J.H. Bondzio et al.

We thank the editor very much for his constructive comments, and discuss them below. The editor's comments are shown in blue, and our responses in black.

1 Editor (Olivier Gagliardini):

RC: Dear Johannes,

I have now read the two reviews, your response to each one and the new version of your manuscript. I think the new version has been improved by accounting for most of the remarks made by both reviewers so that your paper can be accepted in TC. I have anyway found few errors/typos in the new manuscript that you should correct before it goes to TC.

Thanks for having choosing TC for this nice piece of work. Best regards Olivier Gagliardini

Remarks:

- page 3, line 15: (LSM Osher and Sethian, 1988) -> (LSM; Osher and Sethian, 1988)

AC: Done.

RC: - page 3, lines 22-23: Be more precise here. In Pralong and Funk (2014), was it to follow the calving front or the upper surface as in the work by Jouvet work? Add Jouvet references?

AC: Done.

RC: - page 3, line 25: you might add melange as a factor that control calving (see e.g. Krug et al, TC 2015).

AC: Done.

RC: - page 4, line 1: in the LSM is straightforward -> in the LSM should be straightforward

AC: Done.

RC: - page 4, lines 15-17: I don't understand what is really done to distinguish these two areas? Different sliding law? And how the shear margins are accounted for in the model?

AC: The distinction is made for reference in the text only. We moved the part up for more clarity.

RC: - page 7, line 9: to solve eq. (4). -> to solve Eq. (4).

AC: We refer to the equation by its name now.

RC: - page 8, line 2: you should specify here that $a^{\perp} = c^{\perp} + m$, the sum of a calving rate and frontal melting? And then later assume that $m = 0$ in what follow.

AC: Done.

RC: - Eq. (6): I would present it the other way : the level set velocity is the sum of ice velocity and ablation velo. I don't see the interest of equation (6), i.e. the expression of $a^{\perp}$ as a function of v and w will never be used, it is the equation that gives w that you need.
AC: Done.

RC: - page 8, line 12: For SSA, there is no need to extrude the mesh. A 2D mesh in the horizontal plane is enough?
AC: We used a 2D horizontal mesh, and see that this sentence is misleading, as it refers to the 3D case.

RC: - page 8, line 14-16: you should mention that, in an other hand, using the LSM in the vertical dimension would allow for example to account to non-uniform ice front melt and undercutting effects? but would also require to move to a 3d ice flow model (Stokes).
AC: See point above.

RC: - page 9, line 4: I would suggest to be exhaustive here and to give all the variables that need to be extrapolated outside of the ice domain. For the velocity, which is not a scalar field, you should aslo be more precise and specify how it is extrapolated (component by component I guess?).
AC: Done.

RC: - page 11, line 21: not all equations are concerned by the CFL criteria. You should specify which equations require this criteria to be fulfilled in order to have a stable numerical scheme.
AC: Done.

RC: - page 12, line 4: Knowing surface temperature doesn't allow to evaluate B. You would need to know the ice temperature for that. Which assumption is further made for ice temperature?
AC: We used surface temperatures as a rough approximation of the ice temperature, as they range in this area at low values between -8 and -28 °C. We rephrased the sentence.

RC: - page 13, line 5: w.n = 0 is true only if the norm of v and c are also equal? The fact that the two velocities are aligned along n is not sufficient?
AC: This is true, we added a subscript where missing. Done.

RC: - page 13, line 22: equation is out of the page.
AC: Done.

RC: - page 14, line 9-13: Isn't it A which is the constant calving rate forcing? Then I don't understand the sentence : "In experiment A, the calving front undergoes gradual retreat over time". Is there an error here. Are you really speaking about the A experiment?
AC: The calving front of experiment A undergoes gradual retreat of 20m/a, which we explain in the text now.

RC: - page 15, line 14: Fig. 7 shows -> Figure 7 shows
AC: Done.

RC: - page 15, lines 21-23: over which time period should be specified here.
AC: Done.

RC: - page 21, line 7: I think this conclusion is highly dependent on the very simple test used here which is really difficult to link to a real calving front? I would be less affirmative in suggesting a grid size to be applied for a real glacier.
AC: We rephrased the sentence.

RC: - Legend Fig. 6: along-trough. c) ice geometry -> along-trough; c) ice geometry
AC: We rephrased the sentence.

Manuscript prepared for The Cryosphere Discuss.
with version 2014/09/16 7.15 Copernicus papers of the LaTeX class copernicus.cls.
Date: 12 February 2016

Modelling calving front dynamics using a Level-Set Method: Application to Jakobshavn Isbræ, West Greenland

J.H. Bondzio[1], H. Seroussi[2], M. Morlighem[3], T. Kleiner[1], M. Rückamp[1], A. Humbert[1,4], and E. Larour[2]

[1]Alfred Wegener Institute, Helmholtz Centre for Polar and Marine Research, Bremerhaven, Germany
[2]Jet Propulsion Laboratory - California Institute of Technology, Pasadena, CA, USA
[3]Department of Earth System Science, University of California Irvine, Irvine, CA, USA
[4]University of Bremen, Bremen, Germany

Correspondence to: Johannes H. Bondzio (jbondzio@uci.edu)

Discussion Paper | Discussion Paper | Discussion Paper | Discussion Paper |

Abstract

Calving is a major mechanism of ice discharge of the Antarctic and Greenland Ice Sheets, and a change in calving front position affects the entire stress regime of marine terminating glaciers. The representation of calving front dynamics in a two or three dimensional ice sheet model remains non-trivial. Here, we present the theoretical and technical framework for a Level-Set Method, an implicit boundary tracking scheme, which we implement into the Ice Sheet System Model (ISSM). This scheme allows us to study the dynamic response of a drainage basin to user-defined calving rates. We apply the method to Jakobshavn Isbræ, a major marine terminating outlet glacier of the western Greenland Ice Sheet. The model robustly reproduces the high sensitivity of the glacier to calving, and we find that enhanced calving triggers significant acceleration of the ice stream. Upstream acceleration is sustained through a combination of mechanisms. However, both lateral stress and ice influx stabilise the ice stream. This study provides new insights into the ongoing changes occurring at Jakobshavn Isbræ, and emphasises that the incorporation of moving boundaries and dynamic lateral effects, not captured in flowline models, is key for realistic model projections of sea level rise on centennial time scales.

1 Introduction

Calving of icebergs is a major mean of ice discharge for marine terminating glaciers around the world. It accounts for about half of the ice discharge of the Greenland and Antarctic Ice Sheets (Cuffey and Paterson, 2010; Rignot et al., 2013). This process causes calving front retreat, which leads to reduced basal and lateral stress and results in upstream flow acceleration.

[Figure 1 about here.]

In order to assess the impact of calving on the dynamics of outlet glaciers using an ice sheet model, we need to include a dynamically evolving calving front. This requires tracking

the calving front position and adjusting the boundary conditions accordingly. Addressing these issues is rather straightforward for 1D-flowline or 2D-flowband models (Nick et al., 2009; Vieli and Nick, 2011), where the calving front is tracked along the flowline. However, this type of model lacks the consistent representation of lateral momentum transfer and lateral ice influx from tributaries for example, which have to be parametrised instead. This parametrisation may neglect feedback effects important for simulations on decadal to centennial time scales, e.g. catchment area entrainment (Larour et al., 2012a).

It is therefore critical to include a front tracking scheme in 2D-horizontal and 3D models, which has been addressed by only a few ice sheet models (e.g. Jouvet et al., 2008; Winkelmann et al., 2011). Various approaches to model the evolution of the shape of ice exist. Explicit methods track the position of a set of points, which represent the calving front. They require a complex technical framework to allow for geometric operations like folding and intersection of the continuum boundary, tracking singularities in curvature, and determining the position of a point in space relative to the modelled continuum. Alternatively, the Level-Set Method ~~(LSM Osher and Sethian, 1988)~~ (LSM, Osher and Sethian, 1988) represents the continuum boundary implicitly by a contour, or "level-set", of a so-called "Level-Set Function" (LSF). It easily handles topological changes of the modelled continuum, like splitting and merging. The LSM is based on a partial differential equation similar to the mass transport equation solved by ice sheet models. This makes the method straightforward to implement, and allows for the application to continental scale ice sheet simulations. Although the method does not necessarily conserve volume accurately, it is well established in Continuum Fluid Mechanics (Chang et al., 1996; Groß et al., 2006). A LSM has been applied to ~~ice flow modelling in test cases~~ represent the ice surface in 2D-flowband models (Pralong and Funk, 2004), but not to model real ice sheets yet.

Understanding calving dynamics remains challenging because of the diversity of factors involved in calving events. Bathymetry, tides and storm swell, as well as sea ice cover, ice mélange and temperatures of both sea water and air are possible factors influencing calving rates. However, their effect, their respective share and their interplay seem to vary from glacier to glacier, and are not well understood ~~(Cuffey and Paterson, 2010)~~(Cuffey and Paterson, 2

Therefore, no universal calving rate parametrisation exists to date (Benn et al., 2007), and we rely here on user-defined calving rates. However, incorporating calving rate parametrisations in the LSM ~~is~~ should be straightforward.

Jakobshavn Isbræ is a major marine terminating glacier in West Greenland, which drains about 6.5% of the Greenland Ice Sheet (Zwally et al., 2011). It is characterised by two branches, which today terminate into a 30 km long ice-choked fjord (Figs. 1 and 2). The southern branch exhibits high flow velocities, which are confined to a narrow, deep trough of about 5 km width. The trough retrogradely slopes inland to a maximum depth of about 1700 m below sea level (Gogineni et al., 2014), and discharges most of the ice of the drainage basin (Rignot and Mouginot, 2012). We refer to the fast-flowing area as "ice stream", and to the surrounding slow-moving ice as "ice sheet". Those areas are separated by pronounced shear margins on either side of the ice stream. Observations have shown that the fast flowing areas of Jakobshavn Isbræ exhibit a weak bed with a basal layer of temperate, soft ice (Lüthi et al., 2002). Basal sliding and shear in this layer cause most of these areas' horizontal motion. A large fraction of the ice stream's momentum is transferred to the adjacent ice sheet by lateral stress. It is thus well justified to use the two-dimensional shelfy-stream approximation (SSA, MacAyeal, 1989) to simulate this glacier.

~~We partition the catchment area into the confined, deep and fast-flowing trough ("ice stream") and the surrounding slow-moving ice ("ice sheet"). Those areas are separated by pronounced shear margins on either side of the ice stream.~~

[Figure 2 about here.]

Until the late 1990s, Jakobshavn Isbræ had a substantial floating ice tongue, which extended well into the fjord, and was fed by both branches. The calving front position remained fairly constant from 1962 to the 1990s (Sohn et al., 1998), and the glacier exhibited negligible seasonal variations in flow speed (Echelmeyer and Harrison, 1990). In the 1990s, the glacier started a phase of acceleration, thinning and retreat, that followed the breakup of its ice tongue. Seasonal variations in calving front position and flow velocity increased sharply (Joughin et al., 2004, 2008). Today, the glacier is one of the fastest ice streams in the world.

It is still far from equilibrium and is a major contributor to global sea level rise (Howat et al., 2011; Joughin et al., 2014). Observations suggest that the calving front position is a major control on the ice stream dynamics (Podrasky et al., 2012; Rosenau et al., 2013; Moon et al., 2014).

Various hypotheses have been proposed to explain the mechanisms behind this change. All identify the breakup of the floating ice tongue as the initial trigger of this dramatic chain of events, but different mechanisms have been proposed to explain the sustained acceleration, thinning and retreat of the glacier. Studies by Joughin et al. (2012) and Habermann et al. (2013) propose loss of buttressing and changes in basal conditions as the main cause behind the ongoing acceleration. On the other hand, van der Veen et al. (2011) argue that weakening of the lateral shear margins has significantly amplified the upstream acceleration. Several modelling studies of the glacier, which use 1D-flowline and 2D-flowband models, project unstable retreat of the glacier along its southern trough for up to 60 km inland within the next century (Vieli and Nick, 2011; Joughin et al., 2012; Nick et al., 2013). Other modelling studies argue that this type of ice stream is stable as long as it is fed by the surrounding ice sheet (Truffer and Echelmeyer, 2003). However, numerical ~~2D planview~~ 2D-planview modelling efforts of Jakobshavn Isbræ so far lacked the representation of a dynamically evolving calving front. Hence, the hypotheses could not be tested in a satisfactory manner.

We present here a LSM-based framework to model the dynamic evolution of a calving front. This method is a step towards better physical representation of calving front dynamics in 2D and 3D ice sheet models. We describe the implementation of the method into the Ice Sheet System Model (ISSM, Larour et al., 2012b), a parallel, state-of-the-art ice sheet model, and apply it here to Jakobshavn Isbræ in order to model its dynamic response to perturbations in calving rate.

2 Theory

2.1 Ice Flow Model

We employ the SSA on both floating and grounded ice. It neglects all vertical shearing but includes membrane stresses. The ice viscosity, μ, follows Glen's flow law (Glen, 1958):

$$2\mu = B\dot{\varepsilon}_e^{\frac{1-n}{n}} \tag{1}$$

Here, $n = 3$ is Glen's flow law coefficient, B the ice viscosity parameter, and $\dot{\varepsilon}_e$ the effective strain rate. We apply a Neumann stress boundary condition at the ice-air and ice-water interface, corresponding to zero air pressure and hydrostatic water pressure, respectively. A linear friction law links basal shear stress, $\boldsymbol{\sigma}_b$, to basal sliding velocity, $\boldsymbol{v}_b$, on grounded ice:

$$\boldsymbol{\sigma}_b = -\alpha^2 N \boldsymbol{v}_b\,, \tag{2}$$

where α denotes the basal friction parameter. We calculate the effective basal pressure, N, assuming that sea water pressure applies everywhere at the glacier base, which is a crude approximation far from the grounding line. The ice thickness, H, evolves over time according to the mass transport equation:

$$\frac{\partial H}{\partial t} = -\nabla \cdot (H\boldsymbol{v}) + a_s + a_b. \tag{3}$$

Here, $\boldsymbol{v}$ is the depth-averaged horizontal ice velocity, and a_s and a_b are the surface and basal mass balance, respectively. We determine the grounding line position using hydrostatic equilibrium, and treat it with a sub-element parametrisation (Seroussi et al., 2014). We refer the reader to Larour et al. (2012b) for details on the solution of these equations in ISSM.

[Table 1 about here.]

2.2 Level-Set Method

Let Ω be a computational domain in 2D or 3D space, and φ a real, differentiable function on $\Omega \times \mathbb{R}_+$, called "Level-Set Function" (LSF). For any $c \in \mathbb{R}$, we define the contour, or "c-level-set", of φ by $\varphi(\boldsymbol{x}, t) = c$. Taking its material derivative yields the "Level-Set Equation" (LSE):

$$\frac{\partial \varphi}{\partial t} + \boldsymbol{w} \cdot \nabla \varphi = 0. \tag{4}$$

This Hamilton-Jacobi type partial differential equation describes how level-sets move with the local value of the velocity $\boldsymbol{w}$, which is called level-set velocity. We need to provide an initial condition $\varphi_0(\boldsymbol{x}) = \varphi(\boldsymbol{x}, t = 0)$ to solve ~~eq. (4).~~ the LSE.

We use φ to partition Ω into three disjoint subdomains: the ice domain, $\Omega_\mathsf{i}(t)$, its complement, $\Omega_\mathsf{c}(t)$, and their common boundary, $\Gamma(t)$:

$$\begin{cases} \varphi(\boldsymbol{x}, t) < 0 \Leftrightarrow \boldsymbol{x} \in \Omega_\mathsf{i}(t) \\ \varphi(\boldsymbol{x}, t) = 0 \Leftrightarrow \boldsymbol{x} \in \Gamma(t) \\ \varphi(\boldsymbol{x}, t) > 0 \Leftrightarrow \boldsymbol{x} \in \Omega_\mathsf{c}(t) \end{cases}$$

We omit the time dependence of these sets in the remainder of this article. By construction, Γ, the 0-level-set of φ, separates Ω_i and Ω_c.

We extend $\boldsymbol{n}$, the outward-pointing unit normal of Γ, onto Ω using the LSF by:

$$\boldsymbol{n} = \frac{\nabla \varphi}{|\nabla \varphi|}. \tag{5}$$

For details on the Level-Set Method and its applications, we refer to Osher and Sethian (1988) and Sethian (2001).

[Figure 3 about here.]

Discussion Paper | Discussion Paper | Discussion Paper | Discussion Paper |

The boundary position of an ice sheet evolves with the sum of the ice velocity $\boldsymbol{v}$ along $\boldsymbol{n}$ and an ablation ~~velocity $\boldsymbol{a} = -a^{\perp}\boldsymbol{n}$. The ablation rate, $a^{\perp}$, is the difference between the level-set velocity and ice velocity projected along $\boldsymbol{n}$:~~ rate, $a^{\perp}$:

$$a^{\perp}\boldsymbol{w}\cdot\boldsymbol{n} = \boldsymbol{v}\cdot\boldsymbol{n} - a^{\perp}. \tag{6}$$

It follows that the ice boundary is stationary ~~($\boldsymbol{w}\cdot\boldsymbol{n} = 0$)~~ if and only if $a^{\perp} = \boldsymbol{v}\cdot\boldsymbol{n}$, i.e. the ablation rate matches the ice velocity perpendicular to the ice boundary. The ablation rate needs to be prescribed, either based on observations or through a parametrisation.

Note that no limitations have been made so far with respect to the dimension of the problem in this section. Accordingly, the method could be applied to model the evolution of the glacier thickness and lateral extent simultaneously (Pralong and Funk, 2004). However, ~~here~~ in this 2D-planview model study, we use the LSM to model only the horizontal extent of the ice sheet. Its vertical extent is described by the mass transport equation (3). ~~ISSM relies on vertically extruded meshes and the vertical motion of the ice boundary is accurately captured by redistributing the horizontal layers of the mesh. Using the LSM in the vertical dimension would not only significantly complicate its implementation, but it would also reduce the accuracy and precision of the ice boundary tracking (see also section 2.3).~~

We model lateral ablation as the sum of a melting rate, $m^{\perp}$, and a calving rate, $c^{\perp}$: $a^{\perp} = c^{\perp} + m^{\perp}$. For simplicity, we assume in the remainder of the article that lateral ablation occurs in the form of calving ~~, with a calving velocity $\boldsymbol{c} = -c^{\perp}\boldsymbol{n}$.~~ exclusively, i.e. $m^{\perp} = 0$. Calving itself is assumed to be a quasi-continuous process, consisting of frequent, but small calving events. With (5) and (6), ~~equation (4)~~ the LSE becomes:

$$\frac{\partial\varphi}{\partial t} + \boldsymbol{v}\cdot\nabla\varphi = c^{\perp}|\nabla\varphi|, \tag{7}$$

which is also known as "Kinematic Calving Front Condition" (KCFC, Greve and Blatter, 2009). Both the calving rate and ice velocity need to be provided on the entire 2D computational domain Ω in order to solve the KCFC. An example of a calving rate field will be given in section 3.2, and is shown in Fig. 4. The KCFC implies that all level-sets of φ, including

the calving front Γ, move at a given time with the local sum of the horizontal ice velocity and calving rate along the normal $\boldsymbol{n}$ (Fig. 3). We define the calving flux Q_{cf} as the ice flux crossing the calving front:

$$Q_{\text{cf}} = \int_{\Gamma} c^{\perp}(r) H(r)\, dr. \tag{8}$$

Some variables, like the ice velocity , The ice velocity components and the ice thickness are only defined on Ω_{i}, and need to be extended onto Ω_{c} (see also section 2.3). Any scalar field, S, is extrapolated onto Ω_{c} by solving:

$$\boldsymbol{n} \cdot \nabla S = 0, \tag{9}$$

while keeping S fixed on Ω_{i}. This type of extrapolation has the tendency to preserve $|\nabla \varphi| = \mathcal{O}(1)$, when we use the extrapolated ice velocity field to solve the KCFC (Zhao et al., 1996).

2.3 Implementation

ISSM relies on the Finite Element Method (FEM) to solve partial differential equations. It applies a Continuous Galerkin FEM using triangular (2D) and prismatic (3D) Lagrange finite elements, and uses anisotropic mesh refinement to limit the number of degrees of freedom while maximizing spatial resolution in regions of interest.

We discretise the KCFC (7) and extrapolation equation (9) using linear finite elements on the same mesh as the one used to model the ice dynamics. We stabilise both equations with artificial diffusion (Donea and Huerta, 2003), which after thorough testing proved to be the most robust stabilisation scheme. We integrate over time using a semi-implicit time-stepping scheme. We solve the KCFC, and the field equations for ice flow modelling in a decoupled fashion. The KCFC is solved first with input data from the previous time step. We then update the numerical ice domain using the new LSF as described below, and update boundary conditions accordingly. Finally, we solve the momentum balance and the mass transport equation on the updated ice domain.

The 0-level-set of φ, Γ, does in general not coincide with the finite element mesh edges due to its implicit representation. It intersects a number of elements ("front elements") with a hyperplane, which divides them into an ice-filled and an ice-free part (Fig. 3). This has various implications on the numerical level. When assembling the system stiffness matrices for ice flow modelling, exclusive integration over the ice-filled part of the element would be required. The stress boundary condition at the calving front would have to be applied at the intersecting hyperplane. Currently, ISSM is not capable of resolving those submesh scale processes.

Therefore, we either fully activate or deactivate a mesh element at every time step. Only active elements are considered for the numerical discretisation of the respective field equations. We activate an element if at least one of its vertices is in Ω_i or Γ, and the element is then considered to be entirely filled with ice. We flag the element as ice free if it lies entirely inside Ω_c, and it is deactivated. As a consequence, the numerical calving front, Γ^h, runs along mesh edges, and is updated in a discontinuous manner (Fig. 3). We apply the stress boundary condition along Γ^h for numerical consistency. Calving front normals on Γ and Γ^h may differ significantly in direction. However, stress components tangential to $\boldsymbol{n}$ cancel out along Γ^h, so that the integrated stress exerted at the calving front is close to the one applied along Γ. For all further calculations where a normal is involved, like extrapolation, the normal to the LSF (5) is used.

The numerical calving front is by definition further downstream than Γ. This may lead to slightly higher resistive lateral stress at the calving front, whose magnitude depends on the excess ice area of the intersected front element and the front geometry. We use a fine mesh resolution in the vicinity of the calving front to limit this effect.

We extrapolate the calving front thickness onto the ice-free domain using equation (9). This yields realistic ice thickness and ice thickness gradients across the front elements, that would otherwise lead to overestimated driving stress and underestimated water pressure at the ice-ocean interface. If not corrected, those two effects unrealistically increase ice velocities at the calving front, which then feed back into the mass transport and LSM schemes.

We present two experiments for validation of the LSM implemented here in the Appendix. The first experiment shows that the ice margin is advected with the prescribed level-set velocity $\boldsymbol{w}$. The linear representation of the LSF on an unstructured mesh causes a small error in the exact level-set position, which depends on element size and cancels out over time. The second test shows that errors in volume conservation introduced by the LSM decrease with finer mesh resolution, and are below 0.2 % after 100 years for a mesh resolution of 1 km. In the application to Jakobshavn Isbræ, we use a front element size of 0.5 km. The potential volume loss inherent to this implementation of the LSM is thus far below current uncertainties of model input data.

Inclusion of the LSM requires additional computational effort for the extrapolation of field variables, to solve the KCFC, and for extra iterations of the momentum balance solver, since the stress boundary conditions at the calving front change frequently. Its amount depends on the flow approximation and especially on whether the model setup is close to a stable configuration or not. Using SSA, the additional computational cost reaches up to 25%, of which 11% is caused by the solution of the KCFC.

3 Data and model setup

3.1 Jakobshavn Isbræ Model Setup

We use Jakobshavn Isbræ's drainage basin from Zwally et al. (2011) to generate a 2D-horizontal finite element mesh with element size varying from 500 m in the fjord and areas of fast flow to 10 km inland (Fig. 4). We choose this high mesh resolution to minimise calving front discretisation errors, and to resolve the fjord and the deep trough accurately in the model. The resulting mesh has about 10,000 vertices and 19,000 elements. Due to high flow velocities, the Courant-Friedrich-Lewy condition (CFL, Courant et al., 1928) dictates a time step on the order of days for the solution of the momentum balance equation, the mass transport equation, and the KCFC.

We use bed topography from Morlighem et al. (2014), derived using a mass conservation approach (Morlighem et al., 2011). The ice surface elevation is taken from GIMP (Howat et al., 2014), and ice thickness is the difference between ice surface and ice base elevation. Bathymetry of the ice-choked fjord of Jakobshavn Isbræ is difficult to measure and currently poorly known. As a first order estimate, we apply a parabolic profile of 800 m depth along the ice fjord, fitted via spline interpolation to known topography data. We rely on Ettema et al. (2009) for the surface mass balance~~. Their surface temperatures are used to calculate the~~ , and, as a first approximation, use their surface temperatures to initialize our ice viscosity parameter, B, ~~following an Arrhenius relationship (Cuffey and Paterson, 2010) at the beginning of the model simulations.~~ based on the table from Cuffey and Paterson (2010). Surface temperatures range from $\sim -8°$C near the coast to $\sim -28°$C near the divide. Basal mass balance is set to zero and no thermal model is run. All these forcings are kept constant over time.

We infer a basal friction coefficient, α, in (2) using an adjoint-based inversion (MacAyeal, 1993; Morlighem et al., 2010) of surface velocities from 2009 (Rignot and Mouginot, 2012). In regions like the fjord, where there is no ice today, we apply an area-averaged value of $\alpha = 30$ a$^{1/2}$m$^{-1/2}$. At the margins of the computational domain we prescribe zero horizontal ice velocities in order to prevent mass flux across this boundary. The friction parameter is kept fixed over time for all model simulations.

Inconsistencies in model input data cause sharp readjustments of the glacier state at the beginning of each simulation, which would make it difficult to distinguish between such effects and those of the applied forcing (Seroussi et al., 2011). Therefore, we relax the model prior to the experiments using a fixed, piecewise linear LSF φ_0, whose 0-level-set corresponds to the mean annual calving front position of 2009 (Fig. 4). Since the glacier in this configuration is far from steady state, model relaxation causes considerable thinning across the glacier's catchment area. In order not to deviate too much from present day's geometric setting we choose a 100 year relaxation time period. Note that the grounding line retreats during the relaxation due to dynamic thinning, so that the glacier forms a new floating ice tongue. This ice tongue extends about 15 km to a local topographic maximum in the south-

ern trough and 3 km into the northern one (Fig. 4). The relaxed geometry constitutes the initial state for our experiments. Due to this deviation in geometry, providing quantitative insights into Jakobshavn Isbræ is beyond the scope of this study. However, the main characteristics of the ice stream (e.g. its large drainage basin and the narrow outlet channel) are preserved, so that the results presented in this paper qualitatively represent the behaviour of Jakobshavn Isbræ.

[Figure 4 about here.]

3.2 Description of experiments

~~For simplicity, frontal ablation occurs exclusively in the form of calving in the experiments.~~ We set

$$c_0^\perp = q|\boldsymbol{v}_0| \tag{10}$$

as a basic calving rate estimate, ~~motivated by the small observed angle between $\boldsymbol{v}$ and $\boldsymbol{n}$ at the calving front ($\boldsymbol{v} \approx |\boldsymbol{v}|\boldsymbol{n}$). Then $\boldsymbol{w} \cdot \boldsymbol{n} = \boldsymbol{v} \cdot \boldsymbol{n} - \boldsymbol{c} \cdot \boldsymbol{n} \approx 0$, so that we can expect this calving rate estimate to yield a stationary calving front, if applied to a geometry that is in steady state. Here,~~ where $\boldsymbol{v}_0$ ~~denotes~~ is the velocity field at the end of the geometry relaxation run, extended onto Ω_c (Fig. 4). The continuous function q is equal to 1 in areas where the bed lies below -300 m, and linearly drops to 0 in areas of positive bed elevation. It prevents calving to occur in areas with a glacier bed above sea level, as suggested by observations of tidewater glaciers (Brown et al., 1982). The choice of the calving rate estimate is motivated by the small observed angle between $\boldsymbol{v}_0$ and $\boldsymbol{n}$ at the calving front ($\boldsymbol{v}_0 \approx |\boldsymbol{v}_0|\boldsymbol{n}$). Then $\boldsymbol{w}_0 \cdot \boldsymbol{n} = \boldsymbol{v}_0 \cdot \boldsymbol{n} - c_0^\perp \approx 0$, so that we can expect this calving rate estimate to yield a stationary calving front, if applied to a geometry that is in steady state. We scale $c_0^\perp$ over time with a scaling function, s, which allows for the representation of seasonal cycles, and a perturbation function, p, to modify the calving rate for some period of time. The applied calving rate is then: $c^\perp(\boldsymbol{x}, t) = c_0^\perp(\boldsymbol{x})\, s(t)\, p(t)$.

We perform three suites of experiments in order to analyse the impact of the calving rate on the glacier's dynamics. The calving front is now allowed to freely evolve in response to $c^{\perp}$. All experiments run for 120 years.

In experiment A, we keep the calving rate constant over time, i.e. we set both $s(t) = p(t) = 1$. Hence, $c^{\perp}(\boldsymbol{x}, t) = c_0^{\perp}(\boldsymbol{x})$. This experiment, although not physically motivated, is used to evaluate whether a stable calving front position can be reached using the LSM, and for comparison to the experiments described below.

In experiment suites B and C, we represent the seasonal cycle by scaling $c_0^{\perp}$ by $s(t) = \max(0, \pi \sin(2\pi(t/L - \phi_0)))$, with a phase shift $\phi_0 = 4/12$ and a period $L = 1$ a. We perturb the calving rate during a limited duration, Δt, with a perturbation strength $p_0 \geq 0$:

$$p(t) = \begin{cases} p_0, & \text{if } t_0 < t < t_0 + \Delta t, \text{ and} \\ 1, & \text{else.} \end{cases}$$

We start the perturbation at $t_0 = 20$ a for all experiments. In experiment suite B, we perform 5 experiments with $\Delta t = 1$ a, while varying p_0 from 0 to 4 by increments of 1. In experiment suite C, we keep $p_0 = 2$ fixed, and set Δt as 2, 4 and 8 years. We use the notation B<p_0> and C<Δt> to identify single experiments, e.g. B1 for experiment B with perturbation strength $p_0 = 1$, which represents the case of unperturbed periodic calving. B1 is used as a control run the other experiments can be compared to. Table 2 lists all the experiments performed here.

[Table 2 about here.]

4 Results

[Figure 5 about here.]

~~Fig.~~ Figure 5 shows calving front positions for experiments A, B1, B2 and C4. Under constant calving rate forcing, the calving front remains at a stable position after minor readjustments in the first decade of the simulation. In experiment A, the calving front undergoes gradual retreat over time due to the slowdown of the glacier caused by its ongoing thinning.

Discussion Paper | Discussion Paper | Discussion Paper | Discussion Paper |

When we perturb the calving rate, the calving front migrates, and higher calving rates lead to larger retreats. The retreat is highest in areas of fast flow, and strongly decreases towards the ice stream margins. This yields the characteristic concave shape of a retreating calving front. The modelled calving front positions and their shape are in good agreement with observations (Fig. 2). The retreat rate during continued phases of calving decreases to zero, so that the calving front reaches a new stable position 9 km upstream of its initial position (Fig. 5d). In experiments B and C, the calving front returns to a similar position as in the unperturbed experiment B1 within ten to twenty years after the perturbation stops.

[Figure 6 about here.]

~~Fig.~~ Figure 6 shows ice velocity, geometry and strain rates for experiment C4 along two lines, which go along and across the southern trough, respectively (Fig. 4). During the first 20 years prior to the perturbation, the ice thickness in the floating part decreases by about 100 metres (Fig. 6a). As the calving front retreats during the perturbation, the ice velocity increases (Fig. 6b), and the ice thickness adjusts accordingly (Fig. 6a). The ice thinning leads to a fast retreat of the grounding line in the regions of locally retrograde bed, and temporarily stabilises over local along-trough topographic maxima, referred to as "local highs". The southern trough has many local highs, which act as pinning points and are critical for flow dynamics, in agreement with earlier results from Vieli and Nick (2011). The acceleration of the ice stream extends tens of kilometres upstream, to areas of grounded ice (Fig. 6b). Thinning and acceleration are strongest over the ice stream, and spread out to the surrounding ice sheet in a dampened fashion. These thinning and acceleration patterns increase surface and velocity gradients, especially in the shear margins (Fig. 6c), where the effective strain rates gradually increase up to a factor of 4 in experiment C4 (Fig. 6d), which corresponds to a drop in viscosity of about 60% (equation 1). This substantially weakens the mechanical coupling between the ice stream and the surrounding ice sheet.

[Figure 7 about here.]

~~Fig.~~ Figure 7 shows the intra-annual variability of ice properties at the calving front and grounding line for experiments A, B1, B2 and C4. All shown variables reflect the characteristics of the applied calving rate forcing. The constant calving rate applied in experiment A leads to a steady configuration (Fig. 7a and 7b). For an unperturbed periodic calving rate forcing (Fig. 7c and 7d), the calving front position oscillates around a constant annual mean value by ±3 km, while the grounding line position remains unchanged at kilometre 29. Ice velocities and thickness at the calving front act in phase with the calving front position, while the response of strain rates at the grounding line is delayed by about a month. The ice velocity varies over a year by ±20%, which corresponds to about ±2 km a^{-1}, the ice thickness by ±13%, or ±100 m, and effective strain rates at the grounding line by ±7%, or ±0.1 a^{-1}.

The response to a calving rate perturbation scales with p_0 and Δt. When the calving rate doubles (B2, C4), the calving front retreats initially at an average rate of 4.5 km a^{-1}. The calving front stabilizes 9 km upstream for longer perturbations (Fig. 7g). The intra-annual variability of the calving front position doubles to ±6.5 km. The grounding line position is hardly affected by small calving rate perturbations, but large perturbations trigger fast retreats of several kilometres, which in turn cause drastic, but short-lived flow accelerations (Figs. 7g and 7h). The annual average ice velocity increases by 10%, and its intra-annual variability doubles to ±38% (Fig. 7h). The mean calving front thickness decreases by 30% towards the end of the perturbation of experiment C4, and experiences large variations up to ±75%. This high thickness variability is due to the front retreating into areas of thick ice in summer followed by stretching and thinning during calving front advance in winter. For small perturbations, variations of effective strain rates at the grounding line quadruple to ±25% (Fig. 7f). Once the calving rate perturbation stops, all variables display remarkable reversibility.

When calving is temporarily turned off (experiment B0, not shown here), the response of the glacier is reversed: the calving front advances, creating a convex ice tongue. Meanwhile, the ice stream decelerates, thickens, and the grounding line advances. After the perturbation, the glacier retreats into a state slightly thicker and faster than the one of experiment B1.

[Figure 8 about here.]

~~Fig.~~

Figure 8a shows the evolution of the ice volume with respect to experiment B1, the control run. The glacier in experiment B1 continues to lose volume at an average rate of -22.8 km^3a^{-1} due to the ongoing geometry relaxation. In experiment A, Jakobshavn Isbræ loses an additional $0.4\ km^3a^{-1}$, which corresponds to the gradual retreat of the calving front. Enhanced calving causes additional volume loss proportional to $\Delta t(1 - p_0)$, the measure of the time-integrated calving rate perturbation (Fig. 8b). If the calving rate is doubled, the additional volume loss reaches $35.7\ km^3a^{-1}$ in the first year, but decreases with time, as the calving front thins and retreats into areas of lower calving rates. Those numbers agree well with recent ice discharge observations (Howat et al., 2011). Over the first decade after the perturbation, all modelled glaciers recover 40 to 60% of the volume deviation to the control run.

5 Discussion

The applied calving rate determines the behaviour of the calving front and the ice stream. In our simulations, larger perturbation strengths p_0 lead to faster calving front retreats. In the case of long perturbations (experiments C4 and C8), the calving front reaches a new stable position. A stable calving front position requires the calving rate to be larger than the ice velocity if the calving front advances, and similarly, if the calving front retreats, the calving rate needs to be lower than the ice velocity.

Several mechanisms determine how the model responds to the calving rate forcing. First, a calving rate increase leads to a retreat of the calving front position, ice stream acceleration and dynamic thinning in the vicinity of the terminus. Second, this dynamic thinning increases surface slopes and therefore the driving stress. As the glacier locally speeds up, the ice thinning propagates upstream. The ice stream thins much faster than the surrounding ice sheet, which steepens the surface across the shear margins. Lateral inflow of ice into the ice stream hence increases until it balances the calving flux. This limits the thinning

Discussion Paper | Discussion Paper | Discussion Paper | Discussion Paper |

of the ice stream. Thinning of the ice stream in turn leads to grounding line retreat and reduction in basal effective pressure, which both reduce basal drag significantly in the vicinity of the grounding line. We showed that grounding line retreat leads to short-lived, but drastic increases in ice flux. This mechanism is qualitatively the same as the one described in Vieli and Nick (2011) and Joughin et al. (2012). Several pinning points along the retrograde trough of the southern branch, as well as the lateral stress transfer and mass influx prevent the modelled ice stream from being prone to the Marine Ice Sheet Instability (Weertman, 1974; Schoof, 2007), a hypothesis which states that grounding line positions are unstable on retrograde slopes. This corroborates earlier results by Gudmundsson et al. (2012), who presented examples of stable grounding line positions on retrograde beds. However, due to large uncertainties in the input data, and since some physical processes are not represented in our experiments, evaluation of this question for Jakobshavn Isbræ is beyond the scope of this study.

A third mechanism is related to the calving front lengthening during its retreat (e.g. figure 5). The lengthening causes tributaries of the main ice stream to calve directly into the fjord, thereby increasing the calving flux Q_{cf} (equation 8) and thinning of the terminus vicinity.

Finally, the ice stream accelerates faster than the surrounding ice sheet, which increases strain rates at the shear margins. This reduces the ice viscosity in these areas, which mechanically decouples the ice stream from the ice sheet, allowing the ice stream to accelerate further. This positive feedback confines the initial thinning to the ice stream, and is controlled by the rate at which ice enters the ice stream. This mechanism is essential for enabling ice stream acceleration tens of kilometres upstream of the grounding line, since large fractions of the ice stream's driving stress are balanced by lateral stress. This corroborates force balance arguments produced earlier by van der Veen et al. (2011).

In experiments A and B1, we apply the same annual mean calving rate. However, due to the lack of seasonal cycle in calving rate the mechanical coupling between the ice stream and ice sheet is higher in experiment A. The ice stream velocity is therefore lower, causing gradual calving front retreat and additional ice volume loss. This illustrates that volume change estimates from models with and without seasonal cycles of calving may differ. Our

results suggest that including both a dynamically evolving calving front as well as seasonal cycles are critical for accurate projections of future contributions of ice sheets to global sea level rise on decadal to centennial time scales.

Response mechanisms not covered here will likely include feedbacks with damage mechanics and thermodynamics due to the increased strain rates. During longer perturbations, ice surface lowering will probably affect the surface mass balance and the drainage basin outline.

The reversibility of the calving front configuration after the calving rate perturbation is a robust feature across all experiments. The short duration of the perturbation, the prescribed calving rates, and the geometry of the glacier are responsible for this behaviour. The volume change in all experiments never exceeds 0.1% of the initial glacier volume in the experiments shown here. Once the perturbation stops, the surrounding ice sheet continues to replenish the ice stream, which allows for its quick recovery.

The modelled glacier response to enhanced calving is in good qualitative agreement with observations, which corroborates that calving is a major control on this glacier. The similar shape of the modelled and observed calving front suggests that calving rates are indeed proportional to its flow speed during the glacier's current retreat. However, the reversibility of the modelled calving front position is in contrast to Jakobshavn Isbræ's actual behaviour. Sustained high calving rates are therefore necessary to explain the continued retreat of the glacier, as our results suggest that the glacier would have readvanced otherwise. Accurate model input data, representation of all relevant physical processes and incorporation of a suitable calving rate parametrisation will be necessary for quantitative analysis of this dynamic ice stream.

6 Conclusions

In this study, we present the theoretical framework for coupling a Level-Set Method (LSM) to ice dynamics and implement it into ISSM. The LSM proves to be a robust method for modelling the dynamic evolution of a calving front. We apply this technique to Jakobshavn

Isbræ using prescribed calving rates, and we find that the glacier is highly sensitive to this forcing, which agrees well with observations.

Calving rate perturbations strongly affect the ice stream through several linked mechanisms. First, changes in calving rate cause calving front migration and alter the ice discharge. Second, the resulting thickness change at the calving front spreads out to the surrounding ice sheet. Third, thinning-induced grounding line retreat causes further ice stream acceleration and creates a positive feedback. Finally, shear margin weakening caused by the ice stream acceleration decreases lateral drag resisting ice flow. This positive feedback mechanism sustains significant acceleration of the ice stream tens of kilometres upstream of the grounding line.

The surrounding ice sheet is barely affected by short periods of enhanced calving. It stabilises the ice stream and allows for quick reversibility of the calving front position through lateral ice influx and stress transfer once the calving rates are set back to their initial values.

Since the calving front position and dynamic lateral effects are critical to simulate and understand the behaviour of marine terminating glaciers, the inclusion of moving boundaries in ~~planview~~ 2D-planview and 3D models is key for realistic sea level rise projections on centennial time scales. This method is a step towards better physical representation of calving front dynamics in ice sheet models.

Appendix: Validation of the Level-Set Method

We present two simple test setups to validate the LSM. The first is designed to show the accurate advection and shape preservation properties of the method. The second setup aims to give an estimate for the volume change introduced by the LSM for different mesh resolutions.

1 Advection

Let Ω be a 50 km square with the initial LSF as:

$$\varphi_0(\boldsymbol{x}) = \|\boldsymbol{x} - \boldsymbol{x}_0\|_2 - R,$$

where $\boldsymbol{x}_0 = (25, 25)$ km and $R = 12.5$ km, so that the initial 0-level-set describes a circle in the middle of the domain. We prescribe a constant velocity $\boldsymbol{v} = (\cos(\pi/4), \sin(\pi/4))$ km a^{-1} everywhere. We advect φ_0 over 10 years with time steps of 0.1 a, and keep track of the 0-level-set.

[Figure 9 about here.]

~~Fig.~~ Figure 9 shows the 0-level-set position at the beginning of every year. The LSM preserves the initial circular shape, and can be used to model both advance and retreat of a calving front.

[Figure 10 about here.]

We measure the advection speed of the 0-level-set along the diagonal marked in white in Fig. 9. ~~Fig.~~ Figure 10 shows the standard deviation of the numerical error relative to the prescribed advection speed taken over time for different element sizes. The numerical error is due to the linear interpolation of the curved shape, which causes variations of the level-set velocity around the prescribed value. The standard deviation of the error linearly decreases with mesh resolution, and drops below 1% for elements sizes below 0.5 km. We therefore ~~recommend using~~ choose a mesh resolution ~~below 1~~ of 0.5 km in the ~~calving front vicinity for ice sheet~~ vicinity of the calving front in our simulations.

2 Volume conservation

Let Ω be a 200×20 km^2 rectangle with an initial LSF given by:

$$\varphi_0(\boldsymbol{x}) = (1, 0) \cdot \boldsymbol{x} - 100\,\text{km}.$$

Discussion Paper | Discussion Paper | Discussion Paper | Discussion Paper |

The initial lateral extent is thus a 100×20 km^2 rectangle. The geometry corresponds to the Ice Shelf Ramp presented in Greve and Blatter (2009). The ice thickness linearly decreases from 400 m at the grounding line ($x = 0$ km) to 200 m at the calving front ($x = 100$ km). We apply zero surface accumulation and basal melt, as well as zero grounding line velocity and free slip boundary conditions at $y = 0$ km and $y = 20$ km. The ice sheet spreads under its own weight for 100 years. Fig. 11 shows the evolution of the ice volume for different element sizes. All simulations show volume loss due to the free flux boundary condition at the numerical ice front, which is not entirely balanced by the volume added through the ice thickness extrapolation. The volume loss decreases with element size, and is below 0.2% of the initial ice volume after 100 years for an element size of 1 km. This volume loss is far below current uncertainties of other model input data.

[Figure 11 about here.]

Acknowledgements. A. Humbert acknowledges support of the DLR proposal HYD2059 which provides TerraSAR-X data for the project HGF-Alliance Remote Sensing and Earth System Dynamics. The authors thank the referees G. Jouvet and J. Bassis as well as the editor O. Gagliardini for their helpful and insightful comments.

References

Benn, D. I., Warren, C. R., and Mottram, R. H.: Calving processes and the dynamics of calving glaciers, Earth-Science Reviews, 82, 143–179, doi:10.1016/j.earscirev.2007.02.002, 2007.

Brown, C., Meier, M., and Post, A.: Calving speed of Alaska tidewater Glaciers, with application to Columbia Glacier, Alaska, U.S. Geological Survey Professional Paper, pp. 1258–C., 1982.

Chang, Y.-C., Hou, T., Merriman, B., and Osher, S.: A level set formulation of Eulerian interface capturing methods for incompressible fluid flows, Journal of computational Physics, 124, 449–464, 1996.

Courant, R., Friedrichs, K., and Lewy, H.: Über die Partiellen Differenzengleichungen der Mathematischen Physik, Mathematische Annalen, 100, 32–74, 1928.

Cuffey, K. M. and Paterson, W. S. B.: The Physics of Glaciers, Elsevier, Burlington, Mass., 2010.

Donea, J. and Huerta, A.: Finite Element Methods for Flow Problems, John Wiley & Sons, Chichester, UK, 2003.

Echelmeyer, K. and Harrison, W. D.: Jakobshavns Isbrae, West Greenland: seasonal variations in velocity - or lack thereof, 1990.

Ettema, J., van den Broeke, M. R., van Meijgaard, E., van de Berg, W. J., Bamber, J. L., Box, J. E., and Bales, R. C.: Higher surface mass balance of the Greenland ice sheet revealed by high-resolution climate modeling, Geophysical Research Letters, 36, doi:10.1029/2009GL038110, l12501, 2009.

Glen, J. W.: The flow law of ice: A discussion of the assumptions made in glacier theory, their experimental foundations and consequences, IASH Publ, 47, 171–183, 1958.

Gogineni, S., Yan, J.-B., Paden, J., Leuschen, C., Li, J., Rodriguez-Morales, F., Braaten, D., Purdon, K., Wang, Z., Liu, W., and Gauch, J.: Bed topography of Jakobshavn Isbræ, Greenland, and Byrd Glacier, Antarctica, Journal of Glaciology, 60, 813–833, doi:10.3189/2014JoG14J129, 2014.

Greve, R. and Blatter, H.: Dynamics of ice sheets and glaciers, Springer, Berlin, Germany, 2009.

Groß, S., Reichelt, V., and Reusken, A.: A finite element based level set method for two-phase incompressible flows, Computing and Visualization in Science, 9, 239–257, doi:10.1007/s00791-006-0024-y, 2006.

Gudmundsson, G. H., Krug, J., Durand, G., Favier, L., and Gagliardini, O.: The stability of grounding lines on retrograde slopes, The Cryosphere, 6, 1497–1505, doi:10.5194/tc-6-1497-2012, 2012.

Habermann, M., Truffer, M., and Maxwell, D.: Changing basal conditions during the speed-up of Jakobshavn Isbræ, Greenland, The Cryosphere, 7, 1679–1692, doi:10.5194/tc-7-1679-2013, 2013.

Howat, I. M., Ahn, Y., Joughin, I., van den Broeke, M. R., Lenaerts, J. T. M., and Smith, B.: Mass balance of Greenland's three largest outlet glaciers, 2000-2010, Geophysical Research Letters, 38, doi:10.1029/2011GL047565, 2011.

Howat, I. M., Negrete, A., and Smith, B. E.: The Greenland Ice Mapping Project (GIMP) land classification and surface elevation data sets, The Cryosphere, 8, 1509–1518, doi:10.5194/tc-8-1509-2014, 2014.

Joughin, I., Abdalati, W., and Fahnestock, M.: Large fluctuations in speed on Greenland's Jakobshavn Isbrae glacier., Nature, 432, 608–10, doi:10.1038/nature03130, 2004.

Joughin, I., Howat, I. M., Fahnestock, M., Smith, B., Krabill, W., Alley, R. B., Stern, H., and Truffer, M.: Continued evolution of Jakobshavn Isbrae following its rapid speedup, Journal of Geophysical Research, 113, F04 006, doi:10.1029/2008JF001023, 2008.

Joughin, I., Smith, B. E., Howat, I. M., Floricioiu, D., Alley, R. B., Truffer, M., and Fahnestock, M.: Seasonal to decadal scale variations in the surface velocity of Jakobshavn Isbrae, Greenland: Observation and model-based analysis, Journal of Geophysical Research, 117, F02 030, doi:10.1029/2011JF002110, 2012.

Joughin, I., Smith, B. E., Shean, D. E., and Floricioiu, D.: Brief Communication: Further summer speedup of Jakobshavn Isbræ, The Cryosphere, 8, 209–214, doi:10.5194/tc-8-209-2014, 2014.

Jouvet, G., Picasso, M., Rappaz, J., and Blatter, H.: A new algorithm to simulate the dynamics of a glacier: theory and applications, Journal of Glaciology, 54, 801–811, 2008.

Krug, J., Durand, G., Gagliardini, O., and Weiss, J.: Modelling the impact of submarine frontal melting and ice mélange on glacier dynamics, The Cryosphere, 9, 989–1003, 2015.

Larour, E., Schiermeier, J., Rignot, E., Seroussi, H., Morlighem, M., and Paden, J.: Sensitivity Analysis of Pine Island Glacier ice flow using ISSM and DAKOTA, Journal of Geophysical Research, 117, F02 009, doi:10.1029/2011JF002146, 2012a.

Larour, E., Seroussi, H., Morlighem, M., and Rignot, E.: Continental scale, high order, high spatial resolution, ice sheet modeling using the Ice Sheet System Model (ISSM), Journal of Geophysical Research, 117, F01 022, doi:10.1029/2011JF002140, 2012b.

Lüthi, M., Funk, M., Iken, A., Gogineni, S., and Truffer, M.: Mechanisms of fast flow in Jakobshavns Isbræ, Greenland, Part III: Measurements of ice deformation, temperature and cross-borehole conductivity in boreholes to the bedrock, Journal of Glaciology, 48, 369–385, 2002.

MacAyeal, D. R.: Large-scale ice flow over a viscous basal sediment: Theory and application to ice stream B, Antarctica, doi:10.1029/JB094iB04p04071, 1989.

MacAyeal, D. R.: A tutorial on the use of control methods in ice sheet modeling, J. Glaciol, 39, 91–98, 1993.

Moon, T., Joughin, I., Smith, B., Broeke, M. R., Berg, W. J., Noël, B., and Usher, M.: Distinct patterns of seasonal Greenland glacier velocity, Geophysical research letters, 41, 7209–7216, 2014.

Morlighem, M., Rignot, E., Seroussi, H., Larour, E., Ben Dhia, H., and Aubry, D.: Spatial patterns of basal drag inferred using control methods from a full-Stokes and simpler models for Pine Island Glacier, West Antarctica, Geophysical Research Letters, 37, doi:10.1029/2010GL043853, l14502, 2010.

Morlighem, M., Rignot, E., Seroussi, H., Larour, E., Ben Dhia, H., and Aubry, D.: A mass conservation approach for mapping glacier ice thickness, Geophysical Research Letters, 38, doi:10.1029/2011GL048659, l19503, 2011.

Morlighem, M., Rignot, E., Mouginot, J., Seroussi, H., and Larour, E.: Deeply incised submarine glacial valleys beneath the Greenland ice sheet, Nature Geoscience, 7, 418–422, doi:10.1038/ngeo2167, 2014.

Nick, F. M., Vieli, A., Howat, I. M., and Joughin, I.: Large-scale changes in Greenland outlet glacier dynamics triggered at the terminus, Nature Geoscience, 2, 110–114, doi:10.1038/ngeo394, 2009.

Nick, F. M., Vieli, A., Andersen, M. L., Joughin, I., Payne, A., Edwards, T. L., Pattyn, F., and van de Wal, R. S. W.: Future sea-level rise from Greenland's main outlet glaciers in a warming climate., Nature, 497, 235–8, doi:10.1038/nature12068, 2013.

Osher, S. and Sethian, J. a.: Fronts propagating with curvature-dependent speed: Algorithms based on Hamilton-Jacobi formulations, Journal of Computational Physics, 79, 12–49, doi:10.1016/0021-9991(88)90002-2, 1988.

Podrasky, D., Truffer, M., Fahnestock, M., Amundson, J. M., Cassotto, R., and Joughin, I.: Outlet glacier response to forcing over hourly to interannual timescales, Jakobshavn Isbræ, Greenland, Journal of Glaciology, 58, 1212–1226, doi:10.3189/2012JoG12J065, 2012.

Pralong, A. and Funk, M.: A level-set method for modeling the evolution of glacier geometry, Journal of Glaciology, 50, 485–491, doi:10.3189/172756504781829774, 2004.

Rignot, E. and Mouginot, J.: Ice flow in Greenland for the International Polar Year 2008-2009, Geophysical Research Letters, 39, 1–7, doi:10.1029/2012GL051634, 2012.

Rignot, E., Jacobs, S., Mouginot, J., and Scheuchl, B.: Ice-shelf melting around Antarctica., Science, 341, 266–70, doi:10.1126/science.1235798, 2013.

Rosenau, R., Schwalbe, E., Maas, H.-G., Baessler, M., and Dietrich, R.: Grounding line migration and high-resolution calving dynamics of Jakobshavn Isbrae, West Greenland, Journal of Geophysical Research: Earth Surface, 118, 382–395, doi:10.1029/2012JF002515, 2013.

Schoof, C.: Ice sheet grounding line dynamics: Steady states, stability, and hysteresis, Journal of Geophysical Research, 112, F03S28, doi:10.1029/2006JF000664, 2007.

Seroussi, H., Morlighem, M., Rignot, E., Larour, E., Aubry, D., Ben Dhia, H., and Kristensen, S. S.: Ice flux divergence anomalies on 79north Glacier, Greenland, Geophysical Research Letters, 38, doi:10.1029/2011GL047338, l09501, 2011.

Seroussi, H., Morlighem, M., Larour, E., Rignot, E., and Khazendar, a.: Hydrostatic grounding line parameterization in ice sheet models, The Cryosphere, 8, 2075–2087, doi:10.5194/tc-8-2075-2014, 2014.

Sethian, J.: Evolution, Implementation, and Application of Level Set and Fast Marching Methods for Advancing Fronts, Journal of Computational Physics, 169, 503–555, doi:10.1006/jcph.2000.6657, 2001.

Sohn, H.-G., Jezek, K. C., and van der Veen, C. J.: Jakobshavn Glacier, west Greenland: 30 years of spaceborne observations, Geophysical Research Letters, 25, 2699–2702, doi:10.1029/98GL01973, 1998.

Truffer, M. and Echelmeyer, K. a.: Of isbrae and ice streams, Annals of Glaciology, 36, 66–72, doi:10.3189/172756403781816347, 2003.

van der Veen, C., Plummer, J. C., and Stearns, L. A.: Controls on the recent speed-up of Jakobshavn Isbræ, West Greenland, Journal of Glaciology, 57, 770–782, doi:10.3189/002214311797409776, 2011.

Vieli, A. and Nick, F. M.: Understanding and Modelling Rapid Dynamic Changes of Tidewater Outlet Glaciers: Issues and Implications, Surveys in Geophysics, 32, 437–458, doi:10.1007/s10712-011-9132-4, 2011.

Weertman, J.: Stability of the junction of an ice sheet and an ice shelf, Journal of Glaciology, 13, 3–11, 1974.

Winkelmann, R., Martin, M. a., Haseloff, M., Albrecht, T., Bueler, E., Khroulev, C., and Levermann, a.: The Potsdam Parallel Ice Sheet Model (PISM-PIK) – Part 1: Model description, The Cryosphere, 5, 715–726, doi:10.5194/tc-5-715-2011, 2011.

Zhao, H.-K., Chan, T., Merriman, B., and Osher, S.: A variational level set approach to multiphase motion, Journal of computational physics, 127, 179–195, 1996.

Zwally, H. J., Jun, L., Brenner, A. C., Beckley, M., Cornejo, H. G., Dimarzio, J., Giovinetto, M. B., Neumann, T. a., Robbins, J., Saba, J. L., Donghui, Y., and Wang, W.: Greenland ice sheet mass balance: distribution of increased mass loss with climate warming; 2003–07 versus 1992–2002, Journal of Glaciology, 57, 88–102, doi:10.3189/002214311795306682, 2011.

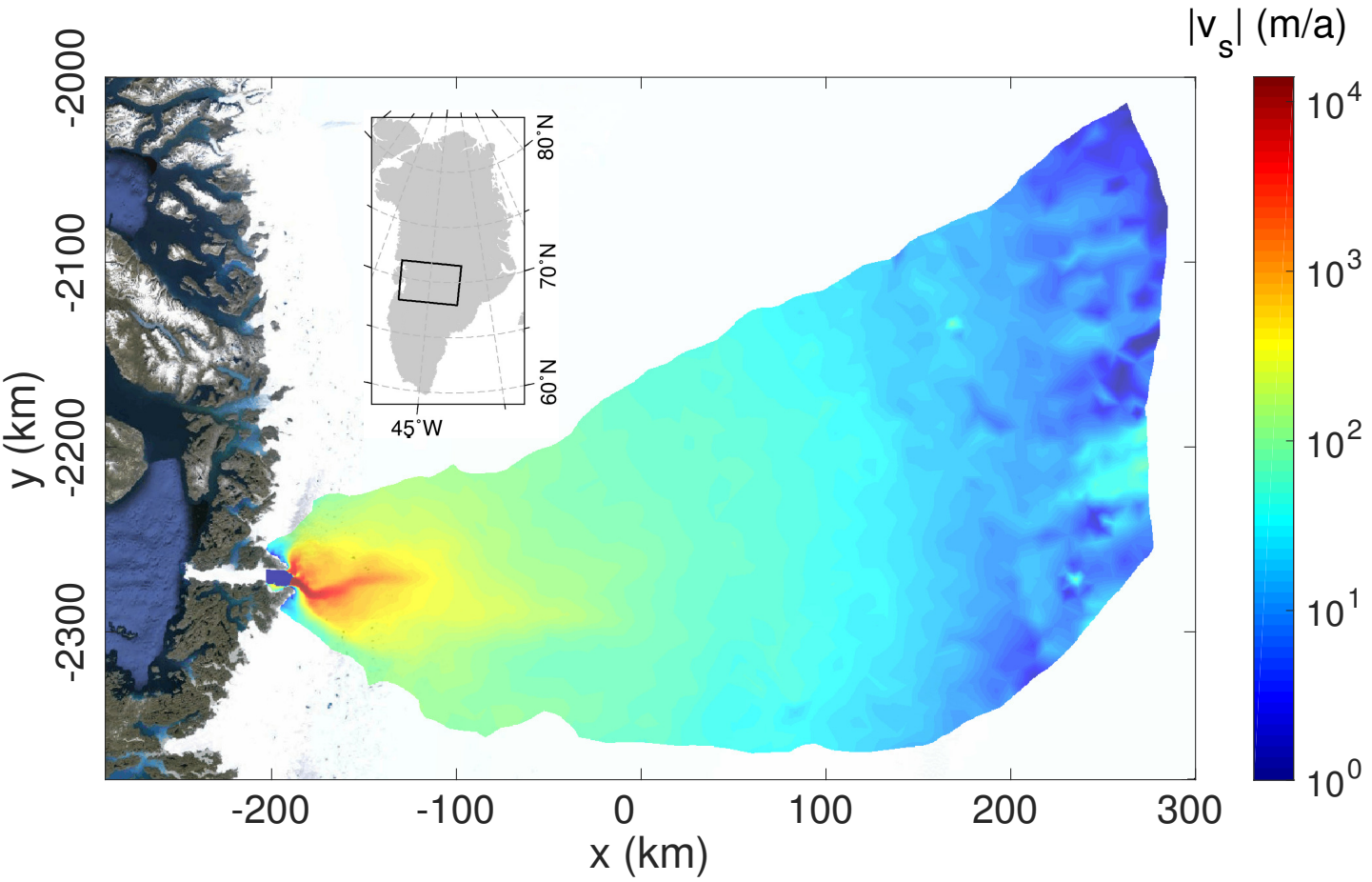

Figure 1. Observed ice surface velocities 2008/2009 (Rignot and Mouginot, 2012) of the Jakobshavn Isbræ drainage basin (logarithmic scale). Background image from Google Earth ©.

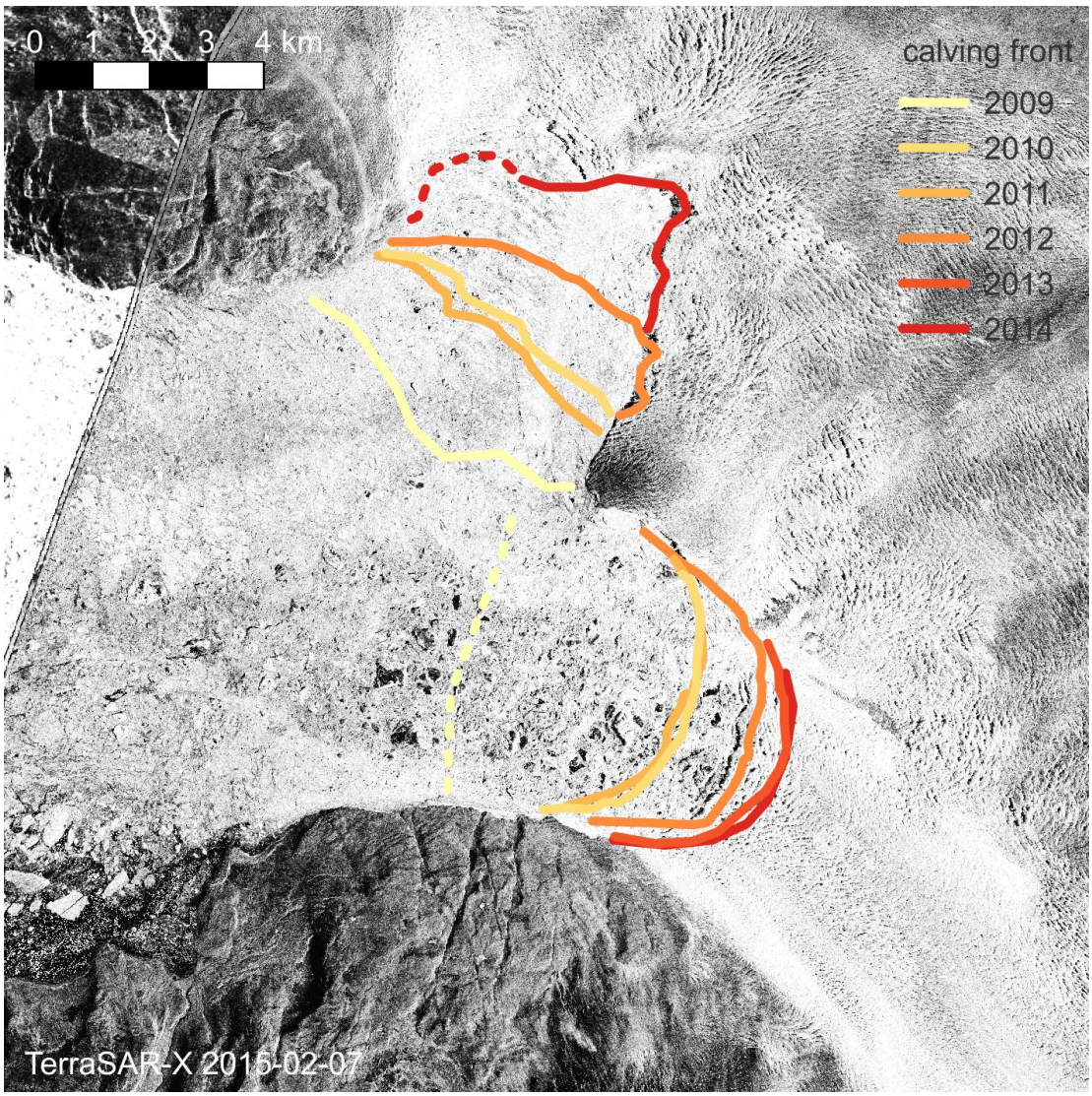

Figure 2. Winter (Feb-Mar) calving front positions from 2009 to 2014 overlaid on a TerraSAR-X scene from 2015-02-07 (© DLR). Dashed lines are used in case of ambiguous calving front positions.

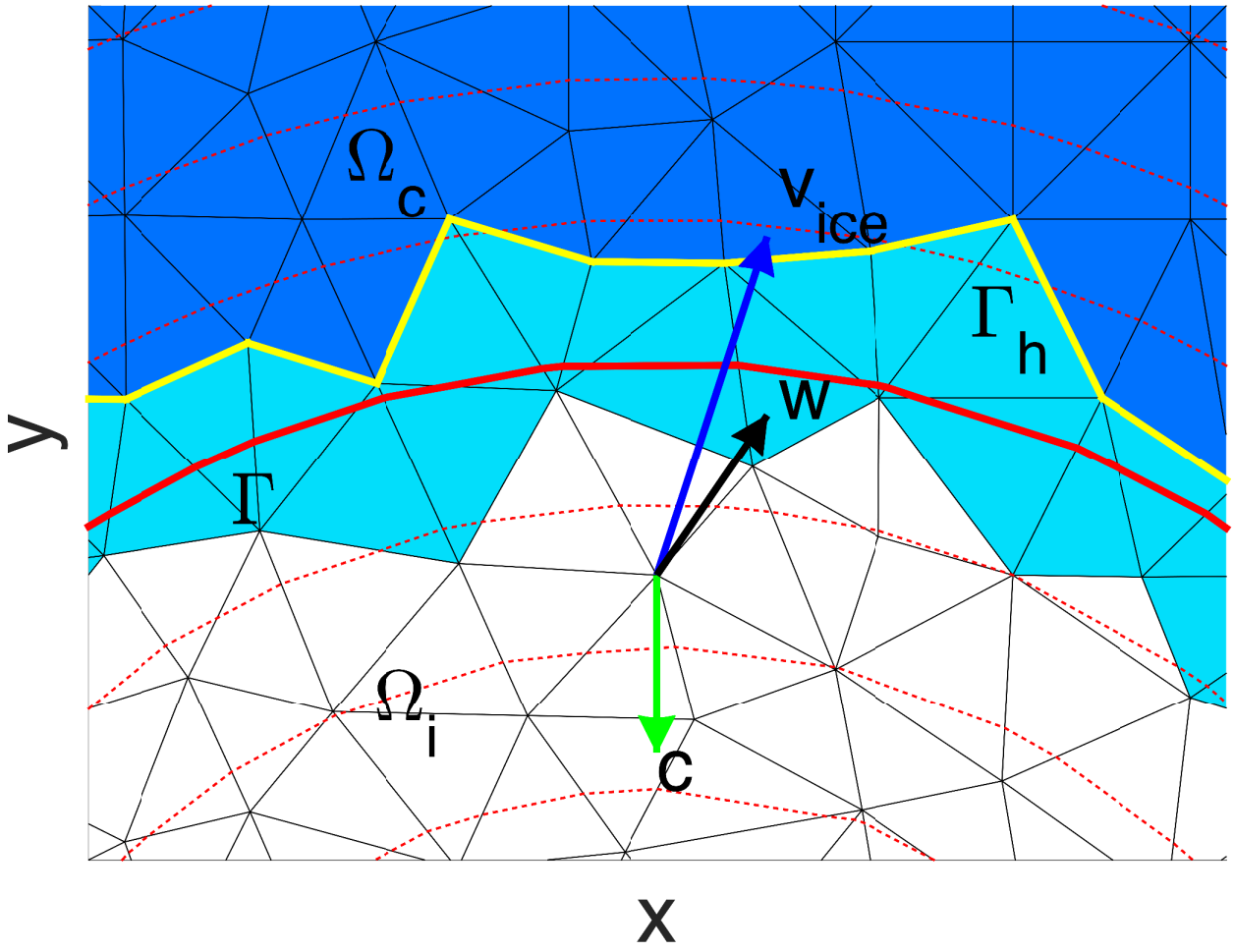

Figure 3. Schematic of the numerical ice margin. The red dashed lines denote different contour lines (level-sets) of the LSF φ. The thick red line marks the 0-level-set, Γ, the yellow line the numerical calving front Γ^h. Dark blue triangles are ice-free elements, white ones are ice-filled and the light blue ones are the front elements. The three vectors show an example of the level-set velocity ~~$\boldsymbol{w} = \boldsymbol{v} + \boldsymbol{c}$~~ $\boldsymbol{w} = \boldsymbol{v} + \boldsymbol{c}, \boldsymbol{c} = -c^{\perp}\boldsymbol{n}$ at a finite element node.

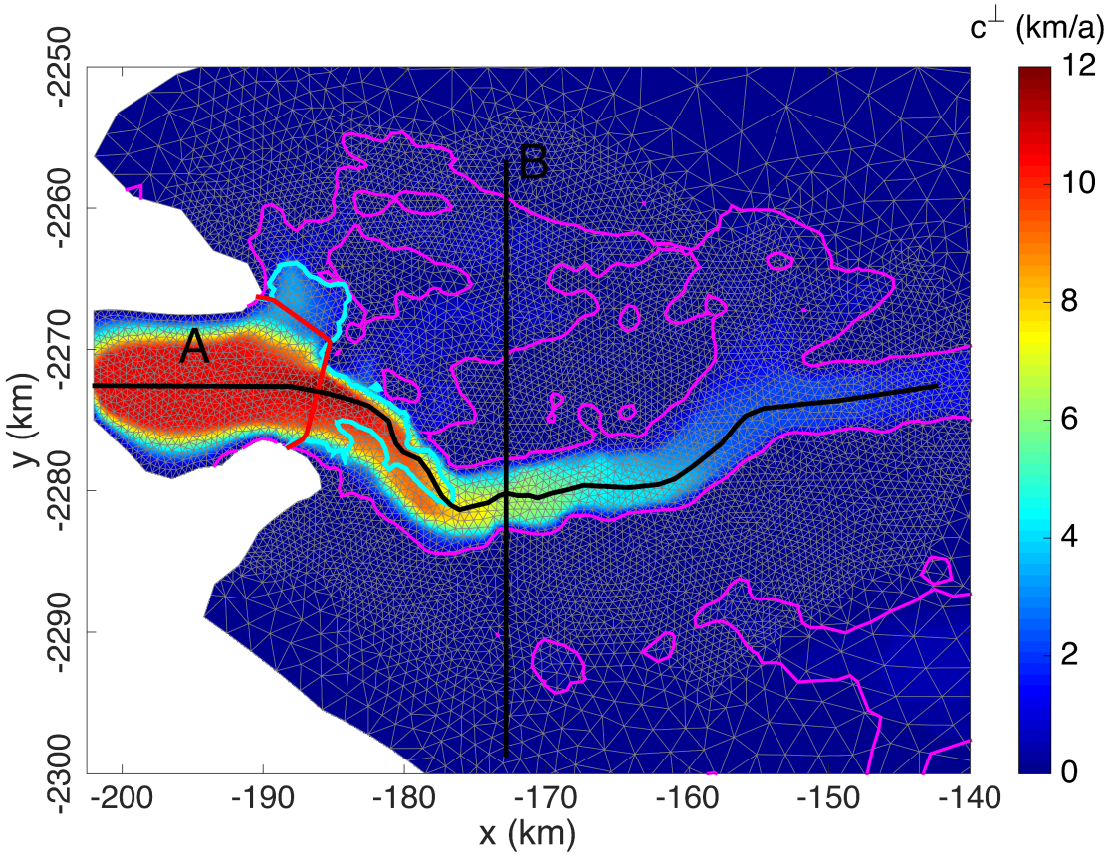

Figure 4. Calving rate field $c_0^{\perp}$ in the region of fast flow, which has been derived from modelled ice velocities at the end of the relaxation run. The red line indicates the 0-level-set of the initial LSF used for geometry relaxation and as start position for the calving front during the experiments. The turquoise line marks the grounding line. Purple contours indicate zero bedrock elevation. Black lines are the "along-trough" (A) and "across-trough" (B) profiles used in Fig. 6. The finite element mesh is displayed in grey.

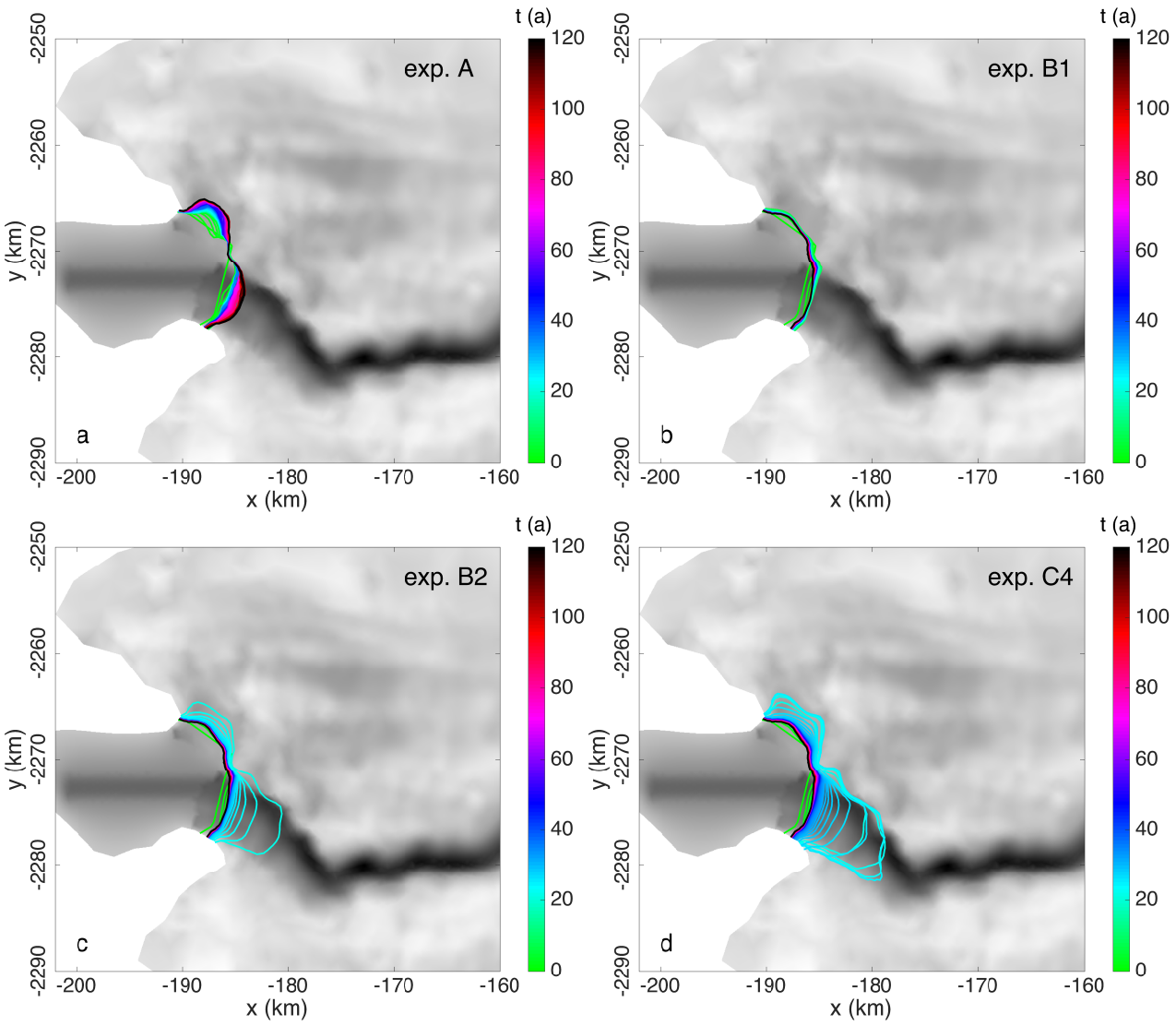

Figure 5. Calving front positions for experiments A, B1, B2 and C4 at the start of each year, plotted over basal topography (grey).

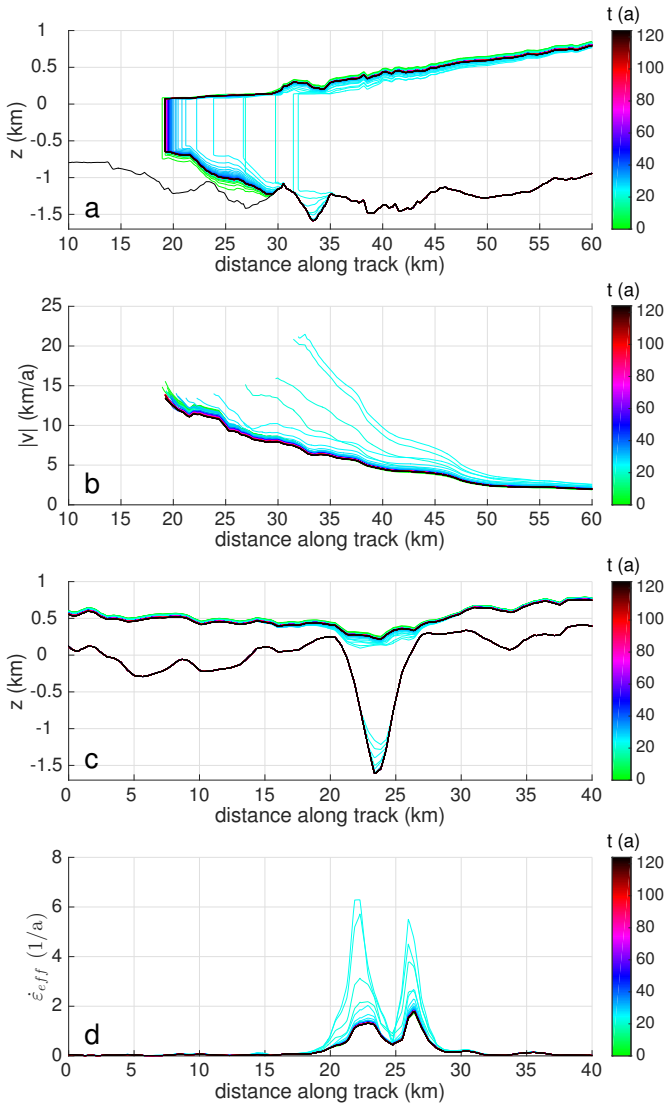

Figure 6. Section profiles of ice geometry (a) and ice velocity (b) along-trough, as well as ice geometry (c) and effective strain rates (d) across-trough for experiment C4 at the end of the calving season in October each year. ~~a) ice geometry and b) ice velocity along-trough. c) ice geometry and d) effective strain rates across-trough.~~ Positions of the lines are given in Fig. 4.

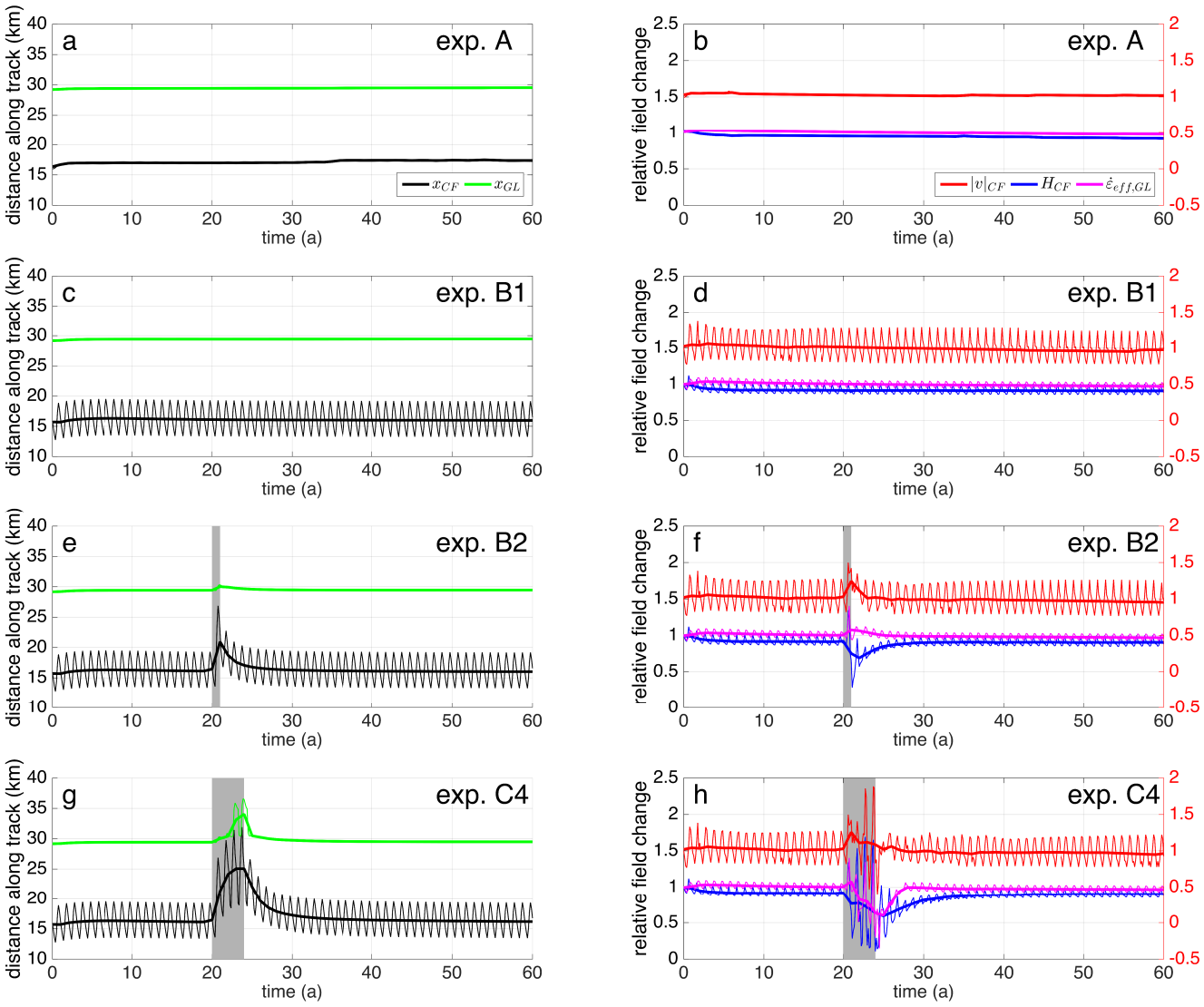

Figure 7. Calving front and grounding line positions along-trough (left column), calving front thickness, ice velocity and effective strain rate relative to their initial value along-trough (right column) over time for experiments A, B1, B2 and C4. Perturbation intervals are marked in grey. Relative values for ice velocity have been shifted up by 0.5 for better visibility (red y-axis).

Discussion Paper | Discussion Paper | Discussion Paper | Discussion Paper |

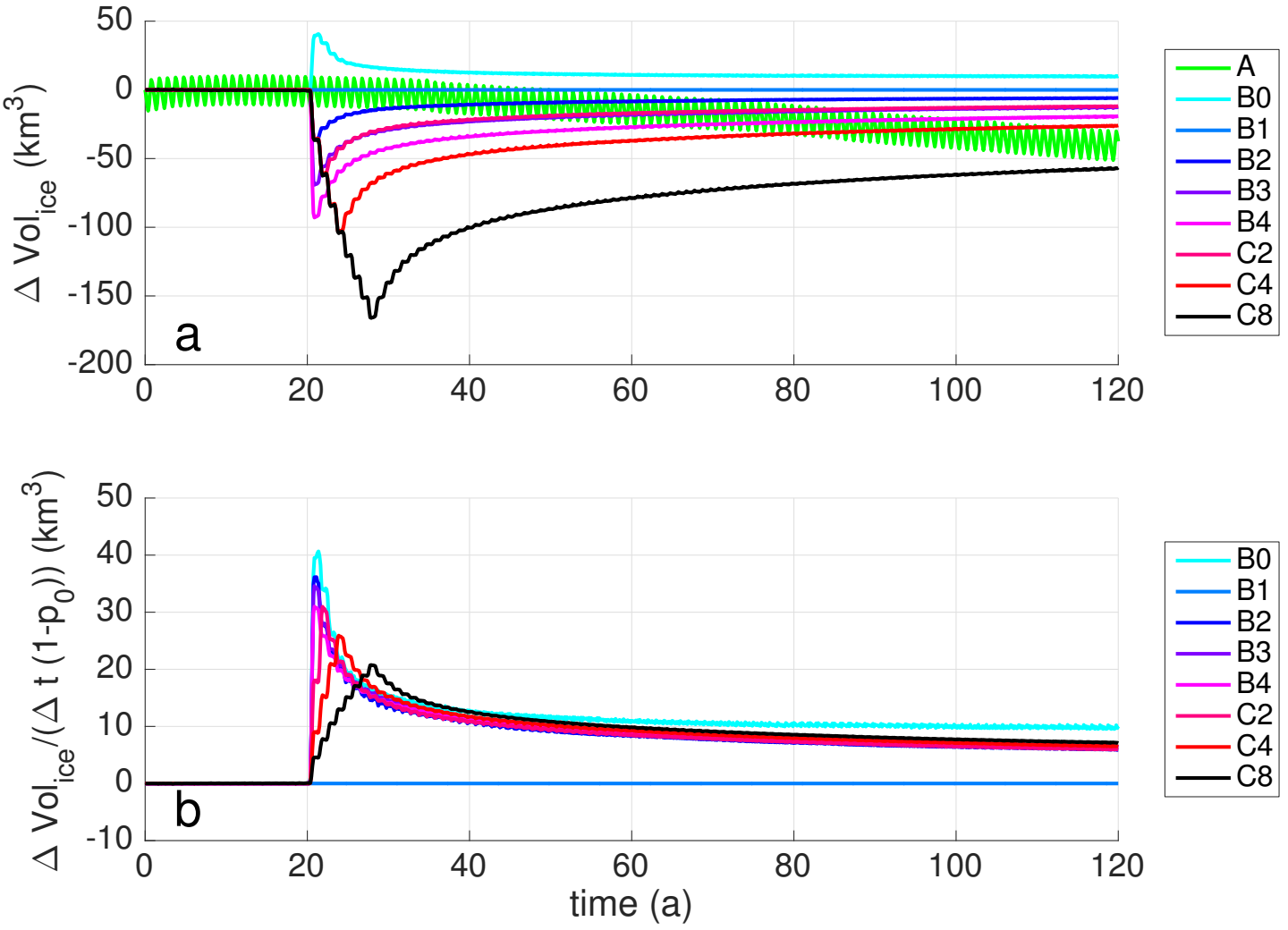

Figure 8. a: Absolute difference in ice volume for the different simulations with respect to experiment B1. The non-oscillating ice volume profile of experiment A causes its difference to experiment B1 to oscillate. b: The volume differences from experiments B and C divided by $\Delta t(1 - p_0)$, the measure of the time-integrated calving rate perturbation.

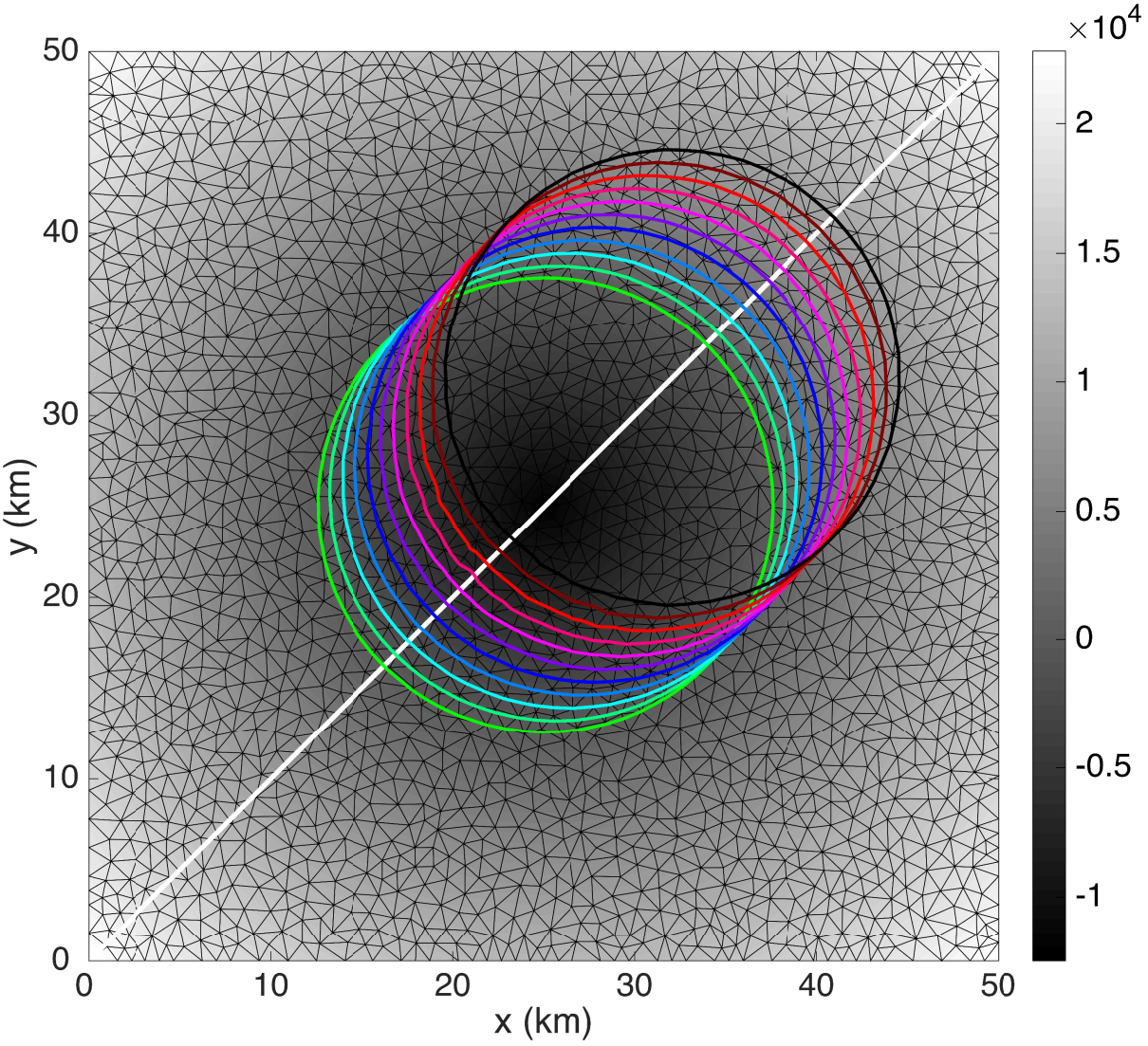

Figure 9. Zero-level-set positions at the start of every year, plotted over φ_0, which is in grey scale. An example of the mesh with element size 1 km is marked in black. The white diagonal marks the line along which the velocity of the 0-level-set is tracked.

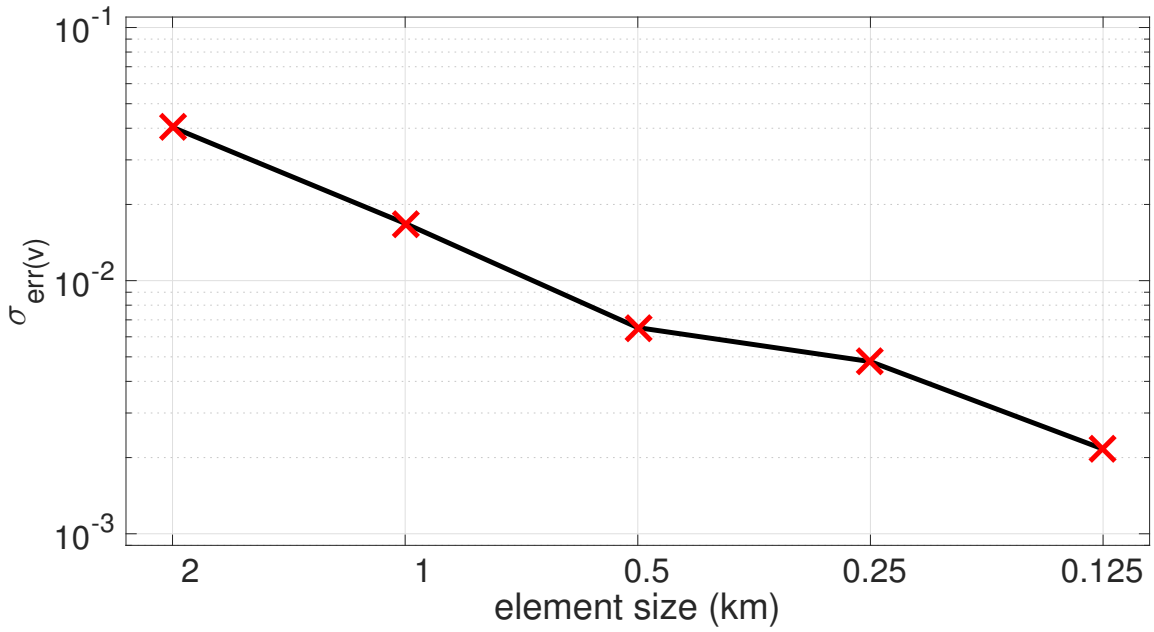

Figure 10. Standard deviation of the relative numerical error in advection velocity of the 0-level-set depending on mesh element size.

Discussion Paper | Discussion Paper | Discussion Paper | Discussion Paper |

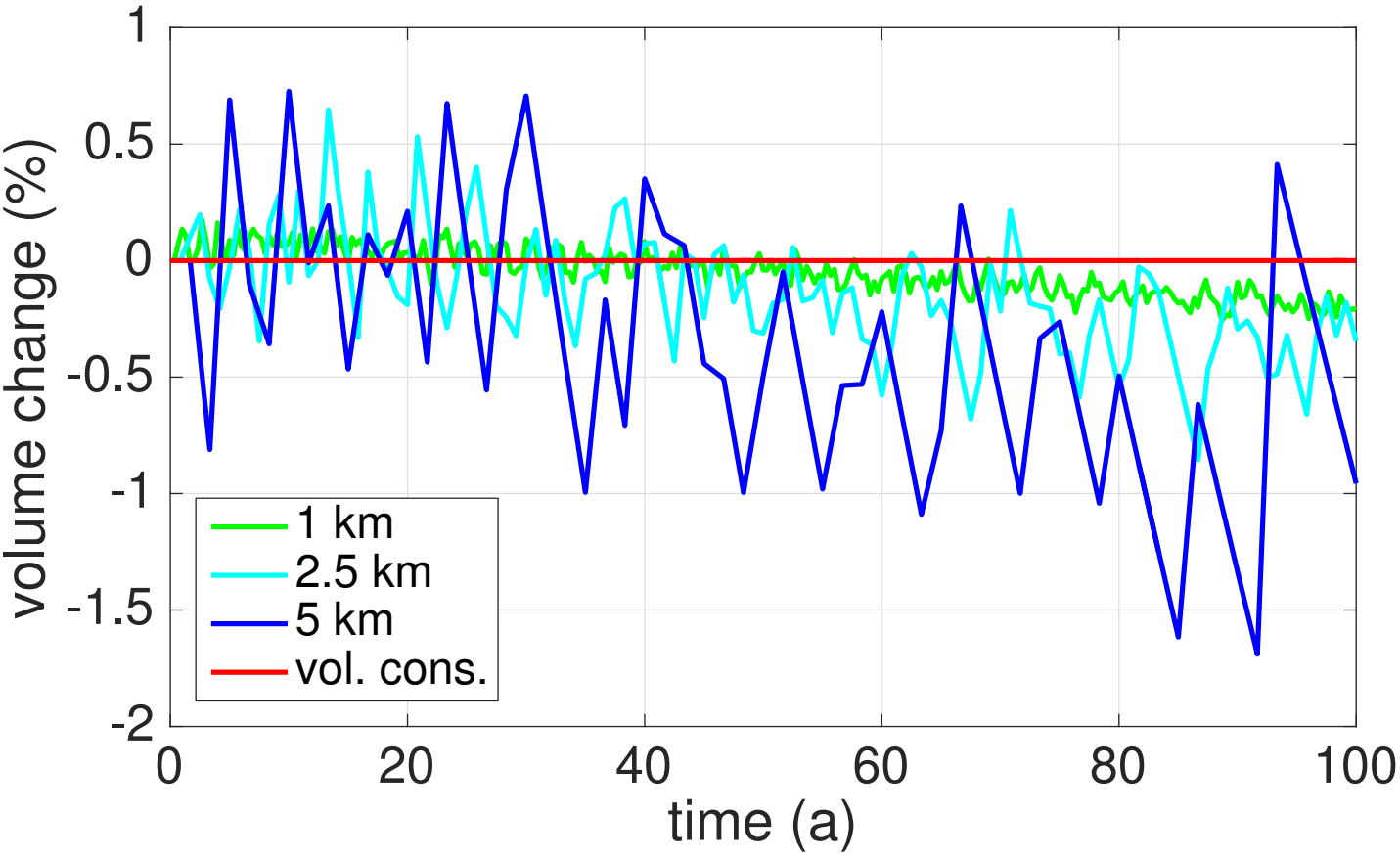

Figure 11. Evolution of the relative ice volume change for different element sizes. The red line shows volume conservation.

Table 1. Symbols and model parameters

Symbol	Quantity
μ	Ice viscosity
B	Ice viscosity parameter
$\dot{\varepsilon}_e$	Effective strain rate
n	Glen's flow law parameter
α	Basal friction parameter
N	Effective basal pressure
$\boldsymbol{v}$	Depth-averaged horizontal ice velocity
H	Ice thickness
a_s	Surface mass balance
a_b	Basal mass balance
Ω	Computational domain
Ω_i	Ice domain
Ω_c	Ice free domain
Γ	Ice boundary
Γ^h	Numerical ice boundary
φ	Level-Set Function
$\boldsymbol{n}$	Unit surface normal
$\boldsymbol{w}$	Level-set velocity
~~$\boldsymbol{a}$ Ablation velocity~~ $a^\perp$	Ablation rate
~~$\boldsymbol{c}$~~ $c^\perp$	Calving ~~velocity~~ rate
~~$c^\perp$~~ $m^\perp$	~~Calving~~ Melting rate
s	Scaling function
p	Perturbation function
Δt	Perturbation duration
p_0	Perturbation strength
L	Seasonal calving period length
ϕ_0	Phase shift
Q_cf	Calving flux

Table 2. Table of experiments

Name	p_0	Δt	Name	p_0	Δt	Name	p_0	Δt
A	1	0	B2	2	1	C2	2	2
B0	0	1	B3	3	1	C4	2	4
B1	1	1	B4	4	1	C8	2	8