

## C++ code for estimating diurnal solar radiation in areas with complex terrain

The code was tested using Microsoft Visual C++ (Win32 Console Applications). The input and output files are put directly under the code folder. Users can copy and save the included input data to a text file to test the code.

The input data needed are: Latitude, slope, aspect, viewshed angles, daily total solar radiation received on a horizontal surface without topographic effects, and the fraction of diffuse radiation. The viewshed angles are the angular distribution of sky visibility versus obstruction, similar to the view taken by upward-looking hemispherical (fisheye) photographs from the site. Sixteen angles are used in the input to represent the sky visibility.

In this code, daily total solar radiation without topographic effects is estimated from daily minimum and maximum air temperature. The parameters are estimated from the observations in Inuvik climate station (68.32 °N, 133.53 °W). The parameters may differ with time and place. Users need to estimate their parameters, or can use observations or better methods if available.

### Copy right and citation:

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Detailed descriptions about the method and equations can be found in the appendix of the above paper.

### -----Beginning of the code-----

```
//Microsoft Visual C++ code for estimating diurnal solar radiation in area with complex terrain
#include <stdio.h>
#include <stdlib.h>
#include <math.h>
#include <string.h>

#define Pi 3.1415926
#define RAD 0.017453292 //radians for one degree: Pi/360.0
#define TimeStep 1.0 //time-step (hour), can be modified directly

void Integration_Factors_Etc(int DOY, double sin_Lat, double cos_Lat, double Factors[], double Mid[]);
double Slope_Solar_Rad(int DOY, double Time, double Day_Length, double sin_Lat, double cos_Lat, double cos_Slope,
    double sin_Slope, double cos_sFactors0, double DayF_Diffuse, double Rad0, double Slope, double Aspect, double
    ViewShed[], double ViewshedF_Diffuse, double sFactors[]);

int main() {
char Char[201];
int i, j, Y, M, D;
int DOY, Leap_Year_Flag, YearDays;
```

```

double Latitude, Slope, Aspect, ViewShed[16];
double sin_Lat, cos_Lat, sin_Slope, cos_Slope;

double Daily_Tmin[366], Daily_Tmax[366], Daily_Tair[366], Daily_DTair[366], Daily_Vap[366];
double RAD_Above[366], Daily_Solar_Rad[366], Day_Length[366], sFactors[366][4], cos_sFactors0[366];

double Time, Sun_Set, Sun_Rise;
double ViewshedF_Diffuse, Rad_Avg, DayF_Diffuse, Rad_S;
double F, P, Mid[2]; //mid variables
FILE *fpt_Input, *fpt_Output;

//open output file and print the head line
if((fpt_Output = fopen("Output.txt", "w")) == NULL) {
    printf("Couldn't open output file");
    exit(0);
}
fprintf(fpt_Output, "DOY   DL   Rad0 ");
for(Time=0; Time<24.0; Time +=TimeStep) fprintf(fpt_Output, "%7.11f ", Time);
fprintf(fpt_Output, "\n");

//open and read input file
if((fpt_Input = fopen("Input.txt", "r")) == NULL) {
    printf("Couldn't open input file ");
    exit(0);
}

fgets(Char, 200, fpt_Input); //a note line
fscanf(fpt_Input, "%lf", &Latitude); fgets(Char, 200, fpt_Input);
fscanf(fpt_Input, "%lf", &Slope);    fgets(Char,200, fpt_Input);
fscanf(fpt_Input, "%lf", &Aspect);   fgets(Char,200, fpt_Input);
fgets(Char, 200, fpt_Input); //a note line
for(i=0; i<8; i++)  fscanf(fpt_Input, "%lf", &ViewShed[i]); fgets(Char, 200, fpt_Input);
for(i=8; i<16; i++) fscanf(fpt_Input, "%lf", &ViewShed[i]); fgets(Char, 200, fpt_Input);

//data range checking
if(Latitude<-90.0 || Latitude >90.0) {
    printf("The Latitude (%lf) is out of the range (-90 to 90)\n", Latitude);
    exit(0);
}
if(Slope<0.0 || Slope>90.0) {
    printf("The Slope (%lf) is out of the range (-90 to 90)\n", Slope);
    exit(0);
}
if(Aspect<0.0 || Aspect>360.0) {
    printf("The Aspect (%lf) is out of the range (0 to 360)\n", Aspect);
}

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    exit(0);
}
for(i=0; i<16; i++) {
    if(ViewShed[i]<0.0 || ViewShed[i]>90.0) {
        printf("The viewshed (No.%d: %lf) is out of the range (0 to 90)\n", i, ViewShed[i]);
        exit(0);
    }
}

//convert from degree to radians
Latitude *= RAD;
Slope     *= RAD;
Aspect    *= RAD;
for(i=0; i<16; i++) ViewShed[i] *= RAD;

sin_Lat = sin(Latitude);    cos_Lat = cos(Latitude);
sin_Slope = sin(Slope);     cos_Slope = cos(Slope);

fgets(Char, 200, fpt_Input);
fgets(Char, 200, fpt_Input);

//calculating Shusen Wang's integration factors, day length and daily extraterrestrial solar radiation
for(DOY=0; DOY<366; DOY++) {
    Integration_Factors_Etc(DOY, sin_Lat, cos_Lat, sFactors[DOY], Mid);
    Day_Length[DOY] = Mid[0];
    RAD_Above[DOY] = Mid[1]; //used for estimating daily solar radiation on the ground
    cos_sFactors0[DOY] = cos(sFactors[DOY][0]);
}
//calculating the effects of viewshed on diffuse radiation
P=0;
ViewshedF_Diffuse = 0;
for(i=0; i<16; i++) { //loop for azimuth directions
    for(j=0; j<90; j++) { //loop for elevation angles (in degrees)
        F = sin(j*RAD)*cos(j*RAD);
        P += F;
        if(j>=ViewShed[i]/RAD) ViewshedF_Diffuse += F;
    }
}
ViewshedF_Diffuse /= P; //relative diffuse radiation or fraction of sky not blocked

//-----add year loop here if more than one year climate is calculated -----
// Estimating daily solar radiation on the ground (without topographic effects)
// -- Users can directly use observations or better estimates if available.
// read daily min and max air temperature (for estimating daily solar radiation)
Leap_Year_Flag = 0; //1 if is a leap-year, 0 for non-leap-year
YearDays = 365 + Leap_Year_Flag;

```

```

for(DOY=0; DOY<YearDays; DOY++) {
    fscanf(fpt_Input, "%d %d %d %lf %lf", &Y, &M, &D, &Daily_Tmax[DOY], &Daily_Tmin[DOY]);
}

//Estimating vapor pressure and daily total solar radiation based on daily max and min air temperature
for(DOY=0; DOY<YearDays; DOY++) {
    Daily_Tair[DOY] = (Daily_Tmin[DOY] + Daily_Tmax[DOY])/2.0;
    Daily_DTair[DOY] = Daily_Tmax[DOY] - Daily_Tmin[DOY];
    Daily_Vap[DOY] = 0.92 * 6.11*exp(17.27*Daily_Tmin[DOY]/(Daily_Tmin[DOY]+237.3)); //0.92: parameter may differ
    with time and location
    if(Daily_DTair[DOY]>0.5) F = Daily_DTair[DOY];
    else F = 0.5;
// parameters 1.06, -0.06, 1.25, 0.02 may differ with time and location
    P = 1.06*(1-exp(-0.06*pow(F, 1.25))) * (1-0.02*Daily_Vap[DOY]);
    Daily_Solar_Rad[DOY] = P * RAD_Above[DOY]; //estimated daily solar radiation on the ground (MJ/m2/day)
}

//calculating durnal variations of solar radiation for each day
for(DOY=0; DOY<YearDays; DOY++) {
    if(Day_Length[DOY] > 0.01) {
        fprintf(fpt_Output, "%03d %5.2lf %5.2lf ", DOY+1, Day_Length[DOY], Daily_Solar_Rad[DOY]);
        Sun_Rise = 12-Day_Length[DOY]/2.0;
        Sun_Set = 12+Day_Length[DOY]/2.0;

//estimating fraction of diffuse radiation in total solar radiation
// -- Users can directly use observations or better estimates if available.
        Rad_Avg = Daily_Solar_Rad[DOY]*1000000.0/(Day_Length[DOY] * 3600.0); //mean solar radiation (w/m2)
        F = Rad_Avg/sFactors[DOY][3];
        if(F>0.9) F = 0.9;
        else if(F<0) F = 0.0;

        if(F<=0.175) DayF_Diffuse=1.0;
        else {
//Parameters 1.05, -4.5, 8.6 may differ with time and location
            DayF_Diffuse = 1.05/(1+exp(-4.5 + 8.6*F));
            if(DayF_Diffuse>0.99) DayF_Diffuse = 0.99;
        }
        for(Time=0; Time<24.0; Time +=TimeStep) {
            if(Time>=Sun_Rise && Time<= Sun_Set) {
                Rad_S = Slope_Solar_Rad(DOY, Time, Day_Length[DOY], sin_Lat, cos_Lat, cos_Slope, sin_Slope,
                cos_sFactors0[DOY], DayF_Diffuse, Rad_Avg, Slope, Aspect, ViewShed, ViewshedF_Diffuse, sFactors[DOY]);
            }
            else Rad_S = 0;
//output results
            fprintf(fpt_Output, "%7.2lf ", Rad_S);

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    } //Time loop
    fprintf(fpt_Output, "\n");
} //if Day_Length >0.01
} //DOY loop

fclose(fpt_Input);
fclose(fpt_Output);
return 1;
}

void Integration_Factors_Etc(int DOY, double sin_Lat, double cos_Lat, double sFactors[], double DL_Rad0[])
{
double S, C, AOB, Time, Step, SC, DS0, Dsinb;
double Declination, Altitude0, Hour_Angle,
    sin_D, cos_D, sin_Altitude0,
    Alt_Noon, cos_Alt_Noon, Alt, cos_Alt;
double Day_Length, SunRise, SunSet, Sum0, Sum1, Sum2, P0;
int N;

Declination = -23.44*RAD * cos (2.*Pi*(DOY+10.0)/365.25);
sin_D = sin(Declination);
cos_D = cos(Declination);

S = sin_Lat*sin_D;
C = cos_Lat*cos_D;

AOB = S/C;
if(AOB<-0.9999) {
    AOB = -0.9999;
    Day_Length = 0.0;
}
else if(AOB>0.9999) {
    AOB = 0.9999;
    Day_Length = 24.0;
}
else Day_Length = 12.0*(1.0+2.0*asin (AOB)/Pi); //day length in hour

//daily solar constant (SC) and daily extraterrestrial radiation (DS0)
if(Day_Length>0.001) {
    Dsinb = 3600.0*(Day_Length*S+24.0*C*sqrt(1.-AOB*AOB)/Pi);
    SC = 1350.0*(1.0+0.033*cos (2.0*Pi*DOY/365.25));
    DS0 = SC*Dsinb/1000000.0; //daily extra-terrestrial solar radiation: MJ/m2/day

Hour_Angle = 0.0; //at noon
sin_Altitude0 = S+C;
Altitude0 = asin(sin_Altitude0);
}
}

```

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if(Altitude0<0) Altitude0 = 0;
Alt_Noon = Pi/2 - Altitude0; //zenith angle
cos_Alt_Noon = cos(Alt_Noon);

SunRise = 12.0 - Day_Length/2;
SunSet  = 12.0 + Day_Length/2;

Time = 0;
N = 0;
Step = 5.0/60.0; //Time-step(in hour) for the integration (5 minutes)

Sum0 = 0;
Sum1 = 0;
Sum2 = 0;
for(Time=SunRise+Step; Time<SunSet; Time += Step) {
    Hour_Angle = 2*Pi*(Time-12.0)/24.0;
    sin_Altitude0 = S+C*cos(Hour_Angle);

    cos_Alt = sin_Altitude0;
    if(cos_Alt > 0) {
        Sum0 += cos_Alt;
        Altitude0 = asin(cos_Alt);
        Alt = Pi/2 - Altitude0;
        P0 = cos((Alt - Alt_Noon)/(Pi/2-Alt_Noon)*Pi/2);
        Sum1 += P0 * cos_Alt /cos_Alt_Noon; //direct ratio
        Sum2 += P0; //diffuse ratio
        N++;
    }
} //Time loop
if(Alt_Noon>89.0*Pi/180.0) Alt_Noon = 89.0*Pi/180.0;
sFactors[0] = Alt_Noon; //solar altitude at noon
sFactors[1] = 1/(Sum1 * Step/Day_Length);
sFactors[2] = 1/(Sum2 * Step/Day_Length);
sFactors[3] = SC * Sum0/N + 0.001; //average solar radiation on the top of the atmosphere
}
else {
    DS0 = 0.0;
    sFactors[0] = 0.0;
    sFactors[1] = 0.0;
    sFactors[2] = 0.0;
    sFactors[3] = 0.001;
}
DL_Rad0[0] = Day_Length; //day length, hr
DL_Rad0[1] = DS0; //daily solar radiation at top of the atmosphere, MJ/m2/day
}

```

```

double Slope_Solar_Rad(int DOY, double Time, double Day_Length, double sin_Lat, double cos_Lat, double cos_Slope,
    double sin_Slope, double cos_sFactors0, double DayF_Diffuse, double Rad0, double Slope, double Aspect,
    double ViewShed[], double ViewshedF_Diffuse, double sFactors[])
{
    int k;
    double Direct_Rad, Diffuse_Rad;
    double Declination, sin_D, cos_D, S, C;
    double Hour_Angle, Altitude0, sin_Altitude0, cos_Altitude0, Zenith, Azimuth;
    double F, P0;

    Declination = -23.44*RAD * cos (2.*Pi*(DOY+10.0)/365.25);
    sin_D = sin(Declination);
    cos_D = cos(Declination);
    S = sin_Lat*sin_D;
    C = cos_Lat*cos_D;

    Hour_Angle = 2*Pi*(12.0-Time)/24.0;
    Altitude0 = asin(S+C*cos(Hour_Angle));
    Zenith = 0.5*Pi - Altitude0;

    sin_Altitude0 = sin(Altitude0);
    cos_Altitude0 = cos(Altitude0);
    if(cos_Altitude0 <= 0.0001) cos_Altitude0 = 0.0001; //avoiding divided by 0
    P0 = cos(0.5*Pi*(Zenith - sFactors[0])/(0.5*Pi - sFactors[0]));

//Azimuth: North:0, clockwise
    F =(sin_Altitude0*sin_Lat-sin_D)/(cos_Altitude0*cos_Lat);
    if(F>0.99999 || F<-0.99999) F = 0.99999;

    if(Time<12.0) Azimuth = Pi - acos(F);
    else Azimuth = Pi + acos(F);

    k = int(Azimuth/(22.5*RAD)); //22.5: the step of azimuth directions (360/16)
    if(Altitude0 > ViewShed[k]) { //un-blocked
        Direct_Rad = cos_Slope*sin_Altitude0 + sin_Slope*cos_Altitude0*cos(Azimuth-Aspect);
        if(Direct_Rad<0) Direct_Rad = 0;
    } //if
    else Direct_Rad = 0;

    Direct_Rad = Rad0 * sFactors[1] * P0 * (1-DayF_Diffuse) * Direct_Rad/cos_sFactors0;
    Diffuse_Rad = Rad0 * sFactors[2] * P0 * DayF_Diffuse * ViewshedF_Diffuse;

    return Direct_Rad + Diffuse_Rad;
}

```

-----The End of the code-----

## A sample input data file

(Users can save the input data into a text file (using the name 'Input.txt' and put directly under the code folder)

(The note lines and the note following the numbers have to be included as well)

-----Following is a same input data-----

A note line about the data

69.0 ..Latitude (degrees)

30.0 ..Slope (degrees)

180.0 ..Aspect (0-360 degrees, North 0, clockwise)

Viewshed (0 - 90 degrees) (lowest blocking angles in 16 directions beginning from north clockwise)

0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 ..8 eastern directions (0,22.5,45,67.5,90,112.5,135,157.5)

30.0 30.0 30.0 0.0 0.0 0.0 0.0 0.0 ..8 western directions (180,202.5,225,247.5,270,292.5,315,337.5)

Daily maximum and minimum air temperature (degree C)

| Year | Month | Date | Tmax  | Tmin  |
|------|-------|------|-------|-------|
| 1971 | 1     | 1    | -23.3 | -44.4 |
| 1971 | 1     | 2    | -23.3 | -44.7 |
| 1971 | 1     | 3    | -22.2 | -43.9 |
| 1971 | 1     | 4    | -23.3 | -32.2 |
| 1971 | 1     | 5    | -16.7 | -31.7 |
| 1971 | 1     | 6    | -20.6 | -24.4 |
| 1971 | 1     | 7    | -21.1 | -40.6 |
| 1971 | 1     | 8    | -42.2 | -43.3 |
| 1971 | 1     | 9    | -47.8 | -49.4 |
| 1971 | 1     | 10   | -25.6 | -50   |
| 1971 | 1     | 11   | -25.6 | -47.8 |
| 1971 | 1     | 12   | -30.6 | -33.3 |
| 1971 | 1     | 13   | -41.1 | -41.7 |
| 1971 | 1     | 14   | -44.4 | -47.8 |
| 1971 | 1     | 15   | -50.6 | -51.7 |
| 1971 | 1     | 16   | -52.8 | -55   |
| 1971 | 1     | 17   | -48.3 | -54.4 |
| 1971 | 1     | 18   | -44.4 | -53.9 |
| 1971 | 1     | 19   | -46.1 | -52.2 |
| 1971 | 1     | 20   | -46.7 | -50   |
| 1971 | 1     | 21   | -40.6 | -48.9 |
| 1971 | 1     | 22   | -35   | -47.2 |
| 1971 | 1     | 23   | -36.7 | -40.6 |
| 1971 | 1     | 24   | -37.2 | -40   |
| 1971 | 1     | 25   | -39.4 | -46.7 |
| 1971 | 1     | 26   | -48.9 | -52.8 |
| 1971 | 1     | 27   | -50   | -53.3 |
| 1971 | 1     | 28   | -48.9 | -53.3 |
| 1971 | 1     | 29   | -46.1 | -52.2 |
| 1971 | 1     | 30   | -30   | -51.2 |
| 1971 | 1     | 31   | -30.6 | -47.8 |
| 1971 | 2     | 1    | -30.6 | -38.3 |
| 1971 | 2     | 2    | -29.4 | -38.9 |
| 1971 | 2     | 3    | -32.8 | -32.8 |
| 1971 | 2     | 4    | -42.8 | -48.9 |
| 1971 | 2     | 5    | -29.4 | -48.9 |
| 1971 | 2     | 6    | -24.4 | -45   |
| 1971 | 2     | 7    | -23.9 | -31.1 |
| 1971 | 2     | 8    | -23.3 | -28.9 |
| 1971 | 2     | 9    | -22.8 | -27.8 |
| 1971 | 2     | 10   | -28.9 | -33.9 |



|      |   |    |       |        |
|------|---|----|-------|--------|
| 1971 | 2 | 11 | -35.6 | -45.6  |
| 1971 | 2 | 12 | -26.1 | -42.2  |
| 1971 | 2 | 13 | -37.8 | -46.7  |
| 1971 | 2 | 14 | -33.3 | -50    |
| 1971 | 2 | 15 | -25.6 | -48.9  |
| 1971 | 2 | 16 | -25   | -35    |
| 1971 | 2 | 17 | -25   | -36.7  |
| 1971 | 2 | 18 | -11.1 | -27.8  |
| 1971 | 2 | 19 | -14.4 | -36.1  |
| 1971 | 2 | 20 | -13.9 | -27.8  |
| 1971 | 2 | 21 | -11.7 | -26.45 |
| 1971 | 2 | 22 | -9.4  | -25    |
| 1971 | 2 | 23 | -16.7 | -21.7  |
| 1971 | 2 | 24 | -28.3 | -30    |
| 1971 | 2 | 25 | -29.4 | -37.2  |
| 1971 | 2 | 26 | -32.8 | -46.7  |
| 1971 | 2 | 27 | -29.4 | -46.7  |
| 1971 | 2 | 28 | -27.2 | -42.2  |
| 1971 | 3 | 1  | -30   | -40.6  |
| 1971 | 3 | 2  | -30   | -33.9  |
| 1971 | 3 | 3  | -33.9 | -48.3  |
| 1971 | 3 | 4  | -30.6 | -46.1  |
| 1971 | 3 | 5  | -27.8 | -38.3  |
| 1971 | 3 | 6  | -27.8 | -31.7  |
| 1971 | 3 | 7  | -26.7 | -32.2  |
| 1971 | 3 | 8  | -25.6 | -37.8  |
| 1971 | 3 | 9  | -24.4 | -42.2  |
| 1971 | 3 | 10 | -20   | -37.8  |
| 1971 | 3 | 11 | -15.6 | -31.7  |
| 1971 | 3 | 12 | -12.8 | -28.9  |
| 1971 | 3 | 13 | -18.6 | -34.7  |
| 1971 | 3 | 14 | -24.4 | -40.5  |
| 1971 | 3 | 15 | -13.9 | -30    |
| 1971 | 3 | 16 | -12.8 | -32.8  |
| 1971 | 3 | 17 | -11.7 | -31.1  |
| 1971 | 3 | 18 | -8.3  | -25    |
| 1971 | 3 | 19 | -4.4  | -23.9  |
| 1971 | 3 | 20 | -11.7 | -28.9  |
| 1971 | 3 | 21 | -13.9 | -29.4  |
| 1971 | 3 | 22 | -11.7 | -31.1  |
| 1971 | 3 | 23 | -15.6 | -25    |
| 1971 | 3 | 24 | -14.4 | -32.2  |
| 1971 | 3 | 25 | -13.9 | -32.2  |
| 1971 | 3 | 26 | -13.9 | -24.4  |
| 1971 | 3 | 27 | -22.2 | -35.6  |
| 1971 | 3 | 28 | -20   | -32.8  |
| 1971 | 3 | 29 | -16.7 | -37.2  |
| 1971 | 3 | 30 | -16.1 | -36.7  |
| 1971 | 3 | 31 | -24.4 | -29.4  |
| 1971 | 4 | 1  | -26.7 | -39.4  |
| 1971 | 4 | 2  | -21.7 | -36.1  |
| 1971 | 4 | 3  | -18.3 | -31.7  |
| 1971 | 4 | 4  | -16.7 | -22.2  |
| 1971 | 4 | 5  | -16.1 | -21.1  |
| 1971 | 4 | 6  | -17.8 | -21.1  |
| 1971 | 4 | 7  | -18.9 | -26.1  |
| 1971 | 4 | 8  | -19.4 | -35    |
| 1971 | 4 | 9  | -18.3 | -37.2  |

|      |   |    |       |       |
|------|---|----|-------|-------|
| 1971 | 4 | 10 | -20   | -26.1 |
| 1971 | 4 | 11 | -13.3 | -25.6 |
| 1971 | 4 | 12 | -11.1 | -22.2 |
| 1971 | 4 | 13 | -3.3  | -20   |
| 1971 | 4 | 14 | -0.6  | -16.7 |
| 1971 | 4 | 15 | -12.2 | -14.4 |
| 1971 | 4 | 16 | -12.8 | -17.2 |
| 1971 | 4 | 17 | -5.6  | -22.8 |
| 1971 | 4 | 18 | -5    | -25.6 |
| 1971 | 4 | 19 | -2.8  | -21.1 |
| 1971 | 4 | 20 | -0.6  | -12.2 |
| 1971 | 4 | 21 | 1.1   | -20   |
| 1971 | 4 | 22 | 3.3   | -17.8 |
| 1971 | 4 | 23 | 4.4   | -10   |
| 1971 | 4 | 24 | 8.9   | -1.7  |
| 1971 | 4 | 25 | 5.6   | -4.4  |
| 1971 | 4 | 26 | -6.7  | -8.3  |
| 1971 | 4 | 27 | -3.9  | -15   |
| 1971 | 4 | 28 | -5.6  | -13.9 |
| 1971 | 4 | 29 | -10   | -16.1 |
| 1971 | 4 | 30 | -6.1  | -16.1 |
| 1971 | 5 | 1  | -3.3  | -15.6 |
| 1971 | 5 | 2  | -2.2  | -13.9 |
| 1971 | 5 | 3  | -7.8  | -15.6 |
| 1971 | 5 | 4  | -5.6  | -13.3 |
| 1971 | 5 | 5  | -2.8  | -11.1 |
| 1971 | 5 | 6  | -2.2  | -12.8 |
| 1971 | 5 | 7  | -1.1  | -8.3  |
| 1971 | 5 | 8  | 3.9   | -10.6 |
| 1971 | 5 | 9  | 5.6   | -6.7  |
| 1971 | 5 | 10 | -0.6  | -3.3  |
| 1971 | 5 | 11 | 3.9   | -5    |
| 1971 | 5 | 12 | 5.6   | -4.4  |
| 1971 | 5 | 13 | 3.3   | -3.3  |
| 1971 | 5 | 14 | 4.4   | -0.6  |
| 1971 | 5 | 15 | 3.9   | 0     |
| 1971 | 5 | 16 | 7.2   | 0.6   |
| 1971 | 5 | 17 | 8.3   | -1.7  |
| 1971 | 5 | 18 | 8.9   | 0.6   |
| 1971 | 5 | 19 | 13.9  | -0.6  |
| 1971 | 5 | 20 | 15.6  | -1.1  |
| 1971 | 5 | 21 | 16.1  | 0.6   |
| 1971 | 5 | 22 | 12.8  | 2.8   |
| 1971 | 5 | 23 | 16.1  | 0     |
| 1971 | 5 | 24 | 11.1  | -0.6  |
| 1971 | 5 | 25 | 13.3  | -0.6  |
| 1971 | 5 | 26 | 16.1  | -2.8  |
| 1971 | 5 | 27 | 16.1  | 5     |
| 1971 | 5 | 28 | 17.8  | 0     |
| 1971 | 5 | 29 | 15.6  | 6.1   |
| 1971 | 5 | 30 | 16.1  | 1.1   |
| 1971 | 5 | 31 | 17.8  | 1.7   |
| 1971 | 6 | 1  | 20.6  | 11.1  |
| 1971 | 6 | 2  | 14.4  | 5.6   |
| 1971 | 6 | 3  | 16.1  | 0     |
| 1971 | 6 | 4  | 19.4  | 4.4   |
| 1971 | 6 | 5  | 22.2  | 5.6   |
| 1971 | 6 | 6  | 23.3  | 7.8   |

|      |   |    |       |       |
|------|---|----|-------|-------|
| 1971 | 6 | 7  | 22.2  | 9.4   |
| 1971 | 6 | 8  | 24.4  | 10.6  |
| 1971 | 6 | 9  | 20.6  | 8.9   |
| 1971 | 6 | 10 | 11.1  | 0.6   |
| 1971 | 6 | 11 | 9.4   | -2.2  |
| 1971 | 6 | 12 | 6.7   | 0.6   |
| 1971 | 6 | 13 | 9.4   | -0.6  |
| 1971 | 6 | 14 | 18.9  | -0.6  |
| 1971 | 6 | 15 | 21.7  | 4.4   |
| 1971 | 6 | 16 | 23.3  | 4.4   |
| 1971 | 6 | 17 | 24.4  | 10.6  |
| 1971 | 6 | 18 | 21.7  | 12.2  |
| 1971 | 6 | 19 | 22.8  | 8.3   |
| 1971 | 6 | 20 | 25.6  | 11.7  |
| 1971 | 6 | 21 | 27.8  | 4.4   |
| 1971 | 6 | 22 | 26.7  | 15    |
| 1971 | 6 | 23 | 26.1  | 15.6  |
| 1971 | 6 | 24 | 24.4  | 3.9   |
| 1971 | 6 | 25 | 22.8  | 9.4   |
| 1971 | 6 | 26 | 16.7  | 8.3   |
| 1971 | 6 | 27 | 15    | 5     |
| 1971 | 6 | 28 | 10    | -0.6  |
| 1971 | 6 | 29 | 11.1  | 0.6   |
| 1971 | 6 | 30 | 15    | 2.2   |
| 1971 | 7 | 1  | 17.8  | 3.9   |
| 1971 | 7 | 2  | 18.9  | 6.7   |
| 1971 | 7 | 3  | 17.8  | 10    |
| 1971 | 7 | 4  | 18.3  | 4.4   |
| 1971 | 7 | 5  | 20    | 8.3   |
| 1971 | 7 | 6  | 23.3  | 6.1   |
| 1971 | 7 | 7  | 24.4  | 8.3   |
| 1971 | 7 | 8  | 27.2  | 8.3   |
| 1971 | 7 | 9  | 26.1  | 8.3   |
| 1971 | 7 | 10 | 26.35 | 11.1  |
| 1971 | 7 | 11 | 17.8  | 2.55  |
| 1971 | 7 | 12 | 18.3  | 5.6   |
| 1971 | 7 | 13 | 22.8  | 11.7  |
| 1971 | 7 | 14 | 28.05 | 12.8  |
| 1971 | 7 | 15 | 15    | -0.25 |
| 1971 | 7 | 16 | 21.1  | 1.7   |
| 1971 | 7 | 17 | 21.1  | 3.3   |
| 1971 | 7 | 18 | 23.1  | 7.8   |
| 1971 | 7 | 19 | 20.6  | 5.3   |
| 1971 | 7 | 20 | 25    | 12.2  |
| 1971 | 7 | 21 | 18.9  | 13.9  |
| 1971 | 7 | 22 | 16.1  | 11.1  |
| 1971 | 7 | 23 | 20.6  | 4.4   |
| 1971 | 7 | 24 | 19.4  | 6.7   |
| 1971 | 7 | 25 | 21.1  | 11.1  |
| 1971 | 7 | 26 | 25.6  | 11.7  |
| 1971 | 7 | 27 | 22.2  | 8.3   |
| 1971 | 7 | 28 | 15.6  | 12.2  |
| 1971 | 7 | 29 | 18.3  | 6.7   |
| 1971 | 7 | 30 | 20    | 5.6   |
| 1971 | 7 | 31 | 20.2  | 9.4   |
| 1971 | 8 | 1  | 16.1  | 8.9   |
| 1971 | 8 | 2  | 19.4  | 8.9   |
| 1971 | 8 | 3  | 14.4  | 3.9   |

|      |   |    |      |      |
|------|---|----|------|------|
| 1971 | 8 | 4  | 13.3 | 2.8  |
| 1971 | 8 | 5  | 17.8 | 0.6  |
| 1971 | 8 | 6  | 20   | -1.1 |
| 1971 | 8 | 7  | 12.8 | 5.6  |
| 1971 | 8 | 8  | 13.3 | 3.3  |
| 1971 | 8 | 9  | 14.4 | 6.7  |
| 1971 | 8 | 10 | 11.1 | 5    |
| 1971 | 8 | 11 | 16.1 | 2.2  |
| 1971 | 8 | 12 | 16.1 | 3.3  |
| 1971 | 8 | 13 | 6.1  | 0.6  |
| 1971 | 8 | 14 | 7.2  | 1.1  |
| 1971 | 8 | 15 | 12.2 | 3.9  |
| 1971 | 8 | 16 | 15.6 | -1.7 |
| 1971 | 8 | 17 | 19.4 | -1.1 |
| 1971 | 8 | 18 | 22.8 | 1.7  |
| 1971 | 8 | 19 | 23.3 | 8.9  |
| 1971 | 8 | 20 | 10   | 7.2  |
| 1971 | 8 | 21 | 10.6 | 3.3  |
| 1971 | 8 | 22 | 11.1 | 1.7  |
| 1971 | 8 | 23 | 7.2  | 1.1  |
| 1971 | 8 | 24 | 12.2 | 2.8  |
| 1971 | 8 | 25 | 16.7 | 1.7  |
| 1971 | 8 | 26 | 16.7 | 2.2  |
| 1971 | 8 | 27 | 19.4 | 2.2  |
| 1971 | 8 | 28 | 19.4 | 7.2  |
| 1971 | 8 | 29 | 15   | -1.7 |
| 1971 | 8 | 30 | 4.4  | 2.8  |
| 1971 | 8 | 31 | 4.4  | -1.1 |
| 1971 | 9 | 1  | 6.7  | 0.6  |
| 1971 | 9 | 2  | 5    | 0.6  |
| 1971 | 9 | 3  | 7.8  | 0.6  |
| 1971 | 9 | 4  | 3.3  | 0.6  |
| 1971 | 9 | 5  | 2.8  | 0    |
| 1971 | 9 | 6  | 4.4  | 1.1  |
| 1971 | 9 | 7  | 2.2  | 0    |
| 1971 | 9 | 8  | 0    | -2.2 |
| 1971 | 9 | 9  | 2.2  | -1.7 |
| 1971 | 9 | 10 | 5.6  | 0    |
| 1971 | 9 | 11 | 7.2  | 0    |
| 1971 | 9 | 12 | 7.2  | 0    |
| 1971 | 9 | 13 | 2.8  | -1.7 |
| 1971 | 9 | 14 | 10   | -4.4 |
| 1971 | 9 | 15 | 6.7  | -3.3 |
| 1971 | 9 | 16 | 10   | -1.1 |
| 1971 | 9 | 17 | 10.6 | -0.6 |
| 1971 | 9 | 18 | 6.1  | 2.8  |
| 1971 | 9 | 19 | 10   | 1.1  |
| 1971 | 9 | 20 | 11.7 | -5   |
| 1971 | 9 | 21 | 11.1 | 1.1  |
| 1971 | 9 | 22 | 8.3  | -0.6 |
| 1971 | 9 | 23 | 11.1 | -5   |
| 1971 | 9 | 24 | 9.4  | -6.7 |
| 1971 | 9 | 25 | 6.7  | -0.6 |
| 1971 | 9 | 26 | 5    | 0    |
| 1971 | 9 | 27 | -1.1 | -2.2 |
| 1971 | 9 | 28 | 1.7  | -4.4 |
| 1971 | 9 | 29 | -2.2 | -7.8 |
| 1971 | 9 | 30 | -2.2 | -6.7 |

|      |    |    |       |       |
|------|----|----|-------|-------|
| 1971 | 10 | 1  | -3.3  | -6.1  |
| 1971 | 10 | 2  | -1.7  | -6.1  |
| 1971 | 10 | 3  | -1.7  | -4.4  |
| 1971 | 10 | 4  | -4.4  | -6.1  |
| 1971 | 10 | 5  | -3.3  | -7.8  |
| 1971 | 10 | 6  | -2.8  | -8.9  |
| 1971 | 10 | 7  | -4.4  | -10   |
| 1971 | 10 | 8  | 0     | -8.9  |
| 1971 | 10 | 9  | 3.9   | -4.4  |
| 1971 | 10 | 10 | 3.9   | -6.7  |
| 1971 | 10 | 11 | 0     | -8.3  |
| 1971 | 10 | 12 | -3.3  | -5.6  |
| 1971 | 10 | 13 | -10   | -11.7 |
| 1971 | 10 | 14 | -10   | -24.4 |
| 1971 | 10 | 15 | -6.1  | -21.1 |
| 1971 | 10 | 16 | -1.1  | -18.3 |
| 1971 | 10 | 17 | -1.1  | -11.1 |
| 1971 | 10 | 18 | -3.3  | -5.6  |
| 1971 | 10 | 19 | -6.7  | -7.8  |
| 1971 | 10 | 20 | -12.2 | -19.4 |
| 1971 | 10 | 21 | -18.9 | -23.3 |
| 1971 | 10 | 22 | -13.3 | -24.4 |
| 1971 | 10 | 23 | -17.8 | -22.8 |
| 1971 | 10 | 24 | -18.3 | -21.7 |
| 1971 | 10 | 25 | -13.9 | -26.1 |
| 1971 | 10 | 26 | -3.9  | -24.4 |
| 1971 | 10 | 27 | -3.9  | -22.2 |
| 1971 | 10 | 28 | -4.4  | -10.6 |
| 1971 | 10 | 29 | -7.8  | -9.4  |
| 1971 | 10 | 30 | -9.4  | -17.2 |
| 1971 | 10 | 31 | -11.7 | -16.1 |
| 1971 | 11 | 1  | -12.2 | -18.9 |
| 1971 | 11 | 2  | -15   | -21.1 |
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| 1971 | 11 | 4  | -18.9 | -28.9 |
| 1971 | 11 | 5  | -25   | -34.4 |
| 1971 | 11 | 6  | -12.8 | -33.9 |
| 1971 | 11 | 7  | -13.9 | -25.6 |
| 1971 | 11 | 8  | -18.3 | -19.4 |
| 1971 | 11 | 9  | -22.2 | -34.4 |
| 1971 | 11 | 10 | -18.9 | -34.4 |
| 1971 | 11 | 11 | -16.1 | -23.3 |
| 1971 | 11 | 12 | -13.9 | -21.7 |
| 1971 | 11 | 13 | -16.1 | -16.1 |
| 1971 | 11 | 14 | -26.1 | -30   |
| 1971 | 11 | 15 | -27.8 | -31.1 |
| 1971 | 11 | 16 | -28.3 | -32.8 |
| 1971 | 11 | 17 | -19.4 | -34.4 |
| 1971 | 11 | 18 | -15   | -33.9 |
| 1971 | 11 | 19 | -15   | -21.7 |
| 1971 | 11 | 20 | -13.9 | -22.2 |
| 1971 | 11 | 21 | -13.9 | -16.7 |
| 1971 | 11 | 22 | -15.6 | -20.6 |
| 1971 | 11 | 23 | -22.8 | -36.7 |
| 1971 | 11 | 24 | -22.8 | -37.8 |
| 1971 | 11 | 25 | -35   | -38.9 |
| 1971 | 11 | 26 | -30   | -42.2 |
| 1971 | 11 | 27 | -20   | -39.4 |

|      |    |    |       |       |
|------|----|----|-------|-------|
| 1971 | 11 | 28 | -20   | -34.4 |
| 1971 | 11 | 29 | -22.8 | -22.8 |
| 1971 | 11 | 30 | -22.8 | -26.1 |
| 1971 | 12 | 1  | -22.2 | -25.6 |
| 1971 | 12 | 2  | -22.2 | -28.3 |
| 1971 | 12 | 3  | -22.8 | -25   |
| 1971 | 12 | 4  | -26.7 | -31.1 |
| 1971 | 12 | 5  | -35.6 | -37.2 |
| 1971 | 12 | 6  | -36.1 | -41.1 |
| 1971 | 12 | 7  | -24.4 | -42.8 |
| 1971 | 12 | 8  | -27.2 | -42.2 |
| 1971 | 12 | 9  | -41.1 | -42.8 |
| 1971 | 12 | 10 | -45.6 | -46.7 |
| 1971 | 12 | 11 | -43.3 | -47.2 |
| 1971 | 12 | 12 | -45   | -47.2 |
| 1971 | 12 | 13 | -45   | -47.2 |
| 1971 | 12 | 14 | -37.8 | -46.7 |
| 1971 | 12 | 15 | -25.6 | -46.1 |
| 1971 | 12 | 16 | -17.2 | -37.8 |
| 1971 | 12 | 17 | -17.2 | -25.6 |
| 1971 | 12 | 18 | -7.2  | -23.3 |
| 1971 | 12 | 19 | -22.8 | -23.9 |
| 1971 | 12 | 20 | -23.9 | -32.2 |
| 1971 | 12 | 21 | -31.7 | -32.2 |
| 1971 | 12 | 22 | -20   | -46.1 |
| 1971 | 12 | 23 | -20   | -41.1 |
| 1971 | 12 | 24 | -13.3 | -30   |
| 1971 | 12 | 25 | -7.2  | -29.4 |
| 1971 | 12 | 26 | -6.1  | -13.3 |
| 1971 | 12 | 27 | -11.1 | -20.6 |
| 1971 | 12 | 28 | -12.8 | -18.3 |
| 1971 | 12 | 29 | -12.8 | -22.8 |
| 1971 | 12 | 30 | -16.1 | -18.9 |
| 1971 | 12 | 31 | -12.2 | -25   |

-----End of the input data-----







|     |       |       |       |       |       |       |       |        |        |        |        |        |         |         |         |         |         |        |        |        |        |        |        |       |
|-----|-------|-------|-------|-------|-------|-------|-------|--------|--------|--------|--------|--------|---------|---------|---------|---------|---------|--------|--------|--------|--------|--------|--------|-------|
| 164 | 24.00 | 36.06 | 2.56  | 3.32  | 5.52  | 8.98  | 13.37 | 63.05  | 245.73 | 485.57 | 743.71 | 975.48 | 1147.68 | 1248.15 | 1147.68 | 975.48  | 743.71  | 485.57 | 245.73 | 63.05  | 13.37  | 8.98   | 5.52   | 3.32  |
| 165 | 24.00 | 32.96 | 4.43  | 5.70  | 9.40  | 15.22 | 22.60 | 70.23  | 233.21 | 445.27 | 672.33 | 875.44 | 1025.92 | 1113.50 | 1025.92 | 875.44  | 672.33  | 445.27 | 233.21 | 70.23  | 22.60  | 15.22  | 9.40   | 5.70  |
| 166 | 24.00 | 34.01 | 3.86  | 4.94  | 8.10  | 13.07 | 19.36 | 68.14  | 237.61 | 458.61 | 695.59 | 907.85 | 1065.27 | 1156.98 | 1065.27 | 907.85  | 695.59  | 458.61 | 237.61 | 68.14  | 19.36  | 13.07  | 8.10   | 4.94  |
| 167 | 24.00 | 27.09 | 10.60 | 13.52 | 22.03 | 35.41 | 52.36 | 97.80  | 219.23 | 371.35 | 530.47 | 670.42 | 772.64  | 831.40  | 850.03  | 831.40  | 772.64  | 670.42 | 530.47 | 97.80  | 219.23 | 97.80  | 52.36  | 35.41 |
| 168 | 24.00 | 20.78 | 18.09 | 22.99 | 37.29 | 59.76 | 88.23 | 131.33 | 206.87 | 292.61 | 376.38 | 446.14 | 494.62  | 521.22  | 529.38  | 521.22  | 494.62  | 446.14 | 376.38 | 292.61 | 206.87 | 131.33 | 88.23  |       |
| 169 | 24.00 | 29.05 | 8.59  | 10.89 | 17.60 | 28.14 | 41.50 | 87.98  | 223.36 | 395.50 | 577.32 | 738.42 | 856.84  | 925.30  | 947.10  | 925.30  | 856.84  | 738.42 | 577.32 | 395.50 | 223.36 | 87.98  | 41.50  |       |
| 170 | 24.00 | 26.64 | 11.67 | 14.77 | 23.81 | 38.00 | 55.98 | 101.68 | 219.23 | 365.53 | 517.95 | 651.63 | 749.05  | 804.94  | 822.64  | 804.94  | 749.05  | 651.63 | 517.95 | 365.53 | 219.23 | 101.68 | 55.98  |       |
| 171 | 24.00 | 36.01 | 3.04  | 3.84  | 6.18  | 9.85  | 14.50 | 66.16  | 247.28 | 483.97 | 738.16 | 966.15 | 1135.51 | 1234.32 | 1265.98 | 1234.32 | 1135.51 | 966.15 | 738.16 | 483.97 | 247.28 | 66.16  | 14.50  |       |
| 172 | 24.00 | 22.25 | 17.30 | 21.84 | 35.10 | 55.94 | 82.33 | 126.45 | 211.62 | 311.03 | 410.17 | 494.19 | 553.54  | 586.64  | 596.92  | 586.64  | 553.54  | 494.19 | 410.17 | 311.03 | 211.62 | 126.45 | 82.33  |       |
| 173 | 24.00 | 20.38 | 18.97 | 23.95 | 38.48 | 61.32 | 90.24 | 133.11 | 205.75 | 287.37 | 366.51 | 432.01 | 477.25  | 501.93  | 509.48  | 501.93  | 477.25  | 366.51 | 287.37 | 205.75 | 133.11 | 90.24  | 61.32  |       |
| 174 | 24.00 | 35.18 | 3.48  | 4.39  | 7.07  | 11.27 | 16.59 | 67.49  | 243.59 | 473.31 | 719.77 | 940.67 | 1104.65 | 1200.28 | 1230.90 | 1200.28 | 1104.65 | 940.67 | 719.77 | 473.31 | 243.59 | 67.49  | 16.59  |       |
| 175 | 24.00 | 27.39 | 10.71 | 13.54 | 21.81 | 34.81 | 51.27 | 97.23  | 220.39 | 374.82 | 536.50 | 678.83 | 782.88  | 842.74  | 861.74  | 842.74  | 782.88  | 678.83 | 536.50 | 374.82 | 220.39 | 97.23  | 51.27  |       |
| 176 | 24.00 | 20.47 | 18.57 | 23.53 | 37.99 | 60.72 | 89.52 | 132.42 | 205.86 | 288.65 | 369.10 | 435.81 | 481.97  | 507.20  | 514.92  | 507.20  | 481.97  | 369.10 | 288.65 | 205.86 | 132.42 | 89.52  | 60.72  |       |
| 177 | 24.00 | 24.48 | 14.15 | 17.97 | 29.13 | 46.65 | 68.85 | 113.69 | 215.49 | 339.00 | 465.53 | 575.06 | 653.95  | 698.74  | 712.82  | 698.74  | 653.95  | 575.06 | 465.53 | 339.00 | 215.49 | 113.69 | 68.85  |       |
| 178 | 24.00 | 27.05 | 10.66 | 13.58 | 22.11 | 35.51 | 52.49 | 97.92  | 219.05 | 370.73 | 529.37 | 668.88 | 770.76  | 829.32  | 847.89  | 829.32  | 770.76  | 668.88 | 529.37 | 370.73 | 219.05 | 97.92  | 52.49  |       |
| 179 | 24.00 | 26.54 | 11.05 | 14.14 | 23.14 | 37.28 | 55.20 | 100.30 | 217.88 | 364.50 | 517.40 | 651.58 | 749.36  | 805.47  | 823.24  | 805.47  | 749.36  | 651.58 | 517.40 | 364.50 | 217.88 | 100.30 | 55.20  |       |
| 180 | 24.00 | 29.43 | 7.48  | 9.61  | 15.83 | 25.60 | 37.99 | 83.73  | 222.72 | 400.51 | 588.91 | 756.19 | 879.34  | 950.62  | 973.33  | 950.62  | 879.34  | 756.19 | 588.91 | 400.51 | 222.72 | 83.73  | 37.99  |       |
| 181 | 24.00 | 30.07 | 6.60  | 8.53  | 14.16 | 23.01 | 34.23 | 79.90  | 223.77 | 408.74 | 605.36 | 780.30 | 909.30  | 984.08  | 1007.93 | 984.08  | 909.30  | 780.30 | 605.36 | 408.74 | 223.77 | 79.90  | 34.23  |       |
| 182 | 24.00 | 26.89 | 9.66  | 12.57 | 21.05 | 34.38 | 51.27 | 95.64  | 216.90 | 369.26 | 528.87 | 669.33 | 771.95  | 830.92  | 849.63  | 830.92  | 771.95  | 669.33 | 528.87 | 369.26 | 216.90 | 95.64  | 51.27  |       |
| 183 | 24.00 | 18.44 | 16.84 | 22.07 | 37.34 | 61.36 | 91.80 | 132.71 | 195.27 | 263.08 | 326.94 | 378.40 | 412.99  | 431.34  | 436.83  | 431.34  | 412.99  | 378.40 | 326.94 | 263.08 | 195.27 | 132.71 | 91.80  |       |
| 184 | 24.00 | 29.64 | 6.16  | 8.14  | 13.94 | 23.07 | 34.63 | 78.82  | 220.82 | 403.75 | 598.33 | 771.45 | 899.06  | 972.99  | 996.55  | 972.99  | 899.06  | 771.45 | 598.33 | 403.75 | 220.82 | 78.82  | 34.63  |       |
| 185 | 24.00 | 25.33 | 10.04 | 13.42 | 23.30 | 38.83 | 58.52 | 101.65 | 212.62 | 350.38 | 493.53 | 618.67 | 709.51  | 761.42  | 777.81  | 761.42  | 709.51  | 618.67 | 493.53 | 350.38 | 212.62 | 101.65 | 58.52  |       |
| 186 | 24.00 | 31.55 | 4.10  | 5.55  | 9.78  | 16.43 | 24.86 | 68.65  | 224.62 | 428.32 | 646.67 | 841.94 | 986.45  | 1070.44 | 1097.27 | 1070.44 | 986.45  | 841.94 | 646.67 | 428.32 | 224.62 | 68.65  | 24.86  |       |
| 187 | 24.00 | 29.58 | 5.14  | 7.06  | 12.66 | 21.47 | 32.65 | 75.09  | 218.24 | 403.69 | 601.50 | 777.74 | 907.72  | 983.04  | 1007.06 | 983.04  | 907.72  | 777.74 | 601.50 | 403.69 | 218.24 | 75.09  | 32.65  |       |
| 188 | 24.00 | 31.20 | 3.71  | 5.19  | 9.49  | 16.27 | 24.86 | 67.03  | 221.77 | 424.35 | 641.75 | 836.25 | 980.16  | 1063.78 | 1090.48 | 1063.78 | 980.16  | 836.25 | 641.75 | 424.35 | 221.77 | 67.03  | 24.86  |       |
| 189 | 24.00 | 30.46 | 3.81  | 5.43  | 10.17 | 17.62 | 27.08 | 68.26  | 218.60 | 415.20 | 626.00 | 814.42 | 953.70  | 1034.54 | 1060.34 | 1034.54 | 953.70  | 814.42 | 626.00 | 415.20 | 218.60 | 68.26  | 27.08  |       |
| 190 | 24.00 | 27.03 | 5.65  | 8.25  | 15.87 | 27.85 | 43.06 | 83.43  | 210.16 | 372.46 | 544.26 | 696.35 | 807.83  | 872.07  | 892.46  | 872.07  | 807.83  | 696.35 | 544.26 | 372.46 | 210.16 | 83.43  | 43.06  |       |
| 191 | 24.00 | 30.74 | 2.93  | 4.42  | 8.75  | 15.58 | 24.24 | 63.78  | 217.26 | 419.33 | 636.72 | 831.37 | 975.40  | 1059.05 | 1085.75 | 1059.05 | 975.40  | 831.37 | 636.72 | 419.33 | 217.26 | 63.78  | 24.24  |       |
| 192 | 24.00 | 26.85 | 4.58  | 7.16  | 14.71 | 26.58 | 41.66 | 80.62  | 207.45 | 370.66 | 543.80 | 697.22 | 809.73  | 874.54  | 895.13  | 874.54  | 809.73  | 697.22 | 543.80 | 370.66 | 207.45 | 80.62  | 41.66  |       |
| 193 | 24.00 | 22.09 | 6.69  | 10.96 | 23.44 | 43.10 | 68.07 | 108.40 | 200.59 | 312.06 | 425.68 | 523.32 | 593.02  | 632.20  | 644.44  | 632.20  | 593.02  | 425.68 | 312.06 | 200.59 | 108.40 | 68.07  | 43.10  |       |
| 194 | 24.00 | 25.43 | 4.02  | 7.01  | 15.75 | 29.51 | 47.00 | 85.00  | 202.94 | 353.57 | 512.54 | 652.77 | 755.14  | 813.87  | 832.46  | 813.87  | 755.14  | 652.77 | 512.54 | 353.57 | 202.94 | 85.00  | 47.00  |       |
| 195 | 24.00 | 30.89 | 1.45  | 2.74  | 6.53  | 12.51 | 20.10 | 55.51  | 212.70 | 422.40 | 649.44 | 854.36 | 1004.44 | 1092.23 | 1120.26 | 1092.23 | 1004.44 | 854.36 | 649.44 | 422.40 | 212.70 | 55.51  | 20.10  |       |
| 196 | 24.00 | 32.88 | 0.78  | 1.66  | 4.25  | 8.33  | 13.52 | 47.98  | 218.60 | 448.53 | 698.82 | 923.38 | 1091.91 | 1189.43 | 1220.60 | 1189.43 | 1091.91 | 923.38 | 698.82 | 448.53 | 218.60 | 47.98  | 13.52  |       |
| 197 | 24.00 | 31.21 | 0.72  | 1.86  | 5.21  | 10.49 | 17.21 | 50.18  | 210.93 | 427.24 | 662.41 | 874.07 | 1031.05 | 1122.30 | 1151.44 | 1122.30 | 1031.05 | 874.07 | 662.41 | 427.24 | 210.93 | 50.18  | 17.21  |       |
| 198 | 24.00 | 27.42 | 0.77  | 2.84  | 8.89  | 18.44 | 30.59 | 63.48  | 199.36 | 379.22 | 572.86 | 745.86 | 873.33  | 947.01  | 970.45  | 947.01  | 873.33  | 745.86 | 572.86 | 379.22 | 199.36 | 63.48  | 30.59  |       |
| 199 | 24.00 | 28.25 | 0.18  | 1.94  | 7.09  | 15.21 | 25.54 | 56.73  | 199.29 | 389.96 | 596.38 | 781.44 | 918.14  | 997.30  | 1022.51 | 997.30  | 918.14  | 781.44 | 596.38 | 389.96 | 199.29 | 56.73  | 25.54  |       |
| 200 | 23.18 | 22.55 | 0.00  | 3.12  | 14.12 | 31.49 | 53.60 | 89.15  | 191.08 | 319.58 | 453.82 | 571.03 | 655.68  | 703.72  | 718.81  | 703.72  | 655.68  | 571.03 | 453.82 | 319.58 | 191.08 | 89.15  | 53.60  |       |
| 201 | 22.65 | 10.12 | 0.00  | 2.44  | 15.54 | 36.22 | 62.57 | 92.19  | 123.97 | 153.08 | 176.29 | 191.88 | 200.22  | 203.47  | 204.17  | 203.47  | 200.22  | 191.88 | 176.29 | 153.08 | 123.97 | 92.19  | 153.08 |       |
| 202 | 22.27 | 10.73 | 0.00  | 1.19  | 14.98 | 36.76 | 64.53 | 95.85  | 130.38 | 162.51 | 188.59 | 206.49 | 216.37  | 220.42  | 221.36  | 220.42  | 216.37  | 206.49 | 188.59 | 162.51 | 130.38 | 95.85  | 64.53  |       |
| 203 | 21.95 | 28.24 | 0.00  | 0.00  | 4.44  | 11.59 | 20.70 | 46.43  | 192.06 | 390.71 | 607.74 | 803.15 | 947.74  | 1031.51 | 1058.19 | 1031.51 | 947.74  | 803.15 | 607.74 | 390.71 | 192.06 | 46.43  | 20.70  |       |
| 204 | 21.67 | 24.11 | 0.00  | 0.00  | 7.32  | 20.49 | 37.31 | 66.46  | 183.93 | 339.28 | 505.98 | 654.10 | 762.47  | 824.61  | 844.28  | 824.61  | 762.47  | 654.10 | 505.98 | 339.28 | 183.93 | 66.46  | 37.31  |       |
| 205 | 21.41 | 18.99 | 0.00  | 0.00  | 10.95 | 33.47 | 62.21 | 98.88  | 179.64 | 276.60 | 374.47 | 457.51 | 515.84  | 548.08  | 558.02  | 548.08  | 515.84  | 457.51 | 374.47 | 276.60 | 179.64 | 98.88  | 62.21  |       |
| 206 | 21.16 | 22.66 | 0.00  | 0.00  | 6.44  | 21.93 | 41.72 | 71.20  | 179.68 | 321.83 | 473.39 | 607.30 | 704.69  | 760.23  | 777.73  | 760.23  | 704.69  | 607.30 | 473.39 | 321.83 | 179.68 | 71.20  | 41.72  |       |
| 207 | 20.93 | 24.00 | 0.00  | 0.00  | 4.25  | 16.61 | 32.40 | 57.76  | 177.24 | 338.20 | 512.50 | 668.08 | 782.15  | 847.63  | 866.33  | 847.63  | 782.15  | 668.08 | 512.50 | 338.20 | 177.24 | 57.76  | 32.40  |       |
| 208 | 20.71 | 6.65  | 0.00  | 0.00  | 4.19  | 19.70 | 39.53 | 61.61  | 83.67  | 102.96 | 117.49 | 126.51 | 130.74  | 131.99  | 132.13  | 131.99  | 130.74  | 126.51 | 117.49 | 102.96 | 83.67  | 61.61  | 39.53  |       |
| 209 | 20.50 | 21.85 | 0.00  | 0.00  | 3.08  | 18.88 | 39.11 | 66.27  | 171.94 | 311.83 | 461.62 | 594.11 | 690.40  | 745.22  | 762.48  | 745.22  | 690.40  | 594.11 | 461.62 | 311.83 | 171.94 | 66.27  | 39.11  |       |
| 210 | 20.30 | 24.75 | 0.00  | 0.00  | 1.18  | 11.17 | 23.97 | 43.32  | 170.62 | 347.53 | 542.02 | 717.08 | 846.08  | 920.37  | 943.23  | 920.37  | 846.08  | 717.08 | 542.02 | 347.53 | 170.62 | 43.32  | 23.97  |       |
| 211 | 20.10 | 19.56 | 0.00  | 0.00  | 0.80  | 20.64 | 46.07 | 76.57  | 167.51 | 283.95 | 406.04 | 512.26 | 588.30  | 630.98  | 644.98  | 630.98  | 588.30  | 512.26 | 406.04 | 283.95 | 167.51 | 76.57  | 46.07  |       |
| 212 | 19.91 | 14.34 | 0.00  | 0.00  | 0.00  |       |       |        |        |        |        |        |         |         |         |         |         |        |        |        |        |        |        |       |

