

An analytical model for wind-driven Arctic summer sea ice drift

H.-S. Park¹ and A. L. Stewart²

[1]{Korea Institute of Geoscience and Mineral Resources, Daejeon, South Korea}

[2]{Department of Atmospheric and Oceanic Sciences, University of California, Los Angeles}

Correspondence to: H.-S. Park (hspark1@gmail.com)

Abstract

The authors present an analytical model for wind-driven free drift of sea ice that allows for an arbitrary mixture of ice and open water. The model includes an ice-ocean boundary layer with an Ekman spiral, forced by transfers of wind-input momentum both through the sea ice and directly into the open water between the ice floes. The analytical tractability of this model allows efficient calculation of the ice velocity provided that the surface wind field is known and that the ocean geostrophic velocity is relatively weak. The model predicts that variations in the ice thickness or concentration should substantially modify the rotation of the velocity between the 10m winds, the sea ice, and the ocean.

Compared to recent observational data from the first ice-tethered profiler with a velocity sensor (ITP-V), the model is able to capture the dependencies of the ice speed and the wind/ice/ocean turning angles on the wind speed. The model is used to derive responses to intensified southerlies on Arctic summer sea ice concentration, and the results are shown to compare closely with satellite observations.

1 Introduction

The drift of Arctic sea ice is largely explained by surface winds and upper-ocean currents. The effect of the mean geostrophic upper-ocean currents on the average circulation of sea ice pack is known to be as important as the mean wind field (Thorndike and Colony, 1982). However, the role of the winds becomes increasingly important over shorter time scales: On time scales from days to months, surface wind variability explains more than 70% of the sea

1 ice motion (Thorndike and Colony, 1982), and is well correlated with the surface ocean
2 velocity (Cole et al., 2014). The synoptic eddy surface winds result in a primary mode of
3 upper-ocean velocity variability with a period of 2–5 days over the ice-covered Arctic Ocean
4 (Plueddemann et al., 1998). The tight connection between surface winds and upper ocean
5 velocity over ice-covered Arctic Ocean suggests that resolving the wind-induced surface
6 Ekman flow is essential for simulating sea ice motions.

7 Many simple sea ice models assume steady ocean currents and prescribe a quadratic
8 relationship with an empirically-chosen turning angle between the ice stress and surface
9 ocean velocity (Hibler 1979; Thorndike and Colony, 1982; Bitz et al., 2002; Liu et al., 2011;
10 Uotila et al., 2012). This model configuration has limitations in simulating wind-induced sea
11 ice drift on intraseasonal time scales, during which time-varying Ekman layer flows in the
12 ice-ocean boundary layer (IOBL) may be important. The effect of the surface Ekman flow on
13 sea ice motion can be resolved by coupling the sea ice model to a comprehensive ocean
14 model (Zhang and Rothrock, 2003; Uotila et al., 2012). However, such an approach is
15 computationally expensive, and makes it difficult to disentangle the physical processes
16 controlling sea ice drift.

17 In the past few decades, considerable advances have been made in understanding the physics
18 of the IOBL, notably via the development of Rossby similarity theory (McPhee, 1979; 1981;
19 1994; 2008). In the case of an unstratified surface layer, this theory connects the ocean’s
20 Ekman layer to the ice base via a thin surface layer in which the velocity shear follows the
21 *law of the wall* and the vertical eddy viscosity varies linearly to zero. In contrast to
22 frequently-used quadratic drag parameterizations (e.g. Hibler 1979; Thorndike and Colony,
23 1982), this results in a quadratic drag coefficient and turning angle that depend on the stress
24 velocity and the hydraulic roughness length of the ice base. However, the assumptions
25 underlying Rossby similarity theory make it inapplicable to the case of a mixture of sea ice
26 and open water, which is typical of the Arctic in summer.

27 In Sec. 2 we derive an approximate analytical model for wind-induced sea ice drift that
28 accounts for the Ekman spiral in the IOBL and allows for an arbitrary mixture of ice and
29 water, but neglects internal stress within the ice. The model is therefore most appropriate to
30 the marginal ice zone, which covers much of the Arctic during summer. This approach has

1 both theoretical and practical merits: because the Ekman layer is resolved in the momentum
2 balance, the turning angle is a prognostic variable in our model, allowing us to explore the
3 dependence of both the ice drift speed and the wind/ice/ocean turning angles on the
4 concentration and thickness of the sea ice. The analytical tractability of the model allows
5 efficient calculation of the sea ice drift, certainly much more so than running a fully coupled
6 model of the Arctic. We compare our model's predictions against observations of Arctic sea
7 ice concentration and velocity: the data sources and reanalysis products used for this purpose
8 are described in Sec. 3.

9 In Sec. 4, we evaluate our model against recent observations from an ice-tethered profiler
10 (Cole et al., 2014), focusing on the angles between the wind and ice velocities and between
11 the ice and ocean velocities. At face value our model may not appear to be applicable to this
12 data because the measurements were made in the Beaufort Sea in winter, when the sea ice
13 concentration is close to 100% and internal stress is likely to be dynamically significant
14 (Leppäranta, 2005). However, the analysis of Cole et al. (2014) suggests that the ice floe
15 velocity was in fact close to a free drift regime, and that the vertical buoyancy flux in the
16 IOBL was small compared to previous winter observations (see *e.g.* McPhee, 2008).
17 Consequently, our model largely captures the dependence of the ice speed and turning angle
18 on the surface wind speed.

19 In Sec. 5 we apply our model to predict the anomalous change in Arctic sea ice concentration
20 associated with intraseasonal intensification of the southerly winds in the Pacific sector. This
21 serves a dual purpose: First, it is a test of our model's assumptions that the summer sea ice
22 drift can be described accurately by neglecting internal stresses and assuming constant drag
23 coefficients at the ice-ocean, atmosphere-ice, and atmosphere-ocean interfaces. Second, by
24 extension, it tests the hypothesis that the anomalous reduction in sea ice concentration in the
25 Pacific sector during southerly wind events can be attributed to the mechanical effect of
26 wind-driven ice drift, rather than thermodynamic effects. Many previous observational
27 analyses provided only statistical connections between the southerly winds and sea ice cover.
28 For example, the strength of south-westerlies over the Barents Sea is well correlated with sea
29 ice cover in winter (Sorteberg and Kvingedal, 2006; Liptak and Strong, 2014) and the
30 development of anomalous southerlies over the Pacific sector of the Arctic is often followed

1 by a reduction of sea ice cover in the spring and summer (Wu et al., 2006; Serreze et al.,
 2 2003). We demonstrate that the southerly wind-induced sea ice advection, accelerated by
 3 wind-induced surface Ekman flow, can substantially decrease sea ice concentration over a
 4 time scale of one week.

5

6 **2 An analytical model for wind-driven sea ice motion**

7 In this section we employ a simplified sea ice model to obtain analytical expressions for the
 8 sea ice velocity as a function of surface wind speed. In Sec. 2.1 we formulate an approximate
 9 sea ice momentum balance appropriate for basin-scale motions, and then in Sec. 2.2 we
 10 derive an analytical solution for the sea ice velocity, assuming that the surface wind speed is
 11 known.

12 **2.1 Model formulation**

13 We employ a “mixture layer” model of Arctic sea ice (Gray and Morland, 1994), which
 14 describes the evolution of ice floes interspersed with patches of open water. The thickness-
 15 integrated momentum balance for such a mixture layer may be written as (Heorton et al.,
 16 2014),

$$\rho_i h_i \frac{D\vec{u}_i}{Dt} = \varphi(\vec{\tau}_{ai} - \vec{\tau}_{io}) - \rho_i h_i f(\hat{Z} \times \vec{u}_i) - \rho_i h_i g \nabla \eta + \nabla \cdot \boldsymbol{\sigma}, \quad (1)$$

17 where h_i is the ice thickness, ρ_i is the ice density, \vec{u}_i is the ice velocity vector, η is the
 18 sea surface height, φ is the sea ice fraction, f is the Coriolis parameter, g is the
 19 acceleration due to gravity, and \hat{Z} is a vertical unit vector. Equation (1) states that the
 20 ice/water mixture layer is accelerated by momentum exchanges between the ice and the
 21 atmosphere ($\vec{\tau}_{ai}$) and between the ice and the ocean ($\vec{\tau}_{io}$), by the Coriolis force, by
 22 horizontal pressure variations due to sea surface tilt, and by the divergence of a stress tensor
 23 ($\boldsymbol{\sigma}$) representing internal stress in the ice.

24 We first write the lateral pressure gradient term in terms of the ocean near-surface geostrophic
 25 velocity \vec{u}_g ,

$$f \hat{Z} \times \vec{u}_g = \rho_i h_i g \nabla \eta. \quad (2)$$

1 We are concerned with sea ice evolution over a typical time scale of one week with a velocity
 2 scale of around 0.2 m/s, implying a length scale of around 100 km. The ice acceleration term
 3 in (1) may therefore be safely neglected (McPhee 1980; Thorndike and Colony, 1982). This
 4 precludes the sea ice undergoing inertial oscillations, though the diameter of such oscillations
 5 would only be a few km at most, much smaller than the drift length scale of 100 km. In
 6 summer, the Arctic sea ice concentration is mostly below 80% (see Fig. 1), so away from
 7 coastal shear margins the internal friction term in (1) is also negligible (Leppäranta, 2005;
 8 Kawaguchi and Mitsudera, 2008). This simplifies the momentum balance to

$$\rho_i h_i f \hat{Z} \times (\vec{u}_i - \vec{u}_g) = \varphi (\vec{\tau}_{ai} - \vec{\tau}_{io}), \quad (3)$$

9 Similar scaling arguments suggest that the pressure gradient due to the sea surface tilt may
 10 also be negligible. For now we retain this term because it is analytically tractable, but in Secs.
 11 4 and 5 below, we will neglect the geostrophic ocean velocity term in (3).

12 Equation (3) states that the shear between the mixture layer and the ocean's surface
 13 geostrophic velocity, or equivalently the total shear across the ice-ocean boundary layer
 14 (IOBL; MCPhee, 2012) lies perpendicular to the vertical stress divergence in the sea ice. This
 15 equation does not account for momentum imparted from the winds to the water between the
 16 ice floes in the mixture layer, which is assumed to be transferred directly to the ocean below
 17 (Gray and Morland, 1994). The total stress felt by the ocean at the base of the mixture layer is
 18 therefore

$$\vec{\tau}_o = (1 - \varphi) \vec{\tau}_{ao} + \varphi \vec{\tau}_{io}, \quad (4)$$

19 where $\vec{\tau}_{ao}$ is the momentum imparted to the ocean from the atmosphere between the sea ice
 20 floes. We adopt an approach similar to Rossby similarity theory for the IOBL, assuming that
 21 the ocean velocity follows an Ekman spiral beneath the mixture layer (McPhee, 2012). The
 22 ocean velocity at the top of the Ekman layer is therefore given as

$$\vec{u}_o - \vec{u}_g = \frac{1}{\sqrt{2K_o^*}} (\vec{u}_o^* - \hat{Z} \times \vec{u}_o^*), \quad (5)$$

23 where $K_o^* = Kf/|\vec{u}_o^*|^2$ is the dimensionless vertical eddy diffusivity, K is the dimensional
 24 vertical eddy diffusivity, \vec{u}_o^* is the stress velocity defined by $\vec{\tau}_o = \rho_o |\vec{u}_o^*| \vec{u}_o^*$, and ρ_o is the

1 ocean surface density. The dimensionless diffusivity K_o^* is taken to be constant, reflecting a
 2 linear dependence of the Ekman layer depth on the stress velocity. This is appropriate for
 3 IOBLs with no surface buoyancy forcing; non-zero surface buoyancy modifies the vertical
 4 profile of K in the IOBL (McPhee, 2008). Our model could be extended to accommodate an
 5 arbitrary K -profile if the surface buoyancy fluxes were known, but for simplicity in this
 6 study we assume zero surface buoyancy forcing.

7 We prescribe the air–ice, air–ocean, and ice–ocean stresses using quadratic drag relations,

$$\vec{\tau}_{ai} = \rho_a C_{ai} |\vec{u}_a| \vec{u}_a = \rho_a |\vec{u}_{ai}^*| \vec{u}_{ai}^*, \quad (6a)$$

$$\vec{\tau}_{ao} = \rho_a C_{ao} |\vec{u}_a| \vec{u}_a = \rho_a |\vec{u}_{ao}^*| \vec{u}_{ao}^*, \quad (6b)$$

$$\vec{\tau}_{io} = \rho_o C_{io} |\vec{u}_i - \vec{u}_o| (\vec{u}_i - \vec{u}_o) = \rho_o |\vec{u}_{io}^*| \vec{u}_{io}^*. \quad (6c)$$

8 where ρ_a and ρ_o are the atmospheric and surface ocean density respectively. Here we have
 9 implicitly assumed that there exist thin turbulent boundary layers between the atmosphere
 10 and the ice floes, between the atmosphere and ocean leads, and between the bases of the ice
 11 floes and the top of the Ekman layer, each of which transfers momentum at a rate that varies
 12 quadratically with the vertical shear. We have further assumed that any momentum imparted
 13 to the ocean leads is transferred directly down to the Ekman layer below. More
 14 comprehensive treatments of the ice–ocean stress may be derived using Rossby similarity
 15 theory (McPhee 2008; 2012). However, this theory cannot be applied in the presence of leads
 16 between the sea ice floes, which continually change the surface boundary condition at any
 17 given point between a free surface and a rigid ice floe. In many previous studies, these
 18 stresses carry a turning angle to account for the effect of the Coriolis force in the boundary
 19 layer (Hibler 1979; Thorndike and Colony 1982; Bitz et al. 2002; Uotila et al. 2012). This is
 20 not necessary here because we use the ageostrophic 10-m winds, and we explicitly account
 21 for the ocean surface Ekman layer.

22 By combining the ice–ocean stress relation (6c), which can be rewritten as $\vec{u}_{io}^* = \sqrt{C_{io}} (\vec{u}_i -$
 23 $\vec{u}_o)$, with equation (5) for the shear across the Ekman layer, we obtain an expression for the
 24 total shear across the IOBL,

$$\vec{u}_i - \vec{u}_g = \frac{1}{\sqrt{C_{io}}} \vec{u}_{io}^* + \frac{1}{\sqrt{2K_0^*}} (\vec{u}_o^* - \hat{Z} \times \vec{u}_o^*). \quad (7)$$

1 Then, substituting (6a), (6c) and (7) into the momentum balance (3), we obtain a relationship
 2 between the unknown stress velocities \vec{u}_{io}^* and \vec{u}_o^* ,

$$\begin{aligned} \frac{\rho_i h_{if}}{\sqrt{C_{io}}} \hat{Z} \times \vec{u}_{io}^* + \frac{\rho_i h_{if}}{\sqrt{2K_0^*}} (\hat{Z} \times \vec{u}_o^* + \vec{u}_o^*) = \\ \varphi (\rho_a |\vec{u}_{ai}^*| \vec{u}_{ai}^* - \rho_o |\vec{u}_{io}^*| \vec{u}_{io}^*). \end{aligned} \quad (8)$$

3 We require an additional equation to obtain an explicit solution for \vec{u}_{io}^* and \vec{u}_o^* , so we
 4 rewrite the total stress at the base of the mixing layer (4) in the form

$$\rho_o |\vec{u}_o^*| \vec{u}_o^* = (1 - \varphi) \rho_a |\vec{u}_{ao}^*| \vec{u}_{ao}^* + \varphi \rho_o |\vec{u}_{io}^*| \vec{u}_{io}^*. \quad (9)$$

5 **2.2 Model solution**

6 In order to derive a solution for the ice velocity \vec{u}_i , we now solve the previously derived
 7 equations (8) and (9) for the stress velocities \vec{u}_{io}^* and \vec{u}_o^* .

8 **2.2.1 Near-100% sea ice cover ($\varphi \approx 1$)**

9 We first consider the case of close-to-100% sea ice cover ($\varphi \approx 1$) because this permits a
 10 closed-form analytical solution that offers physical intuition for the behavior of the model.
 11 Though an actual sea ice concentration of 100% would likely be associated with large
 12 internal stresses, we use it for the purpose of illustration because our results in Sec. 4 indicate
 13 that this closely approximates the general solution for ice concentrations greater than 50%.
 14 The method of solution is similar to that described by Leppäranta (2005), Ch. 6.1, but our
 15 explicit treatment of the oceanic boundary layer and prognostic determination of the turning
 16 angle warrant that the solution be described explicitly.

17 For sea ice concentrations close to 100% ($\varphi \approx 1$) equation (9) implies that the ice-ocean and
 18 ocean surface stress velocities are approximately equal, $\vec{u}_{io}^* \approx \vec{u}_o^*$. Thus equations (7) and (8)
 19 may be rewritten as

$$\vec{u}_i - \vec{u}_g = \left(\frac{1}{\sqrt{C_{io}}} + \frac{1}{\sqrt{2K_0^*}} \right) \vec{u}_{io}^* - \frac{1}{\sqrt{2K_0^*}} \hat{Z} \times \vec{u}_{io}^*, \quad (10a)$$

$$\left(\frac{\rho_i h_i f}{\sqrt{2K_0^*}} + \frac{\rho_i h_i f}{\sqrt{C_{io}}} \right) \hat{Z} \times \vec{u}_{io}^* + \frac{\rho_i h_i f}{\sqrt{2K_0^*}} \vec{u}_{io}^* = \rho_a |\vec{u}_{ai}^*| \vec{u}_{ai}^* - \rho_o |\vec{u}_{io}^*| \vec{u}_{io}^*. \quad (10b)$$

1 We simplify the coefficients by multiplying both sides of (10b) by $\sqrt{2K_0^*}/\rho_i h_i f$ and
2 rearranging to obtain

$$(\alpha + 1) \hat{Z} \times \vec{u}_{io}^* + (1 + k_o |\vec{u}_{io}^*|) \vec{u}_{io}^* = k_a |\vec{u}_{ai}^*| \vec{u}_{ai}^*, \quad (11)$$

3 where

$$\alpha = \sqrt{2K_0^*/C_{io}}, \quad k_a = \rho_a \sqrt{2K_0^*}/\rho_i h_i f \quad \text{and} \quad k_o = \rho_o \sqrt{2K_0^*}/\rho_i h_i f. \quad (12)$$

4 To solve, we first define the components of \vec{u}_{io}^* parallel and perpendicular to the wind stress
5 velocity, or, equivalently, perpendicular the 10 m winds:

$$u_{io}^{*\parallel} = \frac{\vec{u}_{ai}^*}{|\vec{u}_{ai}^*|} \cdot \vec{u}_{io}^*, \quad (13a)$$

$$u_{io}^{*\perp} = \left(\hat{Z} \times \frac{\vec{u}_{ai}^*}{|\vec{u}_{ai}^*|} \right) \cdot \vec{u}_{io}^*. \quad (13b)$$

6 Then taking the dot product of \vec{u}_{io}^* with both sides of equation (11) and rearranging yields an
7 expression for $u_{io}^{*\parallel}$,

$$u_{io}^{*\parallel} = \frac{1}{k_a} \frac{|\vec{u}_{io}^*|^2}{|\vec{u}_{ai}^*|^2} (1 + k_o |\vec{u}_{io}^*|), \quad (14)$$

8 while taking the dot product of $\hat{Z} \times \vec{u}_{io}^*$ with both sides of (11) yields an expression for $u_{io}^{*\perp}$,

$$u_{io}^{*\perp} = -\frac{1}{k_a} \frac{|\vec{u}_{io}^*|^2}{|\vec{u}_{ai}^*|^2} (1 + \alpha). \quad (15)$$

9 Equations (14) and (15) do not constitute an explicit solution for \vec{u}_{io}^* because they depend on
10 its magnitude $|\vec{u}_{io}^*|$. We determine this magnitude using the definition, $|\vec{u}_{io}^*|^2 = (u_{io}^{*\parallel})^2 +$
11 $(u_{io}^{*\perp})^2$, which yields a quartic equation for $|\vec{u}_{io}^*|$,

$$k_o^2 |\vec{u}_{io}^*|^4 + 2k_o |\vec{u}_{io}^*|^3 + (1 + (\alpha + 1)^2) |\vec{u}_{io}^*|^2 = k_a^2 |\vec{u}_{ai}^*|^4. \quad (16)$$

12 In principle, this may be solved analytically for $|\vec{u}_{io}^*|$, but for the purposes of this study we

1 solve (16) numerically. Note that the left-hand side of (16) is a monotonically increasing
 2 function of $|\vec{u}_{io}^*|$, so a unique solution exists for any wind stress velocity magnitude $|\vec{u}_{ai}^*|$.
 3 Having obtained the components of the stress velocity, it is straightforward to solve for the
 4 shear between the sea ice and the geostrophic ocean velocity using (10a).

5 **2.2.2 Sparse sea ice cover ($\varphi \ll 1$)**

6 We now consider sea ice concentrations much below 100%. We begin by simplifying the
 7 coefficients in equations (8) and (9) by defining α , k_a , and k_o as in Sec. 2.1, and
 8 additionally defining $\beta = \rho_a C_{ao} / \rho_o C_{ai}$,

$$\alpha \hat{Z} \times \vec{u}_{io}^* + \hat{Z} \times \vec{u}_o^* + \vec{u}_o^* = \varphi k_a |\vec{u}_{ai}^*| \vec{u}_{ai}^* - \varphi k_o |\vec{u}_{io}^*| \vec{u}_{io}^*, \quad (17)$$

$$|\vec{u}_o^*| \vec{u}_o^* = (1 - \varphi) \beta |\vec{u}_{ai}^*| \vec{u}_{ai}^* + \varphi |\vec{u}_{io}^*| \vec{u}_{io}^*. \quad (18)$$

9 Here we have combined equations (6a) and (6b) to relate the atmosphere-ice and atmosphere-
 10 ocean stress velocities via $\vec{u}_{ai}^* / \sqrt{C_{ai}} = \vec{u}_{ao}^* / \sqrt{C_{ao}}$. Equations (17–18) may in principle be
 11 solved analytically following a procedure similar to that described in Sec. 2.2.1: by defining
 12 stress velocity components parallel and perpendicular to the atmospheric velocity, $u_{io}^{*\parallel}$, $u_{io}^{*\perp}$,
 13 $u_o^{*\parallel}$, and $u_o^{*\perp}$, analogously to definitions (13a) and (13b). Then taking the dot product of \vec{u}_{ai}^*
 14 and $\hat{Z} \times \vec{u}_{ai}^*$ with each of (17) and (18) yields four scalar equations that can be solved
 15 simultaneously for the components of \vec{u}_{io}^* and \vec{u}_o^* . Finally, using the definitions $|\vec{u}_{io}^*|^2 =$
 16 $(u_{io}^{*\parallel})^2 + (u_{io}^{*\perp})^2$ and $|\vec{u}_o^*|^2 = (u_o^{*\parallel})^2 + (u_o^{*\perp})^2$ yields a pair of equations that must be
 17 solved simultaneously for $|\vec{u}_{io}^*|$ and $|\vec{u}_o^*|$. However, this analytical solution is too
 18 complicated to yield physical insight, so in practice we simply solve (17–18) numerically
 19 using least-squares optimization.

20 **2.3 Physical interpretation**

21 Though equations (14–16) constitute an analytical solution to the mixture layer momentum
 22 balance (11), in this form they yield little insight into the wind-driven drift of sea ice. We
 23 therefore provide additional formulae for some key quantities describing the ice drift.
 24 Moreover, we briefly discuss the similarities and differences between our equations and the
 25 equations based on Rossby similarity theory (e.g. McPhee 2008; 2012). We base our
 26 discussion around the solution for near-100% sea ice concentration, given in Sec. 2.2.1,

1 because this solution is completely analytical and thus offers more insight.

2 **2.3.1 Ice velocity**

3 For convenience we re-state equation (10a), which relates the shear between the ice and the
4 geostrophic ocean velocity to the ice-ocean stress velocity in the case of close to 100% sea
5 ice cover,

$$\vec{u}_i - \vec{u}_g = \left(\frac{1}{\sqrt{C_{io}}} + \frac{1}{\sqrt{2K_0^*}} \right) \vec{u}_{io}^* - \frac{1}{\sqrt{2K_0^*}} \hat{Z} \times \vec{u}_{io}^*.$$

6 This equation is similar to the one derived by McPhee (2008; 2012) for the case of an
7 unstratified IOBL, because both approaches assume a traditional Ekman layer solution over
8 most of the IOBL. However, there are some notable differences: Instead of assuming that the
9 turbulent transfer of momentum follows a quadratic drag law, McPhee (2008; 2012) utilized
10 the *law of the wall* equation across the ocean-ice boundary layer, leading to a slightly more
11 complicated version of this equation,

$$\vec{u}_i - \vec{u}_g = \left(\frac{1}{\kappa} \log \left(\frac{|\vec{u}_{io}^*|}{f z_0} \right) + \frac{1}{\kappa} \log \left(\frac{K_0^*}{\kappa} \right) + \frac{1}{\sqrt{2K_0^*}} \right) \vec{u}_{io}^* - \frac{1}{\sqrt{2K_0^*}} \hat{Z} \times \vec{u}_{io}^*,$$

12 where κ is Karman's constant ($\kappa = 0.4$) and z_0 is hydraulic roughness at the bottom of sea
13 ice. Because the velocity profile over the ocean-ice boundary layer is assumed to be
14 logarithmic (i.e. following the *law of the wall*), logarithmic terms appear as coefficients of
15 ice-ocean stress velocity \vec{u}_{io}^* . In our equation (10a) these terms are replaced by $1/\sqrt{C_{io}}$, due
16 to our assumption of a linear relationship between the ice-ocean shear and the ice-ocean
17 stress velocity.

18 Our formulation is arguably a less accurate description of the IOBL when the sea ice
19 concentration is close to 100% because it does not allow the ice speed to vary nonlinearly
20 with the ice-ocean stress velocity. However, in general the sea ice concentration may be
21 much smaller than 100%, and at any given horizontal location the surface boundary condition
22 is transient, varying between a solid upper boundary (the ice) and a free surface (open water).
23 Thus the assumption of a flow following the *law of the wall* and the notion of a hydraulic
24 roughness length no longer applies to this case. We have therefore assumed quadratic drag

1 laws at these interfaces for simplicity, but in principle a more accurate IOBL model could be
 2 derived following the ideas of Rossby similarity theory but using a transient surface boundary
 3 condition that varies between a solid boundary and a free surface.

4 **2.3.2 Turning angles**

5 The IOBL turning angle is the angle between the ice-ocean stress velocity \vec{u}_{io}^* and the ice-
 6 geostrophic shear $(\vec{u}_i - \vec{u}_g)$, and may be defined as

$$\cos(\theta_{IOBL}) = \frac{\vec{u}_{io}^* \cdot (\vec{u}_i - \vec{u}_g)}{|\vec{u}_{io}^*| |\vec{u}_i - \vec{u}_g|}. \quad (19)$$

7 For near-100% sea ice concentration, a closed expression for the IOBL turning angle can be
 8 derived by substituting the right-hand side of equation (10a) for $\vec{u}_i - \vec{u}_g$ in equation (19),

$$\cos(\theta_{IOBL}) = \frac{1 + \alpha}{\sqrt{1 + (1 + \alpha)^2}}, \quad (20)$$

9 which is independent of the surface wind speed and depends only on the parameter
 10 $\alpha = \sqrt{2K_0^*/C_{io}}$. Thus for near-100% sea ice concentration, prescribing an Ekman spiral and a
 11 linear relationship between the ice-ocean stress velocity \vec{u}_{io}^* and the ice-ocean shear
 12 $(\vec{u}_i - \vec{u}_o)$ is equivalent to assuming a constant geostrophic ice-ocean turning angle (e.g.
 13 Hibler, 1979; Thorndike and Colony, 1982). By contrast the IOBL turning angle predicted by
 14 Rossby similarity theory varies as a function of the ice-ocean stress velocity, and the turning
 15 angle varies by a few degrees over a realistic range of ice-ocean stress magnitudes (McPhee,
 16 1979; 2008). Note that in our model θ_{IOBL} is generally not independent of the surface wind
 17 speed when the sea ice concentration is below 100%.

18 Fig. 2 shows the IOBL turning angle θ_{IOBL} as a function of α . The IOBL turning angle
 19 θ_{IOBL} decreases from 45 degrees to zero as α increases from zero to infinity. A larger value
 20 of α corresponds to a relatively large vertical diffusivity K_0^* , which tends to reduce the
 21 magnitude of the shear in the Ekman layer. Thus the shear becomes dominated by the surface
 22 boundary layer, over which the shear does not turn with depth. A smaller value of α
 23 corresponds to a relatively large drag coefficient C_{io} , which tends to reduce magnitude of the
 24 shear in the surface boundary layer. Thus the shear becomes dominated by the Ekman spiral,
 25 over which the shear turns by 45 degrees. This is consistent with Rossby similarity theory

1 (McPhee 2008; 2012) in that multi-year ice pack with a relatively high basal hydraulic
 2 roughness corresponds to a larger turning angle θ_{IOBL} . In this study, we employ the
 3 canonical value of $K_o^* = 0.028$ (McPhee, 1994; 2008), and we use $C_{io}=0.0071$ based on the
 4 estimate of Cole et al. (2014) from the ITP-V data. This combination of K_o^* and C_{io}
 5 produces a θ_{IOBL} of around 15 degrees (red dot in Fig. 2). This value is within the range of
 6 turning angles predicted by Rossby similarity theory, which is about 20 degrees for multi-
 7 year ice pack and 13 degrees for the first-year ice (McPhee 2012).

8 We now turn to the ice drift itself. We derive the angle between the 10m wind speed \vec{u}_a and
 9 the ice-geostrophic shear $\vec{u}_i - \vec{u}_g$ by taking the dot product of \vec{u}_{ai}^* with (10a), noting that
 10 \vec{u}_{ai}^* lies parallel to \vec{u}_a from (6a), and using (14) and (15) for the components of \vec{u}_{io}^* ,

$$\cos(\theta_{ai}) = \frac{\vec{u}_a \cdot (\vec{u}_i - \vec{u}_g)}{|\vec{u}_a| |\vec{u}_i - \vec{u}_g|} = \frac{k_o |\vec{u}_{io}^*|^2}{k_a |\vec{u}_{ai}^*|^2} \frac{1 + \alpha}{\sqrt{1 + (1 + \alpha)^2}} = \frac{|\vec{\tau}_{io}|}{|\vec{\tau}_{ai}|} \cos(\theta_{IOBL}) \quad (21)$$

11 Using equation (16) above, it is straightforward to show that the ratio of the ice–ocean to air–
 12 ice stresses is smaller than one, $k_o |\vec{u}_{io}^*|^2 / k_a |\vec{u}_{ai}^*|^2 = |\vec{\tau}_{io}| / |\vec{\tau}_{ai}| < 1$, so it follows that the
 13 air–ice angle is always at least as large as the IOBL turning angle, $\theta_{ai} \geq \theta_{IOBL}$. This reflects
 14 the fact that the 10-m wind velocity \vec{u}_a always points to the left of the ice–ocean stress $\vec{\tau}_{io}$
 15 (*c.f.* equations (14) and (15)), while the ice–geostrophic shear $\vec{u}_i - \vec{u}_g$ always points to the
 16 right of $\vec{\tau}_{io}$ (*c.f.* equation (10a)). For strong winds ($|\vec{\tau}_{ai}| \rightarrow \infty$) equation (16) implies that the
 17 air–ice and ice–ocean stresses balance one another in (3) (i.e. $\vec{\tau}_{io} \rightarrow \vec{\tau}_{ai}$), so the air-ice
 18 turning angle becomes independent of the wind speed and equal to the IOBL turning angle.
 19 For weak winds ($|\vec{\tau}_{ai}| \rightarrow 0$), equation (16) implies that the ice–ocean to air–ice stress ratio
 20 vanishes¹, $|\vec{\tau}_{io}| / |\vec{\tau}_{ai}| \rightarrow 0$, so from (18) the ice velocity becomes directed 90° to the right of
 21 the winds.

¹ To obtain this result from equation (16), first note that if $|\vec{u}_{ai}^*| = 0$ then the only non-negative real solution to (16) is $|\vec{u}_{io}^*| = 0$, so we can conclude that $|\vec{u}_{io}^*| \rightarrow 0$ as $|\vec{u}_{ai}^*| \rightarrow 0$. Then note that in the limit of vanishing air-ice stress, $|\vec{u}_{ai}^*| \rightarrow 0$, equation (16) can only remain balanced if $|\vec{u}_{io}^*| \sim |\vec{u}_{ai}^*|^2$. It follows that $|\vec{\tau}_{io}| / |\vec{\tau}_{ai}| \rightarrow 0$ as $|\vec{u}_{ai}^*| \rightarrow 0$.

1

2 **3 Observation and Reanalysis Datasets**

3 In this section we detail the various observational and reanalysis datasets used to evaluate our
4 analytical model and to quantify how southerly winds affects Arctic summer sea ice
5 concentration.

6 **3.1 Observations**

7 To evaluate our analytical model with observations, we used observations from an ice-
8 tethered profiler (ITP; Toole et al., 2010) equipped with a velocity sensor (ITP-V; Williams et
9 al., 2010). Specifically, we use data from ITP-V 35, which was deployed on October 8, 2009
10 on an ice floe in the Beaufort Sea at 77° N, 135° W, as part of the Beaufort Gyre Observing
11 System (BGOS). The ice floe was 2.6 m thick, so hydrostatic adjustment resulted in an ice-
12 ocean interface at around 2.3 m depth (Cole et al. 2014). Ocean velocity profiles were
13 obtained every 4 h to 150 m depth, with an effective vertical resolution of 1 m. To examine
14 the ice-ocean shear ($\vec{u}_i - \vec{u}_o$) and the ice-ocean velocity angle, we use the shallowest
15 measurements from the velocity profiles, at a depth of 7 m. The ice velocity (\vec{u}_i) is derived
16 from hourly GPS fixes and linearly interpolated in time to align with the time of the ITP-V 35
17 observations. Further details, including calibrations and a discussion of errors in ITP-V 35,
18 are described by Cole et al. (2014).

19 Arctic sea ice concentration data is from the U.S. National Snow and Ice Data Center
20 (NSIDC), and is based on satellite-derived passive microwave brightness temperature.
21 Specifically, the NASA Team Algorithm (Swift and Cavalieri, 1985) was used to estimate the
22 sea ice concentration. These data are provided as a daily mean on a polar stereographic grid
23 with 25×25 km resolution. We re-gridded this data onto a regular $1.0^\circ \times 1.0^\circ$ grid.

24 **3.2 Reanalysis**

25 Observations of Arctic sea ice thickness are sparse, so instead we use the coupled Pan-arctic
26 Ice-Ocean Modeling and Assimilation System (PIOMAS; Zhang and Rothrock, 2003) to
27 estimate the basin scale Arctic sea ice thickness. PIOMAS consists of a 12-category thickness
28 and enthalpy distribution sea ice model coupled with the POP (Parallel Ocean Program)

1 ocean model (Smith et al., 1992). The data is monthly and covers from the year 1978 to 2013.
2 For the surface wind stress we used 10 m winds provided by the European Center for
3 Medium-Range Weather Forecasts ERA-Interim reanalysis dataset (Dee et al., 2011). The
4 data is 6 hourly with a horizontal resolution of $1.0^{\circ} \times 1.0^{\circ}$.

5

6 **4 Model evaluation**

7 In this section, we evaluate our analytical model against the ITP-V 35 observations of sub-sea
8 ice ocean velocity (Cole et al., 2014). Specifically, we compare the modeled wind-ice and
9 ice-ocean velocity angles against the observed values. As outlined in the introduction, one
10 might not expect the winter Beaufort Sea to serve as a useful test case because the sea ice
11 concentration is typically close to 100%, so the internal stresses neglected in our model may
12 be dynamically significant (Leppäranta, 2005). Additionally, sea ice formation in winter may
13 produce negative buoyancy forcing that induces strong convection and vertically-varying
14 eddy viscosity in the surface mixed layer, inconsistent with our assumption of as uniform
15 vertical viscosity throughout the Ekman layer (McPhee, 2012). However, the ITP-V 35
16 measurements indicate that the ice was very close to a free drift regime and experienced weak
17 vertical buoyancy fluxes in the surface mixed layer (Cole et al., 2014), so these features of
18 the winter sea ice pack may be less prominent than in previous observations. For a complete
19 picture of the stratification regime in the observed near-surface ocean, see figures 3, 4, 8 and
20 9 of Cole et al. (2014). For example, the mixed layer depth over the Beaufort Sea is very
21 shallow in October (~15 m) and deepens to 30–40 m in February and March (Fig. 9 of Cole
22 et al. 2014).

23 **4.1 Model parameters**

24 The ITP-V 35 was deployed upon a 2.6 m-thick ice floe, which is much thicker than the mean
25 ice thickness over the western Beaufort Sea. Fig. 1a shows the PIOMAS sea ice thickness
26 averaged from October 2009 to March 2010. During this time period, sea ice thickness over
27 the western Beaufort Sea (around $74\text{--}78^{\circ}$ N, $135\text{--}150^{\circ}$ W) is around 1.4–1.6 m. It is therefore
28 likely that ITP-V 35 was mounted on a relatively sturdy floe, whereas the surrounding floes
29 were thinner. Sea ice concentration over this region is mostly over 85-90% from October to

1 March (Fig. 1b). We use $\varphi = 1$ as a reference case because, as we will show below, the ice
2 drift speed and angle predicted by our model are insensitive to φ for sea ice concentrations
3 greater than $\sim 50\%$. The velocity of the mixture layer (see Sec. 2) represents a bulk average
4 over many floes, and similarly the ocean Ekman layer in any given location responds to
5 stresses transmitted by a series of ice floes passing overhead. For the purpose of model
6 evaluation we therefore take the sea ice thickness h_i to be 1.5 m, which is appropriate for
7 basin-scale sea ice momentum balance, rather than a momentum balance at the scale of the
8 individual ice floe.

9 Extensive measurements of the ice-ocean boundary layer suggest that the annual mean value
10 of the dimensionless vertical eddy diffusivity K_o^* is about 0.028 (McPhee, 1994; 2008).
11 Below we also present model predictions using a nominal enhanced value of $K_o^* = 0.1$,
12 which yields improved agreement between the model and the observations. A possible
13 explanation for this is that the ITP-V observations mostly cover winter season (from October
14 to March), when surface buoyancy loss due to sea ice formation can enhance the vertical
15 eddy diffusivity by a factor of up to 10 (McPhee and Morison, 2001). However, it is more
16 likely that internal stresses in the ice impede its motion, so the canonical value of $K_o^* =$
17 0.028 overestimates the ice drift. Thus the reader should not infer from our results that using
18 a larger value of K_o^* is more physically realistic. Finally, the geostrophic current in the
19 interior of polar oceans, \vec{u}_g , is poorly constrained, and we assume that this term is small
20 relative to the surface current. This assumption should be more robust on intraseasonal time
21 scales, as surface winds can strengthen rapidly in a few days, so the resultant surface Ekman
22 velocity is likely to be much larger than the interior geostrophic flow.

23 For other parameters, we used standard values used in many previous studies: $\rho_a =$
24 1.35 Kg/m^3 , $\rho_i = 910 \text{ Kg/m}^3$, and $\rho_o = 1026 \text{ Kg/m}^3$. The atmospheric drag coefficients
25 C_{ai} and C_{ao} depend on the season, the ice fraction, and the surface roughness (Lüpkes et al.,
26 2012), but for simplicity we use constant values of $C_{ai} = 1.89 \times 10^{-3}$ and $C_{ao} = 1.25 \times$
27 10^{-3} (Lüpkes and Birnbaum, 2005). We prescribe the ice-ocean drag coefficient C_{io} based
28 on the findings of Cole et al. (2014), who found that $C_{io} = 7.1 \times 10^{-3}$ best fit the ITP-V 35
29 measurements. However, we note that it is difficult to calculate C_{io} accurately from the ITP-
30 V data because measurements of the vertical eddy momentum fluxes were made at a depth of

1 6 m. This depth lies partway into the Ekman layer, so we expect the stress to be rotated and
2 reduced in magnitude relative to the stress at the ice base.

3 **4.2 Results**

4 Fig. 3 shows the observed ice speed (black line) as a function of the 10 m wind speed.
5 Consistent with Thorndike and Colony (1982), the relationship is approximately linear,
6 except for weak winds (speed less than 2 m/s). For moderately strong winds, sea ice moves
7 with a speed around 1.5–2% of the surface wind speed. This is consistent with or slightly
8 weaker than the well-known 2% relationship (Thorndike and Colony, 1982). Fig. 3a shows
9 that the analytical model with the canonical value of K_o^* ($K_o^* = 0.028$) overestimates the
10 observed ice speed by 20–40%, whereas a larger vertical diffusivity (blue-dotted line;
11 $K_o^* = 0.1$) fits better with the observations. As stated above, this is probably because the
12 internal stresses in the relatively concentrated sea ice (85–100% in winter) impede the ice
13 drift. We also compare the observed ice drift speeds with those predicted by ‘classical’ free
14 drift (Leppäranta, 2005), in which we neglect both the Ekman layer velocity and the
15 geostrophic velocity. Mathematically this corresponds to assuming an infinitely large vertical
16 diffusivity ($K_o^* \rightarrow \infty$) in our model. This classical free drift (blue solid line in Fig. 3a) is about
17 30% slower than the ice drift with an interactive Ekman layer (red line in Fig. 3a), verifying
18 that the IOBL substantially increases the wind-induced ice speed.

19 Fig. 3b shows that there is little difference in ice speed between 100% sea ice cover (red line;
20 $\varphi = 1$) and 50% sea ice cover (red line; $\varphi = 0.5$) in this model (Fig. 3b). As shown in
21 equation (10a), the ice-ocean drag coefficient, C_{io} , also directly influences the wind-induced
22 ice velocity. The bottom panels of Fig. 3 show the sensitivity of the ice speed to C_{io} for
23 $K_o^* = 0.028$ (Fig. 3c) and $K_o^* = 0.1$ (Fig. 3d) respectively. Decreasing C_{io} from 0.0071 to
24 0.004 increases ice speed by up to 20–25%. In the Appendix we calculate C_{io} using the ITP-
25 V data and plot C_{io} both as a function of 10 m wind speed and surface stress (Fig. A1).
26 Consistent with Cole et al. (2014), the individual observed values of C_{io} vary widely, by a
27 factor of 10. In general, there is no obvious dependence of C_{io} on the surface stress, so we
28 use the constant value $C_{io} = 0.0071$ of Cole et al. (2014).

1 Fig. 4 shows that the wind–ice velocity angle θ_{ai} decreases as the surface wind strengthens,
 2 consistent with previous observations (Thorndike and Colony, 1982). The velocity angle is
 3 overestimated by 5–10 degrees in the case when the canonical vertical diffusivity $K_o^* =$
 4 0.028 is used (Fig. 4a). The analytical model with $K_o^* = 0.1$ reproduces this curve
 5 remarkably well. Recall from equation (21) that wind-ice velocity angle θ_{ai} decreases as the
 6 ice-ocean to wind-ice stress ratio ($|\vec{\tau}_{io}|/|\vec{\tau}_{ai}|$) increases, and that this stress ratio is always
 7 smaller than 1. Thus, the decrease of θ_{ai} with increasing surface wind speed indicates that
 8 the stress ratio increases as the surface winds strengthen. In other words, the momentum
 9 becomes more efficiently transferred down to the ocean as the surface wind speed increases.
 10 For relatively weak winds, the observational errors in θ_{ai} (gray shadings in Fig. 4) are large,
 11 whereas for stronger winds the air–ice velocity angle is much better constrained (Cole et al.,
 12 2014). The wind–ice velocity angle θ_{ai} estimated using the ‘classical’ free drift case is about
 13 20 degrees smaller than that predicted by the canonical vertical diffusivity $K_o^* = 0.028$.
 14 Moreover, the classical free drift approximation substantially underestimates the observed
 15 θ_{ai} even though the internal friction is neglected. This result indicates that the IOBL is
 16 essential for properly simulating the direction of the ice drift. Fig. 4b shows that sea ice cover
 17 plays a nontrivial role in changing the wind–ice velocity angle θ_{ai} , although the internal
 18 stresses are neglected in the model. Decreasing sea ice cover from 100% ($\varphi = 1$) to 50%
 19 ($\varphi = 0.5$) increases θ_{ai} by 20 degrees for large wind speeds.

20 The shallowest measurement depth of ITP-V 35 is 7 m, which is far below the ice base (~2.6
 21 m). The Ekman spiral rotates the velocity and stress vectors substantially between the ice
 22 base and 7 m. Consequently the ITP-V data cannot accurately quantify the IOBL turning
 23 angle, which also requires an estimate of the near-surface geostrophic velocity to be made.
 24 Instead we test our analytical treatment of the IOBL using the velocity angle between the ice
 25 floe and the ocean at 7 m, $\theta_{io}|_{z=-7\text{m}}$. To calculate $\theta_{io}|_{z=-7\text{m}}$ from the analytical model, the
 26 velocity angle needs to be adjusted using the Ekman layer solution, which can be written as a
 27 function depth, z , as

$$\vec{u}(z) = \vec{u}_o \exp\left(\frac{z + h_o}{\delta_E}\right) \exp\left(i \frac{z + h_o}{\delta_E}\right). \quad (22)$$

28 Here \vec{u}_o is the ocean surface velocity at the bottom of sea ice, $h_o = (\rho_i/\rho_o)h_i$ is the depth

1 of the ice base, and $\delta_E = \sqrt{2K/f}$ is the Ekman depth. We have used complex variables to
 2 describe two-dimensional vectors, *e.g.* $\vec{u}_o = (u_o, v_o) \equiv u_o + iv_o$, because this presents
 3 changes in vector orientation more intuitively. The complex term, $\exp(i(z + h_o)/\delta_E)$,
 4 produces a velocity $\vec{u}|_{z=-d}$ at any depth d that is rotated relative to \vec{u}_o by a
 5 clockwise angle of $(d - h_o)/\delta_E$ radians. Thus the adjusted velocity angle between the ice
 6 and the ocean at any depth in the Ekman layer is:

$$\theta_{io}|_{z=-d} = \theta_{io}|_{z=-h_o} + (d - h_o)/\delta_E. \quad (23)$$

7 In Fig. 5 we plot $\theta_{io}|_{z=-7\text{m}}$ as a function of the ice speed, comparing the predictions of our
 8 model with the data from Cole et al. (2014). In general, the ice–ocean velocity angle
 9 $\theta_{io}|_{z=-7\text{m}}$ decreases as ice speed increases. Consistent with Cole et al. (2014), the variance
 10 in the observationally derived values of $\theta_{io}|_{z=-7\text{m}}$ is quite large, especially for low ice
 11 speeds. Our analytical solution for the ice-ocean velocity angle, adjusted using equation (23),
 12 agrees reasonably well with the ITP-V 35 measurements. Again, the analytical model predicts
 13 the observational curve better when the higher vertical diffusivity of $K_o^* = 0.1$ is used. Fig.
 14 5b shows that ice concentration is certainly a factor affecting the ice-ocean velocity angle,
 15 θ_{io} . Decreasing sea ice cover from 100% to 50% causes a decrease in θ_{io} because the
 16 direction of ice drift is constrained by the wind stress over open water between the ice floes
 17 ($\vec{\tau}_{ao}$) and the associated surface Ekman transport.

18 **4.3 Parameter sensitivity**

19 Having evaluated our model against the ITP-V 35 measurements using the best available
 20 estimates for the model parameters, we now explore the sensitivity of the model’s predictions
 21 to key physical properties of the sea ice itself, namely its thickness and concentration. In Fig.
 22 6 we plot the sensitivity of the wind-ice velocity angle (θ_{ai}) and the IOBL turning angle
 23 (θ_{IOBL}) to a range of sea ice concentrations (φ) and ice thicknesses (h_i). In general, the wind-
 24 ice velocity angle increases substantially with sea ice thickness (Fig. 6a): for a moderate wind
 25 speed of 6 m/s, increasing the sea ice thickness from 0.25 m to 3 m increases this angle from
 26 20° to 50°. It can therefore be inferred from equation (21) and Fig. 6a that thicker ice has
 27 smaller stress ratio $|\vec{\tau}_{io}|/|\vec{\tau}_{ai}|$, implying that thicker ice is less efficient in transferring the

1 momentum into the ocean, leading to larger wind-ice velocity angle. In other words, thicker
2 ice absorbs more of the wind-input momentum into the Coriolis torque, transmitting less to
3 the ocean below.

4 Sea ice concentration also strongly influences these angles. Consistent with Fig. 4b, Fig. 6b
5 shows that wind-ice velocity angle increases as sea ice concentration decreases. There is little
6 difference in this angle between 100% and 75% ice concentrations – the angle is less
7 sensitive to relatively high sea ice concentration. However, the angle rapidly increases as sea
8 ice concentration gets below 50%: at 25% sea ice concentration the wind-ice angle is 20°
9 larger than at 100% concentration, even for the strongest winds in the dataset. The response
10 of the IOBL turning angle to the mixture of sea ice and water ($\varphi \ll 1$) is presented in Fig. 6d.
11 The turning angle is negative for weaker surface winds in the case when sea ice concentration
12 is less than 100%. This is because wind stress over the ice-free component of the mixture
13 layer is transmitted directly to the water below. As the sea ice concentration approaches zero,
14 the stress transmitted through the ice becomes negligible in determining the direction of the
15 surface Ekman velocity (\vec{u}_o). Because the ITP-V 35 track covers mostly ice-covered regions
16 ($\varphi \approx 1$) and the shallowest measurement depth is 7 m, it is difficult to verify whether
17 negative IOBL turning angles appear in the observations.

18 **5 Application to wind-driven summer sea ice changes**

19 In this section, we quantify the effect of intra-seasonal southerly wind strengthening events
20 on Arctic sea ice cover using near-surface wind data, and compare the results with satellite
21 observations. There are several notable Arctic weather perturbations in the spring and
22 summer over the Pacific sector of the Arctic Ocean, such as the development of the Arctic
23 dipole mode (Wu et al., 2006), quasi-stationary cyclonic winds (Serreze et al., 2003) and
24 synoptic cyclones (Zhang et al., 2013). These perturbations are often accompanied by rapid
25 strengthening of southerlies and a reduction of the sea ice concentration (SIC) on
26 intraseasonal time scales. In the Arctic summer, sea ice thickness is mostly below 2 m (Fig.
27 7a) and the area of the marginal ice zone with a moderate SIC (25–75%) is quite large (Fig.
28 7b). We therefore hypothesize that the strengthening of southerlies should efficiently
29 redistribute the sea ice cover in the summer.

1 This analysis simultaneously serves as an additional evaluation of our analytical model
2 described in Sec. 2. Our model is particularly appropriate to motions in the marginal ice zone,
3 where internal stresses are negligible, and to short-duration intensification of the southerly
4 winds, during which the surface ocean velocity is typically large compared to the geostrophic
5 velocity. This evaluation could in principle be extended to compare the modeled sea ice
6 velocities directly against sea ice drift products. However, we have chosen to retain our focus
7 on the sea ice concentration rather than the ice drift velocity. Ice drift products exhibit
8 considerable uncertainty, particularly during summer when the ice is typically thinner
9 (Sumata et al., 2014). Furthermore, there is considerable variance in the ice speed and the
10 wind-ice velocity angle even in the ITP-V data (see Figs. 3 and 4), in which the ice velocities
11 are measured accurately using GPS fixes.

12 **5.1 Methods**

13 For surface wind forcing, we used the ERA-Interim reanalysis. Arctic sea ice concentration
14 data is from the U.S. National Snow and Ice Data Center (NSIDC). The Arctic sea ice
15 concentration shows multi-decadal declining trend and this trend was removed for each
16 calendar day and for each grid. For sea ice thickness, we used the climatological mean
17 PIOMAS sea ice thickness data averaged from 1990 to 2012.

18 Using the analytical solutions derived in Sec. 2, sea ice velocity is calculated from the ERA-
19 Interim daily 10 m winds. Then, lagged composite analyses are performed in order to
20 investigate how a rapid development of southerlies affects sea ice concentration during the
21 Arctic summer. We used data from 1990 to 2012 and focused on the summer, from August 1
22 to September 30 (AS). To define the events of the rapid strengthening of southerlies, the
23 surface winds over the Pacific sector of the Arctic are zonally and meridionally averaged,
24 from 150°E to 230°E and from 70°N to 90°N (cosine weighting is applied to each latitude).
25 Then, the southerly wind event is defined as a time period when the averaged southerly wind
26 value exceeds 1 standard deviation for three or more consecutive days. If the beginning of an
27 event occurs within 7 days of the end of the preceding event, then the latter event is discarded.
28 This procedure identifies 27 events during the analysis period. Lag zero is defined as the day
29 when the averaged southerly winds peak. Prior to generating the composites, a 3-day moving

1 average is applied to filter out noise associated with day-to-day fluctuations.

2 The southerly wind-induced sea ice drifts redistribute sea ice concentration. This effect is
 3 computed using the following evolution equation: $d\varphi = -\left[\frac{\partial(U_i\varphi)}{\partial x} + \frac{\partial(V_i\varphi)}{\partial y}\right]dt$. Here φ is
 4 sea ice concentration, which ranges from 0 to 1, at each grid point, and dt is a time step,
 5 which has a length of one day in this study. To calculate sea ice concentration anomalies we
 6 subtract the long-term climatological mean $d\varphi$ from the daily $d\varphi$ during the southerly
 7 wind events. Then, the anomalous daily $d\varphi$ is integrated from the lag day -8 to estimate the
 8 cumulative changes in sea ice concentration associated with the southerly wind events:

$$\Delta\varphi = -\sum_{t=-8}^{t=lag} (d\varphi)' dt - \sum_{t=-8}^{t=lag} \left[\frac{\partial(U_i\varphi)}{\partial x} + \frac{\partial(V_i\varphi)}{\partial y} \right]' dt \quad (24)$$

9 Here, prime ()' denotes a deviation from the long-term climatological mean. The time
 10 integration starts from the lag -8 because the southerly wind events, on average, start about a
 11 week before they peak. The results we present are not very sensitive to the starting date. The
 12 maximum and the minimum values of the cumulative changes in sea ice concentration ($\Delta\varphi$)
 13 are limited by the mean sea ice concentration, which ranges between 0% and 100%. For
 14 example, if the cumulative changes in the mean sea ice concentration ($\Delta\varphi + \bar{\varphi}$), where $\bar{\varphi}$ is
 15 the climatological-mean sea ice concentration, exceeds 100%, then $\Delta\varphi$ is given as
 16 $(100 - \bar{\varphi})\%$. All of the analytical model results presented here use the canonical value of
 17 vertical diffusivity ($K_o^* = 0.028$) and the ice-ocean drag coefficient of $C_{io} = 0.0071$ (Cole
 18 et al. 2014). As shown in Fig. 3, the wind-induced ice speed is sensitive to both K_o^* and C_{io} .

19 **5.2 Results**

20 Fig. 8 illustrates the response of the SIC (shadings in the left column) to the development of
 21 southerlies (vectors in the left column) from the East Siberian and Chukchi Sea. Over a 10
 22 day period since the development of southerlies, the SIC in these regions decreases by 7–8%.
 23 We suggest that the reduction of SIC is caused by the southerly wind-induced sea ice drift. In
 24 the meantime, because of cross-polar flow, SIC on the Atlantic sector slightly increases (blue
 25 color). To further test this possibility, the wind-induced redistribution of SIC is calculated
 26 using our model, specifically equations (17–18). The result, shown in the right column of Fig.

1 8, captures the spatial pattern in the observed SIC anomalies. The anomalous sea ice velocity
2 (vectors in the right column) is generally directed towards the Beaufort Sea, a little east of the
3 surface wind velocity with the drift angle ranging between 20° and 45° . The calculated SIC
4 anomalies at day +6 (bottom row of Fig. 8) are largely consistent with the satellite observed
5 SIC anomalies. However, the calculated SIC anomalies somewhat underestimate the
6 observation. At day +6, the calculated reduction of SIC over the Pacific sector is about 5–6%,
7 whereas the observed reduction of SIC is up to 6–8%. The increase in SIC over the Atlantic
8 sector associated with cross-polar flow is also slightly underestimated.

9
10 There are several possible explanations for the discrepancy between the modeled and
11 observed sea ice concentration anomalies. Over the Atlantic sector, the cross-polar flow
12 increases SIC and the internal stresses are likely to increase as well. As mentioned earlier, our
13 analytical model neglects internal stresses that can decelerate ice drift and pile up sea ice over
14 the Atlantic sector. It is possible that the real sea ice thickness in the Arctic summer is thinner
15 than the PIOMAS sea ice thickness. While PIOMAS simulates the Arctic sea ice thickness
16 within a reasonable range, the model is known to generally *overestimate the thickness of*
17 *measured sea ice thinner than 2 m* (Johnson et al. 2012; Schweiger et al. 2011). Or, the
18 vertical diffusivity K_o^* in August and September might be smaller than 0.028 due to surface
19 buoyancy input resulting from sea ice melt (McPhee and Morison, 2001). The formation of a
20 summer freshwater layer at the ice base can also reduce the ice-ocean drag coefficient C_{io}
21 (Randelhoff et al., 2014), as can changes in the shape of the ice base. Additionally, the
22 atmosphere-ice drag coefficient may be larger during the summer season due to additional
23 form stress associated with the formation of leads and melt ponds (Lüpkes et al., 2012).

24
25 Finally, we ask: to what extent does the IOBL accelerate the wind-induced ice drift? We have
26 neglected the ocean surface geostrophic velocity in our analytical model calculations,
27 retaining only the surface Ekman layer. However, if the Ekman layer velocity were
28 sufficiently weak compared to the ice velocity then we could simply neglect the ocean
29 velocity altogether. As introduced in Sec. 4, the ‘classical’ free drift (zero Ekman layer
30 velocity) corresponds mathematically to the limit of infinitely large vertical diffusivity
31 ($K_o^* \rightarrow \infty$) in our model. In Fig. 9 we compare the anomalous sea ice speed associated with

1 the wind-induced ice drift with and without an IOBL included in the model. Both curves have
2 been generated by averaging the sea ice speed anomalies over the Pacific sector of the Arctic
3 (from 150°E to 230°E and from 70°N to 90°N), and then calculating lagged composites
4 across all southerly wind events. Consistent with Fig. 3a, this plot illustrates that the IOBL
5 increases the wind-induced sea ice speed up to 40–50%. We therefore conclude that the IOBL
6 plays a substantial role in the rapid reduction of SIC associated with strong southerly wind
7 events.

8

9 **6 Summary and discussion**

10 In this study we have derived an analytical model for wind-induced sea ice drift and
11 evaluated our model against measurements from a velocity sensor-equipped ice-tethered
12 profiler (ITP-V). We then used the model to demonstrate that Arctic southerly wind events
13 can drive substantial reductions in sea ice concentration over short timescales.

14

15 Our model has elements in common with Rossby similarity theory (McPhee, 2008) for the
16 ice–ocean boundary layer (IOBL), but differs crucially in the respect that it allows for an
17 arbitrary mixture of ice and open water. The key features of this model are:

- 18 1. The ice floes and leads containing open water are described via a bulk “mixture layer”,
19 momentum balance, following Gray and Morland (1994).
- 20 2. The IOBL consists of an Ekman layer whose depth is assumed to depend linearly on
21 the surface stress velocity (McPhee, 2011), most appropriate for a neutrally stratified
22 IOBL with no surface buoyancy flux (McPhee and Morison, 2001).
- 23 3. The transfer of momentum between the 10 m winds, the ice and ocean components of
24 the mixture layer, and the ocean surface layer are assumed to follow a quadratic drag
25 law. By contrast Rossby similarity theory assumes the ‘law of wall’ to hold in a
26 narrow boundary layer at the top of the IOBL (McPhee, 2008).

27 Though the simplicity of our model carries several caveats, discussed below, it also confers
28 several advantages. As mentioned in the introduction, the analytical tractability of the model
29 makes it very efficient, certainly much more so than running a fully coupled model of the
30 Arctic. This makes it straightforward to interpret the model; the analytical expressions in Sec.

1 2 yield physical insight into the velocity observations from ITP-V 35 and the sea ice
2 concentration data from NSIDC. The model’s “mixture layer” formulation (Gray and
3 Morland, 1994) also makes it suitable for the marginal ice zone. Our analytical approach was
4 possible because we assumed a constant vertical diffusivity in the surface Ekman layer. This
5 simplification results in an IOBL turning angle (θ_{IOBL}) that is independent of ice–ocean stress
6 \vec{u}_{io}^* in our model, whereas the turning angle slightly decreases as the ice–ocean stress
7 strengthens in observations (McPhee 2008). It may be possible to extend our model to
8 incorporate Rossby similarity theory and a stratified IOBL, but for sea ice concentrations
9 below 100% the surface boundary condition must be modified to account for the presence of
10 patches of open water between the ice floes.

11

12 A shortcoming of our model is that it neglects internal stresses in the ice, which can feature
13 prominently in the momentum balance when the sea ice concentration is close to 100%
14 (Leppäranta, 2005). The model is therefore only formally applicable for sea ice
15 concentrations below ~85%. In this article we have frequently used the case of 100% sea ice
16 concentration ($\varphi = 1$) for the purpose of illustration, as the model solution is qualitatively
17 unchanged for sea ice concentrations greater than ~50%.

18

19 Our analytical model qualitatively reproduces the wind-induced ice speed and wind-ice
20 velocity angles in the ITP-V 35 observations. The agreement is improved by replacing the
21 canonical value $K_o^* = 0.028$ of the vertical eddy diffusivity with an enhanced value of
22 $K_o^* = 0.1$. However, this finding should not be interpreted to mean that the enhanced
23 diffusivity is more physically relevant. While the discrepancy between the model and
24 observations may be due to stronger turbulent mixing due to surface buoyancy loss, it is more
25 likely due to impedance of the sea ice motion by internal stresses, as the sea ice concentration
26 in the vicinity of the ITP-V 35 observations was likely around 85-90%.

27

28 We applied our analytical model to investigate the strong southerly events in the Arctic
29 summer to estimate the wind-induced reduction of SIC. The calculated reduction of SIC is
30 largely consistent with satellite observations. Our results verify that the southerly wind-
31 induced sea ice drift can substantially decrease SIC over the course of a week. Because the

1 wind-induced sea ice drift can be directly calculated from our analytical solution, the
2 underlying processes for the sea ice variability might be better identified by utilizing
3 reanalysis data. We suggest that our analytical model can be a flexible tool for identifying
4 and quantifying the mechanisms for the Arctic and Antarctic sea ice cover variability, which
5 is often associated with the changes in the global-scale circulation pattern (Lee et al. 2011;
6 Holland and Kwok 2012; Bitz and Polvani 2012; Li et al. 2014; Wettstein and Deser 2014;
7 Raphael and Hobbs 2014; Park et al. 2015).

8

9 **Author contributions**

10 A.L Stewart and H.-S. Park developed the analytical model for wind-driven drift of sea ice.
11 H.-S. Park conducted analyses and prepared figures. Both authors contributed equally to
12 writing the manuscript.

13

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21 Cole for assistance with the ITP-V 35 observational dataset.

22

23 **Appendix**

24 In this appendix we estimate the ice-ocean drag coefficient, C_{io} , using the ITP-V data. The
25 ITP-V was programed to record turbulent fluctuations at 6 m depth for 40 minutes on a daily
26 basis. As noted by Cole et al. (2014), C_{io} can be estimated by the relationship between ice-
27 ocean velocity shear and turbulent momentum flux:

$$\sqrt{\overline{u'w'^2} + \overline{v'w'^2}} = C_{io}[(u_i - u_6)^2 + (v_i - v_6)^2]. \quad (\text{A1})$$

1 Here the overbar $\overline{(\)}$ denotes a 40-minute time average and the primes $(\)'$ denote
 2 deviations from the time mean. The ice and 6 m ocean velocities are denoted as (u_i, v_i) and
 3 (u_6, v_6) respectively. Using equation (A1), we calculated daily C_{io} from the ITP-V data,
 4 following Cole et al. (2014). In Fig. A1 we plot C_{io} as a function of the surface wind speed
 5 and the surface stress. These plots support our approximation of the ice-ocean quadratic drag
 6 coefficient as a constant, $C_{io} = 0.0071$. Estimates of the IOBL quadratic drag coefficient C_d ,
 7 obtained by setting $u_6 = v_6 = 0$ in (A1) under the assumption that the interior geostrophic
 8 velocity is negligible, are qualitatively similar to those shown in Fig. A1 (not shown).

9

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1 **Figure Captions**

2 **Figure 1:** (a) sea ice thickness (m) and (b) sea ice concentration (%), averaged from October
3 2009 to March 2010. Sea ice thickness is from PIOMAS and sea ice concentration data is
4 from NSDIC.

5
6 **Figure 2:** Sensitivity of the IOBL turning angle (θ_{IOBL}) to α ($= \sqrt{2K_o^*/C_{io}}$), calculated from
7 equation (20), which is for $\varphi \sim 1$. The red dot corresponds to the canonical value for the
8 vertical eddy diffusivity ($K_o^* = 0.028$) and blue dot corresponds to a nominally increased
9 value ($K_o^* = 0.1$).

10
11 **Figure 3:** Sensitivity of ice speed (cm/s) to 10 m wind speed (m/s). The black line shows the
12 mean value calculated from ITP-V 35 observations binned by 10 m wind speed, and the gray
13 shadings indicate the range of one standard deviation from the mean. The red, dotted blue and
14 solid blue lines correspond to our analytical model, described in Sec. 2, with (a) vertical
15 diffusivities $K_o^* = 0.028, 0.1$ and ∞ (no IOBL) respectively. The sensitivity of the ice speed
16 to the ice concentration (φ) is shown in (b); the red and blue lines indicate 100 % ice cover
17 ($\varphi = 1$) and 50% ice cover ($\varphi = 0.5$) respectively. The bottom panel shows the sensitivity of
18 ice speed to ice-ocean drag coefficient (C_{io}), with vertical diffusivities (c) $K_o^* = 0.028$ and (d)
19 $K_o^* = 0.1$ respectively. The bulk sea ice thickness is taken to be 1.5 m.

20
21 **Figure 4:** The velocity angle (clock-wise rotation angle) between the 10 m winds and the
22 ITPV-35 ice floe as functions of the 10 m wind speed (m/s). Note that typically the ice
23 velocity lies to the right of the wind velocity. In each plot the black line is mean observed
24 value from the ITP-V 35 dataset, binned by wind speed, and the gray shadings indicate the
25 range of one standard deviation from the mean. In (a), the red, dotted blue and solid blue
26 lines correspond to our analytical model, described in Sec. 2, with vertical diffusivities $K_o^* =$
27 $0.028, 0.1$ and ∞ (no IOBL) respectively. In (b), the red and blue lines correspond to 100%
28 ($\varphi = 1$) and 50% ($\varphi = 0.5$) sea ice concentrations, in each case using the canonical vertical
29 diffusivity $K_o^* = 0.028$.

30

1 **Figure 5:** The velocity angle (clock-wise rotation angle) between the ice floe and the ocean
2 velocity at 7 m depth, as functions of the ice speed (cm/s). In each plot the black line is mean
3 observed value from the ITP-V 35 dataset, binned by ice speed, and the gray shadings
4 indicate the range of one standard deviation from the mean. In **(a)**, the red and blue lines
5 correspond to our analytical model, described in Sec. 2, with vertical diffusivities $K_o^* =$
6 0.028 and 0.1 respectively, and using 100 % ice concentration, $\varphi = 1$. In **(b)**, the red and
7 blue lines correspond to 100% ($\varphi = 1$) and 50% ($\varphi = 0.5$) sea ice concentrations, in each
8 case using the canonical vertical diffusivity $K_o^* = 0.028$.

9

10 **Figure 6:** Sensitivity of **(a, b)** the wind-ice velocity angle and **(c, d)** the IOBL turning angle
11 to various values of **(a, c)** sea ice thickness h_i (m) and **(b, d)** sea ice concentration (φ) as a
12 function of 10 m wind speed (abscissa; m/s). In all panels the dimensionless vertical
13 diffusivity is fixed at $K_o^* = 0.028$. In **(a, c)** we use 100% sea ice concentration ($\varphi = 1$), and
14 in **(b, d)** we use a sea ice thickness of $h_i = 1.5$ m.

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16 **Figure 7:** Aug-Sep climatological mean **(a)** sea ice thickness (m) and **(b)** sea ice
17 concentration (%) between 1990 and 2012. Sea ice thickness is from PIOMAS and sea ice
18 concentration data is from NSDIC.

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20 **Figure 8:** Composites of the anomalous sea ice concentration (%) calculated from NSIDC
21 satellite observations (left column) and from our analytical model using ERA-Interim 10 m
22 wind velocity data (right column) for lag -2 days (first row), 0 days (second row), 2 day (third
23 row), and lag +6 days (fourth row). See Sec. 5 for a full description of this calculation.
24 Vectors indicate the anomalous 10m winds from reanalysis (m/s; left column) and calculated
25 sea ice velocity (cm/s; right column). For the anomalous 10m winds (left column) and sea ice
26 velocity (right column), only vectors stronger than 1.5 m/s and 3.0 cm/s are plotted
27 respectively.

28

29 **Figure 9:** Lagged composite of the calculated sea ice speed (cm/s) associated with the strong
30 southerly events in the presence (red line) and in the absence (black line) of an IOBL in our
31 analytical model (in the absence of an Ekman layer the ocean surface velocity is simply set to

1 zero – the classical free drift case). The sea ice speed is area-averaged over the Pacific sector
2 of the Arctic (from 150°E to 230°E and from 70°N to 90°N). The sea ice speeds that include
3 the surface Ekman layer (red line) identical to those used to construct Fig. 8. The
4 dimensionless vertical diffusivity is set to $K_o^* = 0.028$ and $K_o^* = \infty$ for the IOBL (red line)
5 and no-IOBL (black line) cases respectively.

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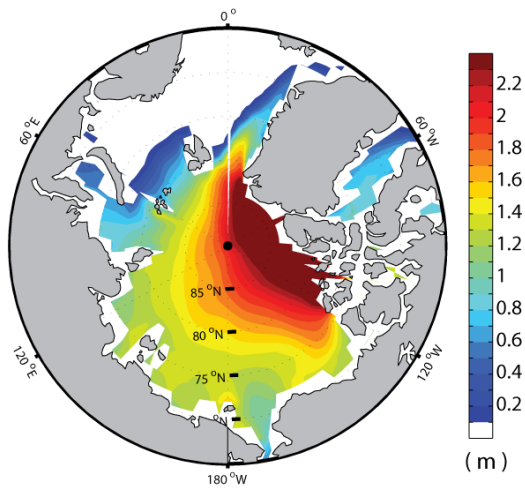
7 **Figure A1:** Sensitivity of the ice-ocean drag coefficient C_{io} to (a) the surface wind speed
8 (m/s) and (b) the surface stress (kg/m/s^2), calculated using equation (A1). The black line
9 shows the mean value calculated from ITP-V 35 observations and the gray shadings indicate
10 the range of one standard deviation from the mean. The red line corresponds to the value
11 estimated by Cole et al. (2014) based on least-squares approximation.

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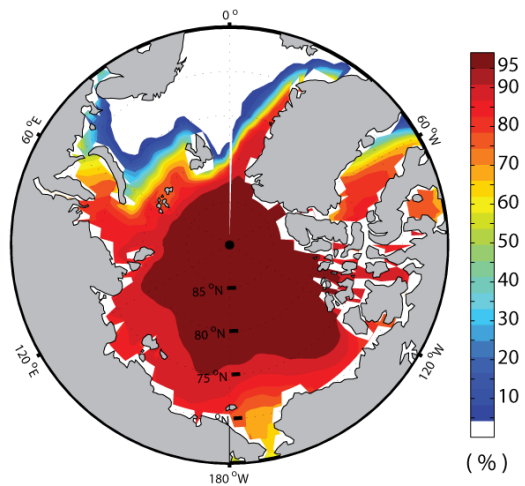
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(a) sea-ice thickness (Oct - Mar)



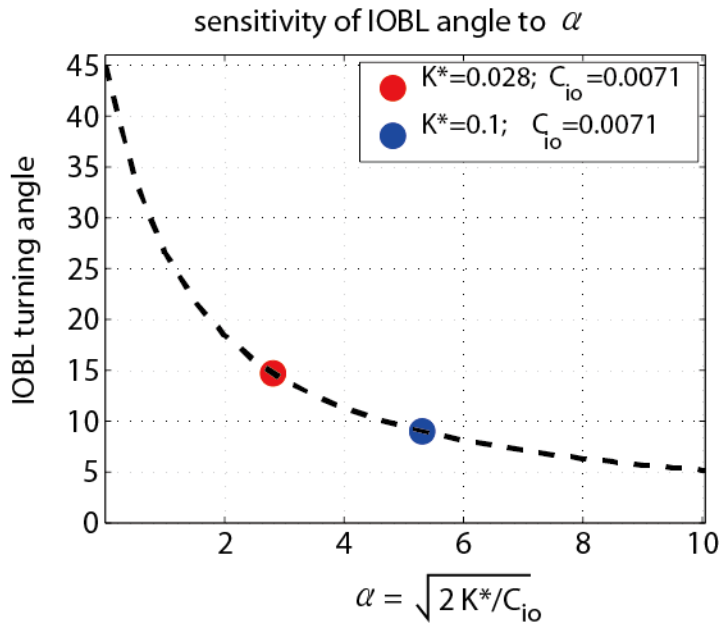
(b) sea-ice concentration (Oct - Mar)



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Figure 1: (a) sea ice thickness (m) and (b) sea ice concentration (%), averaged from October 2009 to March 2010. Sea ice thickness is from PIOMAS and sea ice concentration data is from NSDIC.

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4 **Figure 2:** Sensitivity of the IOBL turning angle (θ_{IOBL}) to α ($= \sqrt{2K_o^*/C_{io}}$), calculated from
5 equation (20), which is for $\varphi \sim 1$. The red dot corresponds to the canonical value for the
6 vertical eddy diffusivity ($K_o^* = 0.028$) and blue dot corresponds to a nominally increased
7 value ($K_o^* = 0.1$).

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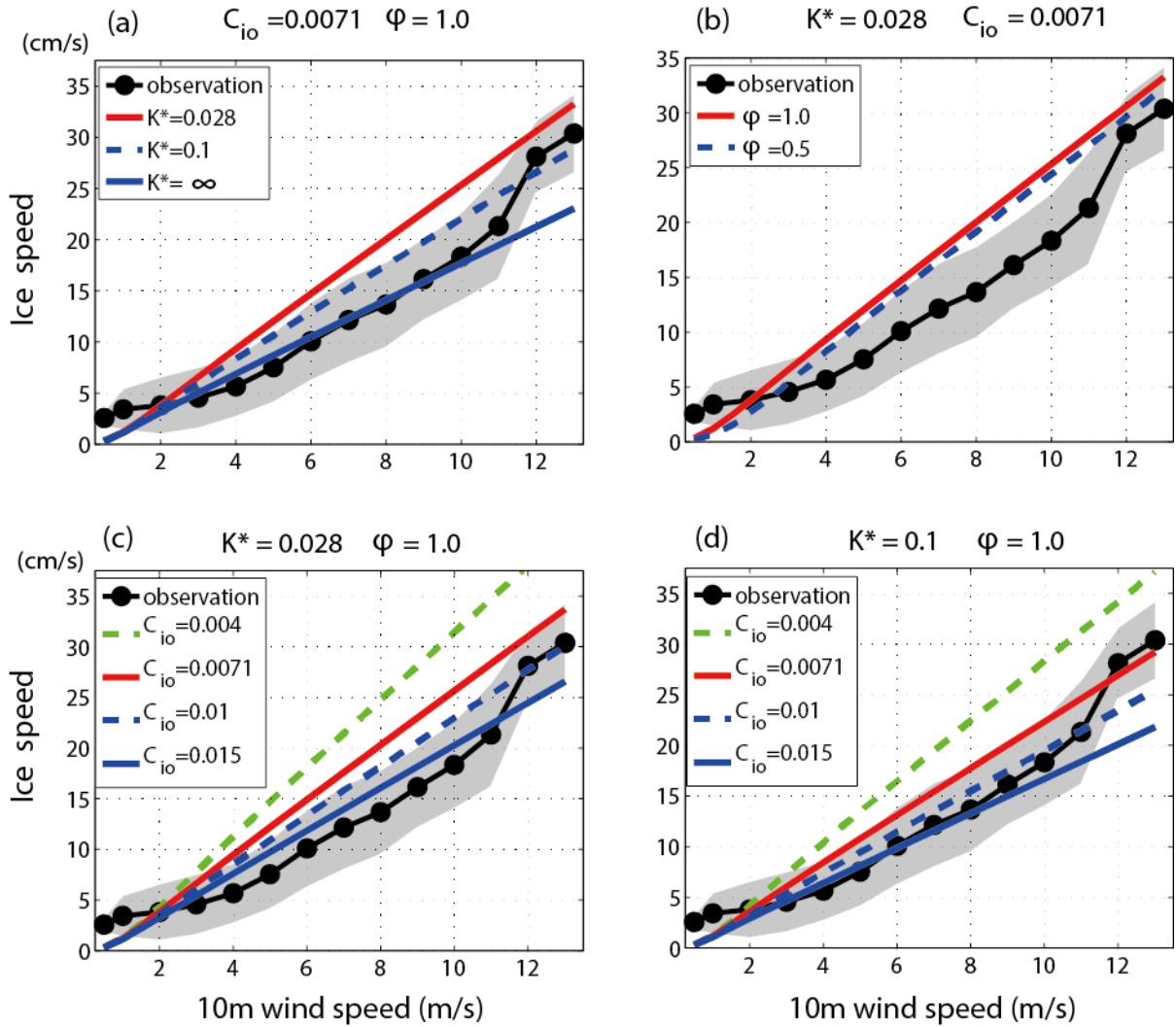
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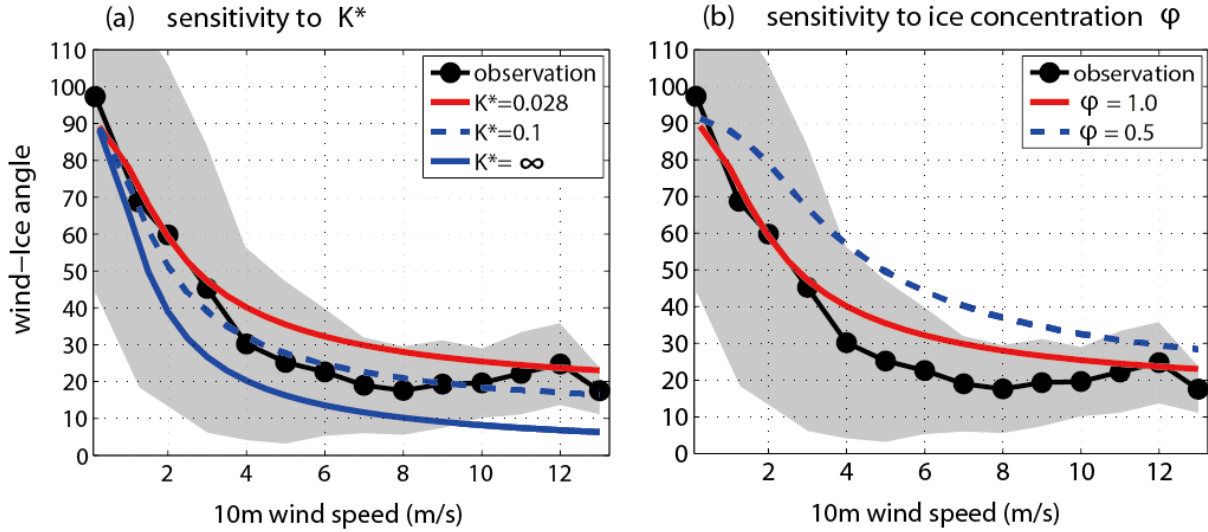
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4 **Figure 3:** Sensitivity of ice speed (cm/s) to 10 m wind speed (m/s). The black line shows the
 5 mean value calculated from ITP-V 35 observations binned by 10 m wind speed, and the gray
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 7 solid blue lines correspond to our analytical model, described in Sec. 2, with (a) vertical
 8 diffusivities $K_o^* = 0.028, 0.1$ and ∞ (no IOBL) respectively. The sensitivity of the ice speed
 9 to the ice concentration (φ) is shown in (b); the red and blue lines indicate 100 % ice cover
 10 ($\varphi = 1$) and 50% ice cover ($\varphi = 0.5$) respectively. The bottom panel shows the sensitivity of
 11 ice speed to ice-ocean drag coefficient (C_{io}), with vertical diffusivities (c) $K_o^* = 0.028$ and (d)
 12 $K_o^* = 0.1$ respectively. The bulk sea ice thickness is taken to be 1.5 m.

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Wind - Ice velocity angle



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4 **Figure 4:** The velocity angle (clock-wise rotation angle) between the 10 m winds and the

5 ITPV-35 ice floe as functions of the 10 m wind speed (m/s). Note that typically the ice

6 velocity lies to the right of the wind velocity. In each plot the black line is mean observed

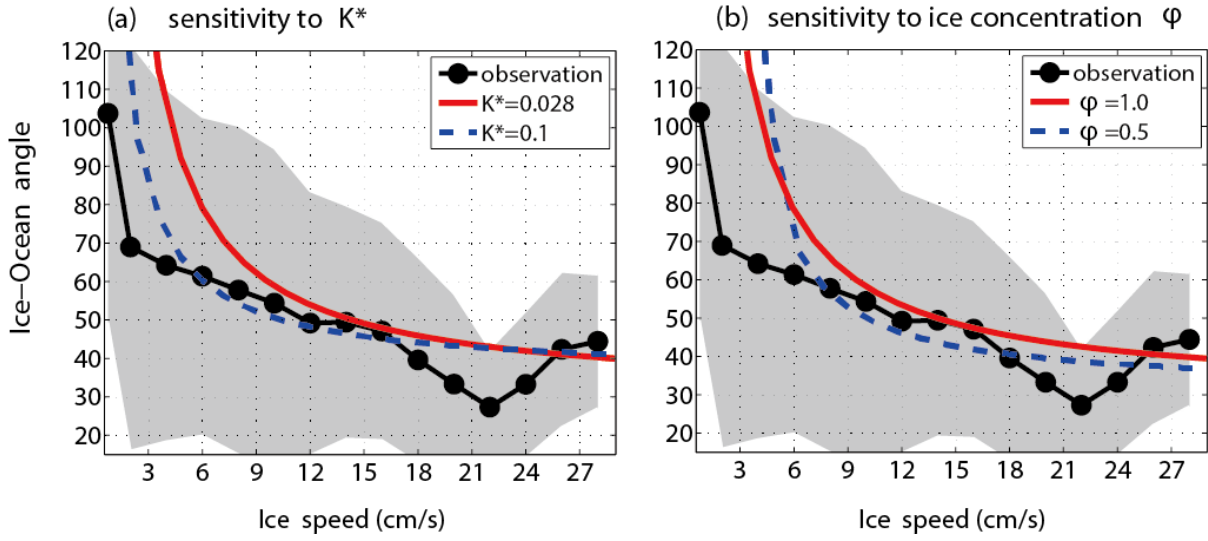
7 value from the ITP-V 35 dataset, binned by wind speed, and the gray shadings indicate the

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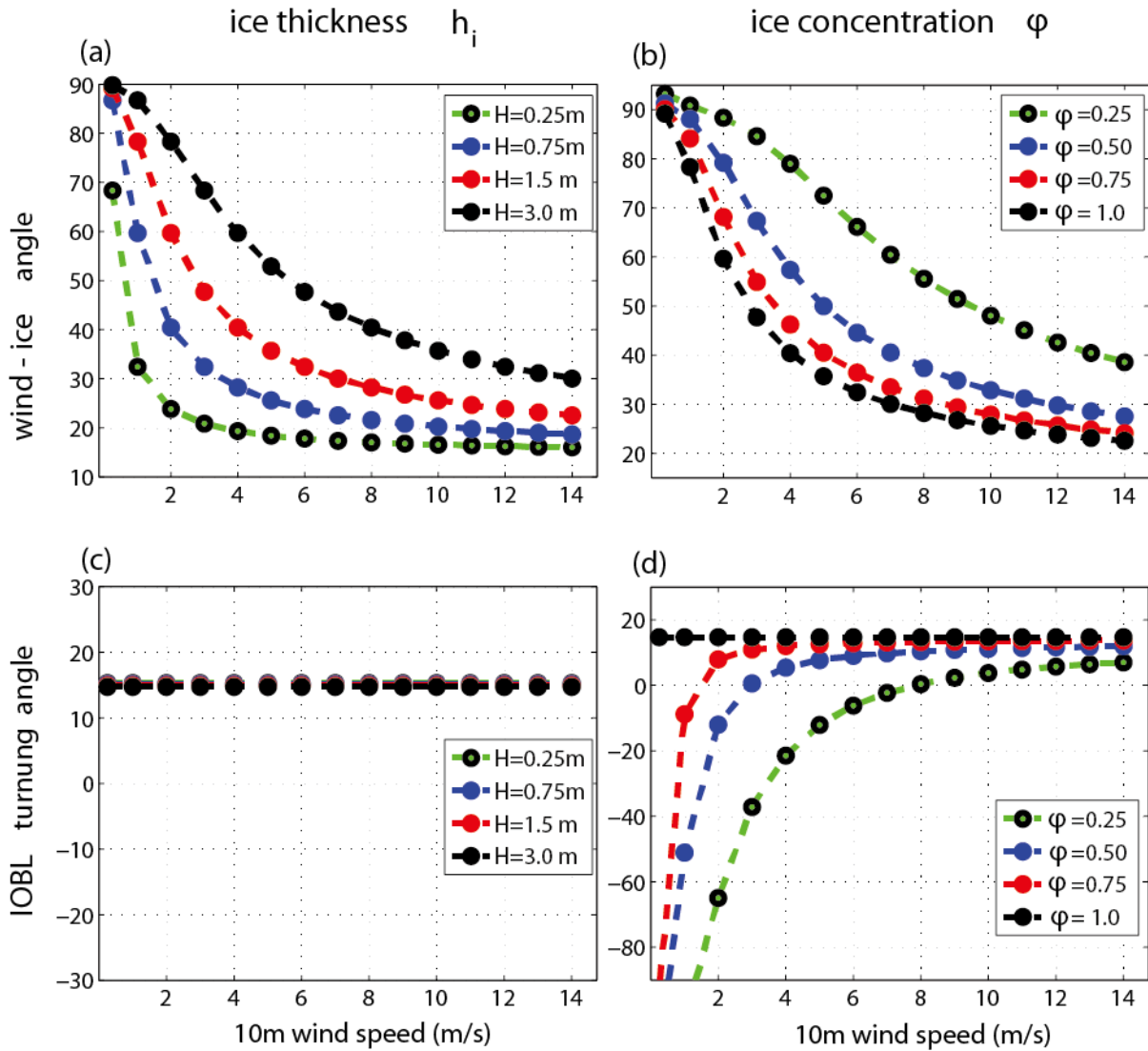
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Ice - Ocean velocity angle



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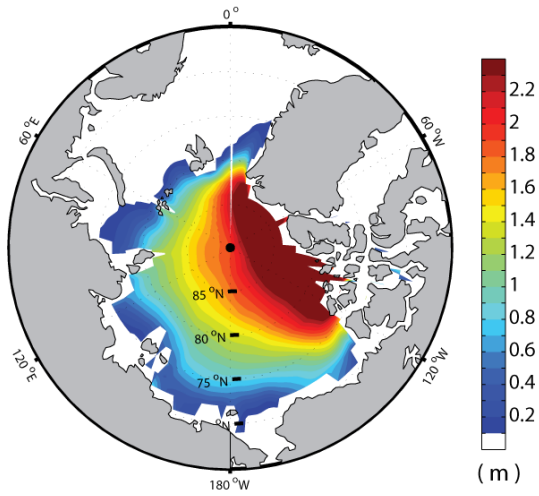
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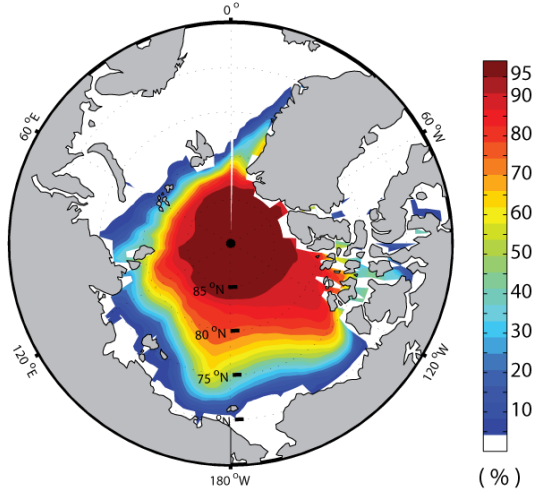
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Figure 6: Sensitivity of (a, b) the wind-ice velocity angle and (c, d) the IOBL turning angle to various values of (a, c) sea ice thickness h_i (m) and (b, d) sea ice concentration (ϕ) as a function of 10 m wind speed (abscissa; m/s). In all panels the dimensionless vertical diffusivity is fixed at $K_o^* = 0.028$. In (a, c) we use 100% sea ice concentration ($\phi = 1$), and in (b, d) we use a sea ice thickness of $h_i = 1.5$ m.

(a) sea-ice thickness (Aug-Sep)

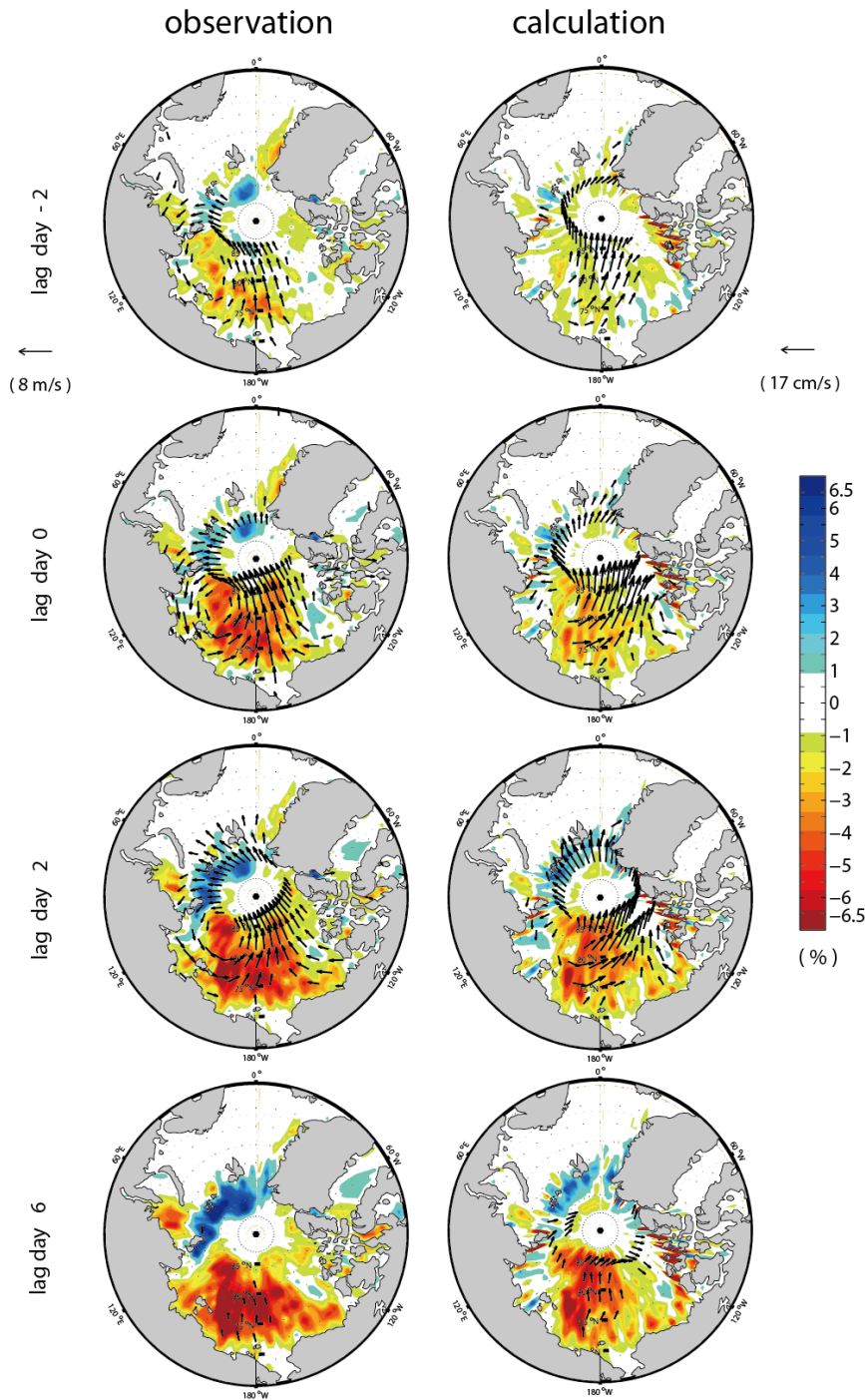


(b) sea-ice concentration (Aug-Sep)



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Figure 7: Aug-Sep climatological mean (a) sea ice thickness (m) and (b) sea ice concentration (%) between 1990 and 2012. Sea ice thickness is from PIOMAS and sea ice concentration data is from NSDIC.

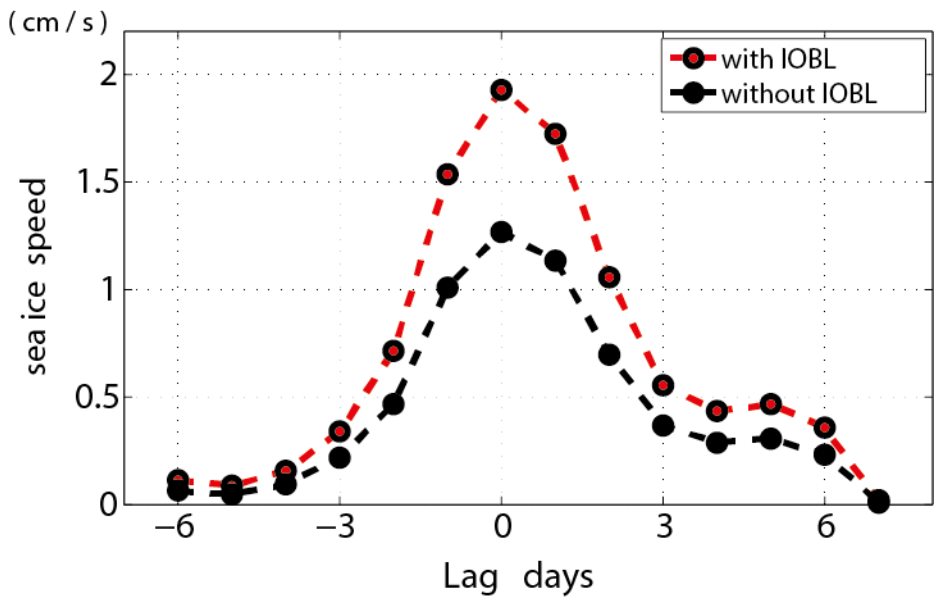


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 4 satellite observations (left column) and from our analytical model using ERA-Interim 10 m
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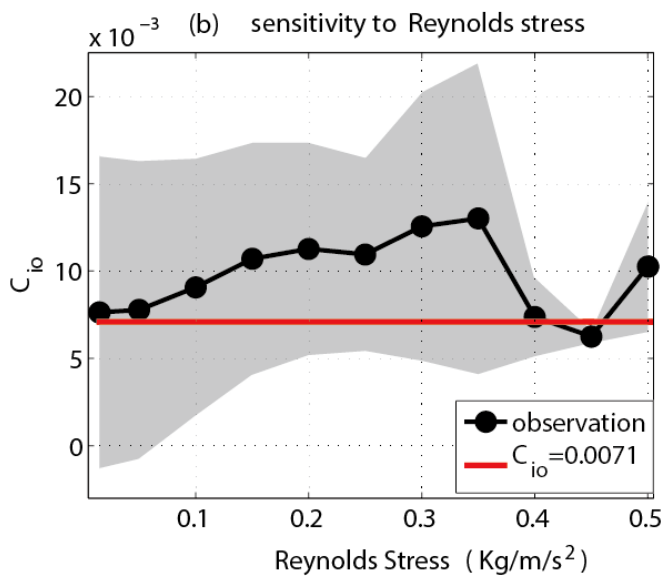
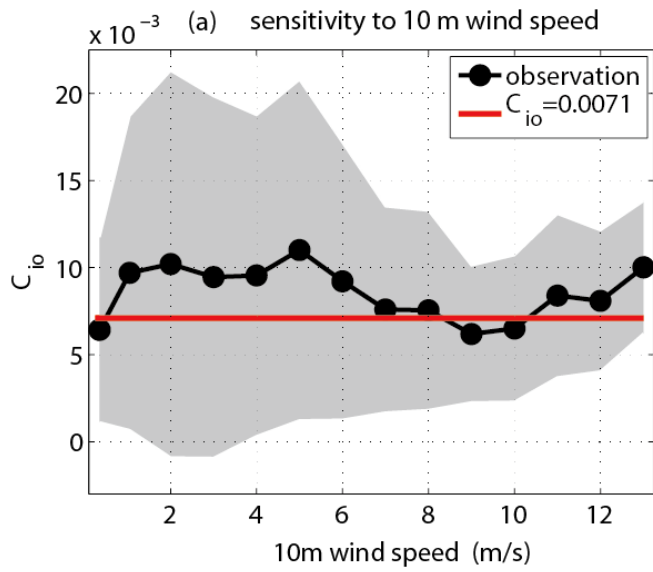


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 11 southerly events in the presence (red line) and in the absence (black line) of an IOBL in our
 12 analytical model (in the absence of an Ekman layer the ocean surface velocity is simply set to
 13 zero – the classical free drift case). The sea ice speed is area-averaged over the Pacific sector
 14 of the Arctic (from 150°E to 230°E and from 70°N to 90°N). The sea ice speeds that include
 15 the surface Ekman layer (red line) identical to those used to construct Fig. 8. The
 16 dimensionless vertical diffusivity is set to $K_o^* = 0.028$ and $K_o^* = \infty$ for the IOBL (red line)
 17 and no-IOBL (black line) cases respectively.

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3 **Figure A1:** Sensitivity of the ice-ocean drag coefficient C_{io} to (a) the surface wind speed
4 (m/s) and (b) the surface stress (kg/m^2), calculated using equation (A1). The black line
5 shows the mean value calculated from ITP-V 35 observations and the gray shadings indicate
6 the range of one standard deviation from the mean. The red line corresponds to the value
7 estimated by Cole et al. (2014) based on least-squares approximation.

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