

Large ensemble  
Antarctic  
deglaciation model

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# A glacial systems model configured for large ensemble analysis of Antarctic deglaciation

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## Abstract

This article describes the Memorial University of Newfoundland/Penn State University (MUN/PSU) glacial systems model (GSM) that has been developed specifically for large-ensemble data-constrained analysis of past Antarctic Ice Sheet evolution. Our approach emphasizes the introduction of a large set of model parameters to explicitly account for the uncertainties inherent in the modelling of such a complex system.

At the core of the GSM is a 3-D thermo-mechanically coupled ice sheet model that solves both the shallow ice and shallow shelf approximations. This enables the different stress regimes of ice sheet, ice shelves, and ice streams to be represented. The grounding line is modelled through an analytical sub-grid flux parametrization. To this dynamical core the following have been added: a heavily parametrized basal drag component; a visco-elastic isostatic adjustment solver; a diverse set of climate forcings (to remove any reliance on any single method); tidewater and ice shelf calving functionality; and a new physically-motivated empirically-derived sub-shelf melt (SSM) component. To assess the accuracy of the latter, we compare predicted SSM values against a compilation of published observations. Within parametric and observational uncertainties, computed SSM for the present day ice sheet is in accord with observations for all but the Filchner ice shelf.

The GSM has 31 ensemble parameters that are varied to account (in part) for the uncertainty in the ice-physics, the climate forcing, and the ice-ocean interaction. We document the parameters and parametric sensitivity of the model to motivate the choice of ensemble parameters in a quest to approximately bound reality (within the limits of 31 parameters).

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## 1 Introduction

The Antarctic Ice Sheet (AIS) is identified as one of the major sources of uncertainty in predicting global sea level change (Meehl et al., 2007). The range of temporal responses to external forcing (e.g. climate, sea-level change) is diverse: locally it can be on the order of decades if not less, whereas vast areas of the interior respond over  $10^3 \rightarrow 10^4$  yr (Alley and Whillans, 1984; Bamber et al., 2007). Without properly attributing the extent to which the behaviour of the glacial system is an artifact of past climate versus an ongoing response to the present climate, the scientific community will struggle to accurately predict how the AIS will respond to future climatic change and what the contribution to eustatic sea level might be (Huybrechts, 2004; Bentley, 2010). Such attribution faces inherent limitations in models and available observational data. As such, there is an urgent requirement for quantitatively evaluated reconstructions with associated uncertainty estimates.

Ice sheet models, like other numerical models, suffer limitations from simplified or missing physics (e.g. reduced equations due to computational restrictions or poorly understood processes that have no physical law), boundary condition uncertainties, and inherent numerical modelling approximations. Parametrizations offer a way to address these issues (even the simplest models may hide many implicit parameters). Many parameters employed in the model have a range of possible values that can produce plausible output. Exploration of these parameter ranges can be performed to generate an ensemble of results, as such we term them ensemble parameters. The interaction of ensemble parameters, considered together, creates a phase-space of possible reconstructions. More complex models invariably have more parametrizations and a larger phase space.

With a handful of ensemble parameters, the traditional method of hand-tuning models with a small number of runs ( $\mathcal{O}(10)$ ) is restrictive and limits exploration of the parameter space. Depending on the non-linearity of the system and the number of parameters, even the generation of relatively large ensembles ( $\mathcal{O}(10^3-10^4)$ ) is likely far from

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adequate. As well, with such large numbers of model runs, an objective and systematic means to quantify run quality is critical.

The plausibility of each model run can be assessed by comparisons against observations. Thus, each run can be evaluated in relation to its misfit to the observational data, and a “misfit score” can be attributed allowing runs to be ranked. Runs can then be combined (for example as weighted averages, using the scores as weights) to produce composite deglaciation chronologies. In addition, by capturing the observational, parametric, and structural uncertainties and propagating them into the evaluation process, the cumulative uncertainties can be computed and presented along with the reconstructions (Briggs and Tarasov, 2013). This developing approach has already been applied to other major Quaternary ice sheets (Tarasov and Peltier, 2003, 2004; Tarasov et al., 2012).

This model description and sensitivity assessment paper is the first in a suite of three articles documenting the steps undertaken to produce a data-constrained deglaciation chronology, with associated uncertainties, for the AIS using a large ensemble analysis approach (2000–3000 runs per ensemble). The second article presents a database of observational data and describes a method that can be employed to quantitatively evaluate model output using the constraint data (Briggs and Tarasov, 2013). The generation of the ensemble and subsequent analysis of the generated chronologies is described in Briggs et al. (2013).

The MUN/PSU model has been developed specifically for ensemble analysis of AIS deglaciation. The dynamical core of MUN/PSU is based on the Penn State University ice sheet model (Pollard and DeConto, 2007; Pollard and DeConto, 2009a; Pollard and DeConto, 2012b). In this paper we document how MUN/PSU differs from the PSU model and describe 31 ensemble parameters used to explore a set of uncertainties in the GSM. We also assess model sensitivity to parameter variations.

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## 2 Model description and spin up

The ice dynamical core of the MUN/PSU is the PSU ice sheet model (Pollard and DeConto, 2012b, and references therein). The original PSU model was developed for continental scale applications over long (up to  $\mathcal{O}(10^6)$  yr) periods. It has been used in many studies for the AIS and other ice sheets (see Pollard and DeConto, 2012b, for a complete list) over a range of spatial and temporal scales and has been a part of the ISMIP-HEINO, ISMIP-HOM, and MISMIP intercomparison tests (Calov et al., 2010; Pattyn et al., 2008, 2012).

The key features of the MUN/PSU GSM are (items marked with an asterisk deviate significantly from the PSU model):

- treatment of both shallow ice and shallow shelf/stream regimes, including a parametrization based on Schoof (2007b) boundary layer theory
- a standard coupled thermodynamic solver including horizontal advection, vertical diffusion and heat generated from deformation work
- \* parametrized basal drag coefficient that accounts for sub-grid topographic roughness, sediment likelihood (based on some specific assumptions), and systematic model-to-observation ice thickness misfit
- \* visco-elastic isostatic adjustment (bedrock response to surface loading) component
- \* parametrized climate forcing that generates three separate temperature and precipitation fields concurrently, these are subsequently merged, through further ensemble parameters, to produce a final “blended” set of climate fields (developed to avoid dependence on a single climate forcing parametrization)
- \* parametrizations for the separate treatment of tidewater and ice shelf front calving

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– \* a new physically-motivated empirical approach to sub-shelf melt (SSM)

The 31 ensemble parameters in the GSM are summarized in Table 1. They are listed in the order they are discussed in the text and organized in accordance with the model functionality they effect: ice dynamics (10 parameters), climate forcing (12 parameters) and ice-ocean mass loss through calving and sub-shelf melt (9 parameters). The evolution of the parameter range and justifications for choosing/excluding parameters are discussed in greater detail in Sect. 3. The ranges presented in Table 1 contains three values, the upper bound, the value of the parameter from the baseline run, and the lower bound. The baseline run is used and discussed fully in the sensitivity assessment (Sect. 3). The baseline run has one of the smallest misfit-to-observation scores of runs to date as identified through the application of the constraint data and the evaluation scheme (Briggs and Tarasov, 2013). Table 2 provides a full list of all the variables and non-ensemble parameters discussed in the text.

## 2.1 Model setup

We adopt the same discretization methodology as the PSU (Pollard and DeConto, 2009b, 2012b). In summary, the MUN/PSU operates at a resolution of 40 km in the horizontal direction and uses a finite-difference Arakawa-C grid. In the vertical the grid has 10 uneven layers, spaced closer at the surface and base of the ice. The horizontal velocities  $u, v$  are located between the grid points (i.e. staggered half a grid cell) whereas the ice geometry (e.g. ice thickness  $H$ , surface elevation  $h_s$ ), vertical velocities, and temperatures are located at the grid centres.

The standard model run is from 205 ka to present day (the initialization conditions are described in Sect. 2.11). The model has adaptive time stepping functionality that, if numerical instabilities occur, enables the GSM to backtrack to a previous state (the state is recorded by a rolling buffer) and re-attempt the calculations with reduced time steps (50% reduction upon each back-track). After 300 yr under reduced time-step conditions, the time-step is doubled. On initialization the ice dynamics are set to be

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computed every 0.5 yr, thermodynamics every 10 yr, and isostatic adjustment every 100 yr.

## 2.2 Ice dynamics

Grounded and floating ice have the same fundamental rheology, but the large scale (simplified) equations that describe them are different. Three regimes classify the type of ice flow: sheet flow, stream flow and shelf flow. Sheet flow, under the zero-order shallow-ice approximation (SIA), is valid for an ice mass with a small aspect ratio (height scale  $\ll$  length scale) and where the flow is dominated by vertical shear stress, i.e. much of the interior of the AIS. It is the simplest type of flow. The driving stress is in balance with basal traction (the retaining force due to friction at the interface between an ice sheet and the underlying bed). The flow is dominated by vertical shear ( $\partial u / \partial z$ , where  $u$  is velocity and  $z$  is the vertical co-ordinate within the ice thickness) determined locally by the driving stress. The driving stress is a function of the surface gradient and the thickness; steeper slopes and/or thicker ice beget larger driving stresses. In shallow shelf flow (SSA), the driving stress is balanced by longitudinal and transverse (horizontal) shear stress gradients. Stream flow is similar to shelf flow, except for the presence of basal drag, and the basal topographic boundary condition (MacAyeal, 1997).

The PSU model offers three approaches to modelling these two different regimes. Computationally, the most costly implements a combined set of SIA-SSA equations over the whole ice sheet. The internal shear and longitudinal stretching is combined, through strain-softening terms that are velocity dependent, into one set, which is applied at all locations. As a consequence, the viscosity is a function of the velocity gradients. Thus the set of equations is nonlinear in the velocity terms, as well as dependent on the state of the ice (e.g. ice thickness, temperatures, etc.). To address the nonlinearity, an iterative approach is taken, whereby the viscosity term is computed based on the previously calculated velocity. The new viscosity term is then used to update the velocities. This is repeated until the difference between the velocities is less than a predetermined convergence criterion (Pollard and DeConto, 2007, 2012b). Significant savings

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in CPU time, with virtually no impact on the results can be earned by limiting the combined SIA-SSA equations to cells where SSA flow is predisposed to dominate due to low basal drag; above a critical threshold (satisfied in the majority of the East Antarctic Ice Sheet (EAIS)) the flow is limited to SIA (Pollard and DeConto, 2009b). Further reductions in computing resource can be achieved by removing the SIA strain softening terms from the SSA equations. This has a slight impact on the results (Pollard and DeConto, 2012b). Because the large ensemble approach is computationally costly (each ensemble contains 2000–3000 runs, each run can take 2–5 days), the latter method is employed for this study.

## 2.3 Ice rheology factor

The sheet and shelf flow ensemble parameters,  $f_{\text{inflow}}$  and  $f_{\text{nshef}}$ , adjust the ice rheology (Pollard and DeConto, 2012b, Eqs. 16a and 16b). They are motivated as providing softening due the unresolved grain-scale characteristics (e.g. ice crystal size, orientation, impurities) of the ice (Cuffey and Paterson, 2010, p. 71). Enhancement values are between 3.5–5.5 for sheet flow and 0.4–0.65 for shelf flow. This approximately follows the bounds defined in Ma et al. (2010). Physically they manifest themselves as a control on the height-to-width ratio of the ice sheet (Huybrechts, 1991).

## 2.4 Basal drag

Though a consensus is developing towards the validity of Coulomb plastic basal drag from subglacial sediment deformation (Cuffey and Paterson, 2010), the Schoof grounding line flux condition (Schoof, 2007a) is only defined for power law forms. We therefore retain the basal drag parametrization of Pollard and DeConto (2007, 2012b),

$$u_b = \text{crh} \cdot \tau_b^2 \quad (1)$$

where  $u_b$  is the basal sliding velocity,  $\text{crh}$  is the basal sliding coefficient, and  $\tau_b$  is the basal stress.

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To capture the large uncertainty in subglacial basal stress regimes, we have introduced a number of ensemble parameters that are used to determine the basal sliding coefficient.

Firstly, following Pollard and DeConto (2012b), we define two baseline basal drag values for different bed characteristics:  $10^{-10} \text{ myr}^{-1} \text{ Pa}^{-2}$  for hard bed (zcrhslid; bare rock, predominantly under the EAIS) and  $10^{-6} \text{ myr}^{-1} \text{ Pa}^{-2}$  for soft bed (zcrhsed; sediment coverage, predominantly under the West Antarctic Ice Sheet (WAIS)). These values are adjusted by respective ensemble parameters fnslid (giving a range of  $10^{-11}$ – $1.08 \times 10^{-9}$ ) and fnsed ( $10^{-8}$ – $3 \times 10^{-6}$ )

The parametrization has three key dependencies. First, as per Pollard and DeConto (2012b), we assume that the distribution of subglacial sediment is largely related to the surface elevation of the unloaded subglacial topography. Areas that are still submerged after glacial unloading are likely to have soft sedimentary surface lithology, and therefore are a precursor for subglacial sediment. With some allowance for uncertainty in the resultant unloaded ice (dependent on ground surface elevations, thus uncertainty in ALBMAP, earth rheology etc.) under the control of a parameter fhbPhif (0.001–1), we define a sediment likelihood parameter

$$Slk = \frac{\text{unloaded water depth in km} - \text{fhbPhif}}{\text{fhbPhif}} \quad (2)$$

and use this to set a sediment presence exponent,  $Se$ , that controls the transition from zcrhslid to zcrhsed (bare rock to sediment):

$$Se = \begin{cases} 1, & \text{if } Slk > 0 & \text{thick sediment cover} \\ 1 + Slk, & \text{if } -1 < Slk < 0 & \text{some sediment} \\ 0, & \text{if } Slk < -1 & \text{no sediment} \end{cases} \quad (3)$$

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The second dependence is on sub-grid roughness, given by the standard deviation of the 5 km resolution ALBMAP (LeBrocq et al., 2010)<sup>1</sup> basal topography for each GSM grid cell ( $\sigma_{hb}$ , in dekametres). We assume an increasing degree of basal drag for combinations of sediment thickness and surface roughness. Any site with sediment cover will have much reduced basal drag compared to sites without sediment cover. For regions with thick sediment cover, as described by Se, we assume that higher roughness will lead to increased basal drag. For minimal or no sediment cover, we assume that enhanced surface roughness increases the surface area available to erosion, promoting trapping of eroded sediments, leading to reduced basal drag.

The final dependence takes into account the ice thickness difference,  $\Delta H_{alb}$  between the present-day field from an early test run and ALBMAP thickness  $H_{ALB}$ . Thus we address some observation-model misfit in the adjustment of crh. This is a similar, albeit much simpler, approach to the inverse method employed by Pollard and DeConto (2012a) to adjust the values of crh to reduce model misfit. The  $\Delta H_{alb}$  is scaled by parameter fDragmod (range 0–9.99).

The basal sliding coefficient crh is set as:

$$crh = \max \left[ \min \left[ zcrhslid \left( \frac{zcrhsed}{zcrhslid} \right)^{Se} \cdot fstd \cdot fDragmod^{(0.8 \cdot \Delta H_{alb})}, zcrhMX \right], zcrhMN \right] \quad (4)$$

<sup>1</sup>The ALBMAP dataset is provided at a resolution of 5 km. To be used in the GSM it must be upscaled to the model resolution of 40 km; the steps taken to upscale the dataset, whilst preserving grounding-line positions and key pinning points, are described in the supporting on-line material (SOM) of Briggs and Tarasov (2013). Unless explicitly stated (as in this case for sub-grid roughness) in the text any references to ALBMAP implicitly refers to the upscaled dataset at 40 km.

where  $f_{std}$ , which introduces the sediment roughness, is given by:

```
if Se > 0.67 then                                ▶ thicker sediment
  if  $\sigma_{hb} \geq 0.75$  then                    ▶ rougher sub-grid topography
     $f_{std} = (0.75/\sigma_{hb})^{powfstdsed}$ 
  else                                             ▶ smoother sub-grid topography
     $f_{std} = (1 + (0.75 - \sigma_{hb})/0.69)^{powfstdsed}$ 
  end if
else if Se < 0.5 then                              ▶ thinner sediment
   $f_{std} = \max[1, \sigma_{hb}^{powfstdslid}]$ 
else
   $f_{std} = 1$ 
end if
```

The ensemble parameters  $powfstdsed$  and  $powfstdslid$  both have ranges of 0–1.2. Numerical coefficients were selected from initial sensitivity analyses while maintaining numerical continuity.

Mass fluxes for grounded ice with  $crh > crhcrit = 10^{-8} \text{ myr}^{-1} \text{ Pa}^{-2}$  are determined by the combined SSA and SIA equations, otherwise only SIA is active. The basal sliding coefficient is smoothly increased from an essentially zero ( $10^{-20}$ ) value as the basal temperature approaches the pressure melting point except at the grounding line where a warm base is always imposed.

## 2.5 Grounding line treatment

At the locality of the grounding line and in ice streams with very little basal traction, a combination of both flow regimes exist (Pollard and DeConto, 2007).

The grounding line treatment in the model is based on Schoof (2007a) who showed that to capture the grounding line accurately, either the grounding zone boundary layer must be resolved at a very high resolution ( $\sim 0.1 \text{ km}$ , impractical on a continental scale),

or an analytical constraint on the flux,  $q_g$ , across the grounding line must be applied. The flux is a function of the longitudinal stress across the grounding line, the ice thickness at the grounding line, and the sliding coefficient discussed above (Schoof, 2007a). The longitudinal stress is calculated by the stress balance equation and also takes into account back stress at the grounding line caused by buttressing from pinning points, downstream islands or side-shear at lateral margins.

The analytically calculated ice flux  $q_g$  and height at the grounding line  $H_g$ , found through linear interpolation, are then used ( $u_g = q_g/H_g$ ) to compute the depth-averaged velocity at the grounding line  $u_g$ . The calculated  $u_g$  is imposed as an internal boundary condition for the shelf-flow equations and is used to overwrite the velocity solution calculated for that position from the stress balance equations (Pollard and DeConto, 2007, 2012b).

## 2.6 Sub-shelf pinning points

Pinning points, sometimes manifest in the form of small ice rises, are found below the ice shelves, generally toward the grounding line. Grounding of the ice shelf onto such pinning points causes additional back stresses that influence the migration of the grounding line upstream (Pollard and DeConto, 2012b). These pinning points are too small to be resolved on a 40 km grid so are parametrized to be a percentage of the equivalent basal drag for grounded ice as a function of the water depth (Pollard and DeConto, 2009b). Ensemble parameter  $\text{fnPin}$  (range 0.01–0.1) scales the computed pinning point drag.

## 2.7 Isostatic adjustment and relative sea level computation

The isostatic adjustment component of the GSM is taken from Tarasov and Peltier (2004) but modified to use the VM5a earth rheology of Peltier and Drummond (2008) which still retains a 90 km thick elastic lithosphere. The earth rheology is spherically symmetric and has reasonable fits to geophysical observations from North America

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(Peltier and Drummond, 2008). The bedrock displacement is computed every 100 yr from a space-time convolution of surface load changes and a radial displacement Greens function, at spherical harmonic degree and order 256.

Ice chronologies from a completed model run are then post-processed using an approximation to a gravitationally self-consistent theory (Peltier, 1998) to generate RSL chronologies. As detailed in Tarasov and Peltier (2004), the approximation invokes eustatic load changes during changes in marine extent (otherwise gravitational effects are accounted for). Rotational components of RSL are not taken into account. The generated RSL curves are then assessed with the RSL constraint data in accordance to the evaluation methodology of Briggs and Tarasov (2013).

This study considers the glaciological and climatic uncertainties in the GSM but assessment of the contribution from rheological uncertainties is a future project. For a preliminary examination of the impact of Earth model uncertainty on inferred Antarctica deglacial history see Whitehouse et al. (2012). Variations in the earth rheology will have some impact on ice evolution, but that will get swamped by the other uncertainties, e.g. the climate forcing.

## 2.8 Geothermal heat flux

There are very few direct measurements of GHF for the AIS. Those that do exist are usually derived from direct temperature measurements in ice cores (Pattyn, 2010), as such, continental scale GHF reconstructions must be derived from proxies. This study employs two GHF datasets which are blended through ensemble parameter fbedGHF. The Shapiro and Ritzwoller (2004) dataset uses a global seismic model of the crust and upper mantle to extrapolate available measurements to regions where they are non-existent or sparse. The Maule et al. (2005) dataset was estimated from satellite measured magnetic data. The datasets are corrected, around a Gaussian area of influence, so that the reconstructions match the observations where available (Pattyn, 2010). The observations are taken from ice-core temperature profiles and based on the location of sub-glacial lakes (the ice/bedrock interface can then be considered to

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be at the pressure melting point, thus the minimum GHF can be computed; Pattyn, 2010).

## 2.9 Climate forcing

Climate forcing over glacial cycles is one of the most difficult components in the GSM to constrain (Tarasov and Peltier, 2004); in the GSM, 12 of the 31 ensemble parameters adjust the climate forcing. The GSM requires both temperature and precipitation fields. For large ensemble analysis, coupled climate–glacial systems model are computationally too expensive, as such the GSM uses a parametrized climate forcing. Three different parametrizations, each of which has one or more ensemble parameters, are used to concurrently generate the temperature ( $T_{f_{1,2,3}}$ ) and precipitation ( $P_{f_{1,2,3}}$ ) fields.

The spatial distribution of the fields are obtained either through empirical parametrizations, from published observational datasets (e.g. Arthern et al., 2006), or, for  $T_{f_3}$  from the Paleo-Modelling Intercomparison Project II (PMIP2, Braconnot et al., 2007) modelling study.

The fields are then projected backwards in time using an ice- or deep sea-core time series (Ritz et al., 2001; Huybrechts, 2002; Tarasov and Peltier, 2006; Pollard and DeConto, 2009a). Finally, the different fields are combined together using a weighed sum, the weight determined by ensemble parameters, to generate the final climate fields that force the GSM.

This approach ensures there is no reliance on a single climate methodology and that each method has one or more ensemble parameter. This affords the model a larger degree of freedom (with respect to climate forcing) than the single climate forcing methodology with limited parametrization employed in other studies (e.g. Pollard and DeConto, 2012b; Whitehouse et al., 2012).

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## 2.9.1 Temperature forcing

Tf<sub>1</sub> models the spatial variation of the temperature field as a function of latitude, height, and lapse rate (Huybrechts, 1993; Pollard and DeConto, 2009a). Using the annual orbital insolation anomaly ( $\Delta q_s$ ) at 80° S ( $\text{W m}^{-2}$ ) and sea level departure from present ( $\Delta s$ ), the modern day temperature field is adjusted to generate a paleo-temperature field. Annual orbital insolation is calculated from Laskar et al. (2004) and, following Tarasov and Peltier (2004), it is weighted by ensemble parameter fnTdfscale (range 0.75–1.3) to account for the uncertainty inherent in using this method to drive the transition between a glacial to interglacial state. The sea level departure from present is taken from stacked benthic  $\delta^{18}\text{O}$  records (Lisiecki, 2005). Present day Tf<sub>1</sub> is shown in Fig. 1a of the Supplement. This field is computed in degrees Celsius as

$$\text{Tf}_1(\mathbf{X}, t) = 30.7 - 0.0081 \text{hs}(\mathbf{X}, t) - 0.6878|\Phi|(\mathbf{X}) + \text{fnTdfscale} \Delta q_s(t) + \frac{10\Delta s(t)}{125}, \quad (5)$$

where hs is modelled surface height (m), and  $\Phi$  is latitude (°). To avoid overly low temperatures over the ice shelves, we follow Martin et al. (2010) and remove the dependence on surface elevation when it is below 100 m,

$$\text{Tf}_1(\mathbf{X}, t) = 29.89 - 0.6878|\Phi| + \text{fnTdfscale} \Delta q_s(t) + \frac{10\Delta s(t)}{125} \text{ when } \text{hs}(\mathbf{X}, t) < 100\text{m}. \quad (6)$$

The second temperature forcing field, Tf<sub>2</sub> (supplemental Fig. 1b), uses the Comiso (2000) present-day surface air temperature map (available as part of ALBMAP) for AIS ( $T_{\text{PD}}$ ) adjusted using the insolation anomaly  $\Delta q_s$ .  $T_{\text{PD}}$  is corrected from the present-day topography ( $\text{hs}_{\text{PD}}$ ), via an ensemble parameter lapse rate (rLapseR), to the modelled surface-elevation (hs). The lapse rate range is 5–11 °C km<sup>-1</sup> (compared with, for example 9.14 °C km<sup>-1</sup> Ritz et al., 2001; Pollard and DeConto, 2009a and 8.0 °C km<sup>-1</sup> Pollard and DeConto, 2012b). Then,

$$\text{Tf}_2(\mathbf{X}, t) = T_{\text{PD}}(\mathbf{X}) + \text{fnTdfscale} \cdot \Delta q_s + \text{rLapseR} [\text{hs}(\mathbf{X}, t) - \text{hs}_{\text{PD}}(\mathbf{X})] \quad (7)$$

where  $\Delta q_s$  and  $h_s$  are as for  $Tf_1$ .

Following Tarasov and Peltier (2004),  $Tf_3$  is calculated by interpolating between PD surface temperature (Comiso, 2000) and a Last Glacial Maximum (LGM) air surface temperature field generated from an amalgam of the results of five high resolution PMIPII (Braconnot et al., 2007) 21 ka simulations (CCSM, HadCM3M2, IPSL-CM4-V1-MR, MIROC3.2 and ECHAM53). The 5 datasets are averaged together ( $Tave_{LGM}$ ) and we also use the first empirical orthogonal basis function (EOF) of inter-model variance for the LGM snapshots<sup>1</sup>. The first EOF ( $Teof_{LGM}$ ) captures 64% of the total variance and is incorporated through ensemble parameter  $fTeof$  (range  $-0.5$ – $0.5$ ) into a run specific reference dataset  $T_{LGM}$  when the model is initialized,

$$T_{LGM}(\mathbf{X}) = Tave_{LGM}(\mathbf{X}) + fTeof \cdot Teof_{LGM}(\mathbf{X}). \quad (8)$$

The computed  $Tave_{LGM}$  and the associated  $Teof_{LGM}$  are shown in supplemental Fig. 2. As with  $Tf_2$ , the present-day and LGM temperature fields are adjusted, through the parametrized lapse rate, to account for the difference between the modelled surface elevation,  $h_s$ , and the reference surface elevation fields  $h_{sPD}$  and  $h_{sLGM}$  (the PMIPII files are supplied with an associated LGM orthography). The interpolation between the Comiso (2000) present-day temperature field and the model derived LGM temperature is weighted using a glacial index,  $I$ , derived from the EPICA temperature record  $T_{epica}$  (Jouzel and Masson-Delmotte, 2007),

$$I(t) = \frac{T_{epica}(t) - T_{epica}(0)}{T_{epica}(LGM) - T_{epica}(0)}, \quad (9)$$

<sup>1</sup>This is a numerical technique to decompose in this case the maps of LGM temperature from the set of PMIP GCM runs into a series of orthogonal spatial maps, ordered with respect to minimizing the residual variance of the subsequent maps in the series. Thus the first EOF captures in some sense the maximum mode of inter-model differences.

and adjusted using ensemble parameter  $fnTdfscale$  giving

$$Tf_3(\mathbf{X}, t) = [(T_{PD}(\mathbf{X}) + rLapseR \cdot (hs(\mathbf{X}, t) - hs_{PD}(\mathbf{X}))) \cdot (1 - (fnTdfscale \cdot I(t))) + [(T_{LGM}(\mathbf{X}) + rLapseR \cdot (hs(\mathbf{X}, t) - hs_{LGM}(\mathbf{X}))) \cdot (fnTdfscale \cdot I(t))]. \quad (10)$$

5 The three temperature fields are then combined in accordance with two ensemble parameters,  $Twa$  and  $Twb$  (both range 0–1), to produce the final temperature field,

$$T(\mathbf{X}, t) = (1 - Twb) \cdot [Twa \cdot Tf_1(\mathbf{X}, t) + (1 - Twa) \cdot Tf_2(\mathbf{X}, t)] + Twb \cdot Tf_3(\mathbf{X}, t). \quad (11)$$

### 2.9.2 Precipitation forcing

10 The precipitation forcing is also subject to a weighted amalgam of three different forcings.  $Pf_1$  assumes precipitation is driven by temperature (Huybrechts, 1993),

$$Pf_1(\mathbf{X}, t) = 1.5 \times 2^{\frac{T(\mathbf{X}, t) - T_m}{10}}. \quad (12)$$

where  $T$  is the blended temperature (Pollard and DeConto, 2009a). The precipitation temperature dependence is motivated by the exponential behaviour of the saturation vapour pressure on temperature. Present day  $Pf_1$  is show in supplemental Fig. 1c.

15  $Pf_2$  is computed in a similar manner to  $Tf_2$ ; at run-time, an observational dataset,  $P_{PD}$  (shown in supplemental Fig. 1d), of present-day precipitation (Arthern et al., 2006) is adjusted using the annual orbital insolation anomaly. Ensemble phase factor,  $fnPdexp$ , (range 0.5–2) accounts for some phase uncertainty in using the insolation anomaly (Tarasov and Peltier, 2004),

$$20 Pf_2(\mathbf{X}, t) = P_{PD}(\mathbf{X}) \times 2^{fnPdexp \frac{\Delta q_3(t)}{10}}. \quad (13)$$

In a similar manner to  $Tf_3$ ,  $Pf_3$  is computed using  $I(t)$  to interpolate between the present-day dataset  $P_{PD}$  and an LGM precipitation field, generated from an amalgam of the PMIP II LGM precipitation simulations,  $Pave_{LGM}$ . Two EOFs are used. The first

(Peof1) captures 62 % of the inter-model variance, the second (Peof2) captures 23 %. The computed  $P_{\text{ave,LGM}}$  and the associated EOF's are plotted in supplemental Fig. 3. As with  $Tf_3$  the EOFs are introduced at model initialization through parameters  $f_{\text{Peof1}}$  and  $f_{\text{Peof2}}$  (range  $-0.5$ – $0.5$ ) to create a run specific reference dataset,

$$P_{\text{LGM}}(\mathbf{X}) = P_{\text{ave,LGM}}(\mathbf{X}) + f_{\text{Peof1}} \cdot \text{Peof1}_{\text{LGM}}(\mathbf{X}) + f_{\text{Peof2}} \cdot \text{Peof2}_{\text{LGM}}(\mathbf{X}). \quad (14)$$

This is scaled and adjusted using ensemble parameter  $fn_{\text{Pre}}$  (range  $0.5$ – $2$ ),

$$P_{f_3}(\mathbf{X}, t) = P_{\text{PD}}(\mathbf{X}) \left( fn_{\text{Pre}} \frac{P_{\text{LGM}}(\mathbf{X})}{P_{\text{PD}}(\mathbf{X})} \right)^{P_{\text{fac}}}, \quad (15)$$

where  $P_{\text{fac}}$  is the glacial index scaled by ensemble parameter  $fn_{\text{Pdexp}}$  (range  $0.5$ – $2$ ),

$$P_{\text{fac}} = \text{sign}[1.0, I(t)] / |I(t)|^{fn_{\text{Pdexp}}}. \quad (16)$$

The final precipitation field is then summed and interpolated using two ensemble parameters  $P_{\text{wa}}$  and  $P_{\text{wb}}$ ,

$$P(\mathbf{X}, t) = q_{\text{des}} \cdot ((1 - P_{\text{wb}}) \cdot [P_{\text{wa}} \cdot P_{f_1}(\mathbf{X}, t) + (1 - P_{\text{wa}}) \cdot P_{f_2}(\mathbf{X}, t)] + P_{\text{wb}} \cdot P_{f_3}(\mathbf{X}, t)), \quad (17)$$

where  $q_{\text{des}}$  accounts for the elevation-desert effect (reduced amount of moisture the atmosphere can hold at elevation) (Marshall et al., 2002; Tarasov and Peltier, 2004). It is simulated as a function of the modelled elevation anomaly from present-day,

$$q_{\text{des}} = \exp^{-f_{\text{desfak}} \cdot (h_{\text{s}}(\mathbf{X}, t) - h_{\text{sPD}}(\mathbf{X}))}, \quad (18)$$

and ensemble parameter  $f_{\text{desfak}}$  ( $0$ – $2 \times 10^{-3}$ ).

The final “blended” temperature and precipitation fields are used to determine the fraction of precipitation that falls as snow and the annual surface melt. Given the small amount of surface melt over the AIS (Zwally and Fiegles, 1994), a simplified positive-degree-day method (PDD) is used with a melt factor of  $5 \text{ mm/PDD}$ .

## 2.10 Ice-ocean interface

The vast majority of mass loss from the AIS occurs from the ice shelves, either due to calving at the ice margin, or from submarine melting beneath the ice shelf (Jacobs et al., 1992). The ice shelves play a crucial role in restricting (buttressing) the upstream flow of ice (Dupont and Alley, 2005). Reduction or removal of the shelves allows the upstream grounded ice to accelerate, drawing down the ice in the interior. Thus, changes at the ice-ocean interface can have an impact hundreds of kilometres inland (Payne et al., 2004).

Iceberg calving has been inferred to be the largest contributor to mass loss. Jacobs et al. (1992) apportioned a loss of  $2016 \text{ Gtyr}^{-1}$  to calving against  $544 \text{ Gtyr}^{-1}$  to sub-shelf melt (the uncertainty estimates for these number are large,  $\pm 33\%$  for iceberg calving and  $\pm 50\%$  for ice shelf). However, there is growing concern and evidence that the sub-shelf melt rate is a primary control on the mass loss (Pritchard et al., 2012). Both processes are modelled in the GSM.

### 2.10.1 Calving

Marine ice margins can either terminate as a floating ice shelf or as a tidewater glacier. The GSM uses two distinct parametrizations to calculate mass loss from either of these regimes, in addition there is an ad-hoc treatment for thin ice.

#### Ice shelf calving

Though there have been significant efforts towards a fully constrained physically-based calving model for ice shelves (e.g. Alley et al., 2008; Albrecht et al., 2010; Amundson and Truffer, 2010), we have found none to be stable for the relatively coarse grid of the GSM. For the present configuration, ice shelf calving is based on a steady state approximation of Amundson and Truffer (2010, Eq. 25) which corresponds to the insertion of the Sanderson (1979) relationship for ice shelf half-width into the empirical

relation of Alley et al. (2008). Due to the coarse grid, it was necessary to upstream, by an extra grid cell from the terminus, the stress and ice thickness gradients used in the parametrization. The calving is computed along each exposed face of the marginal grid-cell. The calving velocity (in the x-direction) is computed as,

$$U_c = -3H_0 \dot{\epsilon}_{xx} \left( \frac{\partial h}{\partial x} \right)^{-1} \quad (19)$$

where  $H_0$  is the terminus thickness and  $\dot{\epsilon}_{xx}$  is the along flow spreading rate. The calving rate (ice loss per grid cell area), adjusted by ensemble parameter  $f_{\text{shcalv}}$  (0.5–2.5), is computed as (x-direction),

$$\dot{C} = f_{\text{shcalv}} \cdot U_c \cdot \frac{H}{\Delta x}. \quad (20)$$

Once calculated  $\dot{C}$  is used in the mass balance equation (Pollard and DeConto, 2012b, Eq. 14).

For ice thinner than 300 m the calving rate computed above is enhanced. Given the present-day correspondence between average shelf front and the mean annual  $-5^\circ\text{C}$  isotherm (Mercer, 1978), for ice thinner than 300 m and thicker than ensemble parameter  $H_{\text{crit2}}$  (10–150 m), we impose a simple temperature dependent ( $T_s$ , sea-surface mean summer temperature in  $^\circ\text{C}$ ) parametrization. For ice thinner than  $H_{\text{crit2}}$ , calving is enhanced by a term  $\text{calvF} \cdot H$ , where ensemble parameter  $\text{calvF}$  ranges from 0–0.2  $\text{yr}^{-1}$ . Thus, the ice shelf calving rate is,

$$\dot{C}_{\text{IS}} = \begin{cases} \dot{C} & \text{if } H > 300 \\ \dot{C} + (T_s + 3^\circ) \frac{H}{5^\circ} \cdot 1 \text{ yr}^{-1} & \text{if } H_{\text{crit2}} < H < 300 \text{ and } T_s > -3^\circ \\ \dot{C} + \text{calvF} \cdot H & \text{if } H < H_{\text{crit2}} \end{cases} \quad (21)$$

## 20 Tidewater calving

For grounded marine ice margins (i.e. large scale tidewater glaciers), we use a slight variant of the temperature-dependent proximity to flotation model of Tarasov and Peltier

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(2004). Three conditions are imposed for such calving: (1) an adjacent ice-free grid-cell with water depth greater than 20 m, (2)  $T_s$  above a critical minimum value  $T_{Cmn}$  and (3) ice thickness less than 1.15 times the maximum buoyant thickness,  $H_{flot}$ . When the above conditions are met, the calving velocity is given by:

$$U_c = fcalvVmx \cdot n_{edge} \cdot \min \left[ 1, \left( \frac{1.15H_{flot} - H}{0.35H_{flot}} \right)^2 \right] \times \left( \exp \left( \frac{3 \cdot (T_s - T_{Cmx})}{T_{Cmx} - T_{Cmn}} \right) - \exp(-3) \right) / (1 - \exp(-3))^{0.5}. \quad (22)$$

Calving velocity is proportional to the number of grid-cell edges ( $n_{edge}$ ) meeting the first calving condition above and uses the maximum calving velocity,  $fcalvVmx$ , as the single ensemble parameter (range 0.1–10  $\text{km yr}^{-1}$ ). Based on best fits from previous ensembles and sensitivity analyses,  $T_{Cmn}$  is set to  $-5^\circ\text{C}$  and  $T_{Cmx}$  to  $2^\circ\text{C}$ . We also invoke an ad hoc extrapolation of ice thickness at the margin for conversion of calving velocity to a mass-balance term. The marginal ice thickness for this conversion is computed as a quadratic reduction of the grid-cell thickness for ice thicker than 400 m with a maximum effective marginal ice thickness of 900 m for grid cells with ice thicker than 1400 m.

### Thin ice treatment

The shelf calving modules, and the sub-shelf component described in the next section, were not designed for excessively thin (in this case  $< 10\text{m}$  thick) ice and we found it necessary to add a separate parametrization for this case. Again using the present-day correspondence between average shelf front and the  $-5^\circ\text{C}$  isotherm (Mercer, 1978), we imposed a simple temperature dependent parametrization. For marine ice  $< 10\text{m}$  thick, the calving rate is

$$\dot{C}_r = \max[\text{calving rate from other modules}, 0.3 + zclim(t) \cdot fcalvwater], \quad (23)$$

where  $f_{calvwater}$  is a calibration parameter with a range 3–10  $\text{myr}^{-1}$  and  $z_{clim}$  is the glacial index factor computed, as in  $Tf_{1,2}$ , from the sea level departure from present ( $\Delta s$ ) with some influence from annual orbital insolation ( $\Delta q_s$ ):

$$z_{clim}(t) = \max \left[ 0, \min \left[ 1.5, 1 + \frac{\Delta s(t)}{85} + \max \left[ 0, \frac{\Delta q_s(t)}{4} \right] \right] \right]. \quad (24)$$

## 2.10.2 Sub-shelf melt

Sub-shelf melt (SSM) is a reaction to a complex interaction of oceanographic and glaciological conditions and processes. The newly developed SSM component used in MUN/PSU is a physically-motivated implementation based on empirical observations. As such we provide a brief review of the SSM process to justify the implementation.

Three modes of melt have been identified (Jacobs et al., 1992). Mode 1 melt occurs in the grounding line zone of the larger shelves; driven by thermohaline circulation, it is triggered by the formation of high-salinity continental shelf water (HSSW). As sea ice forms near the shelf edge, brine rejection occurs producing the dense HSSW. The water mass sinks and, upon reaching the continental shelf, drifts underneath the ice shelf (the continental shelves generally slope down toward the grounding line due to isostatic depression and long-term erosion) into the grounding line cavity. Due to the pressure dependence of the freezing point of water, the in situ melting point of the ice shelf base is lower than the temperature of the HSSW (formed at sea-surface temperatures e.g.  $\sim -1.9^\circ\text{C}$ ). The encroaching water mass, acting as a heat delivery mechanism, melts away at the ice shelf base (Jacobs et al., 1992; Rignot and Jacobs, 2002; Joughin and Padman, 2003; Holland et al., 2008). The melting ice freshens (and cools) the surrounding water mass producing buoyant ice shelf water (ISW), which, if not advected away, rises up and shoals along the base of the ice shelf. As the water mass rises the ambient pressure decreases, increasing the in-situ freezing point until refreezing occurs, and new marine ice accretes onto the base of the ice shelf (Jacobs et al., 1992; Joughin and Padman, 2003).

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The three largest shelves, Amery (AMY), Ross (ROS), and Ronne-Filchner (RON-FIL) differ greatly in draught and cavity geometry, and have distinct melt regimes (Horgan et al., 2011). The long narrow AMY is smallest by area but has a relatively deep draught of  $\sim 2200$  m (Fricker et al., 2001). Grounding line melt rates of  $31 \pm 5 \text{ myr}^{-1}$  have been estimated and accreted marine ice with a thickness up to 190 m have been calculated (Rignot et al., 2008; Fricker et al., 2001). The ROS is the largest shelf by area but is much shallower with a draught of about 800 m, the melt rates are greatly reduced as is the marine ice accretion ( $\sim 10$  m, Neal, 1979; Zotikov et al., 1980). The RON and FIL both have deep grounding lines  $\sim 1400$  m and melt rates that can exceed  $5 \text{ myr}^{-1}$  at some locations, the accreted marine ice can exceed  $> 300$  m under RON, but, unlike the AMY it does not persist to the shelf front (Thyssen et al., 1993; Lambrecht et al., 2007).

Mode 2 and mode 3 melting occur both under the smaller shelves that fringe the AIS (e.g. those that face the Amundsen, Weddell, and Bellingshausen Seas) and proximal to the zone near the calving margin of the larger shelves. Mode 2 melting is associated with the intrusion of “warm” circumpolar deep water (CDW) at intermediate depths (Jacobs et al., 1992, 1996; Joughin and Padman, 2003). The degree of melt is dependent on the amount of heat that can be delivered into the ice cavity, itself a function of oceanographic conditions and the proximity of the ice base to the continental shelf edge. The highest melt rates occur at the grounding lines of the Pine Island ( $40 \text{ myr}^{-1}$ ) and Thwaites ( $30 \text{ myr}^{-1}$ ) glaciers that discharge into the Amundsen Sea. The grounding lines, at a depth of about 1000 m, are melted by the intrusion of CDW water that is almost  $4^\circ\text{C}$  above the in-situ melting point (Rignot and Jacobs, 2002). Mode 3 melting is produced by seasonally warm surface water being advected against and underneath the shelf edge, though the action of tidal pumping and coastal currents (Jacobs et al., 1992). Melt rates of  $2.8 \text{ myr}^{-1}$ , decaying exponentially down to zero around 40 km up-shelf from the calving margin, have been estimated for the ROS. This is 10–40 % of the published total melt estimates for ROS (Horgan et al., 2011).

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There is clear evidence that regional oceanographic forcing of the contemporary AIS is important (e.g. Pine Island, Western AP) and growing evidence that similar regional forcing occurred during deglaciation (e.g. Nicholls et al., 2009; Walker et al., 2008; Jenkins et al., 2010; Pritchard et al., 2012). To accurately model SSM over glacial cycles would require a high resolution coupled GSM and ocean model that are able to represent the major components (e.g. evolving cavity geometry; heat and salt flux exchange between the ice base, the cavity water masses, and the open ocean) of the SSM process (Holland et al., 2003; Payne et al., 2007; Olbers and Hellmer, 2010; Diniman et al., 2011). This approach is at present not computationally feasible. Recent studies with GSMs configured for the AIS have used either parametrized ad hoc implementations (Pollard and DeConto, 2009a) or derivations of the melt equation proposed by Beckmann (2003) (Martin et al., 2010; Pollard and DeConto, 2012b). The Beckmann equation was developed to model the ice shelf ocean-interface. It yields a melt rate dependent on the heat flux between the shelf bottom and the ocean. PISM-PIK used a variant of this law – forced by an continental-wide constant ocean temperature that is adjusted by the pressure-dependent freezing point of the ocean water – to produce an SSM spatial distribution dependent on the draught of the shelf (Martin et al., 2010). The PSU GSM evolved the PISM-PIK method by, amongst other changes, introducing specific regions of ocean temperatures based on observations; this reportedly gives quite reasonable modern day SSM values (Pollard and DeConto, 2012b). For paleo-climatic simulations the regional ocean temperatures were hindcast backward proportional to the Lisiecki (2005) stacked benthic  $\delta^{18}\text{O}$  records. The Beckmann law does not capture the freeze-on nor the effect of enhanced shelf front melt.

For the MUN/PSU GSM, a SSM component was developed that did not have a strong dependence on oceanic temperatures. This removed the associated parameters required to provide both regional tuning of the shelves and paleo-adjustment. The new SSM component is a physically-motivated empirical approach that captures both the melt-freeze-melt regimes of the larger shelves and the simpler melt regimes of the peripheral shelves. There are three ensemble parameters to provide some degrees of

freedom in the component. The geometry of the larger shelves is used to adjust the strength of the melt aspect ratio allowing some regional, and temporal evolution.

## SSM implementation

We merge the exponential shelf front melt law published by Horgan et al. (2011)<sup>2</sup> with quadratic fits to distance-from-grounding line transects for the melt rate and the shelf ice thickness measured for AMY (Wen et al., 2007)<sup>3</sup> and RON (Jenkins and Doake, 1991)<sup>4</sup>. A flowchart of the implementation is shown in Fig. 1.

The SSM component models three regimes under the larger shelves: a draught dependent grounding line zone (GLZ) of melt, an accretion zone (ACZ) where freeze-on occurs, and a zone of melt at the shelf front (SFZ). The smaller shelves only have regions of GLZ and SFZ melt occurring. Being on the periphery of the continent, the smaller shelves lack the embayment protection that the larger shelves have. As such, the sub-shelf environment is not sufficiently quiescent to allow the mode 1 melt water to freeze-on underneath the shelf. For monitoring modelled shelf response, the floating ice is divided into five regions (shown in Fig. 2a) pertaining to the four large shelves (AMY, ROS, RON, and FIL) and, the ice that is not part of the large shelves (e.g. the

<sup>2</sup>The exponential shelf melt law was derived from spatial and temporal variations, measured by ICESat laser altimetry data, of the ice surface at the front of the shelf. The surface changes were attributed to enhanced basal melt within 60 km of the shelf front (Horgan et al., 2011).

<sup>3</sup>The AMY transects were computed from in-situ and remote sensing datasets; a flow line set of flux-gates were defined using the datasets. From the flux gates the mass budgets, basal melting, and freezing rates were derived (Wen et al., 2007).

<sup>4</sup>The RON transects were derived from a glaciological field study of 28 sites that lie along flow lines extending from the grounding line to the shelf front. The objective of the study was to derive ice-ocean interaction behaviour from surface measurements. Physical characteristics, including the thickness data, were measured at each site and the data was used in a kinematic steady state model to derive the basal mass flux (and other fields) (Jenkins and Doake, 1991).

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smaller shelves of the Amundsen, Weddell, and Bellingshausen Seas and the remaining unnamed shelves), is classified as OTHER.

The transitions between the zones were estimated from the AMY and RON transects, shown in Fig. 3a. The raw data for these transects, given in Tables 1 and 2 of the Supplement, were extracted from Wen et al. (2007, Figs. 4 and 6) for the AMY and from Jenkins and Doake (1991, Figs. 9 and 10) for the RON.

The transition from GLZ to ACZ in the larger shelves occurs at a shelf thickness of  $\sim 700$  m. Similarly the transition from the ACZ to the SFZ occurs at a shelf thickness of approximately 300–400 m. The melt-accretion-melt pattern can also be seen, albeit approximately, when comparing the 700 m and/or 300 m contour from ALBMAP (Fig. 4) and the satellite derived melt distribution patterns of the AMY (Fricker et al., 2001, Fig. 3), the FIL (Joughin and Padman, 2003, Fig. 2), and the modelling study of the ROS (Holland et al., 2003, Fig. 10). Sensitivity tests were made adjusting the transition thicknesses within the range of uncertainty in the transects. However, because the melt/accumulation rates before and after the transition zones are very small (Jacobs et al., 1992; Horgan et al., 2011, the dominant melt rates occur at the grounding lines and at the shelf front), there was little impact. As such the transition thicknesses are held constant in the SSM component.

The melt rate in the GLZ is modelled as a function of ice shelf thickness and the aspect ratio of the shelf. Plotting the melt rate as a function of thickness (Fig. 3b) allows a quadratic best-fit to be made (the raw data was pruned so that the quadratic fit is only made with the data that is upstream of the GLZ to ACZ transition thickness threshold i.e. where  $H < 700$  m the melt rate is set to zero); each transect has a different fit, thus each shelf has a different melt rate thickness function. We hypothesize that, because the larger shelves have distinct cavity geometries that affect the oceanographic processes within them (Fricker et al., 2001; Horgan et al., 2011), the melt function is proportional to the physical dimensions of the shelf. We define a thickness to length aspect ratio,  $\epsilon = [H]/[L]$ , to reflect the cavity dimensions. Table 3 summarizes the physical characteristics, computed from ALBMAP<sub>40</sub>, used for defining the aspect

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ratio. The average length is computed as the average minimum distance from each grid cell to open ocean without encountering land or grounded ice. The shelf average melt rate magnitudes are taken from Table 3 of the Supplement. The stronger melt rates are seen under the AMY (thick and short) and FIL (thickest and shortest) which have larger aspect ratios than the RON (thick and long). The ROS (thin and long) has the smallest melt rate.

Using the present-day AMY and RON aspect ratios ( $\epsilon_{\text{AMY}}, \epsilon_{\text{RON}}$ ) and associated quadratic laws as reference melt functions ( $\dot{M}g_{\text{AMY}}, \dot{M}g_{\text{RON}}$ ), the melt rate ( $\dot{M}g$ ) for a shelf of thickness  $H$  with aspect ratio ( $\epsilon_{\text{shf}}$ ) can be computed using  $\epsilon_{\text{shf}}$  as a weighting factor and interpolating between the two reference functions.

$$\begin{aligned}\dot{M}g_{\text{AMY}} &= -7.95 \times 10^{-06} H^2 + 8.38 \times 10^{-03} H - 2.19, \\ \dot{M}g_{\text{RON}} &= -5.10 \times 10^{-06} H^2 + 5.92 \times 10^{-03} H - 1.62.\end{aligned}$$

The shelf weighting factor is computed as

$$W_{\text{shf}} = \frac{\epsilon_{\text{shf}} - \epsilon_{\text{AMY}}}{\epsilon_{\text{RON}} - \epsilon_{\text{AMY}}}. \quad (25)$$

The final melt rate is computed from:

$$\dot{M}g = \text{fnGLzN} [\dot{M}g_{\text{AMY}} + W_{\text{shf}} [\dot{M}g_{\text{RON}} - \dot{M}g_{\text{AMY}}]], \quad (26)$$

where ensemble parameter fnGLzN allows the strength of the computed melt to be adjusted: fnGLz1 (range 0.5–3) for the larger shelves and fnGLz2 (range 0.5–2.5) for the OTHER shelves. The aspect ratio for the OTHER shelves is always set to be the maximum of the large shelves, motivated by the fact that they are closer to the CDW so will likely suffer stronger melt for a given thickness. As the shelves evolve over time, the aspect ratio will also evolve, reducing or increasing the amount of melt proportionally. The calculation of length is computationally costly. As such, it is only performed every 20 yr.

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The basal accretion in the ACZ is modelled using a quadratic function that increases from zero at the two transition zones to a maximum near the centre:

$$\dot{M}_a = -\frac{1}{45000}(H - 550)^2 + 0.5. \quad (27)$$

The maximum accretion is set to be  $0.5 \text{ myr}^{-1}$  for all shelves<sup>5</sup>. ACZ accumulation, being a product of the GLZ mode 1 melt, should not exceed  $\dot{M}_g$ . If this does occur, the total  $\dot{M}_a$  is recomputed to be equal to  $\dot{M}_g$  melt and is re-distributed over the ACZ area. For present-day this condition only occurs in the ROS where, because of the shallow draught, the total GLZ melt is very low. Thus, because of the large area of the ACZ, the redistribution can reduce freeze-on amounts to near  $0 \text{ myr}^{-1}$  values (see Fig. 2).

The SFZ melt is modelled in accordance with the exponential law presented in Horgan et al. (2011). Within the front 60 km of the shelf the melt follows the law,

$$\dot{M}_s = f_{zclimsfz} \times 2.0 \exp\left(\frac{-x}{11900}\right), \quad (28)$$

where  $x$  is distance from the shelf front and  $f_{zclimsfz}$ ,

$$f_{zclimsfz} = 1 + f_{nzclimsfz} \times (z_{clim} - 1), \quad (29)$$

is a shelf front melt climate-dependence scaling factor. With the current 40 km resolution of the GSM,  $\dot{M}_s$  is integrated over the first and second ( $isf1$ ,  $isf2$  respectively) grid cells at the ice shelf front to produce two constants of SFZ melt,

$$\dot{M}_s = \begin{cases} -0.574 & isf1, \text{ if cell is shelf edge} \\ -0.019 & isf2, \text{ if cell is proximal to } isf1. \end{cases} \quad (30)$$

<sup>5</sup>From the transects and the RON (Joughin and Padman, 2003, Fig. 2) and ROS melt maps (Holland et al., 2003, Fig. 10), the accretion is generally very low [ $0.5 \text{ myr}^{-1}$ ]. Only for the AMY does it become significantly higher, with a maximum of  $1.5 \text{ myr}^{-1}$ .

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Ensemble parameter,  $fnSfz1$ , is used to scale  $M_s$  if the region is a large shelf. For the smaller shelves the melt is held constant (in earlier assessments of the GSM, adjustment of the SFZ for the smaller shelves had little impact, as such the parameter was removed). In the event of the ACZ grid cells encroaching into the SFZ (ice thickness in the grid cells at the shelf front being  $> 400\text{m}$ ) the accretion is set to  $0\text{myr}^{-1}$ . We reason that, at the shelf front, ISW would be advected away by CDW and/or coastal currents (Jacobs et al., 1992). The shelf front melt for all types of shelves is then further adjusted by the climate dependence factor  $fnzclimsfz$  (range 0–1.18) following the logic of the  $zclim$  for thin ice (Sect. 2.10.1).

The output from the SSM component is presented in Fig. 4, 5, and 2. Figure 4 shows transects and melt maps for AMY (a and d), RON (b and e), and ROS (c and f). The observed and computed melt rates from the high ( $H_5$  from ALBMAP<sub>5</sub>) and low ( $H_{40}$  from ALBMAP<sub>40</sub>) resolution thickness transects is shown for the AMY and RON. Both  $H_5$  and  $H_{40}$  are presented to compare the effect of the resolution change. All the computed melt rates use SSM ensemble parameters set to unity, thus removing their influence. Given that there are no observations for ROS, only the computed melt rate is shown (i.e. by interpolating between the two references functions using the aspect ratio computed from the estimated length scale and  $H_5$  thickness).

The melt rate spatial distributions of the major shelves, again calculated using  $H_5$  thickness and with the ensemble parameters set to unity, are shown in Fig. 4d–f. The 400 m and 700 m zone transition thresholds are shown on the melt maps; the spatial distribution can be compared with the published melt maps for FIL (Fig. 2 of Joughin and Padman, 2003) and ROS (Fig. 10 of Holland et al., 2003). There is no melt map for AMY, but a comparison can be made with the marine-ice thickness map (Fricker et al., 2001, Fig. 3), e.g. to delineate between the GLZ and ACZ.

### SSM verification

To verify the SSM component, we make comparisons with the available observations. Obtaining direct SSM measurements is understandably difficult given the environment

in which it occurs (Heimbach and Losch, 2012). A variety of techniques, including oceanographic (e.g. Jacobs et al., 1992, 1996), geochemical (e.g. Jacobs et al., 1992; Smethie and Jacobs, 2005; Loose et al., 2009), remote sensing (e.g. Fricker et al., 2001; Joughin and Padman, 2003; Lambrecht et al., 2007), borehole (e.g. Zotikov et al., 1980; Nicholls et al., 1991), and modelling studies (e.g. Holland et al., 2003; Payne et al., 2007) have been employed to obtain SSM volumes, magnitudes, and spatial distributions. The observations, as extracted from the literature, are presented in supplemental Table 3, some processing and conversion was performed to convert the raw data into a dataset that could be used for verification, shown in supplemental Table 4.

The observed and predicted net mass loss for the shelf regions are shown in Fig. 5. Five sets of model derived SSM magnitudes are shown. These include the melt rates computed using the  $H_5$  thickness dataset and unity ensemble parameters; and four computed using the GSM initialized with  $H_{40}$  and with different parameter settings (no ice-dynamic computations were performed, only the shelf melt component is executed, to generate the data): upper bound parameters, unity parameters, run nn2679 parameter values and lower bound values.

The unity parameter run removes the influence of the ensemble parameters. Apart from the FIL, the modelled total melt is similar to observations. The upper and lower bound runs have all ensemble parameters set to the highest and lowest values respectively as defined in Table 1 and are presented to show the maximum and minimum range the SSM component is capable of. Run nn2679 is the baseline run used in the sensitivity assessment (see Sect. 3). Values from the SSM component bracket observational inferences for the AMY, the ROS, and, although biased high, the RON. The component generates excessive melt for the FIL. The higher melt produced by RON and FIL is caused through excess GLZ melt. For the OTHER shelves, the SSM component is at the lower bound of the observations.

The spatial melt-map produced by the runs with upper (run 9164) and lower (run 9165) bound parameters are presented in Fig. 2. The  $H_{40}$  run (with parameters set

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(418 ka has a match to present-day temperature). In other words, the model is equilibrated with the mean surface temperature over an interval that corresponds to the advection time-scale of the interior of the AIS (thickness/accumulation rate = 4 km/2 cm). (2) an internal velocity configuration is generated by initializing the GSM with ALBMAP assuming isostatic equilibrium and the internal temperature computed in step 1. (3) starting from the above configuration, a small ensemble of 134 runs was generated (the parameter ranges were determined from previous runs) that ran from 391 ka to present-day with transient climate forcing and full thermodynamics. However, from 391 ka until 200 ka ice-dynamics is only active every 25 kyr for a period of just 100 yr. From 200 ka to present, ice-dynamics was continuously active. The output of these runs were assessed and the best run (closest to present-day configuration) was used as the starting configuration for the ensemble at 205 ka.

### 3 Sensitivity study

In the context of large ensemble analysis, the objective of the sensitivity study is to verify that: (a) each parameter has a significant effect on at least one characteristic of the model output (e.g. total grounded ice volume) and (b) collectively, the parameter ranges provide adequate coverage to bracket the observed values of the ice sheet metrics (characteristics). For computational efficiency, the sensitivity analysis is also used to reduce parameter ranges when extremal values cause numerical instabilities and/or blatantly unacceptable model results (e.g. suppressing WAIS formation).

The appropriate choice of metrics is driven by the scientific question being addressed, in this case the evaluation of a deglaciation chronology, as discussed in Briggs and Tarasov (2013)<sup>6</sup>. For the purposes of this sensitivity study, we use 6 metrics:

<sup>6</sup>Briggs and Tarasov (2013) present a constraint database of present-day (derived from ALBMAP) and paleo data (Eemian volume estimates, relative sea level curves, past ice surface indicators and grounding line retreat data) for Antarctica. They describe a structured method of applying this data to a large ensemble of model runs. The evaluation process they present

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grounded ice volume (in eustatic sea level equivalent, mESL<sup>7</sup>) for present-day WAIS (vol0gw) and for EAIS (vol0ge)<sup>8</sup>, total grounded ice volume for the LGM (vol20g), the zonal position of the Ross shelf grounding line (RISgl) along the 81° S line of latitude<sup>9</sup>, and the shelf areas for ROS and for RON-FIL.

5 Finding the appropriate range for each parameter is an iterative process. Initially the parameter ranges are set using best guess values, either taken from the literature or from experience gained during the development of the components (e.g. the SSM component). From these initial ranges, sensitivity ensembles are generated, evaluation of which potentially refines the ranges and, if required, might provoke the incorporation  
10 of new parameters to provide more degrees of freedom in the model or, conversely, removal of superfluous parameters.

Once the parameters and associated ranges have been verified to achieve the requirements of objectives (a) and (b), there is, ideally, sufficient confidence to justify the computational expenditure required to generate (and evaluate) a full ensemble. Deeper  
15 analysis of the full ensemble results can then be used to verify that full coverage has been achieved (within the parameter-space created by the 31 parameters).

Sensitivity plots (Figs. 7–9) present the impact each parameter has on the selected metrics. The baseline run (nn2679) is one of the “better” runs as identified through the application of the constraint database and the evaluation methodology presented  
20 in Briggs and Tarasov (2013). This control run is slightly biased to excess ice volume (Fig. 7) with < 0.5 mESL difference from the ALBMAP volume. Similarly the ice shelf areas are smaller than that of ALBMAP. But for all metrics, model results for the indicated parameter ranges fully bracket ALBMAP values.

addresses the uncertainties found in the observational measurements, some of the structural error in the model, and the problems that must be addressed in integrating them together.

<sup>7</sup>Conversion factor of 10<sup>6</sup> km<sup>3</sup> of ice = 2.519 mESL.

<sup>8</sup>WAIS and EAIS are separated along a line-arc-line, defined as 30° W–85° S–170° W.

<sup>9</sup>observed grounding line along the 81° S line of latitude (present-day location taken as 81° S, 155° W).

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### 3.1 Discussion of parameter/metric sensitivity

Many of the parameters exhibit associated non-linear behaviour in one or more of the metrics. For instance, the impact of increasing the shelf pinning parameter ( $f_{npin}$ ) on ROS and RON-FIL shelf areas is non-monotonic. Furthermore, the impact is qualitatively different for each of the two shelf areas.

Over the range of parameters,  $vol0gw$  is more sensitive than  $vol0ge$  ( $\sim 9m$  range of variation in comparison to  $\sim 5m$ ). Only a few of the parameters cause a large spread (predominately calving and climate parameters). The majority of parameters produce less than  $\pm 1$  mESL of variation for both metrics. An unexpected result is the lower sensitivity of  $vol0gw$  to the shelf flow parameter compared to that of  $vol0ge$ . The  $vol0ge$  metric is sensitive to the choice of the GHF.

The ice-ocean parameters have more impact on the present-day WAIS rather than EAIS. The also have less impact during LGM when the shelf area was reduced. The shelf melt parameters have less impact than the calving parameters, except on the shelf area metrics.  $f_{nGLz2}$  is the least influential of the melt parameters.

The climate forcing parameters have much more impact on  $vol20g$  than on  $vol0gw$  and  $vol0ge$ , as many of them only affect past climates, not present-day. The climate mixing parameter,  $Twa$ , is one of the few parameters with a strong influence over all metrics.  $Twa$  is the weight between the two climate forcings  $Tf1$  and  $Tf2$ , where  $Tf1$  is a fully parameterized climate and  $Tf2$  is based on modern observed climatology (Sect. 2.9.1, Eq. 11). Despite this strong influence, the quantitative scores in the Briggs and Tarasov (2013) methodology remain only in mid ranges as  $Twa$  is varied from 0 to 1; i.e. neither a dominant  $Tf1$  or  $Tf2$  produces better runs. The other climate mixing parameter  $Twb$ , which weights the third climate forcing  $Tf3$  in Eq. (11), is also influential but to a lesser degree, probably because  $Tf3$  is based on the same modern climatology as  $Tf2$ .

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## 4 Summary and conclusion

We have modified the PSU ice sheet model through the inclusion of six climate forcing parametrizations, a basal drag parametrization (accounting for sediment likelihood, topographic roughness, and systematic model to observation thickness misfit), a visco-elastic isostatic adjustment solver, tidewater and ice shelf calving functionality, and a newly developed SSM component. To perform ensemble analysis, 31 ensemble parameters are used to explore the uncertainty in the ice physics (predominately the definition of the basal drag coefficients), the climate forcing, and the ice-ocean interface.

The SSM component captures the melt-freeze-melt regime of the larger shelves and the simpler regime of the smaller, peripheral, ice shelves. The SSM component produces total melt comparable to published SSM observations for the AMY, ROS, and RON, but produces too much melt for the FIL. The melt pattern is similar to melt patterns in other published studies. Except for the use of the  $-5^{\circ}\text{C}$  isotherm to mediate the shelf front melt, the SSM component does not directly account for the spatially or temporally diverse regime of oceanographic forcing. However, as the sub-shelf melt law is a function of the aspect ratio of the individual shelf, the current SSM implementation does include regional variability in sub-shelf melt regimes. Future studies will examine the impact of marine temperature variations on sub-shelf melt behaviour and associated shelf evolution.

Through the sensitivity study we have verified that for the 31 parameters described, each has significant influence over at least one of the 6 model metrics. The sensitivity study also highlights the non-linear behaviour of many of the parameters. Considered together, this offers confidence that the parameter ranges provide coverage of the model phase-space and thus warrant the effort required to generate (and analyze) a large ensemble.

Supplementary material related to this article is available online at:  
<http://www.the-cryosphere-discuss.net/7/1533/2013/tcd-7-1533-2013-supplement.pdf>.

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**Table 1.** Ensemble parameters.

Definition	Parameter	Range LB [BA] UB*	Units
<b>Ice dynamics</b>			
1 Flow enhancement factor for grounded ice	fnflow	3.50 [4.84] 5.50	
2 Flow enhancement factor for shelf flow	fnshelf	0.40 [0.57] 0.65	
3 Hard bed enhancement factor	fnslid	$1 \times 10^{-10}$ [ $2.57 \times 10^{-9}$ ] $1 \times 10^{-8}$	$\text{myr}^{-1} \text{Pa}^{-2}$
4 Soft bed enhancement factor	fnسد	$5 \times 10^{-7}$ [ $5.15 \times 10^{-6}$ ] $3 \times 10^{-5}$	$\text{myr}^{-1} \text{Pa}^{-2}$
5 Scaling of sediment presence after iso-static unloading	fhbPhif	0.001 [0.19] 1.00	
6 Model-obs ice thickness misfit scaling	fDragmod	0.00 [3.01] 9.99	
7 Sub-grid roughness exponent for drag modification of sediment	powfstdsed	0.00 [0.47] 1.20	
8 Sub-grid roughness exponent for drag modification of sliding	powfstdslid	0.00 [0.67] 1.20	
9 Pinning Factor	fnPin	0.01 [0.085] 0.1	
10 Geothermal heat flux input blending	fbedGHF	0.00 [0.85] 1.00	
<b>Climate Forcing</b>			
11 Glacial index interpolation scaling factor for temperature	fnTdfscale	0.75 [1.19] 1.30	
12 Lapse Rate factor	rlapseR	5.00 [8.31] 11.00	$^{\circ}\text{C km}^{-1}$
13 LGM temperature EOF field (Tf <sub>3</sub> only)	fTeof	-0.50 [-0.44] 0.50	
14 Temperature blending 1	Twa	0.00 [0.46] 1.00	
15 Temperature blending 2	Twb	0.00 [0.03] 1.00	
16 Phase factor for precipitation	fnPdexp	0.50 [1.94] 2.00	
17 LGM precipitation EOF fields (Pf <sub>3</sub> only)	fPeof1	-0.50 [0.16] 0.50	
18 LGM precipitation EOF fields (Pf <sub>3</sub> only)	fPeof2	-0.50 [-0.44] 0.50	
19 Glacial index interpolation scaling factor for precipitation	fnPre	0.50 [1.67] 2.00	
20 Precipitation blending 1	Pwa	0.00 [0.86] 1.00	
21 Precipitation blending 2	Pwb	0.00 [0.34] 1.00	
22 Desert elevation effect factor	fdesfac	0.00 [1.97] $2.00 \times 10^{-3}$	

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**Table 1.** Continued.

Definition	Parameter	Range LB [BA] UB*	Units
<b>Ice–ocean interface (Sub-shelf melt (SSM) and calving parameters)</b>			
23 Ice shelf calving scaling factor	fshscalv	0.50 [1.40] 2.50	
24 Ice shelf calving minimum thickness threshold	Hcrit2	10.00 [89.5] 150.00	myr <sup>-1</sup>
25 Ice shelf calving sub Hcrit2 enhancement factor	calvF	0.00 [0.08] 0.20	yr <sup>-1</sup>
26 Maximum calving velocity, tidewater glacier	fcalvVmx	0.10 [0.79] 10.00	kmyr <sup>-1</sup>
27 Thin ice calving temperature dependent scaling	fcalvwater	3.00 [7.92] 10.00	myr <sup>-1</sup>
28 Grounding line zone SSM factor (large shelves)	fnGLz1	0.50 [1.51] 2.50	myr <sup>-1</sup>
29 Grounding line zone SSM factor (other shelves)	fnGLz2	0.50 [1.56] 3.00	myr <sup>-1</sup>
30 Shelf front SSM factor (large shelves)	fnSfz1	0.50 [1.70] 2.50	myr <sup>-1</sup>
31 Shelf front melt climate dependence scaling	fnzclimsfz	0.00 [0.65] 1.18	

\* LB = lower bound, BA = baseline and UB = upper bound. Values are rounded to 2 decimal places.

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**Table 2.** Table of symbols and (non ensemble) model parameters discussed in the text.

Symbol	Definition	Units	Value
$\text{calrate}_{T_s}$	ice shelf calving rate	$\text{myr}^{-1}$	
$\text{crh}$	basal sliding co-efficient (between bed and ice)	$\text{myr}^{-1} \text{Pa}^{-2}$	
$\text{crhcrit}$	SSA-SIA critical threshold	$\text{myr}^{-1} \text{Pa}^{-2}$	$10^{-10}$
$\dot{C}$	Calving rate	$\text{myr}^{-1}$	
$H$	ice thickness	m	
$H_{\text{flot}}$	maximum buoyant thickness for tidewater calving	m	
$hb$	basal elevation, relative to sea level	m	
$hs$	ice surface elevation	m	
$hs_{\text{PD}}$	reference present day ice surface elevation	m	
$I$	glacial index, derived from either $T_{\text{epica}}$		
$n_{\text{edge}}$	no. grid-cell edges that meet tidewater conditions	(see Sect. 2.10.1)	
$\text{Mg}$	sub-shelf melt (SSM) rate for grounding line zone	$\text{myr}^{-1}$	
$\text{Mg}_{\text{AMY}}$	reference SSM rate for AMY grounding line zone	$\text{myr}^{-1}$	
$\text{Mg}_{\text{RON}}$	reference SSM rate for RON grounding line zone	$\text{myr}^{-1}$	
$\text{Ma}$	SSM rate for accumulation zone	$\text{myr}^{-1}$	
$\text{Ms}$	SSM rate for shelf front zone	$\text{myr}^{-1}$	
$P$	interpolated (blended) precipitation	$\text{myr}^{-1}$	
$P_{\text{LGM}}$	reference LGM precipitation field	$\text{myr}^{-1}$	
$P_{\text{PD}}$	reference PD precipitation field	$\text{myr}^{-1}$	
$\text{Pave}_{\text{LGM}}$	PMIP2 average LGM precipitation field	$\text{myr}^{-1}$	
$\text{Peof}_{1,2,\text{LGM}}$	PMIP2 reference LGM precipitation EOFs	$\text{myr}^{-1}$	
$\text{Pf}_{1,2,3}$	individual precipitation fields	$\text{myr}^{-1}$	
$\text{Pfac}$	scaled precipitation glacial index		
$\text{Se}$	sediment presence exponent		
$\text{Slk}$	sediment likelihood parameter		
$t$	time	yr	
$T$	interpolated (blended) temperature	$^{\circ}\text{C}$	
$T_s$	sea-surface mean summer temperature	$^{\circ}\text{C}$	



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Table 2. Continued.

Symbol	Definition	Units	Value
$T_{\text{LGM}}$	reference LGM temperature field	°C	
$T_{\text{PD}}$	reference PD temperature field	°C	
$T_{\text{ave,LGM}}$	PMIP2 averaged LGM temperature	°C	
$T_{\text{eof,LGM}}$	PMIP2 LGM temperature EOFs	°C	
$T_{\text{f}1,2,3}$	individual temperature fields	°C	
$T_{\text{Cmn}}$	minimum critical $T_s$ for tidewater calving	°C	−5
$T_{\text{Cmx}}$	maximum critical $T_s$ for tidewater calving	°C	2
$u, v$	total horizontal velocities	$\text{m s}^{-1}$	
$u_b, v_b$	horizontal basal velocities	$\text{m s}^{-1}$	
$U_c$	tidewater calving velocity	$\text{km yr}^{-1}$	
$U_{\text{Cmx}}$	maximum calving velocity	$\text{km yr}^{-1}$	
$z_{\text{chrMN}}$	minimum basal sliding co-efficient	$\text{m yr}^{-1} \text{Pa}^{-2}$	$5 \times 10^{-11}$
$z_{\text{chrMX}}$	maximum basal sliding co-efficient	$\text{m yr}^{-1} \text{Pa}^{-2}$	$6 \times 10^{-5}$
$z_{\text{chrslid}}$	basal sliding co-efficient for hard bed (bare rock)	$\text{m yr}^{-1} \text{Pa}^{-2}$	$10^{-10}$
$z_{\text{chrhsd}}$	basal sliding co-efficient for soft bed (sediment)	$\text{m yr}^{-1} \text{Pa}^{-2}$	$10^{-6}$
$\Delta H_{\text{alb}}$	model -obs ice thickness misfit		
$\Delta s$	$\delta^{18}\text{O}$ sea level departure from present		
$\Delta q_s$	annual orbital insolation anomaly from present day at 80° S	$\text{W m}^{-2}$	
$e_{\text{shf}}$	shelf aspect ratio		
$e_{\text{AMY}}$	AMY shelf aspect ratio		
$e_{\text{RON}}$	RON shelf aspect ratio		
$\sigma_{\text{hb}}$	sediment roughness		
$\tau_b$	basal stress	Pa	
$ \phi $	latitude	° South	



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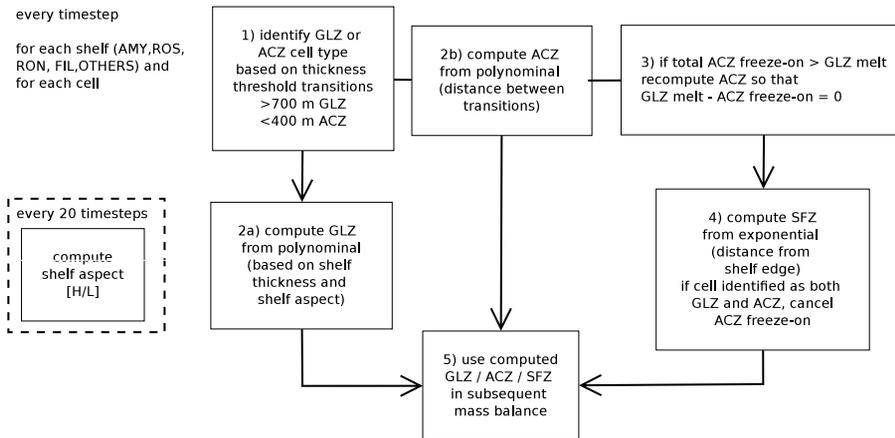


Fig. 1. SSM implementation flowchart.

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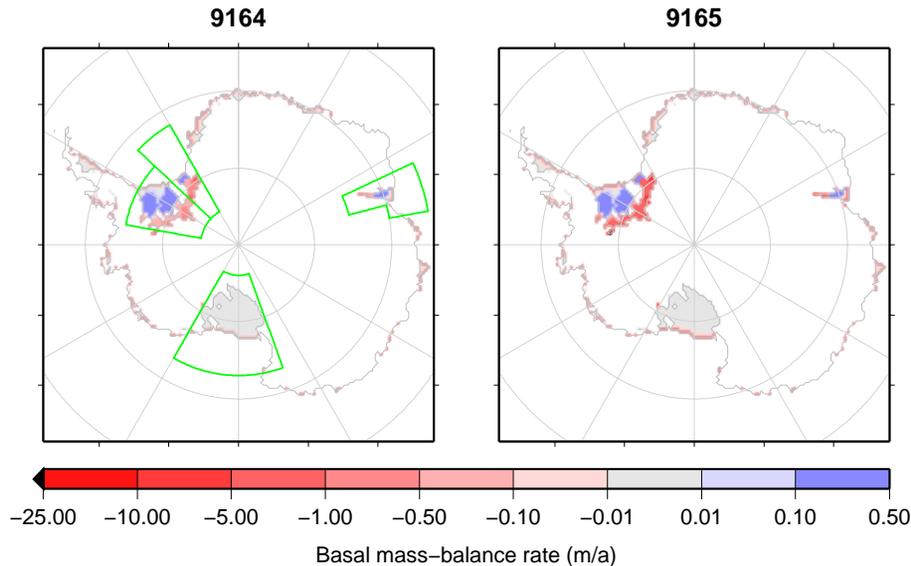
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**Fig. 2.** Melt rate maps generated from lower (9164) and upper (9165) SSM parameter values. The large shelf regions are outlined in green (the latitude,  $\Phi$ , and longitude,  $\lambda$ , boundaries are: AMY =  $\Phi(-75, -65), \lambda(65, 75)$  and  $\Phi(-75, -70), \lambda(75, 80)$ ; ROS =  $\Phi(-86, -73), \lambda(160, 210)$ ; RON =  $\Phi(-85, -75), \lambda(280, 313)$  and FIL =  $\Phi(-72, -85), \lambda(313, 330)$ ).

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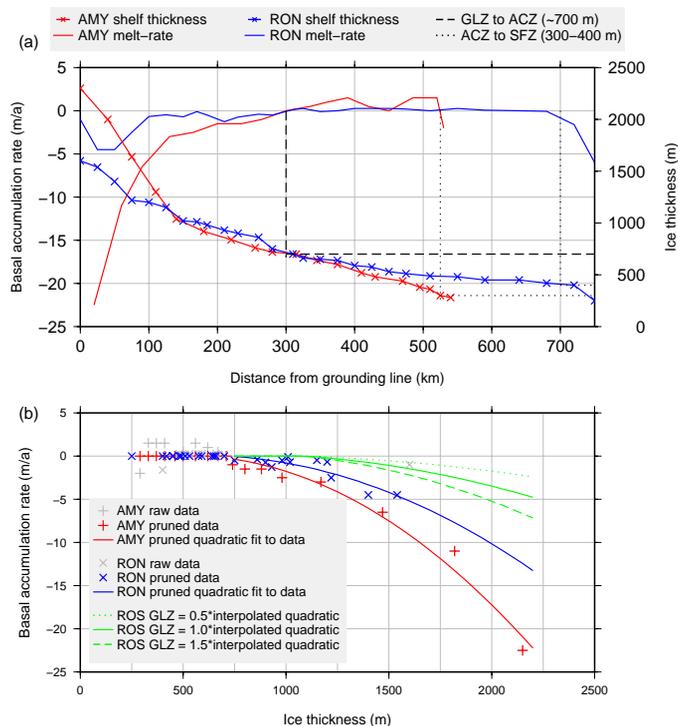
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**Fig. 3.** Plots showing the (a) melt rate and thickness transects and (b) the GLZ quadratic law. The transects are as extracted from source publications for AMY (Wen et al., 2007) and for RON (Jenkins and Doake, 1991). The transitions, from which the threshold thicknesses are estimated, between GLZ to ACZ and ACZ to SFZ are shown in plot (a). For the quadratic fits, once the basal mass-balance rate is  $> 0 \text{ myr}^{-1}$  (i.e. onset of freeze-on and thus part of the ACZ), the remaining data points are all set to zero. The quadratic fit is made to this pruned dataset.

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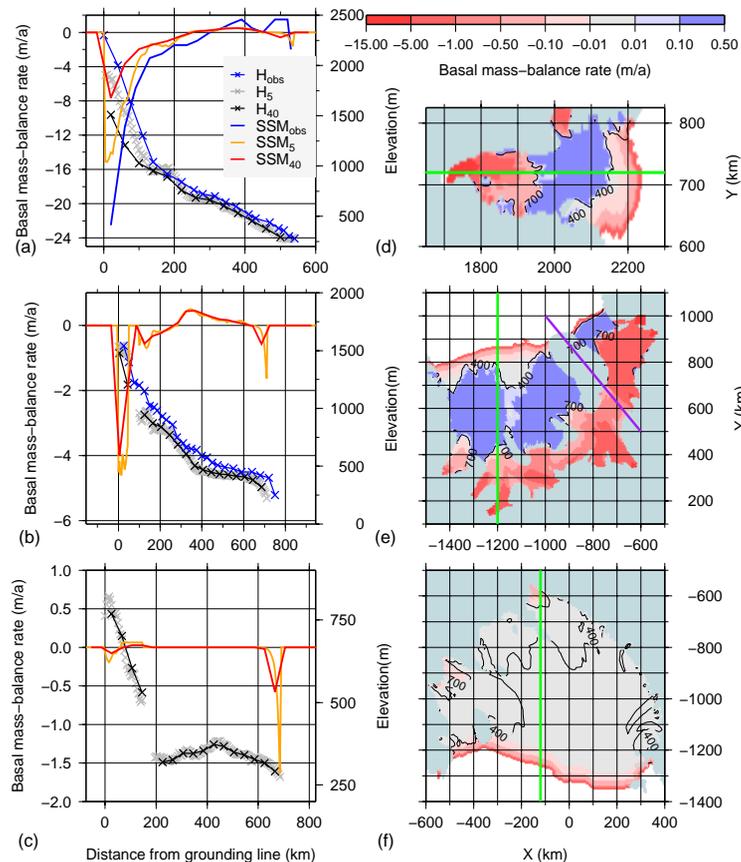
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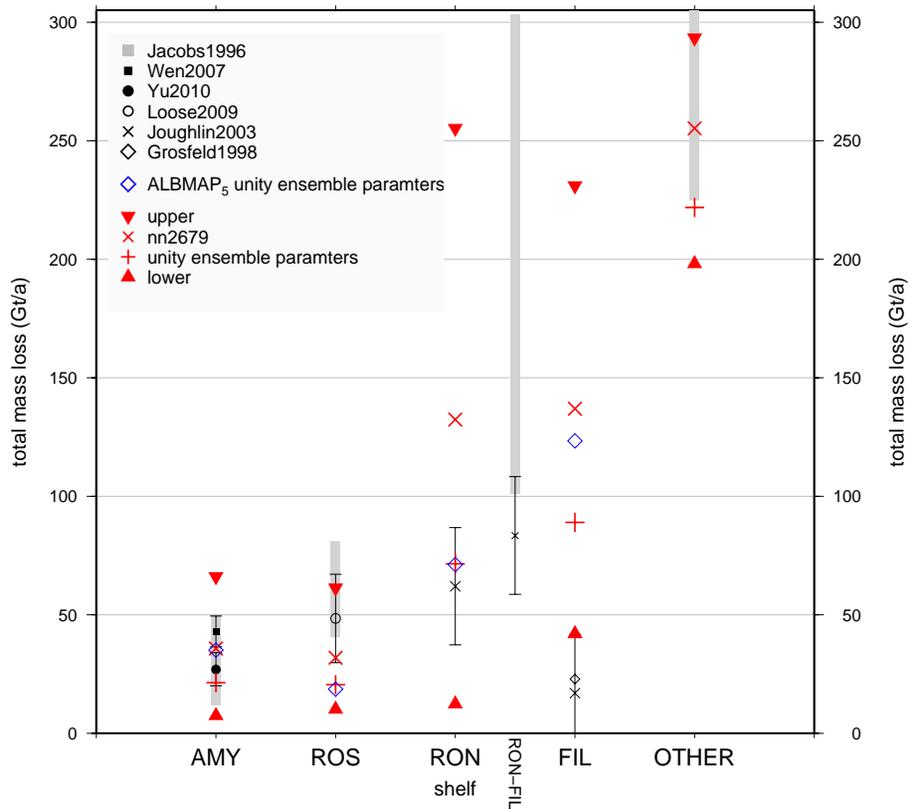


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**Fig. 4.** Thickness and melt transects and spatial melt maps for the three major shelves: AMY (a, d), ROS (b, e), RON-FIL (c, f) computed from the SSM law with unity parameters (see text). Green line on the melt maps shows the locations of the transects. The purple line demarcates the divide between the FIL and RON shelves at  $47^\circ$  W.



**Fig. 5.** Comparison plot showing net melt amounts from observations and the predicted melt amount from the SSM component for each of the five shelf regions; two observations that are for the cumulative RON-FIL are also show. The OTHER observation has been clipped as the maximum, estimated from Jacobs et al. (1996), peaks at  $675 \text{ Gt yr}^{-1}$  (see supplemental Table 4).

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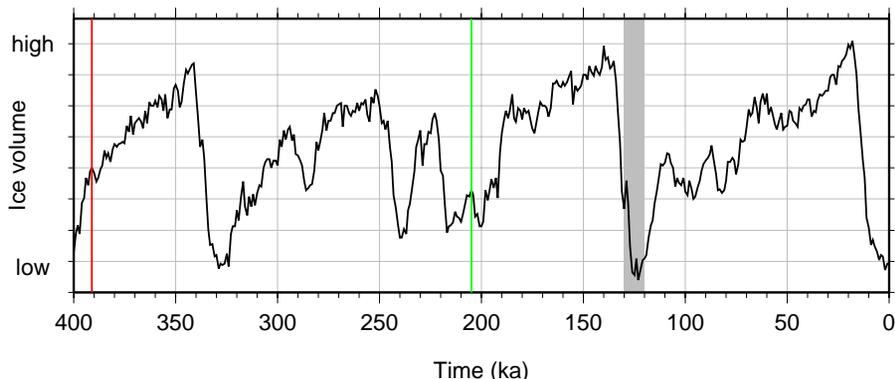
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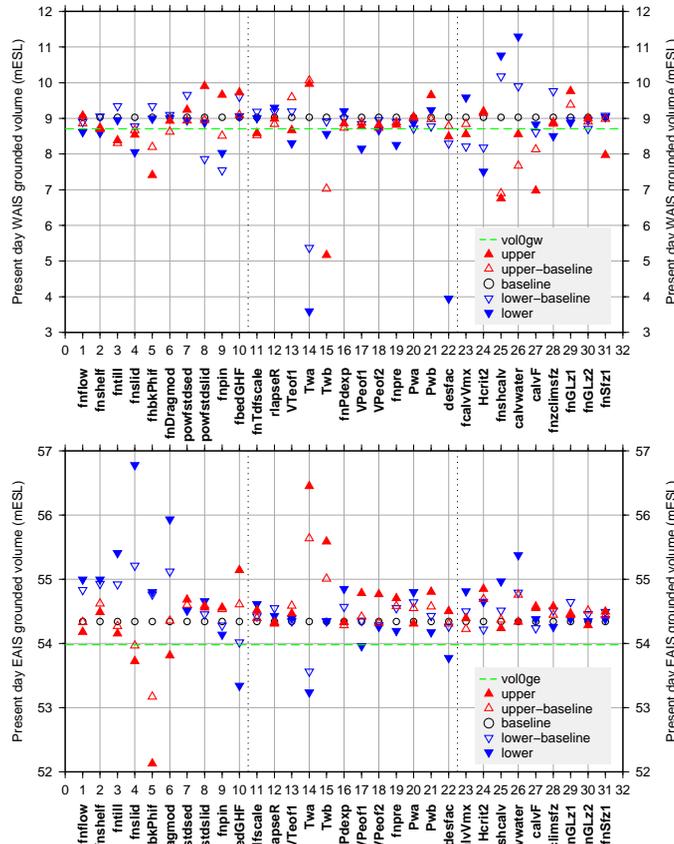


**Fig. 6.** Lisiecki (2005) stacked benthic  $\delta^{18}\text{O}$  record as proxy for global ice volume showing key times for spin up run. For the generation of the spin up ensemble (see text for details), ice dynamics is only intermittently active from 391 kyr (red) until 205 kyr (green). For the ensemble proper, initialization starts at 205 kyr. Approximate period of the Eemian is highlighted in grey.

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**Fig. 7.** Sensitivity results for present-day WAIS (upper) and EAIS (lower) grounded ice volume. The dotted lines segregate the parameters into blocks pertaining to ice physics, climate forcing and ice-ocean forcing. Observational metrics values (dashed green line) are computed from  $H_{40}$ .

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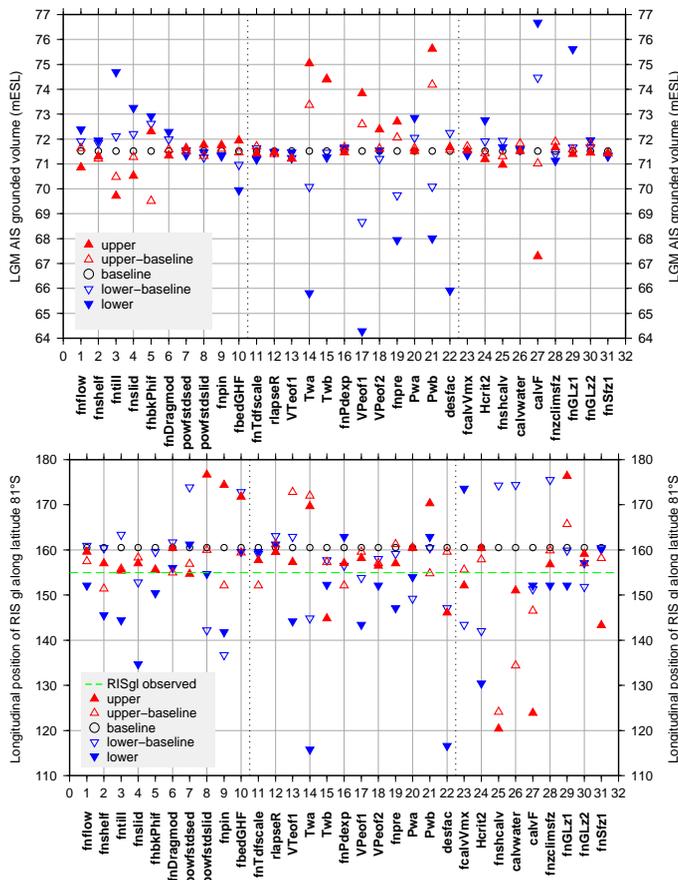
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**Fig. 8.** Sensitivity results for total AIS grounded volume (upper) at LGM and ROS grounding line position (lower). Note the latter metric misfit from observation for the baseline run is ~ 100km, which equates to 2–3 grid cells.

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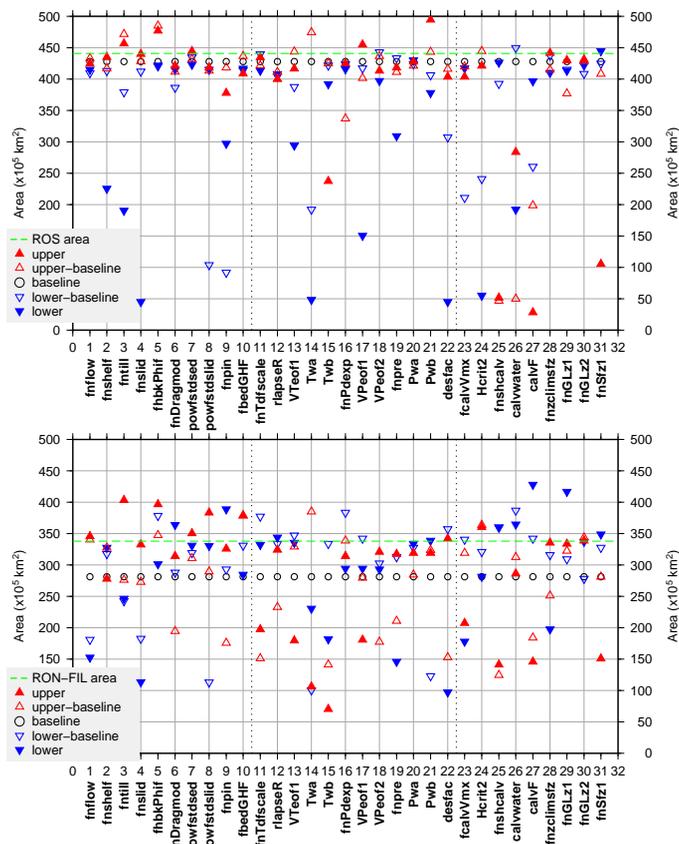


Fig. 9. Sensitivity results for ROS (upper) and RON-FIL (lower) present-day area.

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