γ , and the melting sensitivity, γ , translate into an uncertainty range for the melt time of the Greenland Ice Sheet, assuming uniform probability distributions for both Γ and γ within the above intervals. Fig. 2 shows the histograms of the time until 10% of its present-day ice volume (corresponding to 0.7 m global sea-level rise) are melted for different warming scenarios. The melt time strongly depends on the level of warming beyond the temperature threshold: The median estimate varies from more than 2000 years for a warming of +1°C to less than 500 years for a warming of +5°C.

Existing numerical simulations of a decay of the Greenland Ice Sheet (Ridley et al. 2010; Robinson et al. 2012) differ in their trajectories for the total ice volume, but exhibit a characteristic functional form when the relative ice volume is expressed as a function of the temperature anomaly above the critical temperature threshold (Fig. 2). This characteristic relation is captured by our first-order equation for the decay time, embedding the results from process-based models into a simple analytical framework. This approach provides a good approximation if, on the one hand, the volume loss is significantly large for the melt-elevation feedback to become relevant and, on the other hand, the melting is dominating the ice loss compared to the dynamic ice discharge.

Since the simple equation provided here does not account for any dynamic discharge or even ice motion, the results from Equation 17 strongly deviate from numerical simulations when the ice

has time to adjust dynamically to the volume loss. This can be seen for a stronger ice loss of 50% of the initial volume where the functional dependence between the decay time and the temperature anomaly clearly follows a different functional form than predicted by Equation 17 (Fig. 3).

Since the melt time is a monotonically decreasing function of both the lapse rate and the melting sensitivity, the upper and lower limits of the estimates can be directly computed from the observed uncertainty interval of these quantities. However, the functional form of Equation 17 introduces a specific structure into the histogram of the melt time which is highly skewed towards the low end (Tab. 1 and Fig. 4). For increasing warming levels the histogram is shifting towards lower decay times. At the same time the histogram narrows and higher decay times become less frequent within the chosen parameter range (see description above).

4. Discussion and conclusion

Our estimate for the decay time captures the characteristic slow-down near the critical threshold as can be seen from the divergence of the decay time, τ_a , in the limit of vanishing warming above the threshold (Equation 17). The simple equation of the decay time quantitatively reproduces the range given by simulations with process-based models. the relative speed-up of ice loss due to the melt-elevation feedback (Fig. 5) is estimated, using the central values of the parameter ranges, i.e. equilibrium-line altitude $h_0=1150\text{m}$, atmospheric lapse rate $\Gamma=5\text{ }^\circ\text{C/km}$ and melting sensitivity $\gamma=4.4\text{ cm/year/}^\circ\text{C}$. The feedback becomes more dominant near the threshold compared to larger temperature increase for which the external climatic forcing is more relevant.

The simple equation provided here is clearly limited in its applicability. The role of the ice material properties is comprised into one parameter, the melting sensitivity of the ice to a temperature increase at the surface. This sensitivity will in general vary not only with time but also spatially and due to the melting itself. Similarly, the feedback role of the surrounding climate is represented by only one parameter, the atmospheric lapse rate which will again vary spatially but also with time as the ice surface declines.

Ice dynamics are deliberately excluded in our simple conceptual approach in order to separate and characterize the melt-elevation feedback. In reality, ice dynamics of course play an important role in the ice-sheet mass balance: Radar (ERS-2) and laser (ICESat) altimetry observations show that mass changes in Greenland were dominated by changes in the surface mass balance (SMB) between 1995 and 2001, and both SMB and dynamics contributed equally to mass loss from the Greenland Ice Sheet between 2001 to 2009 (Hurkmans et al., 2014). (Fürst et al., 2015) estimate that 40% of the recent loss (2000-2010) is due to an increase in ice dynamic discharge, 60% due to changes in the surface mass balance. Their results suggest that the future volume loss from the Greenland Ice Sheet might be predominantly caused by surface melting and dynamic discharge is limited by margin thinning and retreat.

Some studies suggest (Graversen et al., 2010; Price et al., 2011) that the dynamic discharge from Greenland is strongly limited by the ice sheet's bottom topography, for which estimates yield an upper bound of approximately 5-13 cm during the next century. Over a period during which the ice loss is dominated by the feedback and the ice-dynamic effect is limited, our approach

provides a quantitative estimate of the melt time based on observable quantities. Equation 17 can thus be used if new observations suggest an altered melting sensitivity or changes in the atmospheric response to Greenland ice loss.

For a temperature increase of 5°C, which could be reached within this century (IPCC, 2013), the median rate of sea-level contribution is about 1.4 mm per year which is about four times that of its current contribution of about 0.4 mm per year (Rignot et al., 2011; Shepherd et al., 2012). Even for extremely high temperatures however, the Greenland Ice Sheet cannot melt infinitely fast – our results show that a complete disintegration within the next two millennia is highly unlikely unless ice dynamics effects become dominant or the melting sensitivity is significantly higher than currently observed. For a global mean temperature increase below two degrees, as agreed upon during the 2015 Paris UNFCCC climate summit, the threshold temperature would only be exceeded mildly and the decay time of the Greenland ice sheet would be multi-millennial.

Volume loss		0.5°C	1°C	2°C	3°C	4°C	5°C
10%	Lower	2140 yr	1320 yr	760 yr	530 yr	410 yr	330 yr
	Median	3430 yr	2040 yr	1140 yr	790 yr	610 yr	500 yr
	Upper	7290 yr	4120 yr	2210 yr	1520 yr	1150 yr	930 yr
50%	Lower	4920 yr	3600 yr	2460 yr	1900 yr	1550 yr	1320 yr
	Median	8740 yr	6170 yr	4040 yr	3040 yr	2450 yr	2090 yr
	Upper	20740 yr	13920 yr	8640 yr	6310 yr	4980 yr	4120 yr
100%	Lower	6340 yr	4920 yr	3600 yr	2910 yr	2460 yr	2140 yr
	Median	11610 yr	8730 yr	6160 yr	4840 yr	4020 yr	3500 yr
	Upper	28710 yr	20740 yr	13920 yr	10630 yr	8640 yr	7290 yr

Table 1: Decay time. Time period after which different percentages of volume loss have occurred at different warming levels. Provided are the median values of the distributions from Figures 2 and 3 together with the lower and upper limit that are derived respectively from the upper and lower limits of the uncertainty range of the observed melting sensitivity and atmospheric lapse rate. The simple decay time equation (Equation 17) does not take any ice dynamic effects into account and its translation to ice volume assumes a constant horizontal ice-sheet area. Thus the values provided here best fit the complex model simulations only when these assumptions are reasonably well justified which is most likely not the case for high ice loss such as 50% or 100% of the original ice volume.

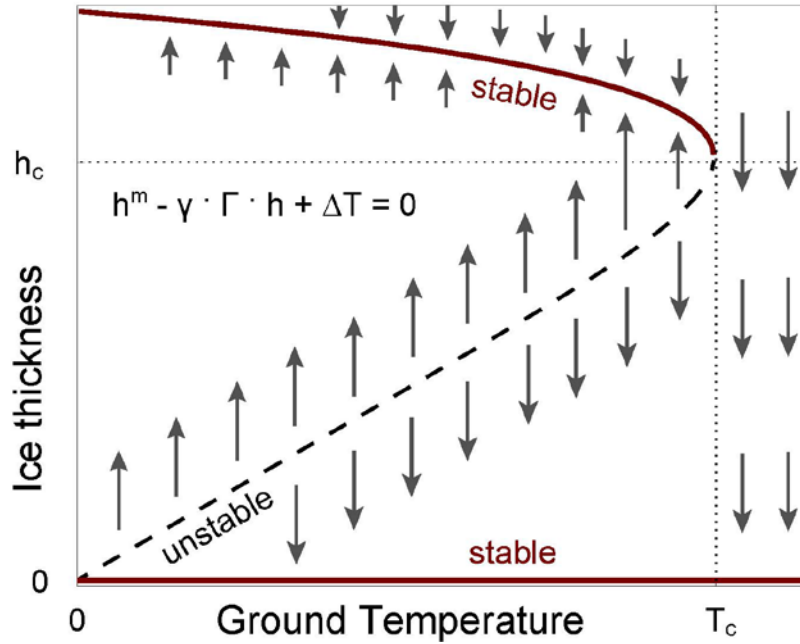


Figure 1: Ice-sheet hysteresis. If the ice-sheet is in an unstable configuration (dashed black branch), a slight perturbation will either cause it to converge into the stable state (upper red branch) or to melt completely. For a given temperature, the dotted line gives the critical surface elevation (Section 3). If the surface elevation is lower than h_c , a complete meltdown of the ice sheet is inevitable. Once the temperature threshold, T_c , is crossed, the time for a collapse of a certain fraction of the ice-sheet can be estimated via Equation 17.

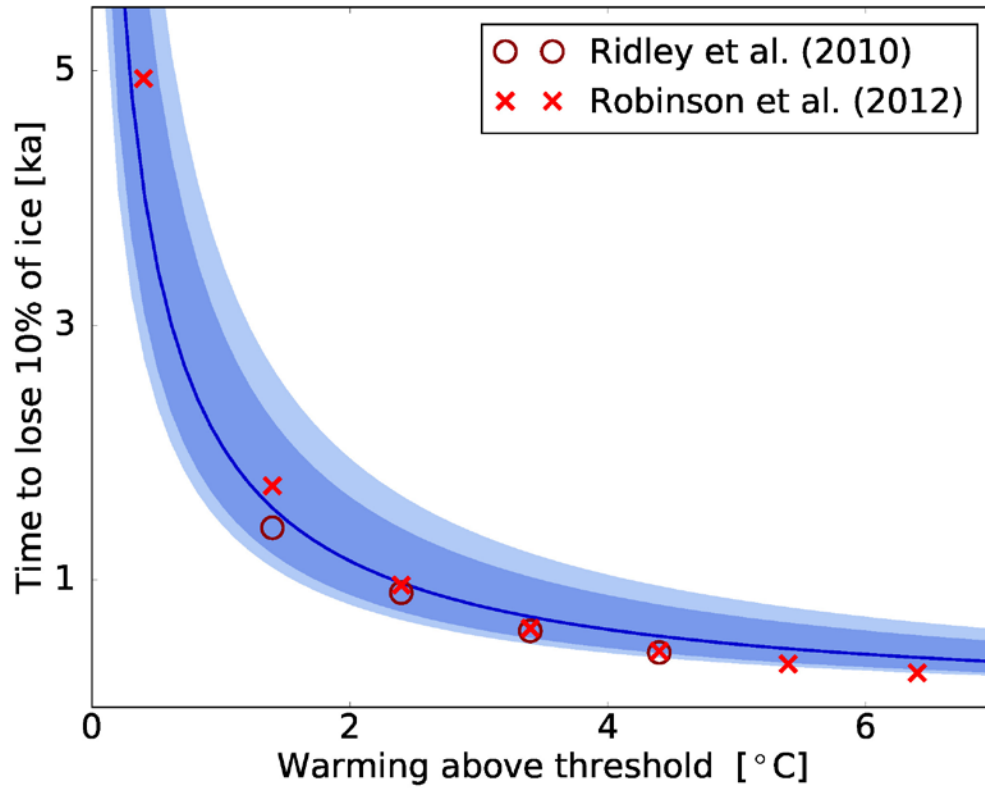


Figure 2. Decay-time of the Greenland Ice Sheet. The decay time depends critically on the level of warming above the temperature threshold. Shown are the median (black line), likely (18% to 83% quantiles, dark blue shading) and very likely (5% to 95% quantiles, light blue shading) ranges for the time to melt 10% of the present-day ice volume, estimated via Equation 17. The red circles and crosses indicate the results from process-based model simulations by Ridley et al. (2010) and Robinson et al. (2012), respectively.

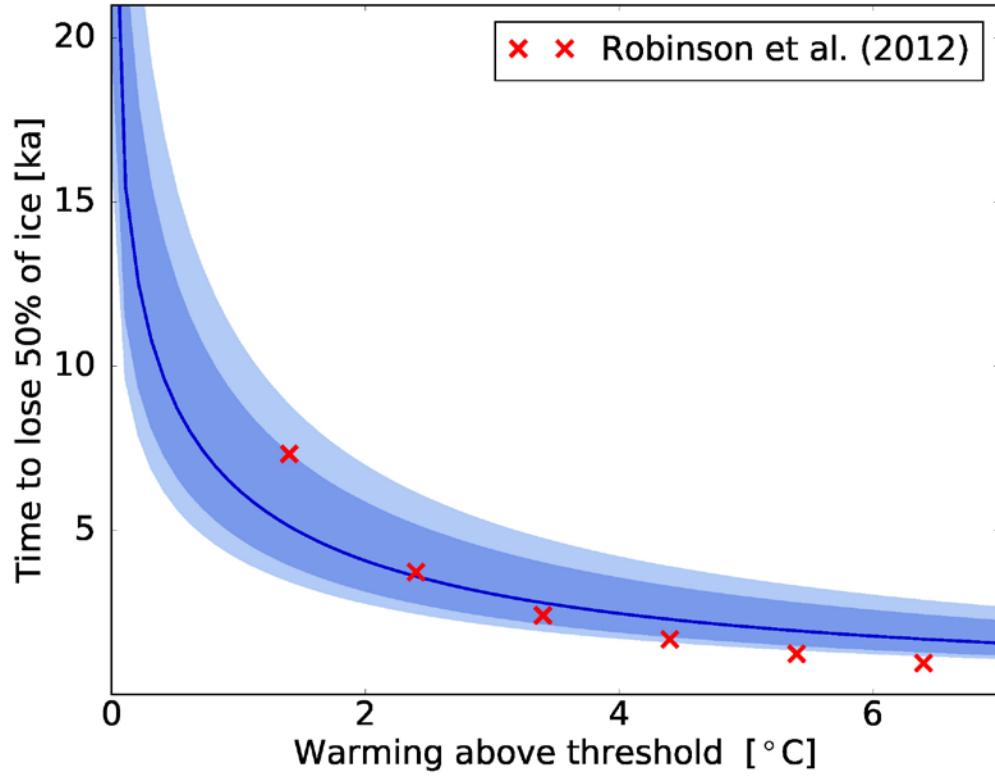


Figure 3: Time until 50% of the Greenland Ice Sheet are melted. Shown are the median (black line) and the likely (18% to 83% percentiles, dark blue shading) and very likely (5% to 95% percentiles, light blue shading) ranges for the time to melt 50% of the present-day ice volume, estimated via the equation for the decay time τ_{α} . The red crosses indicate the results from process-based model simulations by Robinson et al. (2012).

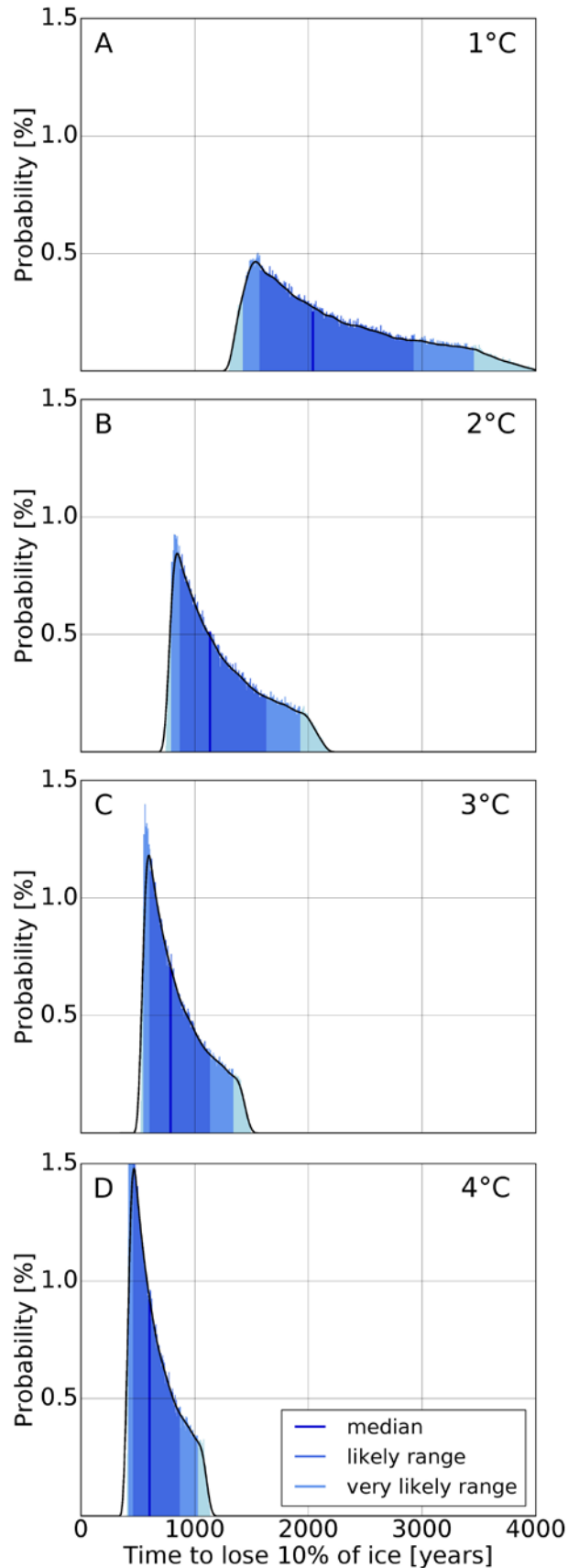


Figure 4. Likelihood for 10%-decay of Greenland Ice Sheet. Shown are the probabilities for the ice-sheet to lose 10% of its initial ice volume in a certain time period for surface warming of +1°C (A), +2°C (B), +3°C (C) and +4°C (D) above the threshold. The median is indicated by the black line, and the likely and very likely ranges are shaded in dark and light blue, respectively.

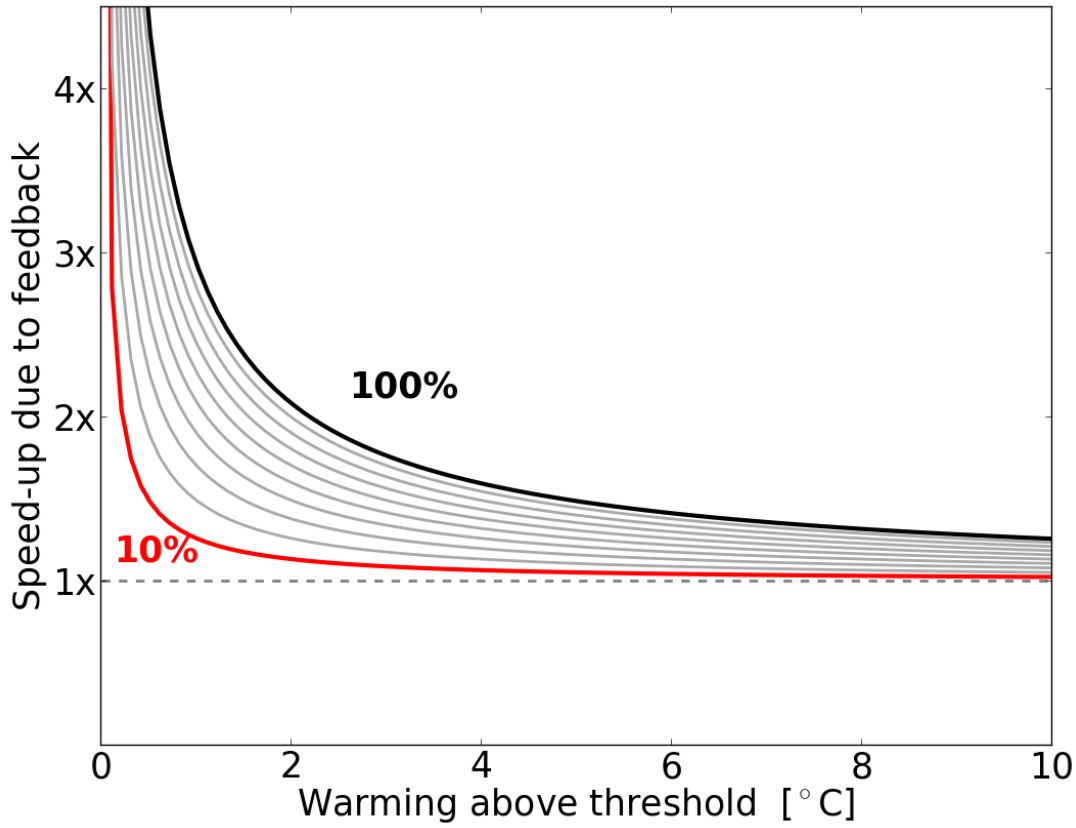


Figure 5: Role of melt-elevation feedback in melting of Greenland ice sheet declines with increasing temperature. Shown is the ratio of melting time with melt-elevation feedback over melting time without the feedback τ_α/τ_0 . Each line represents the ratio for a loss of different percent of the initial ice volume. The red line shows the ratio of the decay time with feedback over the decay time without feedback for a 10% ice loss (corresponding to Figures 2 and 4). The influence of the feedback becomes less dominant with stronger warming above the critical threshold (x-axis). Near the threshold the melting time without feedback diverges stronger ($1/\Delta T$) than the melt time with feedback which declines logarithmically.

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