

S1 Pycnometry and Tomography

S1.1 Derivation of the pycnometry equation

A schematics of the pycnometry system is depicted in Figure S1. When an object, such as a firm sample, is introduced in the first chamber, a part V_s of the volume becomes inaccessible to the gas in the chamber. The physical basis of the pycnometry is the measurement this inaccessible volume, with an ideal gas dilation.

The ideal gas law reads:

$$P(V_1 - V_s) = NRT \quad (1)$$

where P is the pressure in the chamber, V_1 the volume of the first chamber, N the number of molecule in the chamber, R the ideal gas constant and T the temperature. The second chamber of volume V_2 is vacuum pumped, and then connected to the first chamber. After the dilation, the ideal gas law becomes:

$$P'(V_1 + V_2 - V_s) = NRT \quad (2)$$

where P' is the pressure after dilation. Thus

$$P(V_1 - V_s) = P'(V_1 + V_2 - V_s) \quad (3)$$

Re-organizing the equation yields:

$$V_s = V_1 - \frac{\mathcal{R}}{1 - \mathcal{R}} V_2 \quad (4)$$

where $\mathcal{R} = P'/P$.

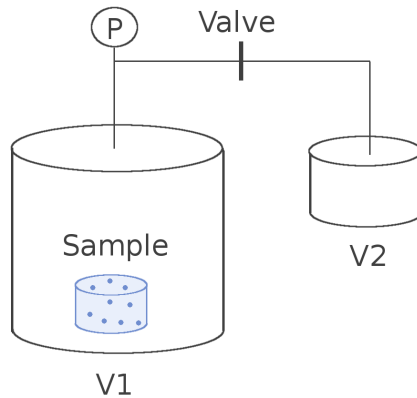


Figure S1. Pycnometry system. The circled P is the pressure gauge monitoring chamber V_1

S1.2 Calibration of the chamber volumes

The usage of the above equations requires the knowledge of the two chamber volumes V_1 and V_2 . They were estimated by using objects of known volumes. Two types of objects were used, stainless steel balls and bubble free ice cylinders. The stainless steel were bought from Marteau & Lemarié and respect the ANSI 440C norm. The ball volumes range from to 22 to 46 cm³. The bubble free ice was produced at IGE, and then carved into cylinders using a lathe. Their volume was determined by measuring

their mass and knowing the pure density at the recorded cold room temperature. The ice cylinders cover volumes from 19 to 104 cm³. Measurements were also performed without any object, corresponding to the condition $V_s = 0$ cm³.

In total 24 dilations were performed, using 8 different known volumes V_s . The chamber volumes V_1 and V_2 were adjusted by a least square method, so the measured volumes V_s match their known values. The measured volumes are displayed Figure S2 against their known values. The calibration yields $V_1 = 138.96 \pm 0.05$ cm³ and $V_2 = 6.875 \pm 0.003$ cm³.

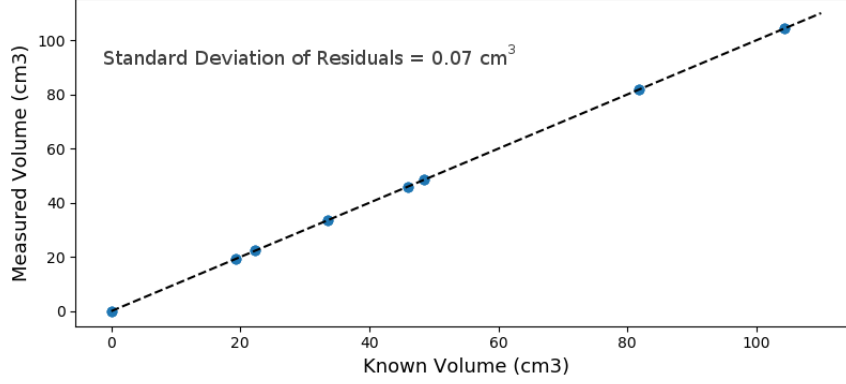


Figure S2. Relationship between the measured volume V_s using pycnometry after calibration, and their known values. The dashed line shows the Known volume = Measured volume line.

S1.3 Uncertainty analysis

There are seven independent sources of error affecting the estimation of the closed porosity ratio and the density of a cylindrical firm sample: the mass M , the radius of the cylinder r , the height of the cylinder h , the chamber volumes V_1 and V_2 , and the pressures P and P' before and after dilation. The possibility of the sample not to have a perfect cylindrical shape is included in the uncertainties on r and h . These errors were quantified during the measurements and propagated to the closed porosity ratio and density using the formula:

$$(\Delta X)^2 = \sum_i \left(\frac{\partial X}{\partial x_i} \Delta x_i \right)^2 \quad (5)$$

where X is either the closed porosity ratio or the density. The x_i correspond to the seven independent sources of error, and ΔA represents the uncertainty on the variable A . The partial derivatives were determined numerically using finite differences. The resulting uncertainties are displayed in Figure S3. It shows that the error on the density of the material is relatively constant and of the order of 0.0082 g cm⁻³, that is to say an uncertainty of 0.09 in relative density to pure ice. On the other hand the closed porosity ratio error grows from 0.02 for low firm densities, up to 0.2 for closed firm.

We also estimated the contribution of each error source. It appears that the error on the radius measurement explains most of the uncertainty on the closed porosity ratio and the density. This is due to the great sensitivity of the volume computation to the value of the radius.

S1.4 Boundary effects on the tomography samples

Figure S4 shows the variation of relative density and closed porosity ratio along a tomography sample taken at 111.68 m depth. The vertical dashed lines correspond to the separation between numerical slices. It appears that the first and last 5 mm of the sample are strongly affected by the cut bubbles due the presence of large boundaries at the top and bottom of the samples.

These boundary effects manifest as a sharp drop of the closed porosity ratio while approaching the end of the sample. The

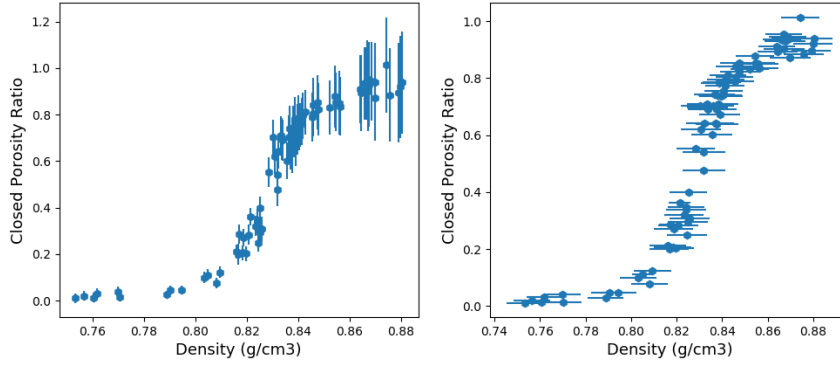


Figure S3. Closed porosity ratio data displayed with uncertainty bars. Left: Uncertainties on the closed porosity ratios. Right: Uncertainties on the densities.

same behavior is observed for the other tomography samples. Therefore, the first and last slices of each tomography image have been discarded to limit the influence of this large boundary effect.

Similarly, in order to estimate the cut-bubble effect, the firm samples were trimmed by an amount of 5 mm at the top and the bottom and by an amount of 2.5 mm on the side. This allows to remove the large boundary effect visible on the first few millimeters (visible in Figure S4), while maintaining a final geometry close to the original one.

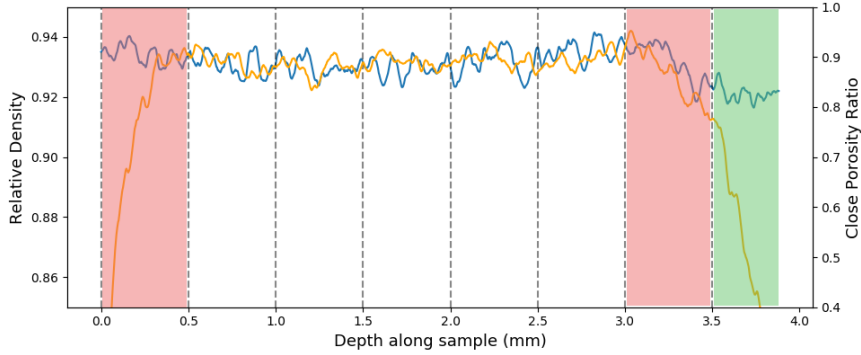


Figure S4. Relative density (blue) and closed porosity ratio (orange) along a tomographic sample taken at 111.68 m depth. The vertical dashed lines correspond to spacing between the numerical slices. The two red shaded sections are particularly affected by boundary effects. The green section at the end of the sample is less than 5 mm thick, and is thus not used as a tomographic slice.

S1.5 Impact of cut-bubbles at low densities

The fraction of re-open porosity due to the cut-bubble effect was estimated in Section 3.1.2 of the main article. For firm samples that are not totally closed, this estimation is based on the tomography images. However, no tomography data is available for relative densities ranging from 0.86 to 0.89. This implies that the cut-bubble effect is poorly constrained for these densities.

In order to estimate a possible impact of this lack of data on the final closed porosity law, we used a second correction relationship, displayed in black in Figure S5. It is expected to overestimate the amount of re-opened bubbles for low values of density. Application of this correction yields the closed porosity ratios depicted in the right panel of Figure S6. For comparison

the data obtained using the correction of the main article are displayed on the left panel. The two datasets differ for relative densities below 0.89, but in a minor fashion. As the closed porosity ratios are low in this part of the curve, the modification of the re-open volume fraction does not result in a large closed porosity ratio change. Therefore, in the case of an underestimation of the re-open volume at low densities, the closed porosity law proposed in the main article is only slightly affected.

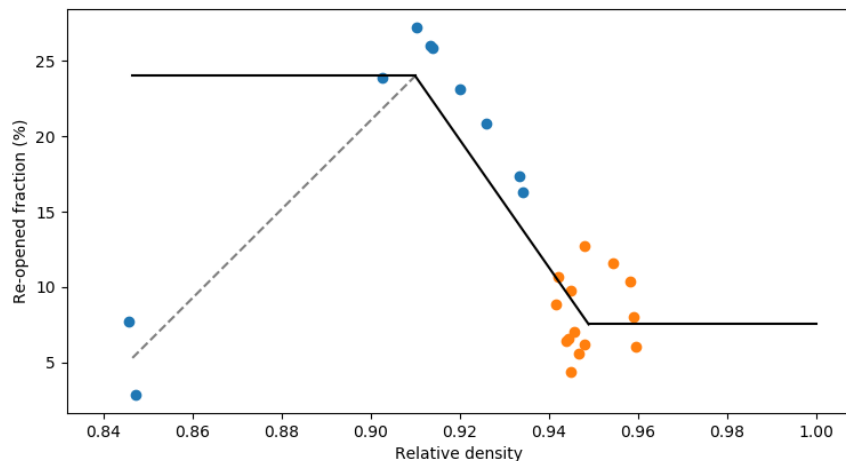


Figure S5. Fraction of re-opened bubbles as a function of relative density. Similarly to the main article, values obtained from tomography samples are represented as blue dots, and values obtained from pycnometry measurements as orange dots. The piecewise linear model used to test the data sensitivity to an overestimation of re-open fraction at low density is shown in black. The dashed line represents the correction used in the main article.

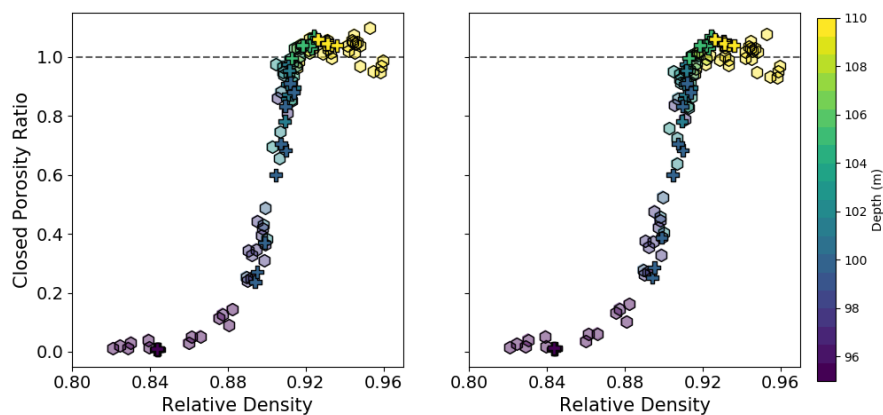


Figure S6. Closed porosity ratios with two different cut-bubble corrections. Left: Using the correction proposed in the main article. Right: Sensitivity test to a large re-open volume fraction at low densities.

5 S1.6 Uncorrected Vostok pycnometry data

In the main article Vostok closed porosity data were corrected for the cut-bubble effect using the correction derived for Lock-In. However, it is not clear that this correction is suited for the Vostok firm, as it might have a different porous network than

Lock-In. For instance Burr et al. (2018) observed a structural difference between the Lock-In and Dome C porous networks. The uncorrected Vostok pycnometry data are displayed in blue Figure S7, alongside with the uncorrected Lock-In data.

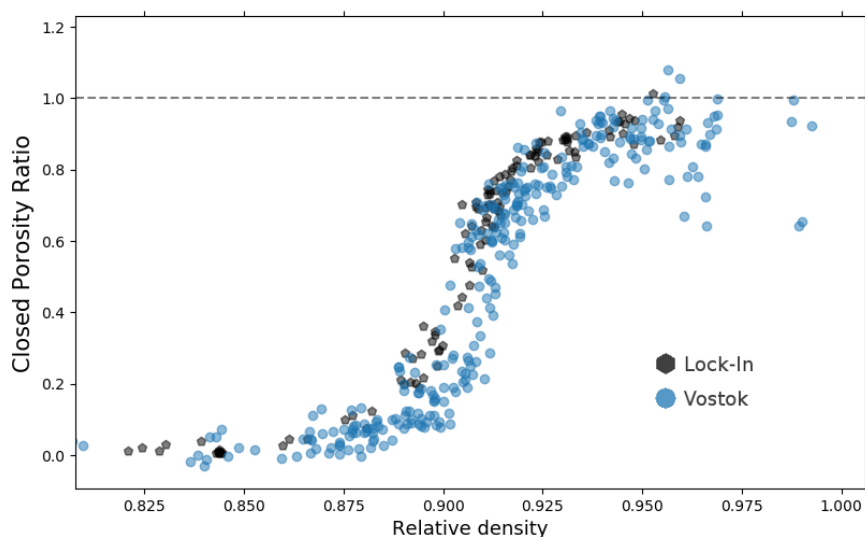


Figure S7. Closed porosity data for Lock-In and Vostok without correction for the cut-bubble effect.

S1.7 Closed porosity versus depth

The figures provided in the article are plotted using relative density as the abscissa. Here, we display in Figure S8 the closed porosity data as a function of the sample depth. This highlights the firm layering, as samples taken at similar depths display a large variability of closed porosity and density values.

S2 Computation of air content following Mitchell et al. (2015)

In the main part of the article, the air content of the Lock-In ice core was modeled using the closed porosity versus depth profile obtained by applying the measured closed porosity versus density relationship (Section 3.1) to a smoothed version of the density profile. As pointed-out by Mitchell et al. (2015), the measured closed porosity curve is obtained with centimeter-scale samples, while the smoothed density data represent a bulk meter-scale profile. The mixing of data at the centimeter and meter scales might be inconsistent and lead to a wrong estimation of the air content. To avoid this issue, Mitchell et al. (2015) propose to apply the closed porosity relationship with density to a centimeter scale density profile, and to subsequently smooth the result in order to obtain the closed porosity versus depth profile needed for the model. We tested whether the approach proposed by Mitchell et al. (2015) could explain the model/data discrepancy for air content.

For this purpose we produce a synthetic high-resolution and stratified density profile by applying a random Gaussian noise to our smooth density profile. We were not able to directly use the high-resolution density measurements, as there are numerous gaps in the data. As displayed in Figure S9, the Gaussian noise was defined with a standard deviation of 7.5 kg.m^{-3} to reproduce the variability observed in the density data. A high-resolution closed porosity profile was then obtained by applying the centimeter-scale closed porosity versus density relationship. It is displayed in blue in Figure S10. This high-resolution profile was finally smoothed to obtain a continuous and monotonous profile, as required by the Rommelaere et al. (1997) model. This new smoothed porosity profile is shown in orange in Figure S10, and compared with the closed porosity profile used in the main article in green.

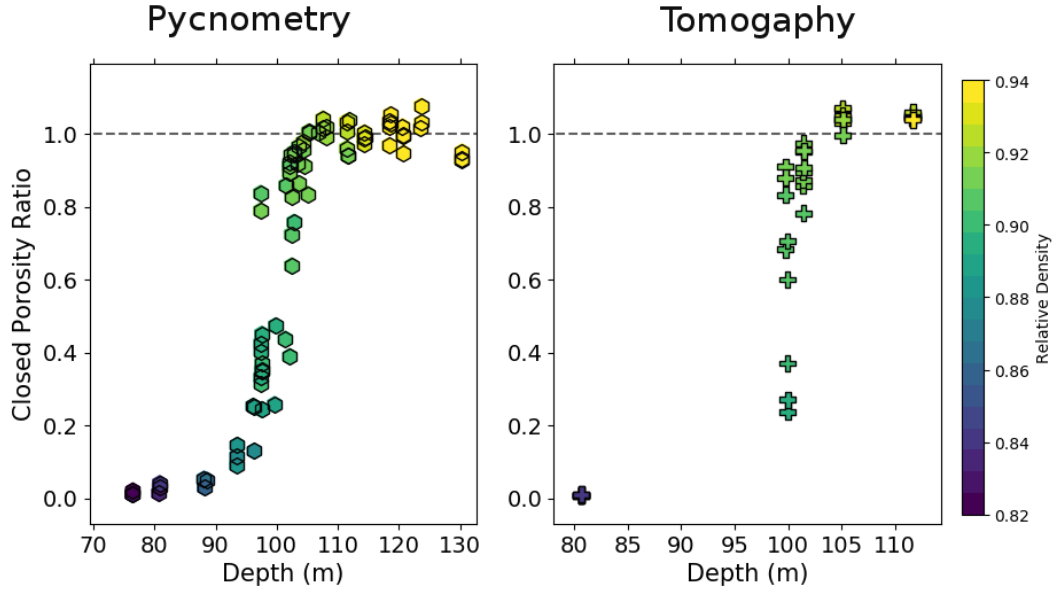


Figure S8. Closed porosity ratios versus sample depth. Colors stand for the measured relative density.

Using the new closed porosity profile in the Rommelaere et al. (1997) model leads to an air content value of $0.1016 \text{ cm}^3 \cdot \text{g}^{-1}$, almost identical to the $0.102 \text{ cm}^3 \cdot \text{g}^{-1}$ value of the main part of the article. Therefore, application of the Mitchell et al. (2015) methodology does not explain the model-data discrepancy. We also performed a sensitivity analysis, by modifying the standard deviation of the Gaussian density noise. This did not improve the model results.

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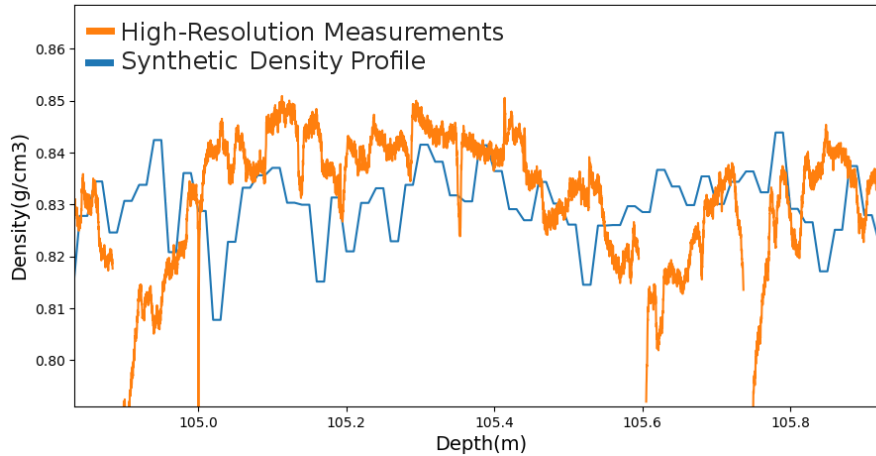


Figure S9. Comparison of the high-resolution density measurements in orange, and the synthetic density data in blue.

Moreover, we would like to point that if all firm layers close in the same fashion (same closed porosity versus density relationship at the centimeter-scale), we should expect similar air content in them, despite their difference in closure depth.

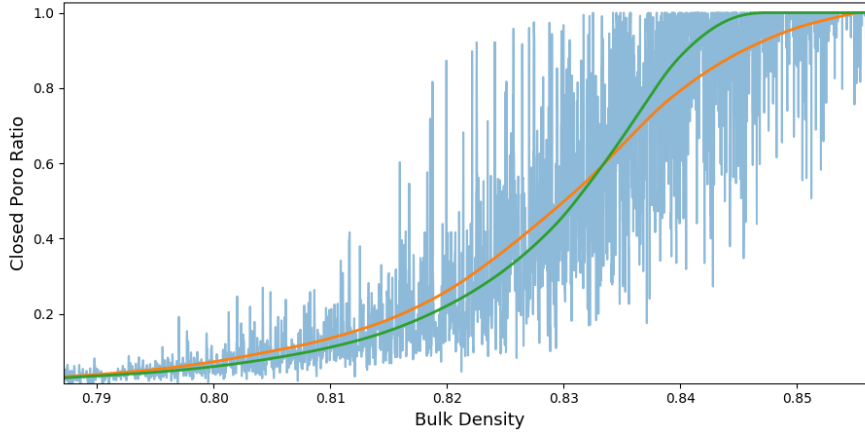


Figure S10. Closed porosity ratios versus bulk meter-scale density of Lock-In firn. In blue: high-resolution closed porosity profile obtained by applying the centimeter scale closed porosity versus density relation to the synthetic high-resolution density profile. In orange: Smoothed version of the synthetic high-resolution closed porosity profile. In green: Closed porosity profile used in the main part of the article, obtained by applying the measured centimeter scale closed porosity versus density relation to the smoothed density profile.

Indeed, assuming that sealing effects can be neglected, the bubbles in the various layers form at similar local porosities, and with similar temperature and pressure in the open porosity, meaning that the same amount of air is trapped. This is consistent with our air content measurements of an early closure layer reported in Figure 10 of the main part of the article. We should therefore expect the application of the Mitchell et al. (2015) and of our methodologies to result in similar air content values.

5 S3 Ion Chromatography

In total four one-meter long sections were analyzed using ion chromatography. One of the sections is displayed in Figure 8 of the main article. The three remaining sections are displayed in Figure S11 to S13 with density, liquid conductivity and major ion concentrations data.

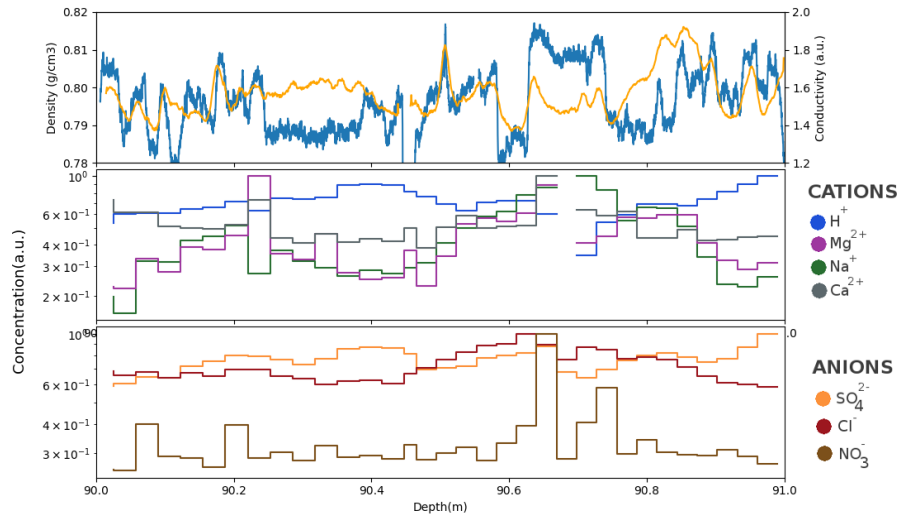


Figure S11. High resolution density (in blue), liquid conductivity (in orange) and major ion concentrations for the section between 90 and 91 m depth. The ion concentrations are split between anion and cations, and normalized to emphasis variability.

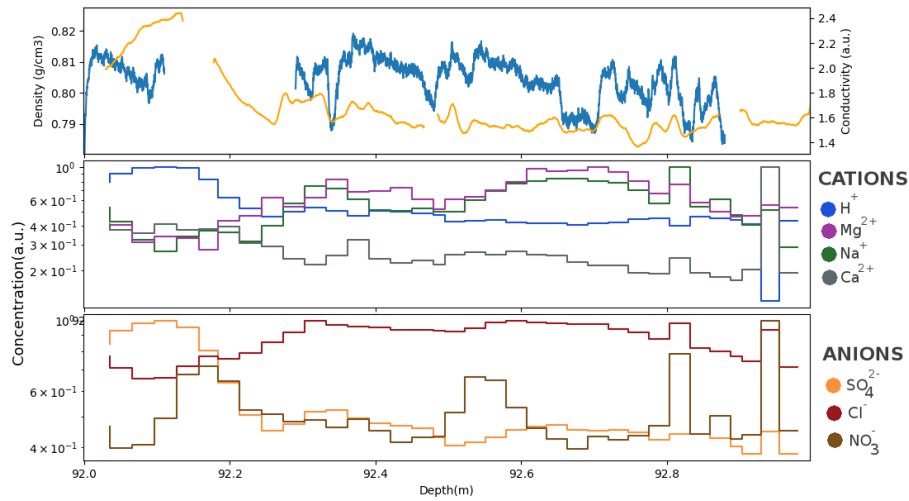


Figure S12. Same as Figure S11 for the section between 92 and 93 m depth.

S4 Gas trapping model

To model the air content in ice, we used a modified version of the Rommelaere et al. (1997) gas trapping model, introducing a limited compressibility for the closed pores. Here, we describe how the new equation representing air trapping is obtained. The derivation is similar to the one of Rommelaere et al. (1997), and we only detail the differences with the original calculation.

5 The symbols used and the quantities they represent are the same as in Rommelaere et al. (1997).

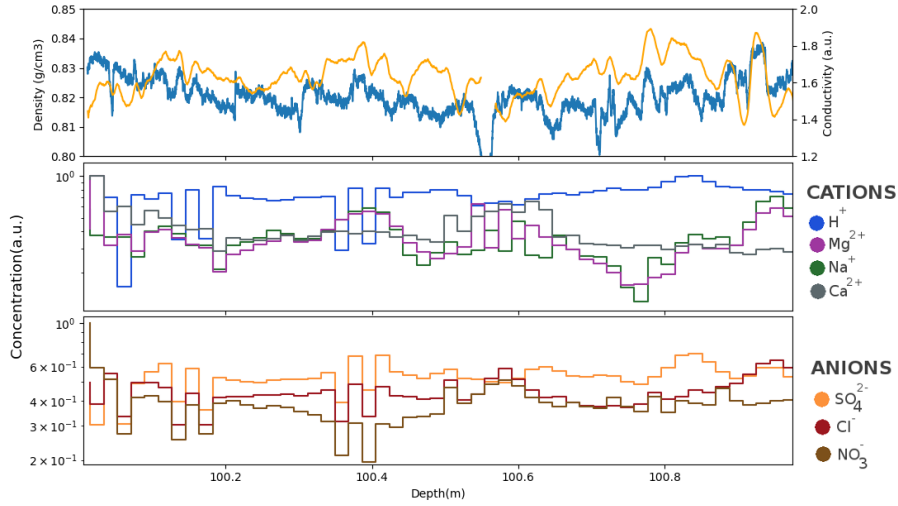


Figure S13. Same as Figure S11 for the section between 100 and 101 m depth.

Our new model is based on the replacement of Equation 8 of Rommelaere et al. (1997) by:

$$\frac{(\epsilon_1 - f_1) - (\epsilon - f)}{\epsilon - f} = \alpha \frac{\epsilon_1 - \epsilon}{\epsilon} \quad (6)$$

where ϵ and ϵ_1 are the total porosity before and after compression, f and f_1 are the open porosity before and after compression, and α is rate of compression of closed bubbles. This equations simply means that during compression, if the total porosity diminishes by $X\%$, the closed porosity diminishes by $\alpha X\%$. The original study by Rommelaere et al. (1997) corresponds to the case $\alpha = 1$.

The air conservation in bubbles is expressed by the Equation 13 of Rommelaere et al. (1997). Re-arranging the equations to eliminate the intermediate subscripts 1, and taking the time step dt as infinitely small leads to the equation:

$$10 \quad d[(\epsilon - f)c_{\text{air}}^b] = -\partial_z v dt (\epsilon - f)c_{\text{air}}^b + (d\epsilon(1 - \alpha + \alpha \frac{f}{\epsilon}) - df)c_{\text{air}} \quad (7)$$

This equation replaces Equation 15 of Rommelaere et al. (1997).

Finally under the assumption of stationarity, this Lagrangian description is converted into an Eulerian one:

$$15 \quad \partial_z (v q_{\text{air}}^b) = -c_{\text{air}} v (\partial_z f + \partial_z \epsilon (\alpha - 1 - \alpha \frac{f}{\epsilon})) \quad (8)$$

The quantity of air trapped in ice q_{air}^b can then be calculated from this equation. The required inputs for the model are density and closed porosity profiles, to compute the v , f and ϵ variables. For this study Equation 8 was solved using a finite difference scheme.

References

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