

**Excess heat in
Greenland Ice Sheet**

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Excess heat in the Greenland Ice Sheet: dissipation, temperate paleo-firn and cryo-hydrologic warming

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Abstract

Ice temperature profiles from the Greenland Ice Sheet contain information on the deformation history, past climates and recent warming. We present full-depth temperature profiles from two drill sites on a flowline passing through Swiss Camp, West Greenland.

5 Numerical modeling reveals that ice temperatures are considerably higher than would be expected from heat diffusion and dissipation alone. The possible causes for this excess heat are evaluated using a Lagrangian heat flow model. The model results reveal that the observations can be explained with a combination of different processes: enhanced dissipation (strain heating) in ice-age ice, temperate paleo-firn, and cryo-
10 hydrologic warming in deep crevasses.

1 Introduction

Vertical ice temperature profiles of the Greenland Ice Sheet (GrIS) carry information on past upstream surface temperature and accumulation rates. This information is modified by vertical and horizontal stretching of the ice during flow, smoothed by diffusion,
15 and altered by subglacial and englacial heat sources.

Characteristic ideal profiles at different locations in the ice sheet have been obtained with numerical advection-diffusion models (e.g. Budd et al., 1982; Letreguilly et al., 1991; Funk et al., 1994; Greve, 1997). Full-depth ice temperature profiles from the ablation zone of the GrIS have been published for only 9 drill sites: five along an approximate flow line downstream of Swiss Camp (Thomsen et al., 1991) and four in Jakobshavn Isbræ (Iken et al., 1993; Lüthi et al., 2002). Despite the limited spatial extent of these observations, comparison between modeled and observed temperature profiles allow us to explore the complexity of heat sources in the ablation zone.

25 Previous work from Jakobshavn Isbrae demonstrates that comparison of modeled and measured ice temperature profiles provides a means to infer ice-dynamical characteristics such as vertical stretching of basal ice as it enters Jakobshavn Isbræ (Iken

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et al., 1993; Funk et al., 1994). In this case, the validity of the assumed initial and boundary conditions was assessed by an almost perfect match of measured and modeled ice temperatures at drill site DUCK at the margins of Jakobshavn Isbræ (Fig. 1) (Lüthi et al., 2002). It is noteworthy that the temperature profile at 500 km from Funk et al. (1994) agrees well with the profile at Swiss Camp (Thomsen et al., 1991) whereas all other temperature profiles from the Paakitsoq area (Thomsen et al., 1991) are considerably warmer. These warmer temperatures must be caused by heat sources not accounted for in the model. Such heat sources are likely flowing water in moulins and englacial pathways, or freezing water in crevasses, processes recently referred to as “cryo-hydrologic warming” (Phillips et al., 2010, 2013). Future increases in melt area extent might therefore lead to more cryo-hydrologic warming, a mechanism considered to cause rapid future warming of the ice sheet (Phillips et al., 2013).

In this study we present full-thickness temperature profiles from four new boreholes at drill sites FOXX and GULL, located on a flow line downstream of Swiss Camp with temperature profile TD5. Using a numerical heat flow model we calculate expected ice temperature profiles for our study sites. Comparison of modeled profiles with measurements shows excess heat of the ice in the ablation area. Possible sources of this excess heat are investigated and discussed.

2 Data and methods

2.1 Drill sites

The location of the three drill sites in the Western ablation zone of the GrIS is indicated on the map in Fig. 1. Sites FOXX and GULL were instrumented in summer 2011 with sensors for ice deformation, subglacial pressure, and ice temperature (Ryser et al., 2014a, b; Andrews et al., 2014). Deep drilling at Swiss Camp and installation of thermometer string TD5 in 1990 was performed by Danish Technological University (DTU; Thomsen and Thorning, 1992; Ahlstrom, 2007).

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2.2 Temperature measurements

At sites FOXX and GULL temperature was measured with the custom-built digital borehole sensor system DIBOSS (described in Ryser et al., 2014b) at depths below 300 m. These deep sensors are complemented with analog thermistors closer to the surface. In each DIBOSS sensing unit an IST TSic-716 semiconductor temperature sensor with integrated 14 Bit AD-converter (resolution 4 mK, ± 70 mK absolute) was mounted in direct contact with the enclosing aluminum housing. These sensors were logged in 10 min intervals for two years with a Campbell CR-1000 data logger.

For measurements close to the surface, sets of two thermistor strings were deployed in two boreholes at site FOXX, and in one borehole at site GULL. Each string consisted of a 18-core cable with nine NTC thermistors (Fenwal 135-103FAG-J01) that were shielded from pressure and moisture, and for which individual calibration curves were determined in a calibration bath at six to eight reference temperatures in the range of -17.5 to 10°C with a digital multi-meter. Reference thermistors, calibrated to an absolute accuracy of 20 mK by the Swiss Federal Office of Metrology, were used to determine the bath temperature. The maximum difference between reference temperatures and the calibration curve was 40 mK. In the field, resistances were measured with a full bridge circuit logged by a Campbell CR-1000 data logger, and occasional readings with a digital multi-meter over the course of two years. With the setup described above, the absolute accuracy of all measured temperatures is estimated to be better than 70 mK.

Figure 2 shows ice temperature measured at sites FOXX, GULL and TD5 (Swiss Camp; Thomsen and Thorning, 1992). Ice temperature increases from the highest site towards the margin. A notable exception is profile FOXX2 which was recorded in 86 m distance from FOXX1, and which is even colder than GULL.

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2.3 Heat sources

Heat sources within the ice are due to dissipation (strain heating), or related to flowing or freezing water. Here we calculate order of magnitude estimates of these effects. For this purpose we assume ice with a density of $\rho_i = 900 \text{ kg m}^{-3}$ heat capacity $C_i = 2093 \text{ J m}^{-3}$ and latent heat of freezing $L = 333.5 \text{ kJ kg}^{-1}$.

2.3.1 Freezing water

The heat energy from freezing water needed to raise the temperature of 1 m^3 of ice by $\Delta T = 1 \text{ K}$ is

$$W = \rho_i C_i \Delta T = 1.88 \text{ MJ m}^{-3}. \quad (1)$$

To produce this amount of heat by freezing, 5.6 kg of water are required. Such water is readily available at the glacier surface during the ablation season, and also in the lower reaches of the accumulation area where permanent storage of water within the firn was recently discovered, although 250 km south of our sites (e.g. Harper et al., 2012; Forster et al., 2013). Water seeping through cracks can freeze and provide an extensive heat source down to the bottom of such cracks.

2.3.2 Strain heating

The volumetric heat production rate P due to dissipation (strain heating) under shear deformation is calculated under the assumption of the shallow ice approximation as

$$P = \dot{\epsilon}_{ij} \sigma_{ij} \sim 2 \dot{\epsilon}_{xz} \sigma_{xz} = 2A(T) \sigma_{xz}^4, \quad (2)$$

where the shear stress $\sigma_{xz} = \rho_i g h \tan \alpha$ is calculated from the density ρ_i , gravity g , surface slope α and depth h below the surface. The value of P therefore varies with current surface slope, and depends on depth and current temperature. The temperature dependent flow rate factor $A(T)$ is taken from Cuffey and Paterson (2010) which agrees

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well with measurements of ice deformation at sites FOXX and GULL (Ryser et al., 2014b). At a shear stress of 0.1 MPa and with $A(-5^{\circ}\text{C}) = 29.3\text{MPa}^{-3}\text{a}^{-1}$ the heating power is $P = 0.006\text{MJ m}^{-3}\text{a}^{-1}$, equivalent to a heating rate of 0.31 K per century.

2.4 Heat flow model

The heat flow model is adapted to model the lower accumulation and upper ablation areas in our region of study. The model tracks a flowline with origin at the ice sheet center (0 km; Fig. 7b in Funk et al., 1994). Figure 3 shows our area of interest, located on this flowline between coordinate 450 and 530 km. In this coordinate system, the 1990 drill site TD5 (Thomsen et al., 1991) at Swiss Camp is located at coordinate 498 km at the equilibrium line. The two 2011 drill sites FOXX and GULL are located at coordinates 520 km and 530 km.

Heat flow is modeled with the Finite Element method in two dimensions. The model implements a block of ice in Lagrangian description. The Finite Element library Libmesh (Kirk et al., 2006) was used to solve the transient heat diffusion equation in a Lagrangian reference frame (i.e. the mesh nodes follow the deforming material; e.g. Hutter and Jöhnk, 2004)

$$\rho_i C_i \frac{\partial T}{\partial t} = \nabla(k\nabla T) + P, \quad (3)$$

with temperature T , density ρ_i , specific heat capacity C_i , heat conductivity k and volumetric heat production rate P . The model domain consists of a block discretized with rectangular Quad4 elements with Galerkin weighting (linear approximation of temperature). Dirichlet boundary conditions (prescribed temperature) were applied at the upper and lower boundary. Implicit time stepping was implemented with a standard Crank-Nicolson scheme.

Each model run consisted of the deformation of the block of ice (the model domain) during horizontal motion over the distance of 100 km (from 450 to 550 km; Fig. 3). The horizontal velocity was taken from Funk et al. (1994), resulting in a travel time from

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Swiss Camp to FOXX of ~ 900 years. During motion along the flow line the model domain (the block) is horizontally and vertically stretched or compressed to comply with the local ice thickness. Vertical shearing was neglected (i.e. $\dot{\epsilon}_{xz} = 0$) so that the block moved in plug-like flow. Stretching was applied homogeneously throughout the ice body honoring mass continuity with $\dot{\epsilon}_{zz} = -\dot{\epsilon}_{xx}$ and $\dot{\epsilon}_{yy} = 0$ (with coordinates x in flow direction, y across, z vertical). Nodes were moved according to their position with respect to the origin of the coordinate system of the Lagrangian model domain. Heat (i.e. temperature at the model nodes as the solution from an earlier time step) is therefore advected with the mesh in horizontal and vertical direction.

Mass accumulation at the upper surface was simulated by adding new elements on top of the domain, in which temperature was set to the surface temperature. Surface temperature and mass balance are taken from Fig. 4 in Funk et al. (1994). Similarly, mass removal by surface melt was implemented by removing elements from the top of the domain. In the Libmesh implementation this was achieved in a simple manner by solving the heat flow equation in a subdomain of a larger mesh with constant topology. With this approach, only the extent of the active subdomain was adjusted in every time step. To obtain a high resolution of the grid close to the surface the mesh was refined to a coarseness of 0.5 m in the top 150 m of the active subdomain, using the adaptive mesh refinement with hanging nodes implemented in Libmesh, as illustrated in Fig. 4. A constant time step size of 1 year was used, which together with the vertical mesh size of 0.5 m at the surface gives a numerically stable solution. This model setup closely reproduced analytical solutions for two setups: Sinusoidal forcing of the surface temperature, and a moving boundary solution for constant surface ablation (Vorkauf, 2014).

The initial dimensions of the model domain were 1000 m length and 2000 m thickness. The mesh was refined around the vertical coordinate 1670 m corresponding to the vertical position of the initial surface. Elements above the current surface were flagged to belong to the inactive subdomain. The heat flow Eq. (3) was solved in the active subdomain below the surface, with Dirichlet boundary conditions (prescribed

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temperature) at the uppermost active element, and melting point temperature at the bottom. Figure 4 illustrates the progressive deformation of the mesh, the refinement of elements around the surface, and the varying number and extent of active elements. In all model runs the mesh was considerably finer than shown in Fig. 4; 200 elements in the vertical, 20 in the horizontal, and the mesh was refined around the surface in 5 steps instead of the 3 steps displayed in the figure for illustration.

The initial temperature profile F450, located 450 km along the flow line, is taken from (Funk et al., 1994, Fig. 8b). This profile was obtained by solving the advection-diffusion equation with a discrete phase-change boundary along the flowline from the ice sheet center, with prescribed surface and basal velocity. In our model, the block is assumed to move at prescribed horizontal velocities, also taken from Fig. 4 in Funk et al. (1994). These velocities are similar to those from recent satellite imagery feature tracking (Joughin et al., 2008).

3 Model results

In the following we compare model runs of the heat flow model with borehole data. The model runs are driven with different internal heat sources, and a modified surface boundary condition. These assumptions are independent from each other, and are combined to investigate the origin of measured temperatures profiles. Designations of model runs implementing these assumptions are given in Table 1. The relative importance of these contributions is evaluated by comparison of modeled to measured vertical temperature profiles from Swiss Camp (TD5), GULL and FOXX (both profiles).

Figures 5–7 show comparisons of measured temperature profiles to model results from the reference run mD, and for runs with additional heat sources. The reference model run mD (dissipation only) reveals that measured ice temperatures are considerably higher than modeled throughout the ice column (Fig. 5). The maximum excess heat energy of 27 MJ m^{-3} corresponds to a temperature difference of up to 14 K. Following Eq. (1), correcting the temperature difference between the modeled (mD) and

observed temperature profiles in the upper part of the model domain would require additional heat from refreezing water equivalent to 9 % by mass.

Adding enhanced dissipation through enhanced shearing ice deformation in the Wisconsin ice (model run mE; Fig. 5) explains the observed excess heat between 500 and 700 m depth. The vertical extent of Wisconsin ice was taken from Ryser et al. (2014b) but the enhancement factor had to be set to 5 instead of the measured (and commonly assumed) value of 3. Since the whole model domain moves at the same velocity, the basal ice moves faster than in reality, and therefore has less time to warm. A model run with half surface velocity (not displayed) shows that enough heat is produced at an enhancement factor of 3 to explain measured temperature in the lowest 200 m.

The effect of accumulation of temperate firn (run mF) is shown in Fig. 6. In this model run the surface temperature between 460–475 km was set to 0 °C, which corresponds to the 160 years time span 1570–1730 C.E. This seemingly arbitrary horizontal extent of temperate firn conditions coincides with reconstructed warm temperatures at the deep drill sites GRIP and Dye3 (Dahl-Jensen et al., 1998) (see Sect. 4).

4 Discussion

Any shape of temperature profile within the ice can be obtained by carefully positioning heat sources during certain time spans within the ice body. The aim of this study is not to perfectly match the observed ice temperature distribution but to investigate how several simple source mechanisms might contribute to the observed temperature profiles. The lower panels of Figs. 5–7 indicate the amount of extra heat per volume needed to match the measured temperatures. This heat is likely provided by several heat sources: dissipation (strain heating), temperate paleo-firn, and cryo-hydrologic warming.

For the ice near the base, strain heating is a crucial process to provide the required 10MJ m⁻³ of heat (Fig. 5). Calculations with Eq. (2) show that for the considered ~900 years of ice flow the warming is of the order 3K which is sufficient to explain the measured temperature of the lowest 200 m.

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The relatively warm ice between 100 and 300 m depth at site Swiss Camp (profile TD5; Fig. 5) can be explained by temperate firn conditions in the past. Setting the surface temperature of the accumulated firn between horizontal coordinate 460 and 475 km to melting temperature (Fig. 3) yields the temperature profile shown in Fig. 6. This time span coincides with reconstructed warm temperatures in 1570–1730 (Dahl-Jensen et al., 1998). We assume that during this warm period surface melt events were frequent in the accumulation zone, and therefore the firn was considerably warmed, or even at melting temperature throughout the year. Such conditions with perennial water within the firn have recently been found in the accumulation area in southern Greenland (Humphrey et al., 2012; Harper et al., 2012). Currently, firn temperatures are again warming in the accumulation zone upstream of the study area (Polashenski et al., 2014), and will leave their imprint in the thermal state of the ice sheet. Warm paleo-firn only affects the upper ablation area, and explains only measured temperatures of borehole TD5, but is not sufficient to reproduce warm temperatures at depth at sites GULL and FOXX.

The temperate paleo-firn and ice accumulated in the lower accumulation area is presently emerging as relatively warm ice in the upper ablation area. Further downstream, ice accumulated under cold conditions in the dry-snow accumulation area emerges at the surface. Both thermal regimes are clearly visible at our drill sites: At GULL a flat, dirty and sluggish ice surface is reminiscent of temperate Alpine glaciers. At FOXX the surface is bright white with many deep cryoconite holes, which is usually found when cold ice emerges in the ablation area (e.g. Ryser et al., 2013). Our near-surface temperature profiles (Fig. 2a) support this notion, with temperatures above -1°C at GULL, but colder near-surface temperatures at downstream drill site FOXX. It is likely this difference in surface temperature, and therefore the distribution of dust (dirty ice vs. cryoconite holes) that leads to the dark band visible in the upper ablation zone of the western GrIS (Wientjes et al., 2011).

For the central ice body an important heat source is needed to provide the 25 MJ m^{-3} heat, corresponding to the observed 12–14 K temperature difference at GULL and

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FOXX (Fig. 5). Strain heating due to horizontal stress gradient is one possible heat source. Caterpillar-like horizontal extension and compression on diurnal and longer time scales has been observed in the study area (Ryser et al., 2014a). This heat source is, however, not strong enough: A quick calculation with Eq. (2), $A(-10^{\circ}\text{C})$ and a continuous, very high horizontal longitudinal stress gradient of 0.1 MPa yields a heat production of only $0.0011\text{ MJ m}^{-3}\text{ a}^{-1}$ which is one order of magnitude lower than the shear strain-induced heating of basal ice discussed above.

To explain the high temperature at GULL and FOXX, the only conceivable heat source at depth is advection of heat through flowing, or ponding and freezing water between Swiss Camp and GULL. A major crevasse zone halfway between the sites, and moulins draining water from the surface have been mapped (Thomsen et al., 1988; Phillips et al., 2011). The extent and amount of such heat sources was investigated with several model runs with simple source geometries and durations. Assuming a single crevasse advected to the drill site, its depth has to be of the order of 400 m , and it needs to be provide 0°C temperature for 100 years. Figure 7 shows results from a model run assuming a series of crevasses of 400 m depth and 100 m spacing which provide 0°C temperature for 50 years.

Very deep crevasses ($300\text{--}400\text{ m}$) with tens of years of activity are only possible if they are water-filled (Van der Veen, 1998), but do not penetrate to the bottom. While there is hydrofracturing as a mechanism to create a crevasse, there must be a mechanism to stop their depth penetration. Limited water supply for hydrofracturing is one possible cause, which is very likely within the small upstream surface area within a crevasse field. Another possible limiting factor for crevasse penetration to the bed is tougher ice at the bottom. Fracture toughness at -20°C is orders of magnitude lower than at temperatures approaching the melting point (Schulson and Duval, 2009, Table 9.1). We therefore suggest that water-driven crevasses stop their downwards growth once they reach warmer ice. If such very deep, water-filled crevasses indeed exist is unknown, although some observational evidence of strong englacial reflectors

was detected in the study area (Catania et al., 2008; Catania and Neumann, 2010). These strong reflectors are likely due to water stored within the glacier ice.

An alternative explanation to crevasses are moulins, vertical shaft systems draining water from the surface. Moulins are stationary drainage features on an undulating surface, and are only active for a few years until they move out of surface depressions (Catania and Neumann, 2010). Their spacing along a flow line amounts to the duration of their activity times the flow velocity, and thus hundreds of meters in the area of our drill sites (Thomsen et al., 1988; Phillips et al., 2011). A series of model runs was performed that implement moulins as vertical shafts at melting temperature during their activity (Vorkauf, 2014). As line sources they provide little warming to the surrounding ice. Modeled temperature difference at the site of a moulin is below 1 K after 10 years of inactivity (Vorkauf, 2014). Furthermore, modeled vertical patterns of ice temperature around moulins do not agree with the observed temperature profiles. Therefore we conclude that very deep water-filled crevasses, rather than moulins, are the main heat sources in the ablation area.

5 Conclusions

We showed that the thermal structure of the ice in the ablation area of the GrIS is dominated by strong heat sources leading to excess heat, as compared to modeled heat diffusion alone. Three types of heat sources were identified with a modeling study: dissipation, temperate paleo-firn, and cryo-hydrologic features, represented by very deep water-filled crevasses.

An important conclusion of the modeling study is that temperate firn was accumulated in the now cold accumulation area during a warm period of about 160 years, during 1570–1730 C.E. (Dahl-Jensen et al., 1998). This temperate paleo-firn is presently emerging as relatively warm ice in the upper ablation area, and is likely the cause for the observed dark band in the ablation area of the western GrIS (Wientjes et al., 2011).

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Future warming of the firn areas of the GrIS by extreme melt events, such as in Summer 2012 (McGrath et al., 2013), are likely in a warming Arctic. Extended areas of surface melt might lead to increasing firn temperatures, affecting large parts of the ice sheet. Such recent warming has already been detected in the study area (Polashenski et al., 2014).

The central ice body at our study sites is 10–15 K warmer than modeled with heat diffusion alone. To heat this ice to observed temperatures, a continuous heat source with melting point temperature is required which penetrates down to 300–400 m below the surface. The most likely sources are very deep, water-filled crevasses which persist for decades as they move through the extensional stress regime of a crevasse zone.

All of these heat sources were inferred from comparison of models with measurements. How important localized sources, such as crevasses and moulins, are for the thermal regime of the ice is still a matter of debate. Sampling ice temperature at sites suited for drilling (uncrevassed depressions with surface streams) yields a skewed picture of the full variability encountered in nature. Without a systematic sampling of ice temperatures to great depth, the information content extracted from individual holes is to be taken with care. This argument is impressively illustrated by the two temperature profiles from site FOXX which are 86 m apart, but show large differences in the upper 300 m (up to 5 K in 200 m depth).

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Table 1. Designation of model runs with different heat sources. These sources are combined in different model runs, e.g. run mEC.

mC	refreezing of water-filled crevasses
mD	dissipation from strain heating/reference run
mE	dissipation from strain heating with enhancement
mF	temperate firn above equilibrium line

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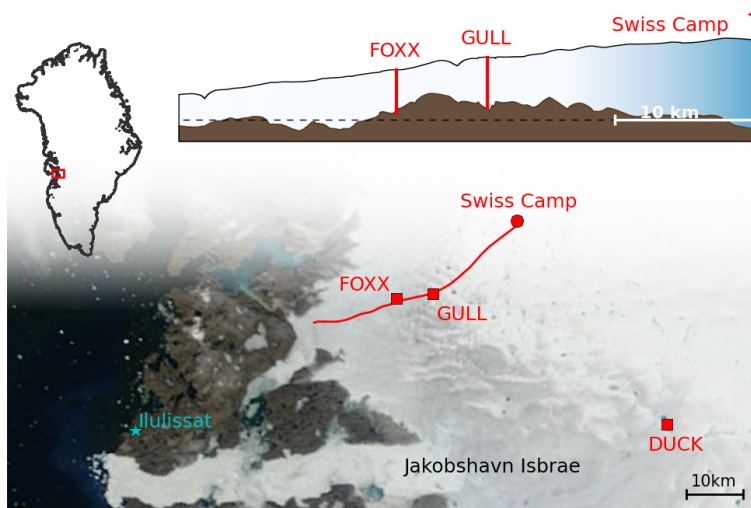


Figure 1. The study site indicated with red area within Greenland outline is illustrated with a MODIS satellite image (NASA/GSFC, 2010). The drill sites FOXX and GULL are located on a flowline downstream of Swiss Camp, and North of Jakobshavn Isbrae. Site DUCK is from 1995 (Lüthi et al., 2002). The inset shows bed and surface topographies along the flowline at five-fold vertical exaggeration (data from DTU Space and Remote Sensing, 2005; Gogineni, 2012).

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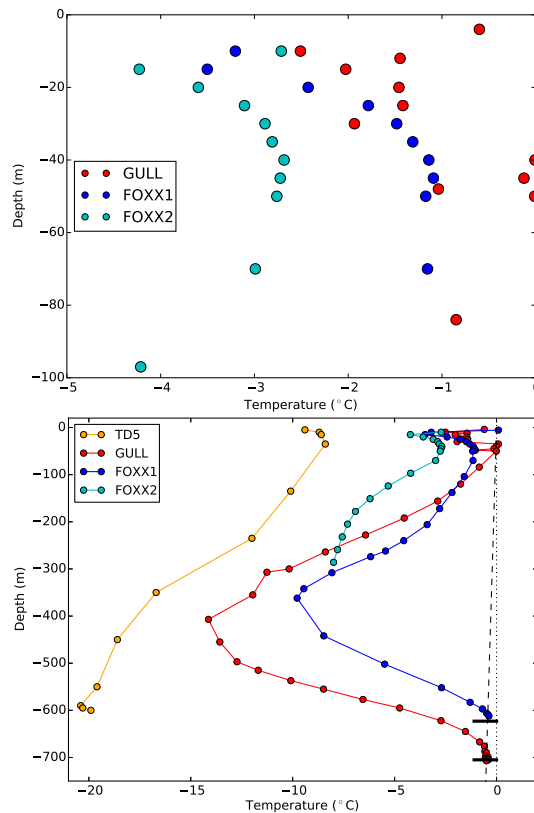


Figure 2. Measured ice temperatures. **(a)** shows near-surface temperatures at sites GULL and FOXX. Holes FOXX1 and FOXX2 are 86 m apart. **(b)** shows measured ice temperatures in four boreholes at the drill sites TD5 (Swiss Camp; data from Thomsen et al., 1991), GULL and FOXX. The dashed line indicates the pressure melting temperature.

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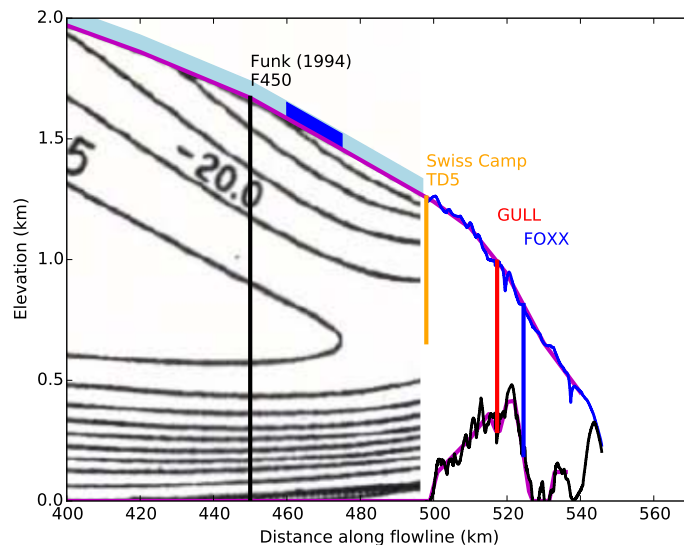


Figure 3. The locations and depths of temperature profiles at sites TD5, GULL and FOXX are shown as colored vertical lines on a background plot of the modeled temperature field from Fig. 7b in Funk et al. (1994). The temperature profile F450 at horizontal coordinate 450 km is used as model input. Bedrock (black) and surface (blue) was obtained from detailed radar data (DTU Space and Remote Sensing, 2005). Smoothed versions, indicated with purple lines, were used as model input. The light-blue area indicates cold firn conditions, the dark blue area between 460 and 475 km the area of temperate firn conditions.

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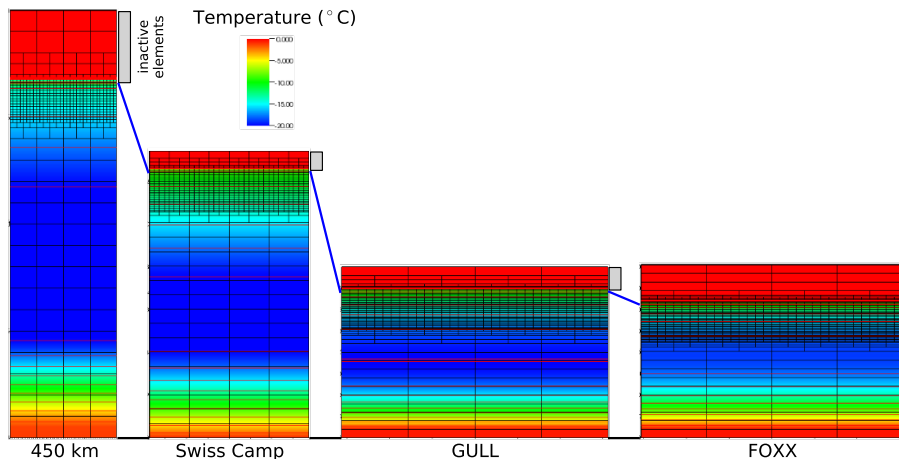


Figure 4. The gradual deformation of the computing mesh along the flow line to accommodate for the varying ice thickness. The ice surface is marked with blue lines between meshes, and inactive elements are indicated with gray bars (red elements on top). The precise position of the surface with respect to the mesh is tracked with adaptive mesh refinement. Modeled ice temperatures are indicated with colors. The greenish elements close to the surface are accumulated during flow (thickest at Swiss Camp at the equilibrium line) and slowly removed from the top due to ablation (sites GULL and FOXX). Note that computational mesh shown is for illustration only, actual model runs were performed on considerably finer meshes.

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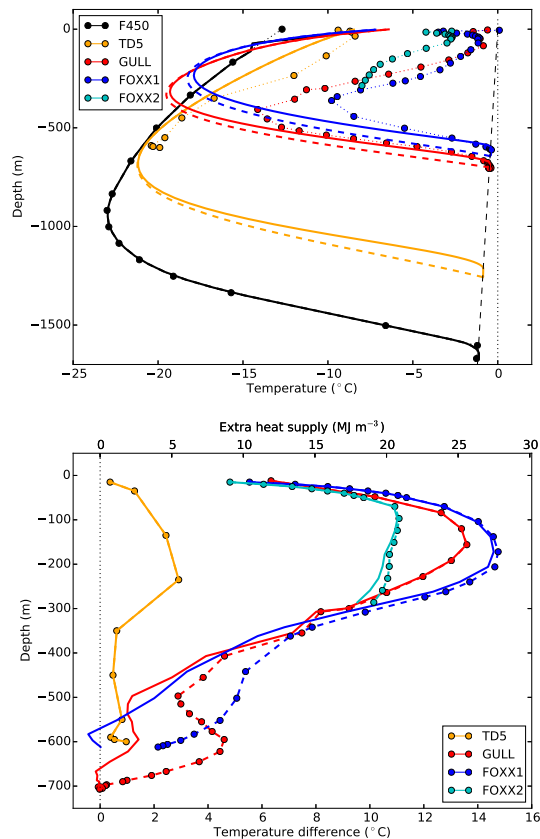


Figure 5. Measured and modeled temperatures at the three sites Swiss Camp (TD5), GULL and FOXX. Dots connected dotted lines indicate measurements. Dashed lines refer to the reference model run mD (dissipation only). Solid lines refer to run mE (additional heat sources from enhanced shear straining in ice-age ice). The scale on top of the lower panel shows the heat per volume with respect to model run mD (dissipation only).

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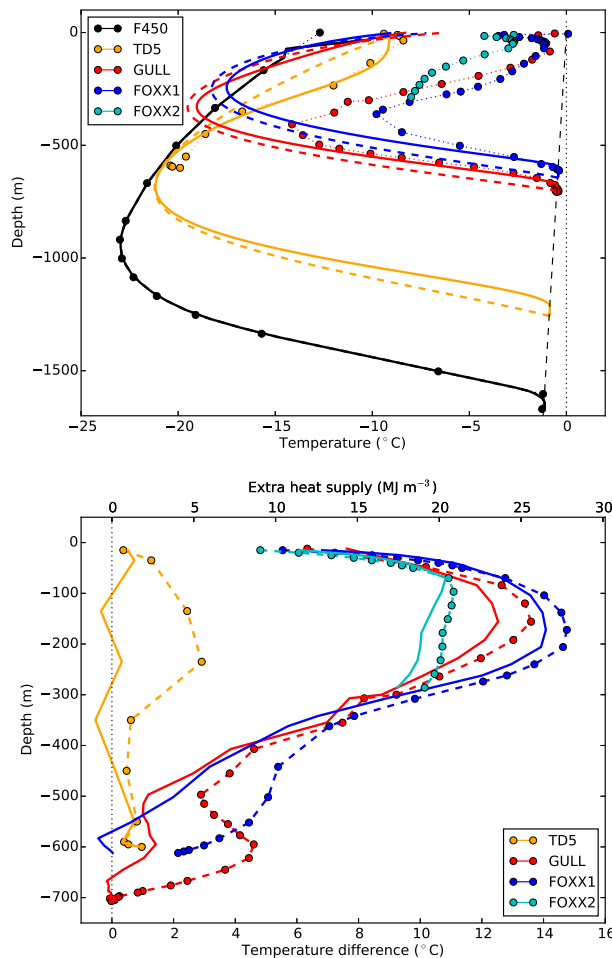


Figure 6. Same as Fig. 5 but for model run mEF (temperate paleo-firn).

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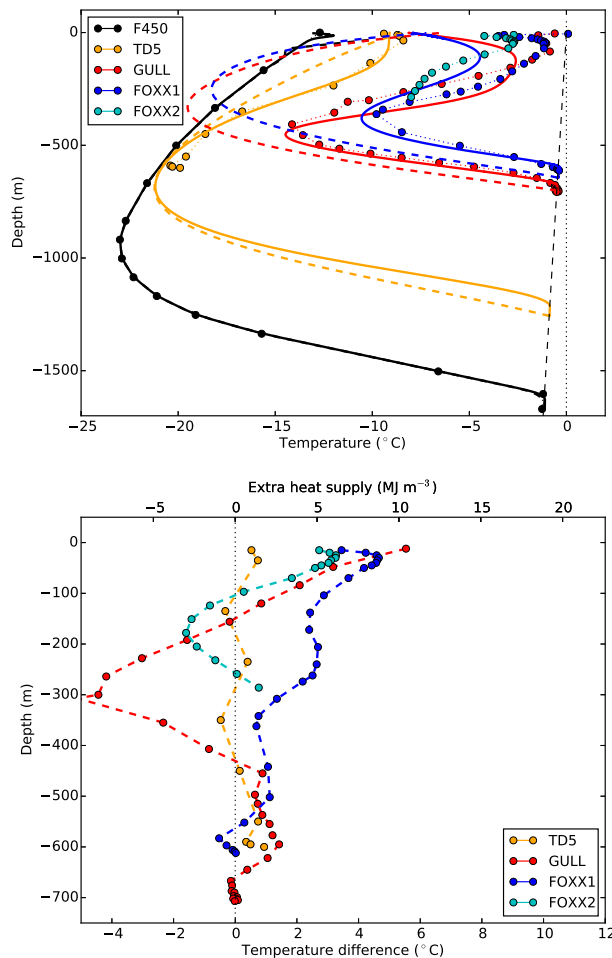


Figure 7. Same as Fig. 5 but for model run mCEF.

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