

1 Two well marked cases of aerodynamic adjustment of sastrugi

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10 **Keywords:** Antarctica - Drag coefficient - Drifting snow – Sastrugi adjustment – Sastrugi
11 form drag

12 Abstract

13 In polar regions, sastrugi are a direct manifestation of drifting snow and form the main surface
14 roughness elements. In turn, sastrugi influence the local wind field and associated aeolian snow
15 mass fluxes. Little attention has been paid to these feedback processes, mainly because of
16 experimental difficulties, and, as a result most polar atmospheric models currently ignore
17 sastrugi. More accurate quantification of the influence of sastrugi remains a major challenge.
18 In the present study, wind profiles and aeolian snow mass fluxes were analyzed jointly on a
19 sastrugi covered snowfield in Antarctica. Neutral stability 10-m air-snow drag coefficients
20 C_{DN10} were computed from six level wind speed profiles collected in Adélie Land during austral
21 winter 2013. The aeolian snow mass flux in the first meter above the surface of the snow was
22 also measured using a windborne snow acoustic sensor. This paper focuses on two cases during
23 which sastrugi responses to shifts in wind direction were evidenced by variations in drag
24 coefficients and aeolian snow mass fluxes. Using this dataset, it was shown that (i) C_{DN10} values
25 were in the range of $1.3-1.5 \times 10^{-3}$ when the wind was well aligned with the sastrugi and
26 increased to 3×10^{-3} or higher when the wind only shifted 20-30°, (ii) as C_{DN10} increases, the
27 aeolian snow mass flux can decrease (to 80%) in response to a shift in wind direction, (iii) the
28 timescale of sastrugi aerodynamic adjustment can be as short as 3 h for friction velocities of 1
29 $m s^{-1}$ or above and during strong windborne snow conditions, and (iv) knowing C_{DN10} is not
30 sufficient to estimate the erosion flux that results from drag partitioning at the surface because
31 C_{DN10} includes the contribution of the sastrugi form drag. These results not only support the
32 existence of feedback mechanisms linking sastrugi, aeolian particle transport and surface drag

1 properties over snow surfaces but also provide orders of magnitude **in terms of changes in drag**
2 **coefficients and aeolian snow mass fluxes as well as sastrugi streamlining timescales**, although
3 further measurements including continuous accurate descriptions of the sastrugi field are
4 certainly still needed. Such measurements are essential to improve parameterization schemes
5 for aeolian snow transport models **and general drag parameterizations for weather, climate and**
6 **earth system models**.

7 **1. Introduction**

8 In polar regions, sastrugi are a direct manifestation of drifting snow. Sastrugi are elongated
9 ridges of wind-packed snow **1 to 2 meters in length** whose longitudinal axis is parallel to the
10 prevailing wind at the time of their formation. These erosional surface roughness features are
11 very widespread over the Antarctic ice sheet (Kotlyakov 1961) where they can be major
12 determinants of surface roughness (Jackson and Carroll 1978; Inoue 1989; Andreas 1995;
13 Andreas and Claffey 1995). Sastrugi orientations have been recognized as useful indicators of
14 the Antarctic near-surface wind direction (Mather 1962, 1969; Mather and Miller 1966; Rémy
15 et al. 1992; Long and Drinkwater 2000) in agreement with continent-scale modeling studies
16 (Parish and Bromwich 1987, 2007; Van Lipzig et al., 2004).

17 The development of sastrugi depends on the ability of snow to be eroded and thus on the
18 threshold velocity needed to lift snow particles from the surface. In the literature, aeolian
19 erosion thresholds have been reported to vary over a wide range of values depending on diverse
20 parameters such as temperature, time of sintering, snow cohesion or snow density, all of which
21 are interrelated. From observations in Antarctica, Mellor (1965) reported that 10-m wind speeds
22 of 3 to 8 m s⁻¹ are strong enough to cause aerodynamic entrainment of loose, unbounded snow,
23 whereas winds exceeding 30 m s⁻¹ are needed to erode snow consolidated by the freeze-thaw
24 process. Budd et al. (1966) suggested a high threshold wind speed (14 m s⁻¹) was needed to
25 trigger snow transport in the cold environment of Byrd station. Schmidt (1980) reported that
26 the threshold wind speed increases with the time since snow deposition, **and that this increase**
27 **slows with time and is slower at lower temperatures**. Schmidt (1982) also showed that the
28 cohesion of the snow surface determines the threshold speed required for snow erosion to occur.
29 In Antarctica, Bromwich (1988) highlighted a seasonal contrast between winter threshold wind
30 speeds of 7 m s⁻¹ and higher thresholds of more than 13 m s⁻¹ in summer because of greater
31 surface adhesion. Pomeroy et al. (1993) identified significantly lower thresholds for fresh,
32 loose, dry snow than for older, wind hardened, dense or wet snow. Yong and Metaxas (1985)

1 referred to age hardening to describe a measured increase in the density of natural fresh snow
2 from 100 kg m^{-3} to 300 and 400 kg m^{-3} after respectively 30 and 50 days at a relatively constant
3 temperature of $-13 \text{ }^\circ\text{C}$. Gray and Morland (1995) reported that snow compaction (related to
4 snow density) increases rapidly after deposition due to the thermal processes of metamorphism
5 (i.e. changes in snow structure over time). Li and Pomeroy (1997) discussed the major role of
6 temperature in surface erodibility (i.e. the potential of a surface to be eroded; Shao 2008) and
7 showed an empirical but generally positive correlation between threshold wind speed and air
8 temperature on the prairies of western Canada. From the work of Guyomarc'h and Mérindol
9 (1998), Gallée et al. (2001) developed an aeolian snow transport model that takes
10 metamorphism into account by allowing the threshold condition for erosion to vary with the
11 properties of the snow such as density, dendricity, sphericity and particle size. All studies
12 suggest that the physical properties of the snow play a major role in the formation of sastrugi.
13 Sastrugi contribute to the drag exerted on the atmosphere over the snow surface and enhance
14 interactions at the air-snow interface compared to over a smooth snow surface. Rougher snow
15 surfaces favor the generation of turbulence in the near surface air stream that is likely to further
16 increase the wind driven snow mass flux (Das et al. 2013). On the other hand, sastrugi are
17 responsible for a loss of wind momentum through pressure fluctuation gradients in their
18 immediate vicinity (sastrugi form drag) that directly reduces the energy budget available for
19 erosion of snow. This attenuating effect on snow erosion is taken into account in the coupled
20 atmosphere-snowpack-aeolian snow transport model MAR (Galleé et al. 2013) and was
21 parametrized as in Marticorena and Bergametti (1995). By comparing observed and simulated
22 aeolian snow mass fluxes over Adélie Land using MAR, Amory et al. (2015) showed that in
23 the model, erosion efficiency is highly sensitive to the parameterization of surface roughness,
24 and underlined the need for observational characterization of interactions between wind-
25 induced roughness features and aeolian transport of snow. Some authors have shown that the
26 sastrugi form drag actually depends on how the wind is oriented with respect to the main
27 sastrugi axis. Based on measurements of wind speed and temperature profile in the atmospheric
28 surface layer at the South Pole, Jackson and Carroll (1978) reported that sastrugi form drag was
29 essentially absent when the wind was perfectly aligned with the sastrugi up to a height of 50
30 cm. As the wind rotated, sastrugi form drag increased, to reach maximum when the wind
31 direction was perpendicular to the prior sastrugi pattern. These authors developed an idealized
32 single sastruga model from Lettau's (1969) findings to reproduce their observations. Using
33 another analytical sastruga model adapted from Raupach (1992), Andreas (1995) also found a
34 minimum and a maximum drag for wind directions respectively parallel and perpendicular to

1 the sastruga longitudinal axis.
2 However, these modeling efforts were undertaken without accounting for the erodible character
3 of sastrugi or for their possible reorganization when realigning with persistent (erosive) winds
4 blowing transversally to their elongated sidewalls. If the crosswise flow continues from a
5 relatively constant direction thereby allowing sufficient shear stress to dislodge snow surface
6 particles, sastrugi can adjust aerodynamically; transversal sastrugi are eroded, and new
7 streamlined sastrugi form parallel to the mean wind (Andreas and Claffey 1995). This results
8 in a gradual decrease in the contribution of the sastrugi to the total surface drag, and hence in
9 an increase in erosion efficiency. Andreas and Claffey (1995) reported that the timescale for
10 this streamlining process on Weddell Sea ice in winter was about half a day with 6-8 m s⁻¹
11 winds, but might be shorter if the winds are stronger. To date, no observational study has
12 provided quantitative insight into the potential effect of erodible roughness elements of the
13 snow surface on snow erosion.

14 Quantifying the variable influence of sastrugi on the local wind field and associated surface
15 drag could improve parameterization of surface roughness and erosion in polar atmospheric
16 models that currently ignore sastrugi. The present paper focuses on two erosion events during
17 which sastrugi responses to shifts in wind direction were interpreted from temporal variations
18 in both measured drag and aeolian snow mass flux in coastal Adélie Land during austral winter
19 2013.

20 **2. Data and Method**

21 **2.1. Field area**

22 Site D17 (66.7°S, 139.9°E; ~450 m asl.) is located about 10 km inland in a coastal accumulation
23 zone of Adélie Land (Agosta et al. 2012), roughly 15 km southwest of the permanent French
24 station Dumont d'Urville (Fig. 1). An annual temperature of -10.8 °C and a mean wind of
25 around 10 m s⁻¹ have been reported at Dumont d'Urville station (König-Langlo et al. 1998).
26 The measurement area consists in a gently sloping snowfield with a long unobstructed upstream
27 fetch several hundred kilometers over a uniform snow surface. Local topographic channeling
28 acts together with the Coriolis force to produce southeasterly flows all year round that result
29 either from pure katabatic or combined katabatic-synoptic forcings (Parish et al. 1993, Naithani
30 et al. 2001).

31 Site D17 is visited only during summer (December to February), when the presence of sastrugi
32 is often reported. Frequent strong winds combined with the permanent snow surface lead to

1 frequent aeolian snow transport events (Trouvilliez et al. 2014), thereby favoring aerodynamic
2 adjustment of the snow surface. This results in a net south-southeast orientation of the sastrugi
3 (Fig. 2).

4 2.2. Instrumentation

5 The measurement structure deployed at site D17 is a 7-m high meteorological mast. Wind
6 speed, relative humidity and air temperature are recorded along the mast at 6 logarithmically
7 spaced intervals between 0.8 and 7 m above the snow surface using Vector A100LK cup
8 anemometers and HMP45A thermo-hygrometers installed in naturally ventilated MET21
9 radiation shields (Fig 3). The anemometers are mounted on roughly 1-m long booms pointing
10 southeastward. Wind direction was only sampled at the upper level by a Vector W200P wind
11 vane. Surface level variations were measured by a Campbell SR50A acoustic depth gauge.
12 Information on drifting snow was obtained from a second-generation acoustic FlowCapt™
13 device that was set up vertically close to the ground to allow detection of the beginning of
14 aeolian snow transport events. The sensor is a 1-m long tube that converts the acoustic pressure
15 caused by snow particles impacting the tube into an aeolian snow mass flux integrated over the
16 length of the tube. The second-generation FlowCapt™ was evaluated in the French Alps by
17 Trouvilliez et al. (2015). The authors reported that the instrument underestimates the aeolian
18 snow mass flux compared to a reference optical sensor (Snow Particle Counter S7; Sato et al.
19 1993), especially during snowfalls. Nevertheless, the equivocal behavior of the second-
20 generation FlowCapt™ does not affect its ability to accurately detect the occurrence of aeolian
21 snow transport. Data were sampled at 15 s intervals, averaged to half-hourly means and stored
22 in a Campbell CR3000 datalogger.

23 2.3. The 10-m drag coefficient in near-neutral conditions

24 Computing the drag coefficient (C_D) is a convenient way to estimate the local drag exerted by
25 the surface on the overlying air. C_D can be computed by measuring the vertical wind speed
26 gradient (profile method) under near-neutral conditions following the Monin-Obukhov
27 similarity theory. Assuming stationarity and horizontal homogeneity when the atmospheric
28 surface layer is statically neutral, the wind speed profile is logarithmic and can be written as

$$U(z) = \frac{u_*}{\kappa} \ln\left(\frac{z}{z_0}\right), \quad (1)$$

1 where $U(z)$ is the average wind speed as a function of height z , κ is the von Kármán constant
 2 (taken as 0.4), z_0 is the aerodynamic roughness length, and u_* the friction velocity describing
 3 the wind shear at the surface and is related to the vertical momentum flux at the surface (τ ; also
 4 known as Reynolds shear stress)

$$\tau = \rho u_*^2 = -\rho \overline{uw} = \rho C_{DNz} U_z^2, \quad (2)$$

5 where ρ is the air density, u and w are fluctuations in the longitudinal and vertical turbulent
 6 velocity, respectively, and C_{DNz} and U_z are the neutral-stability drag coefficient and the average
 7 wind speed at height z , respectively. The overbar stands for a time average. C_{DN} is usually
 8 discussed at a standard reference height of 10 m (C_{DN10}). From (2) and (3), it follows that

$$C_{DN10} = \left[\kappa / \ln \left(\frac{10}{z_0} \right) \right]^2, \quad (3)$$

9 with z_0 expressed in meters. Here C_{DN10} and z_0 are two equivalent quantities for evaluating the
 10 momentum exchange at the air-snow interface that results from the integrated (in space and
 11 time) turbulent drag caused by the roughness elements.

12 The wind profiles used to compute C_{DN10} were selected following a strict procedure. After
 13 discarding icing or malfunctioning cases and half-hourly runs for which a rare (northwesterly)
 14 flow was likely to be disturbed by the measurement structure, stationary conditions were
 15 selected by requiring that temperature changes between two consecutive half-hourly runs not
 16 exceed 0.3 K, as suggested by Joffre (1982). Near-neutral conditions were then selected
 17 requiring $U > 5 \text{ m s}^{-1}$ and an absolute value of the bulk Richardson number below 10^{-2} . The last
 18 selection criterion was applied following a suggestion by Andreas and Claffey (1995) that
 19 demands

$$\frac{\sum_{i=1}^6 [U(z_i) - (u_*/\kappa) \ln(z_i/z_0)]^2}{u_*^2} \leq \varepsilon, \quad (4)$$

21
 22 where ε is an empirical constant determined from visual inspection of the observed wind speed
 23 profiles. Here it was set to 0.15. Wind profiles that survived this filtering process were fitted
 24 (1) using a least-square log-linear regression technique, and u_* and z_0 deduced from the
 25 regression coefficients. All of them yielded a correlation coefficient (r^2) larger than 0.99. The
 26 80% confidence limits of each calculated C_{DN10} value were determined following the statistical

1 method proposed by Wilkinson (1984). The highest uncertainty bounds deduced from these
2 confidence limits reached $\pm 14\%$.

3 **3. Results**

4 The two erosion events depicted in Figure 4 occurred respectively in March (left panels) and
5 October (right panels), 2013, during particularly constant wind direction conditions, which
6 persisted after a wind shift of a few tens of degrees. Such a constancy in wind direction,
7 necessary for the following demonstration, is very rare. Combined to the strict selection
8 procedure, only two cases were exploitable in this context. The 2-m wind speed, wind direction,
9 profiled-derived C_{DN10} values and aeolian snow mass flux recovered by the second-generation
10 FlowCapt™ sensor are shown in Figure 4. As the friction velocity is the actual dynamic quantity
11 involved in aerodynamic entrainment of surface snow particles (Gallée et al. 2001), it is also
12 plotted on the graph. The two events are split into three parts, before (A_i), during (B_i) and after
13 (C_i) the shift in wind direction. The occurrence of precipitation may affect the detection of
14 erosion events because the FlowCapt™ sensor does not distinguish between eroded (saltating
15 particles and/or suspended particles of snow) and precipitating snow particles. No visual
16 observation of precipitation from the nearby Dumont d'Urville station were available for the
17 period concerned. Moreover, as Adélie Land is very prone to aeolian transport of snow
18 Trouvilliez et al. (2014), these observations, if performed, are limited by the inability to
19 discriminate between actual precipitation and pure drifting snow. Here we used the operational
20 analyses of the European Center for Medium-Range Weather Forecasts (horizontal resolution
21 of ~ 16 km) to evaluate the occurrence of precipitation at our measurement site. We assumed
22 that both events were pure erosion events after finding negligible precipitation rates for the fully
23 continental grid point including D17.

24 At the beginning of Julian day (JD) 87 (part A_1), the wind direction was around 140° , the
25 friction velocity was above the erosion threshold with a related aeolian snow mass flux of 100
26 $\text{g m}^{-2} \text{s}^{-1}$, and C_{DN10} was near 1.5×10^{-3} . At the end of JD 87 (part B_1), the wind rotated toward
27 160° while C_{DN10} increased to nearly 3.3×10^{-3} , i.e. by 120%, in response to a wind shift of
28 only 20° . As assumed in Jackson and Carroll (1978) and Andreas and Claffey (1995), it is likely
29 that as the wind turned, it was deflected from the mean sastrugi axis, thereby encountering a
30 rougher surface. As a result, C_{DN10} soared, reflecting the growing contribution of the sastrugi
31 form drag to the vertical momentum flux at the surface, and hence to the total surface drag.
32 Within the same time frame, the measured aeolian snow mass flux fell by $\sim 30\%$ from 365 to

1 $260 \text{ g m}^{-2} \text{ s}^{-1}$, despite increasing friction velocity (wind speed) from 0.7 to 1.6 (18 to 24) m s^{-1} .
2 Then, until the end of the event (part C₁), the wind direction remained centered about 160°.
3 From 0330 UT to 0630 UT on JD 88, $C_{\text{DN}10}$ fell back to 1.5×10^{-3} as high winds presumably
4 streamlined the surface. In other words, $C_{\text{DN}10}$ was reduced by ~50% in only 3 hours. As $C_{\text{DN}10}$
5 decreased, the aeolian snow mass flux again rose above $400 \text{ g m}^{-2} \text{ s}^{-1}$. The erosion event lasted
6 through JD 90 when u_* (wind speed) dropped to 0.7 (15) m s^{-1} , causing a significant decrease
7 in the aeolian snow mass flux. After nearly 48 hours of persistent erosive winds, $C_{\text{DN}10}$ was as
8 low as 1.3×10^{-2} .

9 During the two days that preceded the second erosion event (part A₂), the wind direction was
10 within $\pm 10^\circ$ of 150°, the friction velocity was generally not strong enough to erode the snow
11 surface, and $C_{\text{DN}10}$ was between $1.3 - 1.6 \times 10^{-3}$. $C_{\text{DN}10}$ and wind direction were strongly
12 correlated during this period, with the lowest drag coefficients occurring for a wind direction
13 of around 140°, suggesting that this was the sastrugi alignment before erosion started and the
14 wind changed direction. Then, the same situation depicted in the left panels of Figure 4 occurred
15 again. At mid-JD 286 (part B₂), u_* increased beyond the erosion threshold as the wind rotated
16 from 150° to 180°. Consequently, $C_{\text{DN}10}$ increased to 1.9×10^{-3} . The aeolian snow mass flux
17 dropped simultaneously from 320 to 55 $\text{g m}^{-2} \text{ s}^{-1}$ under increasing friction velocity. That is, for
18 a ~30% increase in $C_{\text{DN}10}$ as the result of a wind deflection of 30°, the aeolian snow mass flux
19 decreased by ~80%. Together with the first case of erosion, this illustrates how the form drag
20 exerted by sastrugi can significantly affect snow erosion when the wind and sastrugi are not
21 aligned (this effect is discussed later in the paper; see Section 4). Then (part C₂), the wind
22 direction remained roughly unchanged until erosion ceased. Again, the rise in aeolian snow
23 mass flux coincided with a decrease in $C_{\text{DN}10}$. After nearly 3 hours of winds above 20 m s^{-1} (u_*
24 $> 0.9 \text{ m s}^{-1}$) from 180°, $C_{\text{DN}10}$ fell from 1.9×10^{-3} to 1.4×10^{-3} , i.e. decreased by ~30%.

25 In summary, for friction velocities (wind speeds) around 1 (20) m s^{-1} and above, the sastrugi
26 streamlining timescale can be as fast as 3 hours. For a windflow initially aligned with the
27 sastrugi, a deviation of 20-30° from the streamlining direction has the potential to both increase
28 $C_{\text{DN}10}$ by 30-120% and to significantly reduce (up to 80%) the aeolian snow mass flux, even
29 under increasing friction velocity.

30 **4. Discussion**

31 At Ice Station Weddell, Andreas and Claffey (1995) measured a decrease in $C_{\text{DN}10}$ of 20-30%
32 in 12 hours with considerably weaker winds ($< 12 \text{ m s}^{-1}$) than those reported here. The

1 observations reported in this paper show that this timescale can be 4 times faster for winds
 2 exceeding 20 m s^{-1} ($u_* > 1 \text{ m s}^{-1}$), and the associated decrease in $C_{\text{DN}10}$ can reach 50%. Andreas
 3 and Claffey (1995) also proposed generic $C_{\text{DN}10}$ values in the range $1.5\text{-}1.7 \times 10^{-3}$ when the
 4 wind is well aligned with the sastrugi, and around 2.5×10^{-3} when the wind is at an angle of 20°
 5 to the dominant orientation of the sastrugi. In both cases, the present results differ slightly from
 6 these values: $C_{\text{DN}10}$ was more in the range $1.3\text{-}1.5 \times 10^{-3}$ for sastrugi-parallel winds, and
 7 increased to more than 3×10^{-3} with wind shifts of similar amplitude. For a given erosion
 8 threshold, the quantity of windborne snow increased with wind strength according to a power
 9 law (Radok 1977; Mann 2000). As sastrugi mainly form through snow erosion/deposition
 10 processes (Filhol and Sturm 2015), it is likely that under the strong wind (shear) conditions in
 11 Adélie Land, rougher snow surfaces develop, whose aerodynamic adjustment ability is greater
 12 than at the less windy Ice Station Weddell.

13 It can be argued that friction velocity also influences the value of $C_{\text{DN}10}$. It is true that changes
 14 in the wind during saltation are perceived by the flow as an increase in surface roughness due
 15 to the straight line extrapolations of the wind velocity on a log-linear plot from above the
 16 saltation layer down to $U=0$ (Anderson and Haff 1991; Bintanja 2001). Therefore, the saltation
 17 layer behaves as solid roughness. Owen (1964) suggested that the aerodynamic roughness
 18 length should scale as u_*^2/g , roughly the height to which saltating particles are ejected. He wrote

$$z_0 = \alpha \frac{u_*^2}{g}, \quad (5)$$

19 with α a constant and g the gravitational acceleration. However, aeolian snow mass flux peaks
 20 did not match $C_{\text{DN}10}$ peaks. However, significant variations in $C_{\text{DN}10}$ strongly correlated to the
 21 wind direction were observed during roughly constant friction velocity conditions and in the
 22 absence of drifting snow (Part A₂, Fig. 4). Moreover, aeolian snow mass flux peaks did not
 23 match $C_{\text{DN}10}$ peaks for both erosion events. A simple order-of-magnitude calculation allows the
 24 assessment of Owen's relation during a period of drifting snow at our measurement site. From
 25 06:00 UT on JD 88 to 06:00 UT on JD 89 during part C₁, the wind speed is around 27 m s^{-1} ,
 26 drifting snow is active with an aeolian snow mass flux around $350 \text{ g m}^{-2} \text{ s}^{-1}$, and u_* and $C_{\text{DN}10}$
 27 are about 1.1 m s^{-1} and 1.5×10^{-3} . According to Eq. (5), the corresponding value for α is $2.7 \times$
 28 10^{-3} . Using Eq. (5) with this value of α to predict the increase in z_0 during period B₁ when u_*
 29 reaches 1.7 m s^{-1} yields $z_0 = 7.8 \times 10^{-4} \text{ m}$, that is, $C_{\text{DN}10} = 1.79 \times 10^{-3}$. This last value is well
 30 below the observed one of 3.3×10^{-3} . Here the height of the saltation layer was probably not a

1 major determinant of the roughness length, and the variability in C_{DN10} (or z_0) due to Owen's
2 effect was presumably swamped by those due to sastrugi alignment. A single-parameter
3 formulation for z_0 as (5) is therefore innately incomplete, a conclusion already reached by
4 Raupach (1991) and Andreas and Claffey (1995).

5 During both erosion events, the FlowCapt™ sensor measured significant aeolian snow mass
6 fluxes for 2-m wind speeds (u_*) of 10 (0.6) $m\ s^{-1}$ or above. As the wind (friction) velocity likely
7 frequently exceeds this threshold on the coastal slopes of Adélie Land, the sastrugi alignment
8 process might be also frequently active, depending on persistence of the wind. As explained in
9 Section 1, this mechanism is probably also strongly controlled by the properties of the snow
10 surface that determine the threshold shear stress required for erosion to begin rather than only
11 the characteristics of the wind. Since the erosion flux is the integrated result of both the capacity
12 of the wind to erode and carry snow, and snow surface erodibility, the sastrugi streamlining
13 timescale presumably mostly depends on this specific quantity. The implication is that the drag
14 coefficient must be strongly related to other factors including the current wind orientation and
15 the history of the wind's interactions with the snow surface as well as past timescales and past
16 temperatures of the snowpack.

17 On the other hand, the sastrugi streamlining timescale also appears to control snow erosion in
18 the form of feedback by fixing the time during which the sastrugi form drag mainly contributes
19 to total surface drag. With friction velocities above the snow erosion threshold, increasing u_*
20 could be expected to result in an increase in erosion efficiency. However, in both cases, the
21 observations showed a significant decrease in the aeolian snow mass flux in phase with an
22 increase in the drag coefficient (Figure 4, parts B). By analogy with measurements made in a
23 water flume (Wiberg and Nelson 1992; Le Bouteiller and Venditti 2015), it can be considered
24 that the flow and turbulence in the sastrugi region are the result of interaction between flow
25 separation and wake formation, which can lead to a local Reynolds shear stress peak
26 corresponding to flow separation. Above the region of influence of the wake, named outer
27 region, the flow has adjusted to increased roughness and exhibited a logarithmic profile, as
28 shown by the relative continuous time series of C_{DN10} and u_* despite the strict selection
29 procedure (Fig. 4). Even if the shear stress of the outer flow (τ) is relatively easy to measure, it
30 cannot be extrapolated to the snow bed. The averaged snow bed shear stress (also referred to as
31 skin friction in the literature), which is the ultimate parameter for aeolian erosion (Li and Shao
32 2003), varies depending on its position along the sastrugi field. In absence of direct
33 measurements, it is necessary to link outer shear stress, sastrugi geometry, and skin friction to
34 be able to estimate aeolian snow mass fluxes. This is quite important since the reduction of

1 shear stress near the surface is crucial in limiting the growth of the mass flux (Groot Zwaafink
2 et al., 2014). For erodible forms in riverbeds such as ripples, Smith and McLean (1977) and
3 later Wiberg and Nelson (1992) developed a method for partitioning the outer shear stress.
4 These authors considered that the averaged bed shear stress is equal to the difference between
5 the outer shear stress and the drag-related stress produced as the flow is forced around the
6 bedform – i.e., in the present case, the form drag induced by the sastrugi. As mentioned above,
7 an increasing form drag can be expected, and hence a decrease in skin friction and in aeolian
8 snow mass flux, when the wind direction gradually shifts away from the longitudinal axis of
9 the sastrugi. Because C_{DN10} reflects the contribution of the sastrugi form drag, knowing the
10 drag coefficient is not sufficient to estimate skin friction. A better knowledge of skin friction
11 over a sastrugi field is also needed to improve aeolian snow mass flux parameterizations in
12 aeolian erosion models. The measurements made in the present study showed that a
13 considerable decrease (even 80%) of the aeolian snow mass flux can occur during the
14 transitional regime during which the wind and sastrugi are not aligned (Figure 4, parts B). But
15 it should be also noted that the rapid aerodynamic adjustment of sastrugi (3 hours) will limit
16 errors if the aeolian snow transport event considered is strong and sufficiently long.

17 5. Conclusion

18 An experimental meteorological dataset collected in coastal Adélie Land during austral winter
19 2013 was exploited to document surface turbulent fluxes of momentum and snow over an
20 Antarctic sastrugi field. The main results of the analysis of two erosion events can be
21 summarized as follows:

- 22 - C_{DN10} values were in the range of $1.3-1.5 \times 10^{-3}$ when the wind was well aligned with
23 sastrugi and increased to 3×10^{-3} or higher with wind shifts of only 20-30°,
- 24 - As C_{DN10} increases, the aeolian snow mass flux may decrease (to 80%) in response to
25 the wind shift in direction,
- 26 - the timescale for the aerodynamic adjustment of sastrugi can be as low as three hours
27 for friction velocities of 1 m s^{-1} or above and during strong windborne snow conditions,
- 28 - because C_{DN10} includes the contribution of the sastrugi form drag, knowing C_{DN10} is
29 not sufficient to estimate the erosion flux that results from drag partitioning at the
30 surface.

1 These results support the existence of mechanisms linking aeolian particle transport and surface
2 drag properties over (Antarctic) snow, as already demonstrated for other erodible natural
3 surfaces (Marticorena and Bergametti 1995). In contrast with non-erodible roughness elements
4 such as rocks or vegetation, these mechanisms involve the time needed for sastrugi to adjust to
5 the main wind (3 hours in both erosion events), during which both the drag coefficient and the
6 aeolian snow mass flux can be greatly modified. In comparison, Andreas and Claffey (1995)
7 reported a longer timescale (12 hours) for the sastrugi to realign with weaker winds. Because
8 lighter winds are supposed to be associated with lower erosion fluxes, it is suggested that the
9 sastrugi streamlining timescale most likely depends on the snow erosion flux.

10 Real-time observations **of the distribution (size, abundance, orientation) of the sastrugi** would
11 further advance understanding of the physical processes involved in the development of sastrugi
12 and enable better characterization of sastrugi aerodynamic adjustment timescales. In addition,
13 having a more accurate representation of the **distribution** of sastrugi would make small-scale
14 modeling in a wind tunnel possible, in which case, it would be possible to realistically estimate
15 shear stress partitioning. One possible way to monitor sastrugi would be to set up an automatic
16 mini laser-scan. Such a device was developed in the framework of the MONISNOW research
17 project (Picard and Arnaud, LGGE, personal communication) and has been operating daily at
18 Dome C in Antarctica since the beginning of 2015. These complementary approaches are vital
19 to improve parameterization schemes for aeolian snow transport models **and general drag**
20 **parameterizations for weather, climate and earth system models.**

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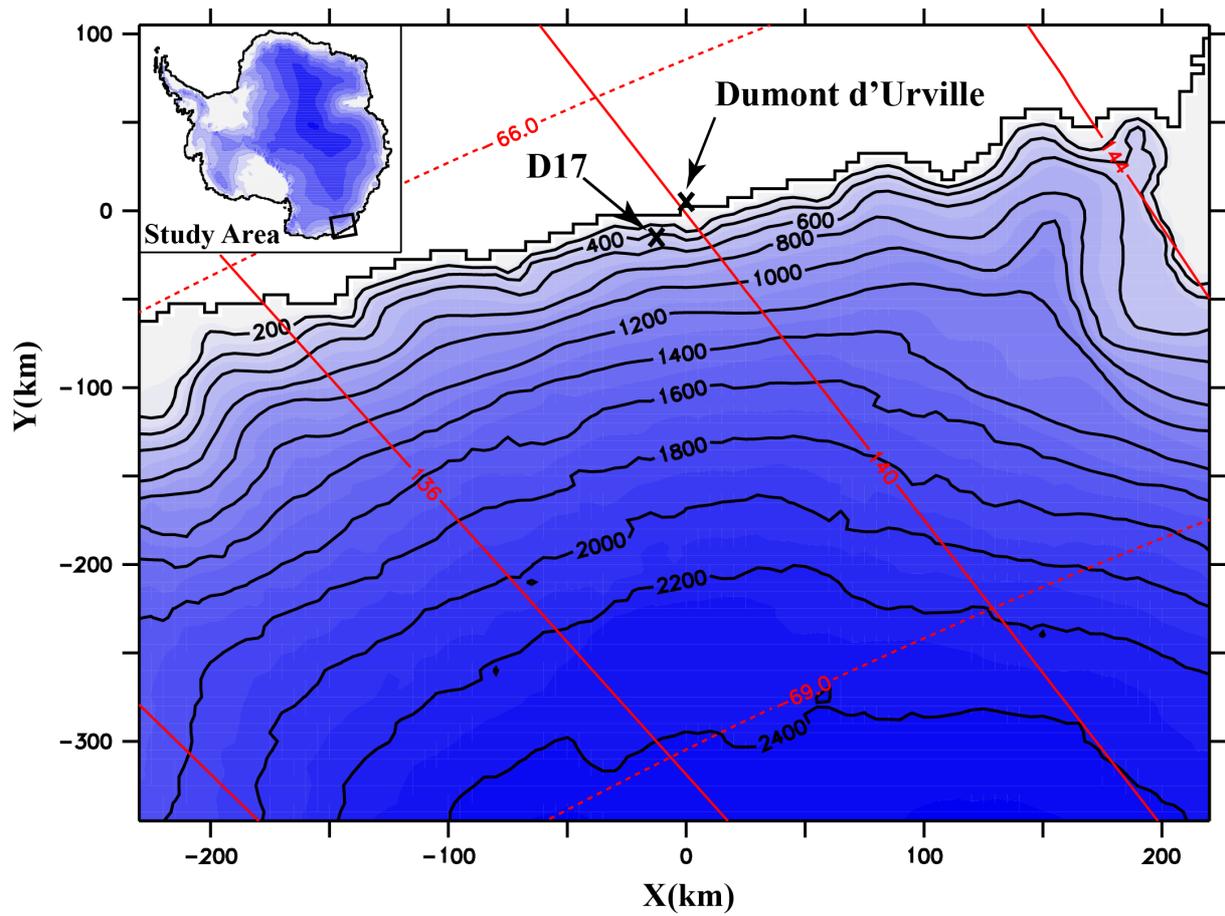
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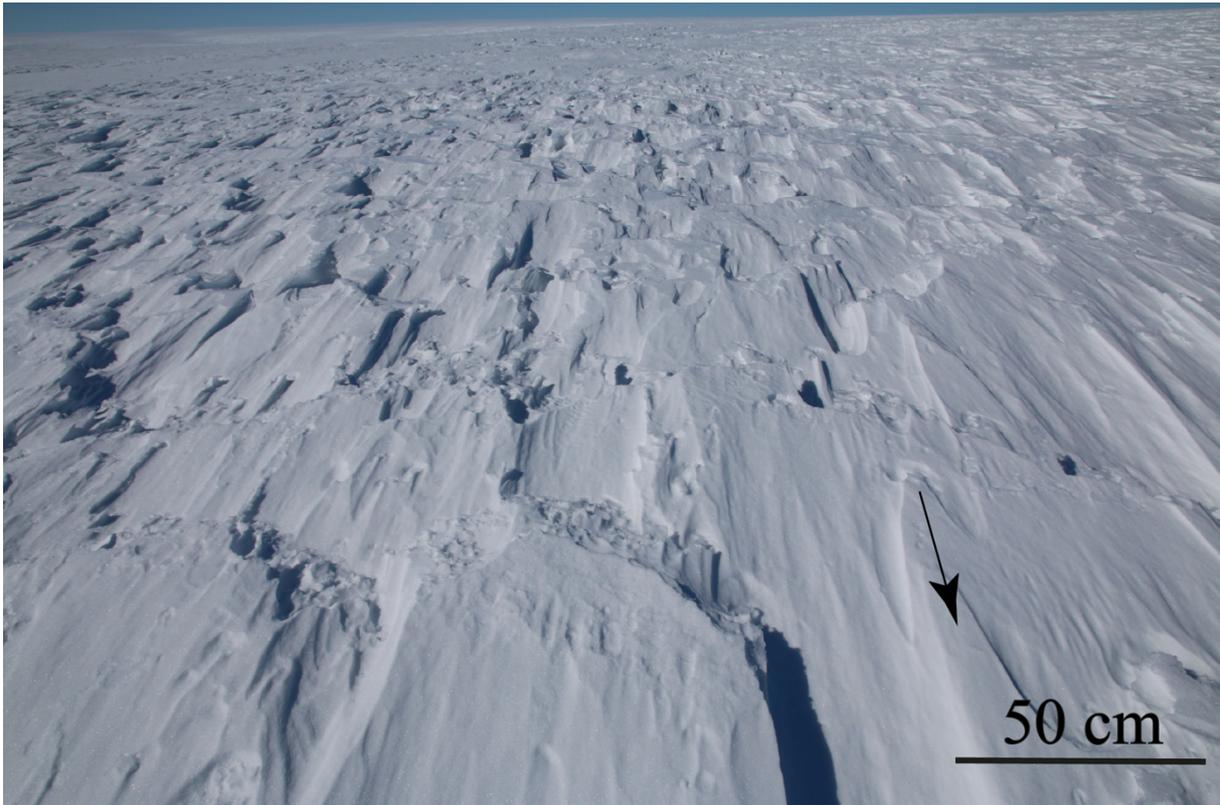
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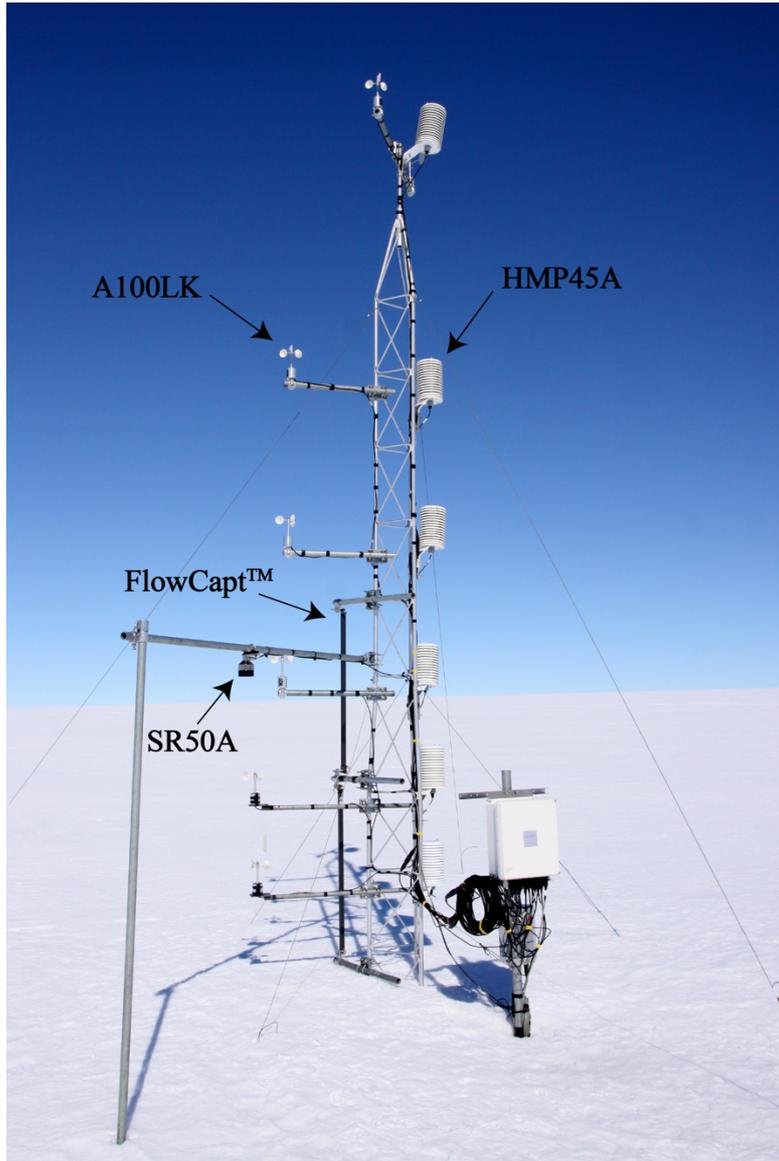


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 2 **Fig. 1.** Map of Adélie Land showing the location of Dumont d'Urville station and measurement
 3 site D17. Contour lines are in meters.



1

2 **Fig. 2.** Photograph of the snow surface at D17 in January 2014. The arrow indicates the mean
3 direction of the wind episode that led to the formation of the sastrugi.



1
2

Fig. 3. The measurement structure deployed at D17.

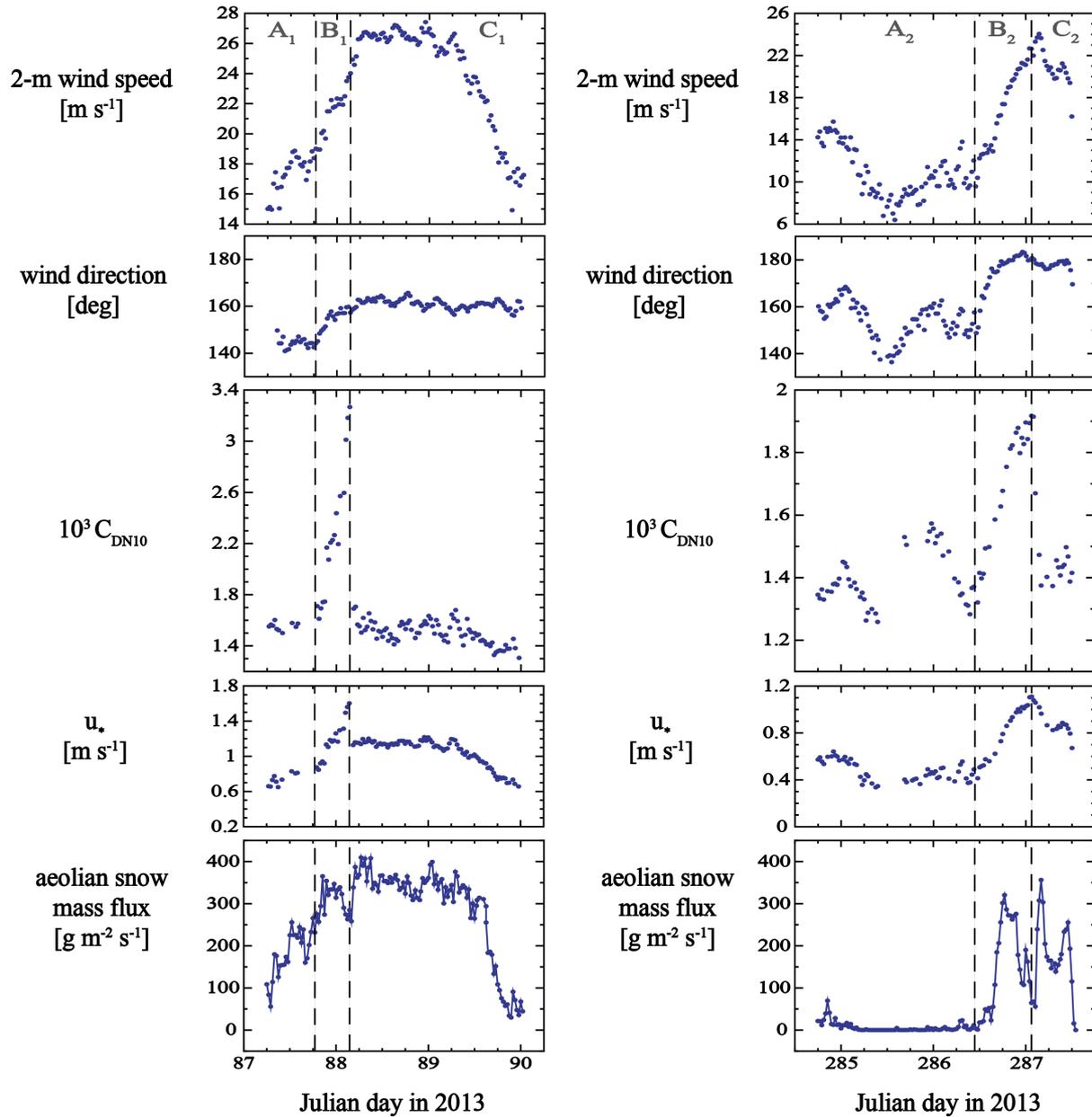


Fig. 4. Two erosion events showing sastrugi responses to shifts in wind direction. Note the different vertical scales between right and left panels concerning measured 2-m wind speed and profile-derived C_{DN10} and u_* values. The aeolian snow mass fluxes come from the second-generation FlowCapt™ sensor set up from 0 to 1 m above the snow surface. In both cases, the event is split into three parts, respectively before (A_i), during (B_i) and after (C_i) the wind shift.